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February 9, 2010

Mr. Bryan Williams, PE

Kestrel Horizons, LLC
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Re: Draft Report: Volume 1
2010 Pinewood Site Improvement Projects
Project 1: Evaluation of Section I Cover System
Project 2: Evaluation of Section I Storm Water Management System
Pinewood, South Carolina
AECOM Project No. 60186203

Dear Mr. Williams:

AECOM is submitting to you three bound copies of Volume 1 the above referenced Draft Report for Projects 1 and 2 of the 2010 Pinewood Site Improvement Projects. Also included is an electronic copy of the document on compact disk.

Per your direction, this report is presented for discussions purposes only and should not be cited or quoted.

Upon your review and comment, we will be happy to discuss our findings, conclusions and recommendations with you and the Kestrel project team. We appreciate the opportunity to provide environmental consulting services to the Kestrel Horizons and the Pinewood Site Custodial Trust. In the mean time, if you have any questions or need additional information, please contact us.

Sincerely,

**AECOM Technical Services, Inc.**

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***Draft for Discussion***
***Do Not Cite or Quote***

# 2010 Pinewood Site Improvement Projects
# Pinewood, South Carolina

**Volume 1**
Project 1: Evaluation of Section I Cover System
Project 2: Evaluation of Section I Storm Water Management System

*Prepared for:*

Pinewood Site Custodial Trust

Kestrel Horizons, LLC,
as Trustee for the Pinewood Site Custodial Trust
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*Prepared by:*

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AECOM Project No. 60186203

February 9, 2011

## EXECUTIVE SUMMARY

Kestrel Horizons, LLC, as Trustee for the Pinewood Site Custodial Trust, awarded to AECOM three site improvement projects. Volume I of this report presents the findings and recommendations for Project 1: Detailed Performance Evaluation of Section I Cover System and Project 2: Section I Storm Water Management Evaluation.

AECOM evaluated the Section I cover system through a series of geophysical, soil gas sampling, test pit excavation and exploratory drilling tasks. Representative samples of the cover soils, liner clay and geomembrane were sampled for testing of physical properties. Pore water within the Section I cover was sampled from shallow cover wells. Leachate generation trends from Section I were compared with precipitation and the settlement of the cover system was evaluated from existing site data. Storm water management relating to Section I was evaluated by examining the water quality from the system of French drains and surface water management swales. The storm water conveyance structures associated with Section I of the landfill were modeled to determine if they were adequate to drain storm water runoff away from the landfill cover.

Based on the results of the evaluations, specific recommendations were developed.

The monitoring programs for soil gas, surface water, French drains and cover wells can be optimized to reduce unnecessary sampling and enhance the understanding of the inter-relationships of these potential contaminant transport pathways. Enhancing the monitoring of cover settlement plates will help identify potential differential or excessive settlement problems in the future. Comparing leachate generation data with water table and potentiometric surface variations over time could shed light on the cause of the increasing leachate generation rates for the Section I landfill. Improvements to the surface water drainage system will help move storm water off of and away from the cover, which will lessen the pooling of water over the landfill cover system.

Implementation of these recommendations will help in the understanding of contaminants in environmental media and aid in the operation and maintenance of the site to ensure environmental compliance and protection of the environment.

Overall, the Section I cover system appears to be in relatively good condition. Precipitation and storm water do not appear to be infiltrating through the cover in a predictable manner. VOC vapors are diffusing through the cover system and impacting pore water in the cover soils. However, the VOCs do not at the present time appear to be affecting the surface vegetation or storm water runoff or discharges to the outfall ponds via the French drains and drainage swales. Additional sampling is recommended to understand the relationship between pore water within the Section I cover and detections of VOCs in the nearby French drain.

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| | |
|---|---|
| 1,1-DCA | 1,1-Dichloroethane |
| 1,1,1-TCA | 1,1,1-Trichloroethane |
| 3-D | 3 Dimensional |
| ASTM | American Society for Testing and Materials |
| BETX | Benzene, Ethylbenzene, Toluene and Xylenes |
| cm/s | Centimeter per Second |
| CO | Carbon Monoxide |
| CSM | Conceptual Site Model |
| EVS | Environmental Visualization Software |
| GIS | Geographic Information System |
| GPM | Gallons per Minute |
| GPR | Ground Penetrating Radar |
| H2S | Hydrogen Sulfide |
| lbs | Pounds |
| IDW | Investigation Derived Waste |
| LEL | Lower Explosive Limit |
| MGD | Million Gallons per Day |
| mm | Millimeter |
| NPDES | National Pollution Discharge Elimination System |
| O2 | Oxygen |
| PCE | Tetrachloroethylene |
| PID | Photo-ionization Detector |
| ppi | Pounds per Inch |
| PPM | Parts per Million |
| PVC | Polyvinyl Chloride |
| PSCT | Pinewood Site Custodial Trust |
| QA/QC | Quality Assurance/Quality Control |
| RCRA | Resource Conservation and Recovery Act |
| SVOC | Semivolatile Organic Compound |
| SWMU | Solid Waste Management Unit |
| TCE | Trichloroethylene |
| ug/l | micrograms per liter |
| USEPA | United States Environmental Protection Agency |
| VOC | Volatile Organic Compound |

# 1.0 INTRODUCTION

The Pinewood Site Custodial Trust (PSCT) owns the former Safety-Kleen, Inc. hazardous waste storage, treatment, and landfill facility near Pinewood, South Carolina in Sumter County (Pinewood Site). Kestrel Horizons, LLC (Kestrel) is Trustee for the PSCT. Kestrel is responsible for overseeing consultants, contractors, and suppliers who provide services in study, design, construction, remediation, operation, maintenance, transportation, disposal, and monitoring for the Pinewood Site. The primary mission of the Trustee for the PSCT is to ensure the responsible use of Trust funds in carrying out the activities required to complete closure of the site and to care for and monitor the site over the next century, in accordance with the applicable laws, regulations, permits and agreements.

The Pinewood Site landfill consists of three sections (Section I, Section II, and Section III). The Section I landfill consists of five disposal cells (Cell 1A through Cell 1E) that occupy between 2.7 and 8 acres each, for a total of approximately 22 acres. Section I, the oldest landfill section at the Pinewood Landfill, was constructed and operated between 1978 and 1984, and cells were sequentially closed between 1980 and 1985. The maximum thickness of waste placed in Section I is approximately 45 feet. Wastes that have been landfilled lie primarily below the rim elevation of the liner system, though some landfill wastes lie above the liner rim. Hazardous wastes disposed in Section I included liquids, which were later banned from land disposal by state and federal regulations.

The final cover system installed for Section I consist of the following layers from top to bottom:

- Six-inch thick topsoil layer;
- Two-foot thick (minimum) protective cover soil layer;
- Two-foot thick low permeability clay layer; and
- 20-mil thick polyvinyl chloride (PVC) geomembrane that reportedly was joined with adhesive to the bottom Hypalon® geomembrane liner (at the anchor trench).

Beneath the cover, a one-foot thick sandy clay layer was placed directly over the waste to establish grade and protect the geomembrane.

## 1.1 SCOPE OF WORK

Kestrel identified three site improvement projects to aid in the understanding of the relationships of the Section I landfill and site infrastructure with the hydrogeology and how best to monitor environmental media for protection of the environment:

- Project 1: Detailed Performance Evaluation of Section I Cover System
- Project 2: Section I Storm Water Management Evaluation

- Project 3 Element 1: Construction of a 3-dimension (3D) visualization of the Hydrogeologic Conceptual Site Model (CSM), landfill and infrastructure components
- Project 3, Element 2: Review, Enhancement, and Optimization of Environmental Monitoring Program

Based on the evaluation of the Section I cover, the goals of the PSCT for Project 1 are the following:

- Reduce infiltration of rainfall, cover surface water, cover drainage, and storm water into the Section I cells, thereby reducing leachate generation, the potential for loss of waste constituents to French drains, storm water, and surface water discharges, and the potential hydraulic pressure on the landfill liner system.
- Address the potential effects of vapor transport from wastes to cover soils in the Section I landfill and isolate affected cover soils from cover surface water, cover drainage, storm water, and surface water discharges to protect the quality of storm water runoff and groundwater.
- Maintain the condition and integrity of the cover system and the seal between the cover and liner system in Section I for the next century to provide a level of certainty that neither hazardous waste nor hazardous waste constituents are released to the environment through groundwater, storm water runoff, surface water discharges, or other means from the cover system or the seam where the cover system and liner system come together.

The primary objectives of Project 2 are to include the following:

- A detailed engineering evaluation of the existing storm water management system for the Section I landfill to identify improvements to the system to more effectively route rainfall, cover surface water, cover drainage, and storm water runoff from the cover for Section I into the perimeter drainage system for management, treatment, if necessary, and discharge to the waters of the State in accordance with a NPDES Permit.
- Provide recommendations, as needed, to include alternatives to segregate sources of water from French drains, primary sumps, surface drainage, cover drainage, storm water runoff, and surface water discharges into one or more new basins or existing basins for treatment (e.g., aeration basins, first flush basin, Pond A and/or Pond B).
- Evaluate the potential need for treatment of a source of water such as the French drains, primary sumps, surface drainage, cover drainage, and storm water runoff and the location of such treatment to meet NPDES Permit requirements.

Project 3 has been subdivided into two elements. Element 1 consists of 3-D visual model of comprehensive site design features relative to a hydrogeologic conceptual site model. The model will illustrate interconnected spatial relationships with stratigraphy and groundwater flow. The 3-D visualization of the site is populated with site-specific details that can be manipulated (e.g., rotated around an axis, overlying layers removed to reveal underlying features, cut or intersects along cross sectional lines) as desired to provide insight when evaluating specific spatial orientation or relationship matters.

This visualization model will serve as a powerful tool for communicating with regulators, members of the public, and other stakeholders. C Tech Development Corporation's Environmental Visualization Software® (EVS) was used to provide a state-of-the-art analysis/visualization of the site data.

Element 2 of Project 3 consists of a critical review of the environmental monitoring program. Element 2 comprises a comprehensive review of the monitoring requirements and the system currently in place for monitoring media at the site (i.e., groundwater, soil, storm water, air, and leachate). The review includes the key historical site characterization and environmental monitoring reports to verify that the environmental monitoring systems are working together to provide an indication if the closed units are functioning as designed.

An environmental monitoring program must include the evaluation of spatial and temporal data trends of environmental media and how the data relate so that potential releases are detected at the earliest possible time. The monitoring program, however, represents a significant portion of the costs to maintain the site over the post closure care period. Therefore, existing and emerging technologies, monitoring strategies, and data evaluation techniques need to be continually evaluated and modified to find the best balance between cost and protection of the environment.

## 1.2 REPORT ORGANIZATION

This report of the 2010 Pinewood Site Improvement Projects is organized into three volumes, as outlined below:

- Volume 1 consists of the field investigation, evaluations and recommendations for Projects 1 and 2.
- Volume 2 consists of the Data Management Plan and documentation for the 3D visualization of the site, electronic deliverables of the 3D model and design elements as shape files that can be used in an ARC-GIS platform.
- Volume 3 consists of the evaluation of the environmental monitoring systems and recommendations for improvements and optimization of the monitoring program at the Pinewood site.

# 2.0 PROJECT 1 - DETAILED PERFORMANCE EVALUATION OF SECTION I COVER SYSTEM

## 2.1 SOIL COVER THICKNESS EVALUATION

Preliminary evaluation of the construction drawings for the Section I final cover system indicated that the thickness of the cover soils over the clay layer could be variable and thicker in some areas of the cover relative to others. It was theorized that surface geophysics might be able to differentiate the two soil types and the relative thickness of the cover soils and clay layer. This information would be useful in the overall evaluation of the condition of the cover and could reduce the number of invasive test pits or penetrations of the cover.

### 2.1.1 Geophysics Field Study

GEL Geophysics performed a 1-day geophysical investigation using ground penetrating radar (GPR) at selected locations on the Section I cover (Figure 2.1-1). The purpose of the investigation was to determine the effectiveness of the GPR in detecting shallow subsurface features in the cover material of the landfill. GPR surveys were conducted at 10 locations near some of the shallow cover wells, test pits and anchor trench locations so that the geophysical data could be compared with actual measured thicknesses of the soils as the excavations progressed:

- Cell A: 2 survey areas,
- Cell B: 1 survey area,
- Cell C: 2 survey areas,
- Cell D: 2 survey areas, and
- Cell E: 3 survey areas.

If meaningful information relating to the soil types and thicknesses could be inferred from the GPR data, a full survey across the Section I cover might be beneficial in understanding the thickness and placement of the cover soils over the clay layer. The GPR survey was conducted and evaluated prior to excavation of the test pits so that AECOM personnel could have an indication of whether the data would be useful in the interpretation of the subsurface soils.

### 2.1.2 Results of Field Study

The GPR survey of each area consisted of multiple parallel profiles. The data were processed and evaluated in the field and later post-processed in the office using Groundvision® software.

The soils were determined to be not conductive for GPR. The maximum effective depth of penetration ranged from 1 to 2 feet below land surface and only gross differences between the top soil and underlying cover soils was discernable on the profiles. A letter report was provided by GEL Geophysics (Appendix

2.1-1). The report includes a description of the GPR methodology, a summary of the field investigation procedure and GEL's interpretation of the data collected during the investigation.

### 2.1.3 Conclusions

Due to the low soil conductivity to GPR and similarity between the cover soils and clay layer, thicknesses of the units could not be discerned using geophysical methods. To provide definitive data regarding the thickness and geotechnical properties of the cover soils and clay layer, sampling by test pits or soil test borings were required.

## 2.2 CLAY LAYER AND PVC GEOMEMBRANE EVALUATION

### 2.2.1 Test Pits, Anchor Trench Pits and Soil Borings

Test pits were excavated at four locations across the Section I cover and five locations across the anchor trenches. The locations for the test pits are illustrated on Figure 2.2-1. The test pits were located and staked by Lindler Surveying prior to mobilizing to the site. The purpose of the four test pits was to determine the thickness and obtain samples of the top soil, cover soils and clay layer, and to examine and sample the PVC geomembrane for analysis of physical properties. The locations across the Section I cover were selected to be close to the previously installed shallow wells where the cover soil is known not to be excessively thick. The purpose of the five anchor trench test pits was to examine the physical relationship of the bottom Hypalon® geomembrane liner and PVC cover geomembrane and to determine if they were bonded and if so, the condition of the bond. A sample of the PVC geomembrane also was obtained for analysis to determine the physical properties of the membrane at each anchor trench and test pit location.

#### 2.2.1.1 *Test Pit Excavation Procedures*

A large tracked excavator was initially used at each test pit to excavate cover soils and partially excavate the clay layer of the cap. The lower portion of the clay layer was excavated using a small excavator with a plate welded across the teeth of the bucket. As the excavation progressed, AECOM provided ambient air quality monitoring using a photo-ionization detector (PID) and tri-gas meter. The soils were segregated between cover soils and clay layer soils and these were stockpiled on plastic near each excavation. The depth to each soil horizon was measured and documented. The test pit sides were cut back to a 1:1 slope and benched, when necessary. When the clay liner soils were encountered, the surface was scrapped smooth and cleaned off by the operator.

The air quality within the test pits was monitored by AECOM in accordance with the Site-Specific Health and Safety Plan. Air monitoring was conducted for volatile organic compounds (VOCs), oxygen (O2), lower explosive limit (LEL), carbon monoxide (CO) and hydrogen sulfide (H2S) as the excavations progressed and while any personnel were in the pits.

A 30-inch long Shelby tube was used to collect an undisturbed sample of the clay layer for geotechnical testing. AECOM personnel entered the test pit and set a Shelby tube with its pusher bar on the clay layer to be sampled. AECOM personnel directed the excavator operator in pushing the Shelby tube into the soil and then extracting it.

All sampled tubes were sealed with wax at both ends and then capped. The Shelby tubes were labeled and stored in an area without direct sunlight or excessive heat. The undisturbed samples were shipped to AECOM's geotechnical laboratory in Green Bay, Wisconsin for testing. As the soil samples were extruded from the Shelby tubes, they were photographed. The photographs were reviewed by the Project 1 team in Greenville, South Carolina for a consensus on representative intervals of the clay layer or cover soils to be tested (Appendix 2.2-1). One test also was conducted on soil below the PVC geomembrane.

After the Shelby tube sample was collected, the test pit excavation continued to the PVC geomembrane. Caution was taken so that the excavation equipment did not damage the PVC geomembrane. The final six-inches of excavation were generally performed by hand digging by Leak personnel to avoid damaging the PVC geomembrane. The test pit was again monitored by AECOM for oxygen and volatile vapors while any persons were in the test pit. No persons entered a pit until the air quality was deemed safe by AECOM oversight personnel. Soils were cleaned off the PVC geomembrane using a shovel and paper towels, as appropriate, by Leak personnel. AECOM personnel then inspected and documented the exposed liner material and cut a typical 15-in x 15-in piece out of the liner in the interior of the test pit. The coupon of PVC geomembrane material was rinsed, dried and photographed prior to shipping to TRI/Environmental Laboratory in Austin, Texas for testing. Photographs of the PVC geomembrane coupons are presented in Appendix 2.2-1.

The total depth of each excavation from land surface to the PVC geomembrane was measured and documented. The thicknesses of the varying soil units were also measured and noted and typical bulk soil samples were collected in bags. Table 2.2-1 provides a summary of the depths and thicknesses of the soils that comprise the Section I cover system and illustrates the depth intervals sampled.

#### 2.2.1.2 *Anchor Trench Test Pit Excavation Procedures*

The liner anchor trenches were excavated and examined in five locations, as illustrated on Figure 2.2-1. In general, excavation procedures followed those outlined in Section 2.2.1.1, above. When the PVC geomembrane was encountered, the trench was continued laterally until the bottom Hypalon® geomembrane liner was found. The physical relationship of the bottom geomembrane and cover geomembrane was examined to determine their physical condition, if they were bonded together, and if so, the condition of the bond. Air quality monitoring was performed in the excavations and at the bond between the two geomembranes to determine if volatile organic vapors were emanating from between the two liners. The anchor trench test pits were also monitored by AECOM for oxygen and VOC vapors while any persons were in the test pits. No persons entered a test pit until it was deemed safe. Soils were cleaned off the PVC geomembrane by Leak personnel using a shovel. AECOM personnel then inspected and documented the exposed geomembrane material and cut a typical 15-in x 15-in piece out of the

geomembrane in the interior of the test pit. The coupon of PVC geomembrane material was rinsed, dried and photographed prior to shipping to TRI/Environmental in Austin, Texas for laboratory testing.

#### 2.2.1.3 *Test Pit Restoration Procedures*

Where the PVC geomembrane coupons were sampled, AECOM installed a new 20-mil PVC geomembrane repair patch with a minimum 6-inch overlap of the hole on each side. The patch was sealed to the existing liner with a non-volatile adhesive bead around the entire perimeter of the PVC patch. AECOM assessed the existing PVC geomembrane to determine whether it was competent enough to install a repair patch. It was determined that the PVC geomembrane was in satisfactory condition to make the repairs with new PVC material. The epoxy at each repair patch was allowed to cure for at least 30 minutes and checked for bonding before placing clay back in the excavation. Representative photographs of the test pits with geomembrane repairs are presented in Appendix 2.2-1.

Leak performed the placement, moisture conditioning, and compaction of the excavated clay and cover soils. The clay cover soil was conditioned to between 20 and 27 percent moisture and the soil was placed in a 1-foot thick compacted lift just above the PVC geomembrane. Leak utilized walk-behind sheepsfoot for the cohesive soils and vibratory plate compactors for the non-cohesive or granular soils. An AECOM geotechnical technician supervised the placement, moisture conditioning, and compaction of the cover soils. In-situ density and moisture content tests were performed with a nuclear density gauge to check that compaction in the restored clay and cover soils was achieved similar to compaction of the original clay and cover soils. The procedure was repeated on the next two 6-inch lifts.

The cover soils were then placed in lifts to achieve 8-inch thick compacted soil lifts. These lifts were continued until the pit area had been returned to its former grade. Leak then installed top soil, an appropriate grass seed mixture, fertilizer and erosion control measures in order to establish a stand of grass.

#### 2.2.1.4 *Soil Test Borings*

Soil borings were completed at 10 locations across the Section I cover to gather additional information about the thickness of the cover soils and liner clay. The locations of the soil test borings are illustrated on Figure 2.2-1. The soil test borings were located and staked by Lindler Surveying prior to mobilizing to the site. EarthCon, of Greenville, South Carolina, was subcontracted to drill the soil test borings. The ten borings were drilled with a Mobile B-53 drill rig using hollow stem augers. Continuous soil samples were collected by pushing a 2-foot long split spoon sampler.

All drilling operations were supervised by an AECOM geologist. Detailed test boring reports were maintained by the AECOM geologist to record pertinent field observations and conditions encountered. Soils were logged and described on site using the Unified Soil Classification System. Representative samples were placed into appropriate containers for headspace screening with the PID and/or geotechnical laboratory analysis. Lithologic descriptions and headspace readings are included on the

Test Boring Reports, which are provided in Appendix 2.2-2. Table 2.2-1 provides a summary of the depths and thicknesses of the soils that comprise the Section I cover system and illustrates the depth intervals sampled.

Upon logging of the soil samples, undisturbed samples of the clay layer were collected from an adjacent boring using Shelby tubes that were pushed by the drill rig. The Shelby tubes were prepared in the field and delivered to the geotechnical laboratory in the same manner as described in Section 2.2.1.1.

Portions of the soil samples were collected from each soil core for headspace screening using a PID to provide a qualitative indication of the presence of VOCs. Soils were placed into plastic bags where any VOCs emanating from the soil were able to collect. The head space of the bagged soil samples was then scanned by inserting the tip of a PID probe through the plastic bag. PID readings were recorded on the Test Boring Reports (Appendix 2.2-2).

The borings were abandoned with a grout mixture consisting of five percent bentonite by weight with Portland cement. The grout mixture was placed into the hole from the bottom of the hole up to the ground surface.

Drilling equipment and tooling was decontaminated by pressure washing and steam cleaning prior to drilling and after the ten borings were completed. Wash waters and soils were collected on plastic sheeting and transferred to a drum as investigation derived waste (IDW). Soil cuttings/cores and purge water generated during completion of the soil test borings were also temporarily stored in drums. During this investigation, two drums containing soil and one drum containing aqueous liquids (groundwater and decontamination water) were generated.

The soil and aqueous IDW was retained and temporarily stored at three locations on Section I in Department of Transportation approved 55-gallon drums. The drums were labeled according to the contents and dated when the drum was filled. The soil and aqueous IDW was handled by other Pinewood site contractors.

### 2.2.2 Summary of Field Observations

#### 2.2.2.1 *Top Soil and Cover Soils*

The upper cover soil typically consisted of six inches of topsoil vegetated with native grass. The vegetative cover also appeared to have an adequate stand of grass. No distressed vegetation was observed. Based on the results of the test pits, anchor trench test pits, and soil test borings, the cover soil thickness ranges from 1.5 feet in the test pits near the perimeter of the landfill to 6.0 feet in the interior portions of the cover (see Table 2.2-1).

The anchor trench test pits typically encountered stiff, red brown and yellow, sandy clay cover soils that ranged from 1.5 to 3 feet thick. Cover soil encountered in the soil borings and cover test pits ranged from

2 to 7 feet thick (Table 2.2-1). The test pit cover soils typically consisted of brown, sandy loam over dense, red brown, clayey sand and stiff, sandy clay. The soil test borings typically encountered a 0.5 foot layer of topsoil over a 2 to 6.5-foot thick layer of cover soils (Table 2.2-1). These brown and red brown cover soils typically consisted of dense, slightly silty sand, silty sand, clayey sand, and stiff sandy clay. The cover soils were dry. Organic vapor concentrations measured with the PID on cover soils were generally low and ranged from 0.0 to 0.4 parts per million (ppm) in ambient air. Photographs of representative test pit excavations are included in Appendix 2.2-1

#### 2.2.2.2 *Clay Layer*

Clay soils were encountered below the cover soils in each test pit, anchor trench pit and soil test boring. Thicknesses of the clay generally ranged from 2.0 to 3.0 feet, although not all explorations were extended to the PVC geomembrane (Table 2.2-1). These soils consisted of stiff highly plastic clay, lean clay, and dense clayey sand above the PVC geomembrane. Field descriptions indicate that the clay layer was still moist (averaged 24 percent). Hydraulic conductivities ranged from $1.7x10^{-7}$ to $1.4x10^{-8}$ centimeters per second (cm/sec), which is deemed adequate for clays used in landfill covers in conjunction with a geosynthetic membrane (see Section 2.2.3 below).

Organic vapor concentrations measured on the base of the clay soils ranged from 0.0 to 20.5 ppm on samples collected from test pits and borings in Cells 1A, 1B, and 1C. VOC concentrations in clay soils from Cell 1D ranged from 0.2 to 25 ppm. The highest VOC concentrations measured on clay soils were from test pit TP-1E-01 and ranged from 79 to 166 ppm, with a bagged soil sample result of 662 ppm. Strong chemical odors were also noted at this test pit.

#### 2.2.2.3 *PVC and Hypalon® Geomembranes*

PVC geomembrane was encountered in all cover test pits, anchor trench test pits, and in 5 out of 10 soil test borings at depths ranging from 3.4 to 8 feet below grade (Table 2.2-1). Those borings that did not contact the geomembrane presumably terminated above it.

The PVC geomembrane samples that were examined appeared to be in good condition at each of the test pits and anchor trench pits. None of the PVC geomembranes were observed to be torn or punctured by soils above or below. Some of the PVC geomembranes had been wrinkled but were not torn (see photographs in Appendix 2.2-1).

After the clay soils were removed from above the PVC geomembrane at anchor trench pit AT-1E-02, the membrane began to rise up due to gas/vapor pressure beneath the geomembrane. Measurements made with the PID and multi-gas meter above the geomembrane prior to cutting a sample indicated that:

- VOCs were detected at 23 ppm,
- Oxygen was at 21.3%, and

- LEL, CO, and H2S were all equal to zero.

Directly beneath the PVC geomembrane:

- VOCs were detected at 23.7 ppm,
- Oxygen was 11.4%, and
- LEL was high, and CO was 259 ppm.

After the PVC geomembrane sample was removed, measurements were made at 0.5 foot from the soil surface beneath the geomembrane.

- VOCs were measured at 2.0 ppm,
- Oxygen was normal, and
- LEL remained high and CO was 120 ppm.

Measurements in the breathing zone, at head level indicated:

- Low VOCs, and
- Normal oxygen, LEL, and CO concentrations.

The bond between the PVC and Hypalon® geomembranes was observed in each anchor trench test pit and appeared to be in good condition with no holes or tears observed. None of the bonds could be pulled apart. PID measurements of VOCs at the bonds ranged from 0.2 to 0.6 ppm above ambient background.

### 2.2.3 Geotechnical and Geosynthetic Laboratory Testing

The undisturbed soil samples and select bulk samples of the clay and cover soils were obtained from the soil test borings, cover test pits, and anchor trench test pits. These samples were submitted for geotechnical laboratory testing. Most of the undisturbed samples were obtained in the clay layer above the geomembrane. Two Shelby tubes obtained samples of the cover soil material above the clay layer and one soil sample was obtained below the PVC geomembrane. These soil samples were shipped to AECOM's geotechnical laboratory in Green Bay, Wisconsin. The bulk soil samples were tested in AECOM's Greenville, South Carolina laboratory. The following geotechnical tests were performed on the undisturbed soil samples:

- Hydraulic Conductivity (ASTM D5084)
- Moisture Content and Dry Unit Weight (ASTM D2216)
- Grain Size, with Hydrometer (ASTM D422)

- Atterberg Limits (ASTM D4318)

Hydraulic conductivity testing was performed on eight undisturbed samples of the clay layer from above the geomembrane. Based on the laboratory results of these samples, the hydraulic conductivity of this clay layer did not exceed 1.71 x $10^{-7}$ cm/sec. The original specification required the hydraulic conductivity of the clay layer to not exceed of 1.0 x $10^{-6}$ cm/sec. Six out of eight samples tested had hydraulic conductivities in the $10^{-8}$ cm/sec range. Although, the two soil samples with hydraulic conductivities in the $10^{-7}$ cm/sec range characterized as silty and clayey, the also contained some mica, and therefore these samples did not exhibit as much cohesion as the other more clayey material.

The gradation of the clay layer ranged from 37 to 90 percent passing the No. 200 sieve, with 9 out of 11 samples having more than 71 percent passing the No. 200 sieve. The Atterberg liquid limits ranged from 33 to 59 and the plasticity index ranged from 17 to 38 for this layer. The percent clay (*i.e.,* finer than 0.005 mm) ranged from 26 to 47 percent and the in-situ moisture content ranged from 16 to 30 percent for the clay layer. The activity of the clay (defined as the ratio of the plasticity index/clay content) ranged from 0.64 to 0.84.

The index properties of the clay soils are characteristic of those with low hydraulic conductivities, as reported by the laboratory testing (Table 2.2-2). The preferred index properties for a clay capping soil for use in landfill covers are liquid limits greater than 20, a plasticity indices greater than 10, clay contents greater than 25 percent, and activity greater than 0.30. The index properties of the Section I clay layer, therefore, are representative of material that is considered suitable for clay used in landfill covers.

About seven of the Shelby tubes included both the clay layer and the overlying cover soils. Hydraulic conductivity was performed on two of the overlying cover soil samples. The test results for the soil layer directly above the clay layer had a maximum hydraulic conductivity of 2.85x$10^{-6}$ cm/sec (soil sample SB-1D-06). Although it was from the upper portion of the Shelby tube and obtained at a depth of 4 to 6 feet below grade, this silty sandy clay with more than 60 percent sand and had a moisture content of less than 17 percent. Based on these facts, this hydraulic conductivity is reasonable for the sample tested. This same material with higher moisture content would likely be able to achieve a lower hydraulic conductivity. Soil sample SB-1E-8 had a hydraulic conductivity of 2.33 x$10^{-6}$ cm/sec. This sample was obtained in the upper portion of the Shelby tube at a depth of 1.5 to 3.5 feet below grade. Trace roots and a small seam of sandier soil along the side of the test sample were observed. These features could be typical in a protective cover soil above the clay layer.

The geotechnical test results from the undisturbed soils are summarized in Table 2.2-2. Copies of the geotechnical testing reports are included in Appendix 2.2-3.

The following geotechnical tests were performed on the bag/bulk soil samples:

- Grain size (ASTM D422)
- Atterberg limits (ASTM D4318)

The gradation of the bulk samples of cover soils above the clay layer ranged from 15 to 52 percent passing the No. 200 sieve. The cover soils were either non-plastic or had Atterberg liquid limits ranging from 53 to 25 and the plasticity index range from 11 to 24. These index properties are typical of silty sands, clayey sands, and sandy clay that were used as cover soils over the clay layer of a cap. Geotechnical test results from the bulk samples are summarized in Table 2.2-3. Copies of the geotechnical testing reports are included in Appendix 2.2-3.

The samples of the PVC geomembrane were shipped to TRI/Environmental, Inc. in Austin, Texas for geosynthetic laboratory testing. The following analyses were performed on the PVC geomembrane:

- Tensile Properties (ASTM D 882)
- Thickness (ASTM D 5199)
- Peel and Shear (ASTM D 6392 / GRI GM19/D4437/NSF 54, D 6214)
- Percentage Plasticizer Content (ASTM D 2124)

The tensile strength at 100% strain also ranged from 31 to 54 pounds per inch (ppi). The recommended minimum tensile strength at 100% strain for new 20-mil PVC liner is 20 ppi. The break strength ranged from 44 to 60 ppi, with only three samples testing below the recommended break strength of 48 ppi. The break elongation of the samples ranged from 178 to 462%. The mean thickness measured of the 20-mil PVC geomembrane ranged from 16.7 to 20.3 mils. The tolerance for thickness of new PVC geomembrane is from 19 to 21 mils. About half the samples tested were thinner than 19 mils. As demonstrated by the test results, the tensile strength at 100% strain increased as the PVC got thinner, its break elongation also decreased.

The seam peel strength and shear strength results of 18 ppi and 46 ppi exceed the requirements of 12.5 ppi and 38.4 ppi, respectively. These results are summarized in Table 2.2-4. A copy of the laboratory testing report is included in Appendix 2.2-3.

As the PVC geomembrane looses it plasticizer, the tensile strength increases and the percent strain decreases. Therefore, the sample with the lowest percentage of break elongation and the maximum tensile strength was selected to for the percent plasticizer test. The percent of plasticizer was measured on sample AT-1A-01, which had a mean thickness of only 16.7 mils. This sample was reported to have 16.3 percent plasticizer remaining. New PVC typically has about 30% plasticizer, which tends to decrease over time. If there is too much reduction in plasticizer, the geomembrane could become brittle and susceptible to cracking. However, one field study by US Bureau of Reclamation on 10-mil PVC geomembrane concluded that even with a 40 percent reduction of the original amount of plasticizer, the PVC geomembrane maintained its design strength parameters for adequate performance (Levin and Hammond, 1990). Another laboratory study reported that as much as 75% of the plasticizer could be lost and the ultimate strain would be expected to exceed 100% (McKelvey, 1993).

### 2.2.4 Conclusions

Review of facility design documents and results of the test pit and drilling program indicate that the low permeability clay layer was installed above the PVC geomembrane. This construction method is not an industry standard today because the clay can be exposed to cyclic periods of desiccation or wetting, which could be detrimental to a clay layer.

Considering the fact that the clay layer in the Section I cover is above the geomembrane and it has been exposed to cyclic weather elements over a 25-year period, it still appears to be in good condition. This 2 to 3 foot thick clay soil layer is still fairly moist and did not appear to be desiccated. The laboratory test results of the samples from this clay layer indicated that had retained a lower permeability than the design specifications. The clay layer was covered with 1.5 to 6.0 feet of cover soils with a viable stand of native grasses.

As expected, some of the PVC geomembrane was found to be slightly thinner than specified. The PVC geomembrane exceeded the minimum recommended the tensile strength at 100% strain and break strength requirements. The thickness of cover over the geomembrane did not appear to have affected its performance. However, the samples from the anchor trench, located closer to the edge of the landfill, had low break strain percentages than the other samples. Even with a 46 percent loss of its original 30 percent plasticizer, the thinnest sample with the highest tensile strength still had a minimum break strain of 178%. However, field and laboratory studies have found that 40% to as much as 75% of the plasticizer could be lost without significant degradation of the performance properties of the material. Therefore, it can be concluded that this PVC geomembrane should have enough plasticizer to continue to perform as designed for some time into the future. The PVC geomembrane still appears to be performing satisfactorily as an infiltration barrier

Overall, the final cover system appears to be in serviceable condition considering its age, material make-up and construction placement.

## 2.3 LEACHATE GENERATION VS. RAINFALL TREND EVALUATION

### 2.3.1 Historical Leachate Generation and Rainfall Data

One of the primary purposes of the cover system is to minimize infiltration of rain water into the landfill. As part of the Section I cover evaluation, AECOM walked the cover. There were no observable breaches of the cover. In discussions with the PCST staff and review of the Critical Elements Analysis report (Golder Associates Inc., April 2007), AECOM learned that historically rainfall had been entering the landfill at the sump risers but recent improvements had eliminated this leakage.

However, even with these improvements, leachate generation rates for the Section I landfill are significant and increasing. As discussed in the Critical Elements Analysis report, leachate generation rates in closed landfills historically decrease one to three orders of magnitude within one year after closure (Golder

Associates Inc., April 2007). Therefore, the increasing leachate generation rate in the Section I landfill raises a concern about leakage into the landfill either through the cover system or the bottom liner.

Since leakage into the landfill cannot be measured directly, it must be inferred based on observable data. One line of evidence that the cover could be leaking would be a correlation between leachate generation rates and rainfall. Therefore, AECOM performed an analysis of the leachate data and rainfall data to determine if such a correlation exists.

Monthly leachate pumping data was provided by PCST for the period October 1996 through September 2010. Rainfall data for this same period was obtained from the nearest NOAA weather station in Rimini, SC, located approximately 1.5 miles from the site.

### 2.3.2 Analysis of Leachate Generation vs. Rainfall Data

Section I is comprised of five cells, A through E. Each cell has several vertical primary sumps. Leachate production data is collected for each leachate collection sump in Section I. By adding the data from each sump within a cell, leachate pumped from each cell was determined. By adding flow data from all of the sumps, monthly leachate pumped from Section I as a whole was determined. PCST indicated that leachate data was deemed to be significantly more reliable starting in 2005. Therefore, the trend analysis focused on the period from January 2005 through September 2010.

Monthly rainfall data was plotted against monthly leachate production data by sump, by cell and for the Section I landfill as a whole. Plots were also prepared showing raw data, linear trend lines, moving averages, and departures from normal (see Appendix 2.3-1). The plots were used to visually evaluate the data for significant correlations.

The narrative below discusses the analysis of leachate versus rainfall graphs for each of the four cases selected for analysis. The four cases selected were the following:

- Cell C,
- Cell E,
- Sump D2, and
- All of Section I.

Cell C was selected for analysis because each of its three sumps generates more than average quantities of leachate relative to the other cells in Section I. Cell E was selected because it has the largest surface area and has flat surface grades, which allow ponding on its surface. Sump D2 was selected because it currently generates significantly more leachate than any of the other sumps. And finally, a sum of all of the leachate generated by Section I was compared to the rainfall data.

Graphs of monthly leachate generation compared to monthly rainfall totals, including linear trend lines are presented in Appendix 2.3-1. Analysis of these plots of the raw data and linear trend lines did not yield any clear correlation between the leachate generation rates and the rainfall data. In fact the linear trend lines demonstrate that the leachate generation rates are trending upward in each case while the rainfall rate is relatively constant.

Graphs comparing 5-month running averages of monthly leachate generation and monthly rainfall totals are presented in Appendix 2.3-1. Analysis of these plots data did not yield any clear correlation between the leachate generation rates and the rainfall data. The leachate generation highs coincided with the rainfall highs at the same frequency that they coincided with the rainfall lows. (Note: Other periods of running average were also evaluated, with similar results)

Graphs were produced that compared leachate linear trend lines with the cumulative departure of rainfall totals from the norm (Appendix 2.3-1). Analysis of these plots clearly shows that in every case, the leachate generation rates are trending upward while rainfall is consistently less than the norm. When rainfall is less than normal, more of the rainfall is subject to evapotranspiration and less is available for seepage into the landfill.

### 2.3.3 Conclusions from Leachate Generation Analysis

All of the analyses summarized above support the conclusion that the Section I landfill cover is not a significant source of precipitation leakage into the landfill.

However, the fact that the landfill has been closed for over 20 years and the leachate generation rates are continuing to increase suggests that there may be a source of leakage into the Section I landfill other than the cover imperfections. The increasing leachate generation rates in Section I is especially telling when contrast with the sharply decreasing leachate generation rates for Sections II and III.

The Critical Elements Analysis report points to groundwater inflow through the bottom liner of Section I as a potential source of significant leachate (Golder Associates, Inc., April 2007). Analyzing the trends in water table and potentiometric surface elevations versus the leachate generation rates might be revealing. Currently the number and location of wells in the water table aquifer prevent a meaningful evaluation of the water table around the perimeter of Section I.

## 2.4 SETTLEMENT ANALYSIS

### 2.4.1 Historical Settlement Data

Evaluation of settlement data can be helpful in understanding the dynamics of the cover system. Settlement of a landfill's cover is normal due to consolidation and degradation of waste. The waste placed in Section I was either bulk waste, free liquid waste or, most often, was contained in drums. Bulk

waste would be expected to consolidate and drums would be expected to degrade over time leading to consolidation, especially if they held liquid wastes.

Excessive settlement of the cover system could result in the cracks in the clay layer, thinning of the clay layer, strain or rupture of the PVC geomembrane system or could result in surface depressions that allow rainfall to pond on the cover. Therefore, gathering and analysis of the cover settlement data is important in order to monitoring changes that may be affecting cover performance.

Thirteen settlement plates are installed on the Section I cover. Settlement data is available for five of the plates starting in 1983 and the remaining eight plates have been monitored since 2002. Settlement has typically been measured quarterly and is summarized on Table 2.4-1. The plates are dispersed as follows:

- Cell A – 1 plate
- Cell B – 3 plates
- Cell C – 1 plate
- Cell D – 5 plates
- Cell E – 3 plates

Figure 2.4-1 illustrates the topography of the Section I cover along with settlement plate locations and the cumulative settlement at each plate.

### 2.4.2 Settlement Trends

Plots of the settlement data for each of the thirteen settlement plates are presented on Figure 2.4-2. The plots provide an understanding of the settlement history. The five markers on Cell D (D-1 through D-5) were installed in 1983, which was immediately after completion of the cover for this cell. These plots depict greater settlement for the first 2 or 3 years followed by a relatively slow settlement trend. The data for the remaining markers starts in 2002, approximately 15 years after installation of the cover and therefore, do not show the initial settlement period.

The settlement data indicates a relatively gradual and uniform settlement of the Section I cover. This type of settlement is a positive factor in the long-term performance of the cover system. Significant differential settlement would put additional strain on the cover system and potentially lead to damage to the cover system. Periodic small localized settlement is to be expected as drums and wastes decompose. Depressions formed due to this type settlement can be handled by backfilling and re-seeding and should not significantly impact the performance of the cover system.

The continued settlement of the cover, more than 20 years after closure, may in part be due to the quantities of leachate being removed. Analysis of settlement that may be associated with leachate removal is provided below.

### 2.4.3 Analysis of Settlement vs. Leachate Removal Volumes

Between 100,000 and 400,000 gallon of leachate is removed from the Section I landfill annually. Removal of such significant quantities of leachate would be expected to result in settlement of the cover. The volume of leachate removed was used to calculate the settlement that would be projected to result. Calculations were performed for each sump and for each cell. Table 2.4-2 summarizes the results of the calculations and compares the results to the measured settlement. The average projected settlement results for each cell compares well with the measured settlement for the same period of time. The difference between projected and the measured settlement is between 0.10 feet and 0.30 feet.

### 2.4.4 Conclusion from Settlement Data Analysis

The settlement measurements appear to have some inaccuracies. Upward movement of the cover is not consistent with the expected movement of the waste. It is more likely that the survey data was collected with varying vertical datum, varying equipment, measuring different location on the settlement plate, taking side shots rather than a closed loop, reduction errors, recording errors or a combination of the above. Due to the minute amount settlement between measurements, the use of accurate and consistent surveying methods and prompt review and validation of the data are critical to gathering useful data for assessment of cover settlement.

Overall, the settlement of the Section I cover does not appear to be excessive and is relatively uniform. Therefore, the cover system condition should not have been impacted significantly due to settlement.

Settlement data plots should be maintained and updated with new data as it is received in order to identify measurement errors and to identify changes in settlement trends.

Additional settlement markers are needed to provide a more uniform distribution of settlement data.

## 2.5 SOIL GAS EVALUATION

AECOM conducted a soil gas investigation over the Section I cover to determine if vapor transmission is occurring through the current cover, which includes a PVC geomembrane, low permeability clay, sandy clay cover soils and top soil. This study used Gore-Sorber® modules installed across the 22 acres of the final cover. This study was designed to identify the areas of the cover that may exhibit impact and identify the type of vapor that may be coming up through the cover.

Gore-Sorber® modules are passive, sorbent-based samplers that collect volatile and semi-volatile organic compounds present in air, soil, and water. The modules are constructed of a GORETEX® membrane tube, which is chemically inert, vapor permeable, and waterproof.

Specially engineered adsorbents with an affinity for a broad range of organic compounds are located in the bottom of a one-foot long membrane tube. Additional information regarding the design and properties of Gore-Sorber® modules is available at www.gore.com/surveys.

AECOM installed 50 survey points in a grid across the five cells that comprise Section I. The soil gas survey locations are illustrated on Figure 2.5-1. In addition, two background locations were selected along the service road near the east end of the site (near the MW-098 monitoring well vicinity) to provide a comparison to the Section I survey points (Figure 2.5-2). Four modules were selected at random and retained as trip blanks.

Prior to mobilization, the survey locations were marked and staked by Lindler Surveying. The Gore-Sorber® modules were installed over a two-day period. At each survey point, a ¾-inch diameter hole was drilled into the ground to a depth of two feet below land surface using a hammer-drill. A Gore-Sorber® module was then tied to an inert polypropylene cord and inserted into the drilled hole using a stainless steel tool supplied by the manufacturer. The cord was then tied to a natural cork and the cork used to plug the top of the hole. Approximately 2 pounds of clean fine-grained sand was poured onto the top of the cork plug to hold it in place.

The Gore-Sorber® modules were retrieved 14 days after installation (allowing for the maximum exposure time). The modules were resealed in their respective numbered glass vials after retrieval and shipped back to the manufacturer for laboratory analysis along with completed chain-of-custody documentation.

Each exposed Gore-Sorber® module (as well as four trip blank modules and two method blanks) were analyzed by WL Gore & Associates in their in-house laboratory for the A1 suite of volatile and semi-volatile organic compounds by thermal desorption, gas chromatography, and mass spectroscopy via modified United States Environmental Protection Agency (USEPA) methods 8260/8270:

**Standard Analytical Suite (A1)**

| | | |
|---|---|---|
| MtBE | Benzene | Toluene |
| Ethylbenzene | m,p-xylene | o-xylene |
| Octane | Undecane | Tridecane |
| Pentadecane | 1,3,5-TMB | 1,2,4-TMB |
| Naphthalene | 2-Methylnaphthalene | trans-1,2-DCE |
| cis-1,2-DCE | TCE | PCE |
| 1,1-DCA | 1,2-DCA | 1,1,2-TCA |

| | | |
|---|---|---|
| 1,1,1-TCA | 1,1,2,2-TetCA | 1,1,1,2-TetCA |
| Chloroform | Carbon tetrachloride | Chlorobenzene |
| 1,2-DCB | 1,3-DCB | 1,4-DCB |
| TPH | | |

### 2.5.1 Results of Soil Gas Field Study

The soil gas analytical data are reported on Table 2.5-1 as a mass of analyte in micrograms (µg) per sample. A copy of WL Gore's report is presented in Appendix 2.5-1. Included in the report are color isoconcentration maps for the following constituents, which were detected most often by the laboratory:

- Total benzene, ethylbenzene, toluene and xylenes (BETX)
- Tetrachloroethene (PCE)
- Trichloroethene (TCE)
- 1,1,1-Trichloroethane (1,1,1-TCA)
- 1,1-Dichloroethane (1,1-DCA)

Results for the background samples indicated low detections of petroleum-related constituents but not chlorinated solvents. None of the four trip blank samples and two method blanks contained target analytes. Thus, the data are deemed valid for the purposes of screening soil gas at the Pinewood Site.

Results of the soil gas study show that petroleum and chlorinated solvent vapors are present in the soils above Section I. As illustrated on the color isoconcentration maps in Appendix 2.5-1, the highest masses of VOC constituents were detected in soils above Cell E. In particular, "hot-spots" seems to occur at in Cell E at location SG-1E-44 and to a lesser extent at location SG-1C-20 in Cell C with all VOC constituents plotted. Total BETX constituents appear more wide-spread across the cover, although at lower constituent masses.

Ambient monitoring during the test pit excavations and test drilling program indicated the presence of VOCs in soils and beneath the geomembrane. The soil gas survey however, was better able to quantify the distribution and relative abundance of VOCs diffusing through the PVC geomembrane and into the clay layer and cover soils. For example, Figure 2.5-3 illustrates the occurrence of 1,1-dichloroethane in soil gas and the concentration of total VOCs in air above immediately above each of the geomembrane perforations. In general, the PID indicated that VOC concentrations measured from the test pits located on the cover were higher than those VOCs measured from the anchor trench test pits at the edge of the landfill, beyond the limits of the waste. This data may indicate that VOCs are not migrating laterally from beneath the cover.

The presence of VOC mass in the cover soils is not unique to the Pinewood Site. Virtually all landfills generate gasses, whether through biodegradation or volatilization.

Virtually all landfill covers allow some portion of the gasses to pass through via diffusion. The Section I cover was constructed using PVC geomembrane rather than the HDPE geomembrane that is commonly used today. Studies indicate that the diffusion rate through a PVC geomembrane is about twice as fast as through a Polyethylene (PE) geomembrane (McWatters and Rowe, 2009). Thus, the presence of VOCs in the cover soils is not unexpected given the high concentrations of solvent-based waste placed within the Section I landfill and the permeability of the 20-mil PVC geomembrane to certain VOCs by diffusion. Based on the field observations and geotechnical testing results, the physical properties of the clay soil layer did not appear to be impacted by the vapors diffusing through the PVC geomembrane. Furthermore, the VOCs in soil gas are not at concentrations that are impacting the vegetative cover of the landfill.

### 2.5.2 Conclusions

Results of the soil gas study show that petroleum and chlorinated solvent vapors are present in the soils above Section I. "Hot-spots" seems to occur at in Cell E at location SG-1E-44 and to a lesser extent at location SG-1C-20 in Cell C with all VOC constituents plotted. Total BETX constituents appear more wide-spread across the cover, although at lower constituent masses.

The soil gas survey was able to quantify the distribution and relative abundance of VOCs diffusing through the PVC geomembrane and into the clay layer and cover soils. PID data from the test pit excavations indicated that VOC concentrations measured from the test pits located on the cover were generally higher than those VOCs measured from the anchor trench test pits at the edge of the landfill, beyond the limits of the waste. This data may indicate that VOCs are not migrating laterally from beneath the cover.

The presence of VOCs in the cover soils is likely due to high concentrations of solvent-based waste placed within the Section I landfill and the permeability of the 20-mil PVC geomembrane to certain VOCs by diffusion through the membrane. However, the physical properties of the clay soil layer did not appear to be impacted by the VOC vapors and the soil gases are not at concentrations that are impacting the vegetative cover of the landfill.

## 2.6 SHALLOW COVER WELLS

### 2.6.1 Summary of Historical Data and Sampling Results

PSCT installed shallow wells directly into the cover of Sections I, II, and III of the landfill to monitor the accumulation of any long term perched water on the landfill clay liner. This was done to detect any residuals from previous spills or leaks on the landfill covers from past activities at the site, and to monitor for the effects on perched water due to gas emissions up through the geosynthetic and clay liners of the

landfill covers. The locations of the shallow cover wells for Section I of the landfill are presented in Figure 2.6-1.

AECOM's observations concerning these shallow cover wells during a site visit on October 26 - 27, 2010 are noted below.

| **Section I – Shallow Cover Well Information** | | | |
|---|---|---|---|
| Well | Top of Casing Above Ground (feet) | Well Depth from Top Of Casing (feet) | Well Depth From Top of Ground (feet) |
| SILC-1 | 3.5 | 8.32 | 4.82 |
| SILC-2 | 2.7 | 7.2 | 4.5 |
| SILC-3 | 4.0 | 8.7 | 4.7 |
| SILC-4 | 3.5 | 8.2 | 4.7 |
| SILC-5 | 3.5 | 7.05 | 3.55 |

Based on these observations, these wells, with a PVC casing diameter of approximately 1 to 1 ½ inches, have a depth from top of ground ranging from approximately 3.6 to 4.8 feet. The total depth of the cover to the PVC geomembrane liner, in the vicinity of the shallow cover wells is approximately 4.5 feet. However, during field investigations of the cover system of Section I in November of 2010, it was determined that this total depth of the cover soils and liner clay varied for the five cells of Section I and ranged from 3.4 to greater than 8 feet, across the landfill cover. Therefore, the above described shallow cover wells for Section I were typically installed at some depth in the clay layer above the geomembrane liner.

The height of the water column in these wells above the well bottoms during the October 26 to 27, 2010 site visit was measured and is presented below:

| **Section I - Shallow Cover Wells Water Column Height October 26 - 27, 2010** | |
|---|---|
| Well | Water Column Height In Well (feet) |
| SILC-1 | 0.61 |
| SILC-2 | 0.25 |
| SILC-3 | Dry |
| SILC-4 | 1.63 |
| SILC-5 | 0.15 |

Well SILC-3 on that date was dry, and the height of the water column in the other wells ranged from only 0.15 feet to 1.63 feet. Since the wells are so shallow, the height of the water column in the wells is highly variable and dependent on many factors, including the intensity and duration of the most recent rainfall events.

PSCT collected water samples from these wells on May 29, 2009 and October 22, 2009 for VOCs. Semi-volatile organic compounds (SVOCs) and metals were also sampled during the October 22, 2009 event. The analytical results from these sample events are provided in Table 2.6-1. On November 10, 2010, these shallow wells were sampled by AECOM personnel for VOCs. Analytical results of this sampling are also presented in Table 2.6-1. A summary of this analytical data is presented in Table 2.6-2 and shows eight of the constituents that had the highest concentrations during these three separate sampling events. A copy of the laboratory analytical report from the November 2010 sampling event is presented in Appendix 2.6-1.

AECOM personnel planned to sample these wells for other constituents such as metals and SVOCs, but there was not sufficient water in any of these wells for the collection and analyses of samples for these additional constituents. It was AECOM's intent to sample for these additional constituents in an effort to differentiate between any constituents in the water due to gas emissions (VOCs) through the cover and constituents from previous spills or leaks on the landfill cover from past activities at the site (e.g., SVOCs and metals).

### 2.6.2 Analysis of Shallow Cover Well Water Quality

The sampling and analytical data presented in Tables 2.6-1 and 2.6-2 show the presence of significant concentrations of VOCs in water from these shallow wells; with the highest concentrations detected in shallow cover surface wells SILC-2, SILC-3, and SILC-5. These three wells are located in Cells D and E of Section I of the landfill (Figure 2.6-1). As shown in the above referenced tables:

- methylene chloride ranged from a low of less than detectable to a high of 4,030 ug/l;
- 1,1 dichloroethane ranged from a low of 286 ug/l to a high of 2,210 ug/l;
- chloroform ranged from a low of less than detectable to a high of 1,710 ug/l;
- 1,1,2-trichloroethane ranged from a low of less than detectable to a high of 947 ug/l;
- trichloroethylene ranged from a low of less than detection to a high of 986 ug/l;
- cis-1,2-dichloroethylene ranged from a low of 11.9 ug/l to a high of 803 ug/l;
- tetrachloroethylene ranged from a low of 0.62 ug/l to a high of 253 ug/l;
- 1,1,1 trichoroethane ranged from a low of less than detectable to a high of 248 ug/l.

The highest concentrations of VOCs were observed in SILC-3 located in Cell D of Section I (October 2001, Table 2.6-1). Such concentrations in the Section I shallow subsurface are significantly higher than

concentrations observed in shallow cover surface wells for Sections II and III of the landfill, as presented Table 2.6-3. The highest concentration of any VOC in the shallow cover surface wells for Sections II and III was tetrachloroethylene at 24.3 ug/l for S2LC-04 on December 29, 2009. Most of the VOC concentrations in water from the Section II and III cover wells during 2009 sampling events were low, estimated values (J-flagged).

For the October 22, 2009 sampling event for Section I, two SVOCs were detected in SILC-3 with 1,4 dioxane at 53.9 ug/l and m,p cresols at 8.1 ug/l. Metals were also analyzed and detected in SILC-3 and these results are provided in Table 2.6-1.

Some lower concentrations of VOCs were also observed in shallow cover wells SILC-1, located in the northeast corner in Cell A, and SILC-4, located in the southwest corner of Cell D at the edge of the landfill and near Manhole 5 of the Section I French drain. However, for SILC-1, concentrations ranged from less than detectable to 14.7 ug/l and were more similar to concentrations observed in shallow cover wells for Sections II and III of the landfill, as presented Table 2.6-3. For SILC-4, VOC concentrations ranged from less than detectable to 46.7 ug/l.

It should be noted that due to the low volume of water in these shallow cover wells, typical groundwater sampling procedures could not be followed and standing water was not purged prior to sampling. Any VOCs in the water, regardless of their source from gas emissions or historical leaks or spills of leachate on the landfill cover could skew the significance of the VOC analytical results. Furthermore, given the reported construction methodology for the shallow cover wells (e.g., exploratory excavations that were backfilled while the PVC wells were held in place) the wells may be acting more as shallow collection sumps rather than representing transient water within the cover soils.

### 2.6.3 Conclusions

The sampling and analytical data show the presence of significant concentrations of VOCs in pore water from the shallow cover wells, especially wells SILC-2, SILC-3, and SILC-5, which are located in Cells D and E of Section I. These VOC concentrations are significantly higher than those observed in wells SILC-1 and SILC-4 in Section I and in the shallow cover wells installed in Sections II and III.

Seven of the eight the VOCs with the highest concentrations detected in pore water from the Section I cover wells, were also detected in soil gas on the Section I cover. Therefore, it is apparent that a primary source of the VOCs in the shallow cover well water is due to gas emissions of the VOCs diffusing through the PVC geomembrane and clay layer of Section I.

If constituents such as metals and semi-volatile organics were consistently shown to be present in water samples from the Section I shallow cover wells, contributions of these constituents from other sources would need to be considered. These other sources could include residuals of constituents from previous spills or leaks on the landfill cover. However such data, including data from background shallow wells, is limited at present and not sufficient to make definitive conclusions.

There is some potential for the VOC impacted pore in the water on the Section I cover to enter storm water or French drain systems, discussed below, and then eventually migrating to off-site surface waters from Outfall 001 of Pond A. However, due to the extremely low concentrations of VOCs detected in the French drains (as discussed in Section 2.7, below) and in surface water (as discussed in Section 2.8, below) as compared to the high VOC concentrations observed in perched water on the landfill cover, it appears unlikely that the VOCs in this perched cover water are a source of VOCs in either the French drains or surface waters at the site. This conclusion is further supported by the tight nature of cover soils and the apparent low volume of the perched water on Section I.

## 2.7 FRENCH DRAIN WATER QUALITY EVALUATION

### 2.7.1 Summary of Historical Data and Sampling Results

French drains were installed by the previous owners/operators to lower groundwater tables or levels during the construction of Sections I, II, and III of the landfill and to divert off-site groundwater around the landfill site. There is one perimeter French drain beginning at a location near the old tank farm and extending along the eastern edge of the property toward the entrance road/guard gate and then along the northern edge of the site along the North Road and ending near the intersection of North Road and West Road. There is a breakpoint on this perimeter French drain located near the entrance road/guard gate at which the groundwater collected in the French drain flows by gravity and discharges either into Pond A or Pond B. In one direction from the breakpoint, the groundwater in the French drain flows along the east edge of the site and then into hard piping near the old tank farm and eventually flows or discharges (at the water surface elevation) into Pond A. In the other direction from the breakpoint, the groundwater in the French drain flows for a short distance along the east edge of the site, along the north edge of the site following the North Road, and then into hard piping near the intersection of North Road and West Road and eventually flows or discharges (at the water surface elevation) into Pond B (Figure 2.7-1).

There is an additional French drain that extends along a portion of the east and west sides and along the south end of Section I of the landfill. This French drain was also installed to lower groundwater table during the construction of Section I. Five manholes are installed on the Section I French drain that are used to sample the water from the drain. Groundwater collected in this French drain flows by gravity from Manhole 4 on that French drain into hard piping along the west edge of Section I and eventually flows or discharges (at the water surface elevation) into Pond A in close proximity to the discharge from the perimeter French drain into Pond A (Figure 2.7-1).

The locations of the perimeter French drains around Sections I, II, and III of the landfill and discharge locations from these drains into Ponds A and B are presented on Figure 2.7-1.

The above described French drains, constructed of perforated corrugated plastic piping surrounded by gravel, remain in place and in operation at the site. AECOM personnel collected samples of the three separate French drain discharges at the point of those discharges into Pond A and B on November 10 -

11, 2010 for VOCs. The results of this sampling event are provided in Table 2.7-1 and are discussed below.

PSCT has been monitoring the groundwater within the Section I French drain and perimeter French drain discharges into Pond A and Pond B as one of many measures to monitor for the detection of any leakage or release of waste residuals from the landfill cells. Monitoring has included VOCs and metals. A summary of the results of this monitoring from 2008 through 2010 is provided in Table 2.7-2 and is discussed below.

The discharges from the French drains into Pond A and Pond B were observed by AECOM personnel during the site visit on October 10, 2010. The discharge water at that time was clear with little, if any, visible suspended solids.

### 2.7.2 Analysis of French Drain Water Quality

As observed from Table 2.7-1, no VOCs were detected in the two discharges from the perimeter French drain discharges into Pond A or Pond B or the Section I French drain discharge into Pond A for those samples collected by AECOM personnel on November 10 - 11, 2010.

A summary of the results of monitoring by the PSCT from 2008 through 2010 is provided in Table 2.7-2. A few VOCs and metals have been detected in the discharges from the perimeter French drains to both Pond A and Pond B and within the manholes of the Section I French drain, but at very low concentrations, Methylene chloride was detected in a February 2008 sample at a concentration of 2.37 ug/l in the primary French drain discharge to Pond A; 2.41 ug/l in the Section I French drain discharge to Pond A; and 2.13 ug/l in Manhole 4 within the Section I French drain. Methylene chloride was not detected in the discharge from the perimeter French drain to Pond B for that sample event. The other VOC that was consistently detected, but again at low concentrations was 1,1-dichoroethane within the Section I French drain manholes ranging from < 1 ug/l to 2.94 ug/l. Other VOCs detected in the manholes within the Section I French drain system include chloromethane and tetrachloroethylene at < 1 ug/l. The only VOC detected in the perimeter French drain discharge to Pond B was chloromethane, also reported at < 1 ug/l. Of these VOCs detected within the French drains or the French drain discharges to Pond A or Pond B, methylene chloride, 1,1-dichloroethane and tetrachloroethylene were detected in either or both the groundwater in the shallow surface cover wells and soil gas samples collected within the Section I landfill.

NPDES Permit No. SC0042170, discussed in more detail in Section 2.8 below, specifies effluent limitations and other requirements for discharges of storm water and water from the French drains to Outfall 001 (discharge from Pond A) and Outfall 002 (discharge from Pond B). However, there are no specific monitoring requirements or effluent limitations specified for VOCs in the existing NPDES Permit. The permit, however, is currently scheduled for re-issuance or renewal.

Metals have been detected, but at low concentrations, in the water samples from the discharges of the French drains to both Pond A and Pond B. These include cadmium, arsenic, lead, and silver. The most

consistently detected metal is cadmium, with detections ranging from 0.2 to 1.23 ug/l. Arsenic concentrations have ranged from 0.06 to 0.4 ug/l. Lead concentrations have ranged from 0.01 to 0.08 ug/l. Silver concentrations have ranged from 0.004 ug/l to 0.009 ug/l. Cadmium concentrations appear to be slightly higher in the discharge from the Section I French drain to Pond A and the perimeter French drain discharge to Pond B than in the discharge from the perimeter French drain to Pond A.

In the current NPDES permit for the site, there is a monthly average and daily maximum effluent limitation for cadmium of 0.34 ug/l and 1.9 ug/l, respectively, for the Outfall 001 discharge from Pond A. As stated previously, cadmium has been detected in the discharges from the perimeter French drain and the Section I French drain ranging from 0.2 ug/l to 1.23 ug/l and is presumably a source of the cadmium in the discharge to Pond and the Outfall 001. However, those cadmium detections are for the influent into Pond A from the French drains and not for the total discharge (including storm water from Pond A) to the 001 Outfall. In the current NPDES permit, there is also a monthly average and daily maximum effluent limitation for lead of 3.4 ug/l and 88 ug/l, respectively, for the discharge from Pond A to the Outfall 001. However, lead concentrations in the French drain discharge (0.01 ug/l to 0.08 ug/l) are well below those permit limits.

### 2.7.3 Conclusions

The sampling and analytical data show the presence of only low detections of a few VOCs and metals in the discharges from the French drains to Pond A, Pond B and within the Section I French drain collection system. The reported concentrations of these constituents are not at significant levels to impact surface water outfalls (001 and 002). [Note: Currently there are no specific monitoring requirements or effluent limitations specified for Outfall 001 or Outfall 002 for VOCs in the NPDES Permit, however the permit is scheduled for re-issuance or renewal.]

No VOCs were detected in the discharge of water from the French drain that flows into Pond B, located primarily around Sections II and III.

Storm water quality (as discussed in Section 2.8, below) does not appear to be a source of contaminants to the Section I French drain system.

The comparison of VOCs from water samples in the Section I French drain are orders of magnitude lower that those measured in pore water on the adjacent Section I cover. Due to the tight nature of soils and the low volume of the perched water on Section I it appears unlikely that the VOCs in this perched cover water are a source of VOCs in the French drains at the site. However, additional sampling will be needed to understand whether the cover soil pore water contributes to the VOCs in the Section I French drain.

The number of Section I French drain sampling events and analytical parameters evaluated are not sufficient to evaluate the source of the contaminants in the Section I French drain (e.g., soil gas vapors or landfill leachate). Additional sampling events and an expanded suite of analytes will be required.

## 2.8 SURFACE WATER QUALITY EVALUATION

### 2.8.1 Description of Surface Water Discharges

Surface water discharges from the site include groundwater collected in the perimeter French drain and the Section I French drain; groundwater collected in a French drain installed to address a Solid Waste Management Unit (SWMU) in the vicinity of the First Flush Basin; and storm water runoff from Sections I, II, and III of the landfill site after rainfall events. As previously described, groundwater collected in the perimeter and Section I French drains flows via underground piping into surface water ponds A or B. Storm water collected on site flows through a series of ditches, pipes, and/or culverts off the covers of Sections I, II, and III of the landfill and other drainage basins around the landfill directly into surface water Pond A or Pond B or into the First Flush Basin. The First Flush Basin discharges to Pond A through a deeply incised influent channel. Additionally, the groundwater from the French drain constructed beneath the First Flush Basin is collected and pumped to one of two aeration basins (termed North and South Aeration Basins) for air stripping of any VOCs (if needed) prior to being directed to the influent channel that leads to Pond A. The combined flow of groundwater and storm water from Pond A or Pond B is then discharged into an un-named tributary of Lake Marion in accordance with effluent limitations and other requirements of NPDES Permit No. SC0042170. A copy of this NPDES Permit is provided in Appendix 2.8-1. The effective date of NPDES Permit SC0042170 was August 1, 2005 and the expiration date was July 31, 2010. Even though the expiration date of the permit has passed, the facility is operating under the effluent limitations of that existing permit until a new permit has been issued.

The potential pathways for any waste constituents to move from the Section I landfill via French drains and eventually to off-site surface waters along with the characteristics of that water in the French drains have previously been discussed in Sections 2.6 and 2.7. These pathways include: 1) the shallow or perched water on the Section I landfill cover, as observed in the shallow surface cover wells, following subsurface drainage contours off of the landfill cover and ultimately infiltrating into the French drains; 2) the condensation of soil gases from Section I within the French drains; or 3) some other pathway between the Section I landfill and French drains. However, due to the extremely low concentrations of VOCs detected in the French drains and in surface water (as discussed below) as compared to the high VOC concentrations observed in perched water on the landfill cover, it appears unlikely that the VOCs in this perched cover water are a source of VOCs in the French drains at the site. This conclusion is further supported by the tight nature of soils and the low volume of the perched water on Section I.

There is also the potential for any VOCs in the groundwater from the French drains at the First Flush Basin to enter Pond A and then discharge to off-site surface waters. The two collection points within that French drain system are designated as SBD#1 and SBD#2, which are pumped to the North and South Aeration Basins for treatment by volatilization/air stripping. NPDES Permit No. SC0042170 requires monitoring and reporting of tetrachloroethylene for the discharge from either the North or South Aeration Basin, as Outfall 01A. Even though there is no specific effluent limitation for tetrachloroethylene, monitoring is required to determine the effectiveness of the air stripping process on VOC removal in the basins.

Another potential pathway for landfill waste constituents to enter surface water is through storm water by contact of that storm water with long term standing or perched shallow groundwater containing VOCs on the Section I landfill cover or any residuals from previous spills or leaks of leachate on the landfill cover from past activities at the site. PSCT has periodically collected of storm water samples from within the ditches, piping, and culverts of the storm water collection system for the Section I landfill. The most recent sampling event was in December of 2009. Storm water sampling locations are presented in Figure 2.8-1.

### 2.8.2 Analysis of Water Quality Data

The primary waste constituents in the groundwater from the two collection points designated as SB#1 and SB#2 within the French drain system at the First Flush Basin are summarized in Table 2.8-1. The constituents include:

- tetrachloroethylene ranging from 7.93 to 159 ug/l;
- cis-1,2 dichloroethylene ranging from 5.12 to 46.6 ug/l; and
- trichloroethylene ranging from 2.02 to 24.1 ug/l.

Other VOCs detected in this groundwater include 1,1-dichloroethane; 1,1,2-trichloroethane, 1,1-dichloroethylene; and 1,1,2,2-tetrachloroethylene ranging from less than dectectable to 6.45 ug/l.

A summary of the discharge of Outfall 01A from the North and South Aeration Basins is presented in Table 2.8-2. This data shows that tetrchloroethylene concentrations are reduced from a range of 8 to 159 ug/l to less than 1 ug/l via volatilization/air stripping. Even though VOCs are introduced into the aeration basins, the data indicates that the discharge of water from the French drain at the First Flush Basin does not contribute any VOCs to Pond A or off-site surface waters due to the treatment of this groundwater via air stripping. No monitoring of the groundwater from the French drain system at the First Flush Basin is provided for SVOCs, 1,4 dioxane, or metals.

Data from the December 2009 storm water sampling event for Section I of the landfill is presented in Table 2.8-3. Acetone (a possible laboratory artifact) was detected at concentrations of 1.96 ug/l and 1.74 ug/l from storm water sampling stations SI-SW-5 and SI-SW-7, respectively. Choromethane was the only other VOC constituent detected; less than 1 ug/l at sampling station SI-SW-6. There also was one detection of acetone (1.73 ug/l) at sampling location SI-SW-2 during a November 2009 sampling event. Based on the limited storm water sampling data presented in Table 2.8-3, it does not appear that any waste constituents are being contributed to storm water or to surface water from the Section I landfill area via contact with shallow water on the landfill cover or any waste residuals from past activities at the site.

NPDES Permit No. SC0042170 specifies monitoring and effluent limitations for the discharge from Outfall 001 (Pond A) and Outfall 002 (Pond B). A copy of these monitoring requirements and effluent limitations is provided in the permit in Appendix 2.8-1. Those outfalls or discharges are routinely monitored for

VOCs, pesticides/herbicides, and metals, including mercury. A summary of the results of this monitoring from 2008 to 2010 is provided for Outfalls 001 and 002 in Table 2.8-4. The results of this monitoring show that the characterization of the discharges from both Pond A, which receives groundwater from French drains around Section I and storm water runoff from Section I, and from Pond B, which does not receive any groundwater or storm water runoff from Section I, are similar. These discharges have historically been characterized by low concentrations (less than 1 ug/l) of cadmium, lead, silver, mercury, and arsenic; a few detections of pesticides/herbicides less than 0.1 ug/l; and few detections of VOCs, which could be laboratory artifacts (chloromethane at less than 1 ug/l, acetone at 1.56 to 6.56 ug/l, and acrolein at 2.34 ug/l). No discharge monitoring data was available for 1,4 dioxane.

Even at such low concentrations, the cadmium concentrations have occasionally approached or exceeded the monthly average discharge limitation of 0.34 ug/l for Outfall 001. Similar low concentrations of cadmium have been observed in the perimeter and Section I French drains that eventually discharge into Pond A and Pond B. Cadmium has not been monitored in the storm water discharges from the landfill site, including Section I. Therefore, the contribution of cadmium in the discharges from Outfall 001 and Outfall 002 from storm water, if any, is unknown.

The source of mercury in the discharges from Outfall 001 and Outfall 002 is not known. Mercury has not been monitored in the storm water discharges from the landfill site, including Section I or in French Drains. Therefore, the contribution of mercury from storm water, if any, is unknown. Analysis of quality assurance/quality control (QA/QC) data relating to mercury have indicated that the detections are not statistically significant in that mercury in blank samples was detected at concentrations similar to those being detected in the discharges from Outfall 001 and 002. Some additional evaluation including background data in storm water and groundwater and laboratory methodology is needed to verify the low concentrations of cadmium and mercury being detected at the site.

### 2.8.3 Conclusions

Based on the limited storm water sampling data discussed above, it does not appear that any waste constituents are being contributed to storm water or to surface water discharges from Pond A or Pond B from the Section I landfill area via contact of storm water with shallow water on the landfill cover or any waste residuals from past activities at the site.

Due to the extremely low concentrations of VOCs detected in the French drains and in surface water as compared to the high VOC concentrations observed in perched water on the landfill cover, it is not clear that the VOCs in this perched cover water are a source of VOCs in the French drains at the site.

Even though VOCs are present in the groundwater being pumped from the French drain at the First Flush Basin to the North and South Aeration Basins, those VOCs are being removed by volatilization/air stripping in those basins. Therefore, no VOCs are being contributed to Pond A or to off-site surface water discharges from that source.

The results of these monitoring programs indicate that the characterization of the discharges from both Pond A and from Pond B are similar. These discharges are characterized by low concentrations (less than 1 ug/l) of cadmium, lead, sliver, mercury; a few detections of herbicides/pesticides less than 0.1 ug/l; and few detections of VOCs which could be laboratory artifacts (chloromethane at less than 1 ug/l and acetone at 2 to 7 ug/l).

The cadmium concentrations in the discharge from Outfall 001 have approached or exceeded the monthly average discharge limitation of 0.34 ug/l about half of the time. Similar low cadmium concentrations have been observed in the perimeter and Section I French drains, which eventually discharge into Pond A and Pond B. Cadmium has not been monitored in the storm water discharges from the landfill site, including Section I. Therefore, the contribution of cadmium in the discharges from Outfall 001 and Outfall 002 from storm water, if any, is unknown.

In order to verify the low concentrations of cadmium and mercury being detected are valid, additional storm water and groundwater background data is needed as well as an evaluation of laboratory methodologies.

# 3.0 SECTION I STORM WATER CONVEYANCE EVALUATION

Project 2 of the 2010 Pinewood Site Improvement Projects is focused on evaluating the condition and adequacy of the Section I storm water conveyance system. The purpose of this effort is to identify any inadequacies that may impact the performance of the cover and recommend corrective measures.

In order to evaluate the system, AECOM first performed field reconnaissance to observe the condition of the conveyance system and inventoried the components. Following the field reconnaissance, surveying was completed to map components that were not identified on existing drawings. Once the mapping was complete, the system was modeled hydraulically to determine the adequacy of the system components during various rainfall events. Following is a more detailed account of the evaluation performed including the results of the evaluation.

## 3.1 INVENTORY OF STORM WATER SYSTEM COMPONENTS

A 1-foot topographical map of the Pinewood Section I cover and the surrounding area was prepared in December of 2006 by Glenn Associates Surveying, Inc. The map outlines features such as roads, culverts, swales, and catch basins. A second map of the Pinewood Section I landfill was created in March of 2009 by Kestrel following construction activities associated with the sump and leachate transfer system installation. This map details areas where the cover was re-graded and also provides additional storm water conveyance information; culvert pipe sizing, materials of construction, and culvert invert elevations and storm water flow direction.

### 3.1.1 Drawing Review

The Section I leachate transfer system was installed on top of the existing cover and soil was placed over the force main. This additional cover created berms across the top of Section I, which divided the center of the cover into four areas. The center of the cover is relatively flat and is sloped approximately 1.5 percent; it is graded to drain storm water runoff away from the cover. A 12-foot wide road is located on the outer perimeter of the force main berms. This road allows access to the force main system. The landfill cover slopes approximately 5 percent between the access road and the perimeter of the cover. The entire cover is currently grassed.

A series of swales are located along the perimeter of the cover in order to drain storm water runoff off of the cover without flowing over the access road. The swales are grassed and are sloped approximately 2 percent. The topography of the Section I cover, including identified swales, is illustrated on Figure 3.1-1.

Storm water culverts were installed through the leachate transfer system berms at various locations in order to drain runoff away from the cover. These culverts are constructed of 15-inch corrugated plastic pipe and range in slope from 2 percent to 6 percent. Additional culverts are installed near the perimeter of the cover and vary in size from 12-inch to 18-inch. Culvert materials include corrugated metal,

reinforced concrete, and corrugated plastic. The locations of the culverts are also illustrated on Figure 3.1-1.

### 3.1.2 Field Reconnaissance

Field reconnaissance was performed in November 2010. The purpose of the site visit was to verify the location and characteristics of storm water conveyance structures identified using the existing topographical maps. Overgrown grass was noted near the vicinity of many of the culvert inlets during the site visit.

Following a review of available topographical information and data collected from the field reconnaissance, areas where additional information was needed to evaluate the conveyance capability of the Section I cover storm water system were identified. Storm water structures not on the existing maps were located and additional invert elevations were obtained in December 2010 by Lindler Surveying. Storm water features not in close proximity to the Section I cover were assumed to have adequate capacity and, therefore, were not included in the survey request.

## 3.2 MODELING OF EXISTING STORM WATER SYSTEM

The existing storm water conveyance system was modeled to evaluate the system's ability to drain storm water runoff away from the landfill cover. A 10 year, 24 hour and 25 year, 24 hour designed storm event were used in the analysis. The peak flow rates associated with the designed storm events were calculated using PondPack V8i. PondPack is widely used to model storm water systems and calculate flow rate characteristics.

The watershed associated with the cover was delineated using the topological information described above. The acreage was then segregated into drainage areas in order to determine the peak runoff flow rate associated with each storm water conveyance structure, as illustrated on Figure 3.2-1.

The entire cover is grassed; therefore, a curve number of 69 was used in the storm water model. The time of concentration, or the time required for a drop of water to travel from the most hydrologically remote point in the drainage area to the point of collection, was calculated in PondPack using inputs such as curve number, slope, and hydraulic length. Culvert capacities were calculated using CulvertMaster Version 3.1 and channel capacity was calculated using SedCAD 4. Modeling results are provided in Appendix 3.2-1.

### 3.2.1 Summary of Modeling Results

Approximately 6.8 acres of the watershed is located beyond the perimeter of the Section I cover. Runoff from this acreage is directed towards the landfill and consists of a portion of drainage area CM-29 and CM-14 as shown on Figure 3.2-1.

Existing culvert and channel characteristics, including their ability to convey runoff associated with the design storm events, are presented on Table 3.2-1. All channels in the vicinity of the cover are appropriately sized. However, channel CO-89 is positioned directly above the cover on the southernmost portion of the landfill.

### 3.2.2 Conclusions

The Section I cover is generally effective in conveying storm water off of and away from the landfill. The cover was grassed and there were no significant areas of erosion or settlement noted. The soil mounds that cover the leachate piping and utilities prevent direct radial flow of storm water off of the cover. Piping has been installed to covey water from these areas and is generally effective. However, AECOM confirmed that there are areas of surface water ponding on the Section I cover. Some of the culvert inlets were partially blocked with sediment and grass and some were determined to be undersized for the given drainage areas. In addition, the conveyance system is designed to gather water in swales on top of the cover. While this is not a preferred design, it does not seem to be a problem based on the analysis of leakage through the cover (see Section 2.3, above).

Further, there are areas where rainfall is directed onto the cover from the surrounding topography. These areas are low and prone to ponding. Section 4.9 of this document provides specific recommendations for correcting these concerns.

# 4.0 RECOMMENDATIONS

The following recommendations are provided to the PSCT based on the Project 1 and Project 2 investigations and findings described in this document. These recommendations are also incorporated into the Project 3, Element 2 program, which is presented in Volume 3.

## 4.1 SOIL COVER

Site personnel should continue to maintain the cover to prevent erosion. There are no specific recommendations related to the cover soil evaluation.

## 4.2 CLAY LAYER AND PVC GEOMEMBRANE

Although the PVC geomembrane still appears to be performing satisfactorily as an infiltration barrier, due to the loss of plasticizer that has occurred since closure of Section I, it is recommended that samples of the membrane be re-evaluated in five years. There are no specific recommendations related to the clay liner.

## 4.3 LEACHATE GENERATION ANALYSIS

### 4.3.1 Leachate Trend Analysis

Regular monitoring of leachate generation data versus rainfall should be continued. With the improved accuracy of the leachate generation data, trends may emerge that could not be recognized currently. As the Section I cover ages, leakage of precipitation through the cover system may become more likely and the trend plots could help identify if and when this occurs.

Comparing leachate generation data with water table and potentiometric surface variations over time, is recommended to determine if there is a meaningful correlation between the head difference (gradient) between the surrounding aquifers and leachate levels maintained in the landfill. This could shed light on the cause of the increasing leachate generation rates for the Section I landfill. Adequate wells do not currently exist in the water table aquifer to accurately depict the water table surface around the Section I landfill. Volume 3 of this report outlines additional water table monitoring wells that would provide adequate data to accurately depict water levels in and around the Section I landfill.

### 4.3.2 On-Site Weather Station

The addition of an on-site weather station would provide more accurate, site specific precipitation data.

## 4.4 SETTLEMENT ANALYSIS

The settlement plates are not distributed uniformly across the cover. The plates are located only on the high points. More uniform distribution of settlement plates would provide a more accurate understanding of the cover settlement. Recommended locations for additional settlement markers on Section I are presented on Figure 4.4-1.

Monitoring of settlement across the Section I cover can be enhanced and made more useful in identifying trends and significant settlement events by adopting the following:

- Develop a more rigorous and scheduled surveying program to minimize data inconsistencies, and
- Plotting the data expeditiously to validate the values and quickly identify inconsistencies.

A topographic survey was last performed in 2006. A new topographic survey is recommended to identify settlement that may have occurred in areas without settlement markers.

## 4.5 SOIL GAS MONITORING

The final cover over Section I does not incorporate gas management into its design. VOC "hot spots", particularly over Cell E, may be reflective of diffusion of the VOCs through the geomembrane and clay, historic surface spills, construction flaws in the cover placement, or a degraded condition of the cover in these particular areas.

Although there is an apparent issue with VOC vapors diffusing through the PVC geomembrane and clay layer, the occurrence of VOCs in the cover soils does not appear to present a problem for the growth of the vegetative cover and VOCs are not detectable by a PID within the breathing zone in ambient air above the cover. Based on the field observations and geotechnical testing results, the physical properties of the clay soil layer did not appear to be impacted by the VOC vapors.

Soil Gas is, however, apparently impacting pore water contained within the cover soils on the landfill. The contribution of these constituents to adjacent groundwater, storm water runoff, and French drain discharge to surface water is unknown.

Soil gas survey points are recommended to monitor the vapors in the cover soils over the landfill on an annual basis. Soil gas survey points are also recommended to be installed at three areas adjacent to the landfill "hot-spots" to evaluate whether vapor emissions may be moving into the soils adjacent to the landfill and beyond the cover. The recommended soil gas survey points should be installed as permanent shallow (2-foot) gas monitoring wells. Permanent soil gas survey points are illustrated on Figure 4.5-1.

Three shallow groundwater monitoring wells are also recommended to be installed adjacent to the "hot-spots". These wells could be used to evaluate groundwater occurrence and quality near the French

drains. Analysis of water from these wells, compared with the soil gas data may be useful in evaluating the low VOC detections in water from the Section I French drain, particularly at Manhole 5. The wells should be sampled contemporaneously with the soil gas survey points and analyzed for VOCs, including 1,4-dioxane. The presence of chlorinated VOCs in groundwater and absence of 1,4-dioxane could provide an indication that groundwater contaminants are originating from soil gas as opposed to a release of landfill/leachate constituents. The recommended locations of the monitoring wells are illustrated on Figure 4.5-1.

## 4.6 SHALLOW COVER WELLS

The analytical data from the Section I shallow cover surface wells are highly variable due to shallow depth of these wells and the low volume of water they contain. Given that these wells may be acting more as sumps rather than monitoring transient water, the ongoing need to continue monitoring these shallow cover wells should be re-evaluated. The data collected from these wells should only be used to establish long term trends such as any increasing or decreasing concentrations of constituents in the cover pore water. If PSCT feels the need to continue to monitor these shallow cover wells, the analytical and sampling recommendations for the existing shallow cover surface wells in all landfill sections are noted below:

- All shallow surface cover wells should be sampled for VOCs on an annual basis to establish and monitor long term trends in the characteristics of water in the shallow cover wells on Sections I, II, and III of the landfill. This monitoring should be performed to determine if there are any significant changes in shallow or perched water quality on the landfill covers, such as increases or decreases in VOCs. If any such significant changes are observed, further investigations could be conducted to determine the cause of such changes.
- If such constituents as metals and semi-volatile organics (which would not be expected to be transferred by diffusive migration through a geosynthetic membrane and through the clay layers via gas emissions) were consistently shown to be present in water samples, contributions of these constituents from other sources would need to be considered. These other sources could include residuals of constituents from previous spills or leaks on the landfill cover from past activities at the site. Therefore, the following additional monitoring is recommended:
    - One existing water table well (WT032), located near Section I should be used as a background well for the shallow cover wells. This well should be sampled on an annual basis for VOCs; SVOCs; pesticides/herbicides, 1,4 dioxane and RCRA metals. The location of water table well WT032 in relation to Section I is illustrated on Figure 4.6-1.
    - One shallow cover well in each of the three landfill sections (Sections I, II, and III), should also be sampled on an annual basis for SVOCs, pesticides/herbicides, 1,4 dioxane and RCRA metals. These wells should be selected based on water samples exhibiting the historically highest VOC concentrations. The monitoring data from each shallow cover well should be compared with the results from well WT032.

## 4.7 FRENCH DRAIN WATER QUALITY MONITORING

Sampling, analytical, and other recommendations for the site-wide system of French drains are noted below:

- The three main discharges from the French drains should be sampled for VOCs, 1,4 dioxane, and RCRA metals on a quarterly basis at the discharge points into Ponds A and B or the first manhole upstream on the French drain piping from the discharge points into Ponds A and B. On an annual basis, these three discharges should also be monitored for SVOCs and pesticides/herbicides. The recommended sampling points are illustrated on Figure 4.7-1.
- At least one groundwater monitoring well should be installed between the edge of the Section I landfill cover and the Section I French drain between manholes 4 and 5 and monitored for VOCs, 1,4 dioxane, and RCRA metals on a quarterly basis in order to determine if any of the water observed in the shallow cover wells on Section I is flowing off of the cover and toward the Section I French drain. The recommended monitoring well location is illustrated on Figure 4.5-1.
- Due to such low concentrations of VOCs and metals in the French drain water discharge to Pond A and Pond B, no additional treatment of this water is deemed necessary or recommended at this time.
- The collection and treatment of this French drain water may need to be considered at some point in the future if cadmium becomes an issue with regard to the NPDES effluent limitations for Outfall 001. Pump stations could be installed to intercept the French drain water and direct it back to the area of the existing aeration basins for VOC removal and metals treatment/removal. However, additional treatment processes would need to be designed, permitted and constructed if metals removal is required. The total volume of all three French drain discharges to either Ponds A or B is estimated to be in the range of 30 to 50 gallons per day (GPD) (0.043 to 0.072 million gallons per day [MGD]) based on observations during site visits in October and November 2010.

## 4.8 SURFACE WATER QUALITY MONITORING

Sampling, analytical, and other recommendations for the storm water discharges are noted below:

- Storm water sampling should be in accordance with any requirements of a revised Storm Water Pollution Prevention Plan (SWPPP) for the site specified in the revised General NPDES Permit for storm water discharges associated with industrial activity, which became effective January 1, 2011.
- NPDES Permit No. SC0042170 specifies monitoring requirements for various outfalls or discharges from the site. The facility should continue to monitor in accordance with the existing or renewed permit.

- The rationale for the basis of any re-issued NPDES Permit effluent limitations should be thoroughly reviewed before accepting any effluent limitations specified in that permit, especially effluent limitations for any metals such as cadmium and/or mercury.
- It is recommended that storm water sampling at the present storm water sampling stations that discharge into Pond A (Figure 2.8-1) be discontinued.
- For discharges to Pond A, new sampling stations should be established at the following locations:
  - two influent piping locations to the First Flush Basin from the Section I landfill area,
  - the discharge from the First Flush Basin, and
  - the existing storm water sampling location SI-SW-3.
- For discharges to Pond B, new sampling locations should be established at the two influent piping locations to Pond B.

These sampling locations are illustrated on Figure 4.8-1. Monitoring at these new sampling locations should include VOCs, RCRA metals, and 1,4 dioxane on a quarterly basis and SVOCs and pesticides/herbicides on an annual basis.

Mercury has been reported at such low concentrations that it cannot be demonstrated to be a statistically significant contaminant to environmental media at the Pinewood site. No regulatory decisions should be made based on mercury data until any future detections can be demonstrated to be statistically valid with respect to the laboratory analytical methods and quality control procedures. Similarly, some additional evaluation, including background data in storm water and groundwater and laboratory methodology, is needed to verify the low concentrations of cadmium being detected at the site.

## 4.9 STORM WATER MANAGEMENT

### 4.9.1 Culvert Improvements

Various culverts are currently undersized to accommodate runoff from the modeled storm events. Preliminary sizing for replacement culverts is presented in Table 4.9-1. The majority of the replacement culverts are similar in size to those recommended for replacement. For example, culvert J-21 is currently 18-inches in diameter and a 24-inch replacement culvert is required.

Acreage near the inlet of culvert J-43 is currently subject to ponding; this culvert is currently undersized and needs to be replaced. The culvert is currently composed of two 12-inch pipes; two 30-inch pipes are required to accommodate runoff from the designed storm event. The culvert should also be lowered and relocated approximately 60 feet to the southeast in order to ensure positive drainage. The recommended location of culvert J-43 is illustrated on Figure 4.9-1.

### 4.9.2 Redirecting Drainage Away From the Section I Cover

Allowing storm water to run onto the landfill cover should be avoided whenever possible. Culvert J-43 drains drainage area CM-14. CM-14 is approximately 5.5 acres in size and extends beyond the landfill cover. Re-grading may be possible to reduce the amount of runoff reaching culvert J-43. Reducing the acreage of drainage area CM-14 would in turn reduce the required size of the J-43 replacement culverts. A berm is proposed to divert runoff away from the cap and reduce the size of drainage area CM-14. The location of this berm and the proposed reduction in the drainage area size is illustrated on Figure 4.9-1.

A portion of drainage area CM-29 is also located beyond the cover. A culvert in this drainage area discharges to the high point of channel J-129. This portion of the channel is located on the perimeter of the cover. It may be possible to install a berm to redirect storm water into the channel at a point down gradient of the cover. Proposed measures to reduce the size of drainage area CM-29 are illustrated on Figure 4.9-1.

## 5.0 REFERENCES

Golder Associates, Inc., April 2007, Critical Elements Analysis, Pinewood Facility, Sumter, South Carolina.

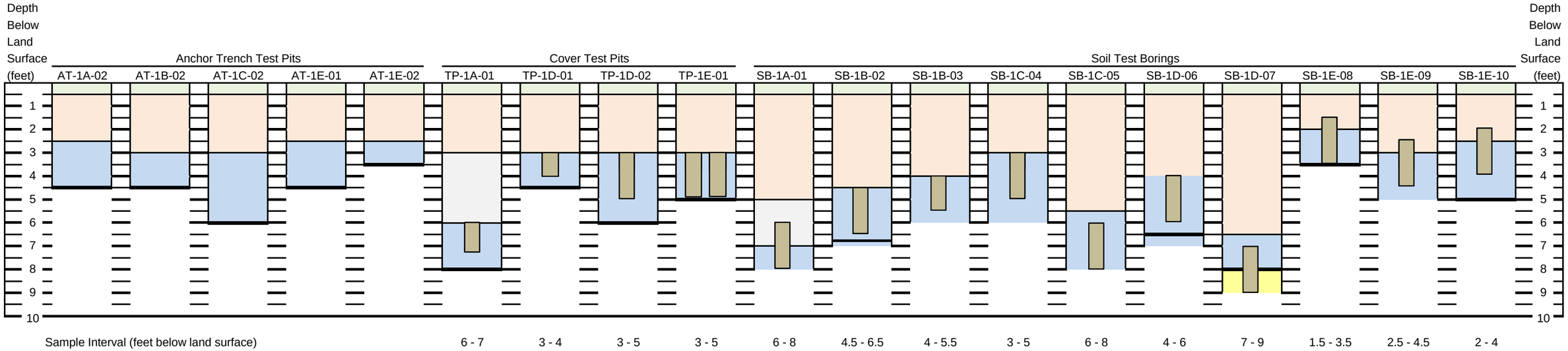
Levin, S. B. and Hammond, M. D., 1990, Examination of PVC in a 'Top Cap' application, Geosynthetic Testing for Waste Containment Applications, ASTM STP 1081, Robert M. Koerner, Ed., American Society for Testing and Materials, Philadelphia *in* Environmental Protection, Inc., http://www.geomembrane.com

McKelvey III, James A., November 1993, Demonstrating PVC geomembrane durability landfill closures, PVC Geomembrane Institute, PGI Technical Bulletin, Environmental Protection, Inc., http://www.geomembrane.com

McWatters, R. S., and Rowe, R. K., 2009, Transport of volatile organic compounds through PVC and LLDPE geomembranes from both aqueous and vapour phases, Geosynthetics International, vol 16, number 6, pp 468-481.

# TABLES

TABLE 2.2-1
Summary of Soil Depths and Thicknesses
Section I Cover
Pinewood Landfill
Pinewood, South Carolina




**Notes:**

Thickness and Depth of Soil Layers in Test Pits is illustrated at the Geomembrane Sampling Locations.

Depth intervals are rounded to the nearest 0.5 feet for illustrative purposes.

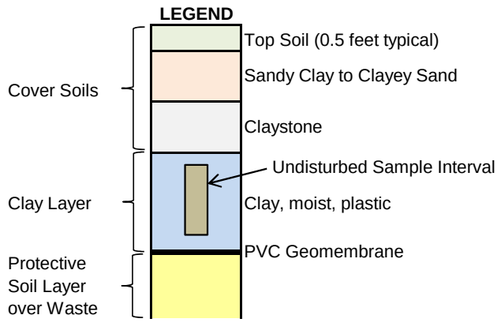


TABLE 2.2-2
Summary of Geotechnical Laboratory Tests on Undisturbed Soil Samples
Section I Cover
Pinewood Landfill
Pinewood, South Carolina

| | Sample Number | Sample Depth Below Grade (feet) | Date | | Atterberg Limits | | | Moisture Percent | Dry Density (pcf) | Soils Passing P200 Sieve (%) | Soils <0.005 mm (%) | Hydraulic Conductivity (cm/s) | USCS Classification |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | | | Sample Received | Sample Extracted | LL | PL | PI | | | | | | |
| Cover Test Pits | TP-1A-01 | 6-7 | 12/23/2010 | 01/04/11 | 50 | 23 | 27 | 29.2 | 96.2 | 79.3 | 37.8 | $1.04x10^{-7}$ | CH |
| | TP-1D-01 | 3-4 | 12/23/2010 | 01/04/11 | 46 | 23 | 23 | 21.5 | | 74.7 | | | CL |
| | TP-1D-02 | 3-5 | 12/23/2010 | 01/04/11 | 55 | 23 | 32 | 22.8 | 103.1 | 81.4 | 41.9 | $5.58x10^{-8}$ | CH |
| | TP-1E-01A | 3-5 | 12/23/2010 | 01/04/11 | 59 | 21 | 38 | 27.6 | 96.4 | 78.5 | 45.0 | $7.74x10^{-8}$ | CH |
| | TP-1E-01B | 3-5 | 12/23/2010 | 01/04/11 | | | | 29.6 | | | | | |
| Soil Test Borings | SB-1A-01 | 6-8 | 12/23/2010 | 01/04/11 | | | | 50.7 | | | | | |
| | SB-1A-01(A) | 6-8 | 12/23/2010 | 01/04/11 | 47 | 23 | 24 | 33.4 | 87.4 | 85.8 | 37.1 | $1.71x10^{-7}$ | CL |
| | SB-1B-2 | 4.5-6.5 | 12/23/2010 | 01/04/11 | | | | 24.1 | | | | | |
| | SB-1B-2(A) | 4.5-6.5 | 12/23/2010 | 01/04/11 | 58 | 25 | 33 | 30.2 | 91.6 | 90.6 | 47.7 | $2.65x10^{-8}$ | CH |
| | SB-1B-3 | 4-5.5 | 12/23/2010 | 01/04/11 | 44 | 23 | 21 | 27.9 | 99.5 | 71.1 | 33.0 | $1.38x10^{-8}$ | CL |
| | SB-1C-04 | 3-5 | 12/23/2010 | 01/05/11 | | | | 13.4 | | | | | |
| | SB-1C-04(A) | 3-5 | 12/23/2010 | 01/05/11 | 33 | 16 | 17 | 16.7 | 108.9 | 45.8 | 26.0 | $8.74x10^{-8}$ | SC |
| | SB-1C-05 | 6-8 | 12/23/2010 | 01/05/11 | | | | 21.5 | | | | | |
| | SB-1C-05(A) | 6-8 | 12/23/2010 | 01/05/11 | 38 | 17 | 21 | 16.2 | 112.6 | 37.2 | 27.9 | $1.85x10^{-8}$ | SC |
| | SB-1D-06 | 4-6 | 12/23/2010 | 01/05/11 | 43 | 21 | 22 | 16.9 | 124.8 | 36.3 | 22 | $2.85x10^{-6}$ | SC |
| | SB-1D-06(A) | 4-6 | 12/23/2010 | 01/05/11 | | | | 16.9 | | 58.8 | | | CL |
| | SB-1D-07 | 7-9 | 12/23/2010 | 01/05/11 | 50 | 21 | 29 | 26.1 | | 77.6 | | | CH |
| | SB-1D-07(A)* | 7-9 | 12/23/2010 | 01/05/11 | | | | 11.6 | | | | | |
| | SB-1E-8 | 1.5-3.5 | 12/23/2010 | 01/05/11 | 57 | 20 | 37 | 22.8 | 104.8 | 72.0 | 46.3 | $2.33x10^{-6}$ | CH |
| | SB-1E-8(A) | 1.5-3.5 | 12/23/2010 | 01/05/11 | | | | 18.2 | | | | | |
| | SB-1E-9 | 2.5-4.5 | 12/23/2010 | 01/05/11 | | | | 24.7 | | | | | SC |
| | SB-1E-9(A) | 2.5-4.5 | 12/23/2010 | 01/05/11 | 50 | 21 | 29 | 25.2 | | | | | CH |
| | SB-1E-10 | 2-4 | 12/23/2010 | 01/05/11 | | | | 10.7 | | | | | |
| | SB-1E-10(A) | 2-4 | 12/23/2010 | 01/05/11 | 50 | 21 | 29 | 22.1 | | 73.9 | | | CH |

Notes:

LL = Liquid Limit
PL = Plastic Limit
PI = Plasticity Index
pcf = pounds per cubic foot
cm/s = centimeters per second
mm = millimeters
USCS = Unified Soil Classification System
(A) ~ denotes the bottom portion of the Shelby tube
Unless Noted Otherwise Testing Was Performed on Clay Layer above PVC Geomembrane

Cover Soils above Clay Layer
* ~ soil below PVC geomembrane

TABLE 2.2-3
Summary of Geotechnical Laboratory Tests on Bulk Soil Samples
Section I Cover
Pinewood Landfill
Pinewood, South Carolina

| | Sample Number | Sample Depth Below Grade (feet) | Date Sample Received | Atterberg Limits | | | Soils Passing P200 Sieve (%) | USCS Classification |
|---|---|---|---|---|---|---|---|---|
| | | | | LL | PL | PI | | |
| **Anchor Trench Test Pits** | AT-1B-01 | | 12/23/2010 | 40 | 28 | 12 | 52.2 | ML |
| | AT-1C-01 | | 12/23/2010 | 40 | 27 | 13 | 43.4 | SM |
| | AT-1E-01 | | 12/23/2010 | 53 | 29 | 24 | | CH |
| **Soil Test Borings** | SB-1A-01 | 0-2 | 12/23/2010 | 34 | 25 | 9 | | SC |
| | SB-1B-02 | 2-4 | 12/23/2010 | 36 | 23 | 13 | 29.2 | SC |
| | SB-1C-04 | 2-4 | 12/23/2010 | NP | NP | NP | | SM |
| | SB-1D-06 | 2-4 | 12/23/2010 | 47 | 36 | 11 | 15.5 | SM |
| | SB-1D-07 | 0-2 | 12/23/2010 | NP | NP | NP | 36.6 | SM |
| **Cover Test Pits** | TP-1A-01 | | 12/23/2010 | 39 | 18 | 21 | 39.1 | SC |
| | TP-1D-01 | | 12/23/2010 | NP | NP | NP | 26.4 | SM |
| | TP-1D-02 | | 12/23/2010 | NP | NP | NP | 27.2 | SM |
| | TP-1E-01 | 1-2 | 12/23/2010 | 25 | 14 | 11 | 18.6 | SC |
| | TP-1E-01 | 2-2.9 | 12/23/2010 | NP | NP | NP | 15.4 | SM |

Notes:
LL = Liquid Limit
PL = Plastic Limit
PI = Plasticity Index
USCS = Unified Soil Classification System

TABLE 2.2-4
Summary of PVC Geomembrane Test Results
Section I Cover
Pinewood Landfill
Pinewood, South Carolina

| | Sample No. | Mean Thickness (mils) | Tensile Strength at 100% Strain (ppi) | Break Strength (ppi) | Break Elongation % | Depth Below Grade or Cover Thickness (feet) | Seam Peel Strength @100% Peel Incursion (ppi) | Seam Shear Strength @ 100% Shear Elongation (ppi) | Percent Plasticizer % |
|---|---|---|---|---|---|---|---|---|---|
| **Anchor Trench Test Pits** | AT-1A-01(A) | 16.7 | 54 | 60 | 210 | 4.0 | | | 16.3 |
| | AT-1A-01(B) | | 50 | 53 | 178 | | | | |
| | AT-1B-01 (A) | 18.2 | 48 | 55 | 198 | 4.5 | | | |
| | AT-1B-01 (B) | | 48 | 54 | 209 | | | | |
| | AT-1C-01 (A) | 20.2 | 42 | 58 | 270 | 6.0 | 18.0 | 46.0 | |
| | AT-1C-01 (B) | | 38 | 52 | 266 | | | | |
| | AT-1E-01 (A) | 19.6 | 35 | 44 | 232 | 4.5 | | 47.0 | |
| | AT-1E-01 (B) | | 32 | 45 | 263 | | | | |
| | AT-1E-02 (A) | 19.2 | 36 | 50 | 278 | 3.5 | | | |
| | AT-1E-02 (B) | | 36 | 53 | 323 | | | | |
| **Cover Test Pits** | TP-1A-01(A) | 18.6 | 37 | 54 | 302 | 8.0 | | | |
| | TP-1A-01(B) | | 31 | 46 | 302 | | | | |
| | TP-1A-01-Lower (A) | 18.8 | 36 | 51 | 285 | 8.0 | | | |
| | TP-1A-01-Lower (B) | | 31 | 50 | 367 | | | | |
| | TP-1D-01(A) | 20.3 | 31 | 55 | 462 | 4.7 | | | |
| | TP-1D-01(B) | | 35 | 54 | 362 | | | | |
| | TP-1D-02(A) | 18.6 | 35 | 57 | 342 | 5.8 | | | |
| | TP-1D-02(B) | | 32 | 52 | 357 | | | | |
| | TP-1E-01(A) | 19.9 | 46 | 59 | 337 | 5.0 | | | |
| | TP-1E-01(B) | | 31 | 48 | 334 | | | | |

Notes:
mil = one-thousandth of an inch
ppi = pounds per inch

**SPECIFICATIONS FOR NEW 20-mil PVC GEOMEMBRANE:**
Thickness ~ 20mils (+/- 1mil)
Tensile Strength at 100 percent Strain ~ 20 ppi
Break Strength at 100 percent Strain ~ 48 ppi
Break Elongation ~ 360 %
Peel Strength 12.5 ppi
Shear Strength 38.4 ppi
Percent Plasticizer ~ 30%

TABLE 2.4-1
Summary of Settlement Plate Survey Data - Section I Cover
Section I Cover
Pinewood Landfill
Pinewood, South Carolina

| PLATE NUMBER | A-1 | B-1 | B-2 | B-3 | C-1 | D-1 | D-2 | D-3 | D-4 | D-5 | E-1 | E-2 | E-3 |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| DATE | | | | | | | | | | | | | |
| Apr-83 | | | | | | 140.230 | 144.100 | 145.880 | 140.380 | 139.070 | | | |
| May-83 | | | | | | 141.000 | 143.930 | 145.630 | 141.210 | 138.900 | | | |
| Jan-84 | | | | | | 140.780 | 143.780 | 145.400 | 141.040 | 138.710 | | | |
| Jan-85 | | | | | | 140.650 | 143.660 | 145.230 | 140.890 | 138.560 | | | |
| Jul-86 | | | | | | 140.470 | 143.450 | | 140.660 | 138.380 | | | |
| Aug-87 | | | | | | 140.400 | 143.430 | | 140.630 | 138.300 | | | |
| Dec-87 | | | | | | 140.390 | 143.420 | | 140.620 | | | | |
| Jan-88 | | | | | | 140.380 | 143.410 | | 140.620 | | | | |
| Mar-88 | | | | | | 140.350 | 143.380 | | | | | | |
| Oct-89 | | | | | | 140.170 | 143.280 | | | 138.110 | | | |
| May-90 | | | | | | 140.170 | 143.280 | | | 138.110 | | | |
| Mar-92 | | | | | | 140.100 | 143.220 | | | 137.930 | | | |
| Jan-94 | | | | | | 140.400 | 143.390 | 145.220 | 140.620 | 138.190 | | | |
| Mar-94 | | | | | | 140.390 | 143.410 | 145.230 | 140.640 | 138.200 | | | |
| Jun-94 | | | | | | 140.360 | 143.410 | 145.220 | 140.640 | 138.200 | | | |
| Sep-94 | | | | | | 140.330 | 143.400 | 145.190 | 140.630 | 138.190 | | | |
| Dec-94 | | | | | | 140.310 | 143.390 | 145.170 | 140.630 | 138.190 | | | |
| Mar-95 | | | | | | 140.320 | 143.410 | 145.170 | 140.650 | 138.180 | | | |
| Jun-95 | | | | | | 140.290 | 143.390 | 145.150 | 140.630 | 138.160 | | | |
| Sep-95 | | | | | | 140.260 | 143.370 | 145.110 | 140.600 | 138.130 | | | |
| Dec-95 | | | | | | 140.250 | 143.370 | 145.100 | 140.600 | 138.120 | | | |
| Mar-96 | | | | | | 140.290 | 143.410 | 145.130 | 140.640 | 138.150 | | | |
| Jun-96 | | | | | | 140.270 | 143.400 | 145.120 | 140.630 | 138.150 | | | |
| Sep-96 | | | | | | 140.240 | 143.370 | 145.070 | 140.600 | 138.110 | | | |
| Dec-96 | | | | | | 140.230 | 143.370 | 145.070 | 140.610 | 138.120 | | | |
| Mar-97 | | | | | | 140.240 | 143.380 | 145.070 | 140.620 | 138.120 | | | |
| Jun-97 | | | | | | 140.220 | 143.380 | 145.050 | 140.600 | 138.100 | | | |
| Sep-97 | | | | | | 140.220 | 143.380 | 145.050 | 140.600 | 138.100 | | | |
| Dec-97 | | | | | | 140.190 | 143.360 | 145.020 | 140.540 | 138.080 | | | |
| Mar-98 | | | | | | 140.180 | 143.340 | 144.990 | 140.480 | 138.040 | | | |
| Jun-98 | | | | | | 140.130 | 143.310 | 144.950 | 140.420 | 137.990 | | | |
| Sep-98 | | | | | | 140.120 | 143.300 | 144.930 | 140.390 | 137.960 | | | |
| Dec-98 | | | | | | 140.160 | 143.340 | 144.960 | 140.430 | 137.990 | | | |
| Mar-99 | | | | | | 140.170 | 143.360 | 144.970 | 140.430 | 137.990 | | | |
| Jun-99 | | | | | | 140.150 | 143.350 | 144.950 | 140.400 | 137.970 | | | |
| Sep-99 | | | | | | 140.105 | 143.303 | 144.900 | 140.344 | 137.905 | | | |
| Dec-99 | | | | | | 140.142 | 143.350 | 144.933 | 140.370 | 137.623 | | | |
| Mar-00 | | | | | | 140.122 | 143.334 | 144.906 | 140.348 | 137.896 | | | |
| May-00 | | | | | | 140.156 | 143.372 | 144.934 | 140.375 | 137.925 | | | |
| Sep-00 | | | | | | 140.099 | 143.303 | 144.864 | 140.301 | 137.850 | | | |
| Dec-00 | | | | | | 140.128 | 143.334 | 144.887 | 140.331 | 137.873 | | | |
| Mar-01 | | | | | | 140.070 | 143.279 | 144.829 | 140.278 | 137.818 | | | |
| Jun-01 | | | | | | 140.084 | 143.292 | 144.832 | 140.284 | 137.823 | | | |
| Sep-01 | | | | | | 140.083 | 143.294 | 144.827 | 140.286 | 137.825 | | | |

TABLE 2.4-1
Summary of Settlement Plate Survey Data - Section I Cover
Section I Cover
Pinewood Landfill
Pinewood, South Carolina

| PLATE NUMBER | A-1 | B-1 | B-2 | B-3 | C-1 | D-1 | D-2 | D-3 | D-4 | D-5 | E-1 | E-2 | E-3 |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| DATE | | | | | | | | | | | | | |
| Jan-02 | | | | | | 140.079 | 143.296 | 144.815 | 140.281 | 137.812 | | | |
| Mar-02 | | | | | | 140.053 | 143.271 | 144.782 | 140.257 | 137.787 | | | |
| Jun-02 | | | | | | 140.092 | 143.312 | 144.821 | 140.300 | 137.831 | | | |
| Sep-02 | | | | | | 140.048 | 143.269 | 144.768 | 140.250 | 137.778 | | | |
| Dec-02 | 132.065 | 141.269 | 143.198 | 138.548 | 143.692 | 140.039 | 143.265 | 144.756 | 140.250 | 137.772 | 143.259 | 142.961 | 141.442 |
| Mar-03 | 132.067 | 141.270 | 143.203 | 138.551 | 143.679 | 140.042 | 143.272 | 144.752 | 140.253 | 137.769 | 143.271 | 142.958 | 141.447 |
| Jun-03 | 132.041 | 141.234 | 143.178 | 138.527 | 143.624 | 140.008 | 143.256 | 144.720 | 140.235 | 137.748 | 143.251 | 142.938 | 141.435 |
| Sep-03 | 132.047 | 141.233 | 143.184 | 138.535 | 143.604 | 140.012 | 143.247 | 144.705 | 140.224 | 137.735 | 143.249 | 142.929 | 141.431 |
| Dec-03 | 132.045 | 141.229 | 143.187 | 138.536 | 143.584 | 140.017 | 143.256 | 144.699 | 140.227 | 137.731 | 143.260 | 142.929 | 141.437 |
| Mar-04 | 131.953 | 141.093 | 143.063 | 138.433 | 143.488 | | 143.206 | 144.646 | 140.193 | 137.688 | 143.186 | 142.876 | 141.367 |
| Jun-04 | 132.019 | 141.200 | 143.184 | 138.518 | 143.496 | | 143.238 | 144.652 | 140.199 | 137.693 | 143.239 | 142.888 | 141.423 |
| Sep-04 | 132.005 | 141.176 | 143.165 | 138.501 | 143.483 | | 143.219 | 144.631 | 140.183 | 137.675 | 143.226 | 142.878 | 141.408 |
| Mar-05 | | | | | | 139.937 | 143.202 | 144.602 | 140.157 | 137.642 | | | |
| Aug-05 | | | | | | 139.952 | 143.227 | 144.597 | 140.157 | 137.632 | | | |
| Sep-05 | 132.011 | 141.167 | 143.188 | 138.516 | 143.447 | 139.982 | 143.252 | 144.631 | 140.204 | 137.681 | 143.261 | 142.893 | 141.441 |
| Dec-05 | 132.029 | 141.182 | 143.206 | 138.534 | 143.456 | 139.995 | 143.259 | 144.636 | 140.211 | 137.681 | 143.270 | 142.894 | 141.448 |
| Mar-06 | 131.988 | 141.153 | 143.175 | 138.494 | 143.397 | 139.951 | 143.219 | 144.588 | 140.172 | 137.636 | 143.231 | 142.852 | 141.412 |
| May-06 | 132.005 | 141.149 | 143.188 | 138.506 | 143.403 | 139.969 | 143.240 | 144.600 | 140.189 | 137.653 | 143.252 | 142.871 | 141.436 |
| Sep-06 | 132.034 | 141.173 | 143.219 | 138.535 | 143.418 | 139.999 | 143.270 | 144.619 | 140.212 | 137.676 | 143.283 | 142.895 | 141.465 |
| Nov-06 | 132.019 | 141.17 | 143.215 | 138.523 | 143.401 | 139.986 | 143.262 | 144.609 | 140.209 | 137.664 | 143.279 | 142.879 | 141.458 |
| Feb-07 | 132.038 | 141.181 | 143.238 | 138.546 | 143.405 | 140.000 | 143.281 | 144.615 | 140.219 | 137.668 | 143.290 | 142.887 | 141.473 |
| May-07 | 132.009 | 141.142 | 143.214 | 138.517 | 143.369 | 139.966 | 143.261 | 144.589 | 140.192 | 137.637 | 143.272 | 142.867 | 141.456 |
| Aug-07 | 131.976 | 141.133 | 143.186 | 138.493 | 143.339 | 139.961 | 143.246 | 144.567 | 140.176 | 137.616 | 143.258 | 142.848 | 141.441 |
| Nov-07 | 131.964 | 141.103 | 143.177 | 138.48 | 143.305 | 139.929 | 143.221 | 144.539 | 140.150 | 137.584 | 143.231 | 142.813 | 141.413 |
| Mar-08 | 131.95 | 141.088 | 143.169 | 138.469 | 143.282 | 139.927 | 143.216 | 144.524 | 140.140 | 137.574 | 143.229 | 142.802 | 141.410 |
| May-08 | 131.944 | 141.073 | 143.162 | 138.459 | 143.265 | 139.896 | 143.193 | 144.510 | 140.129 | 137.553 | 143.215 | 142.791 | 141.405 |
| Aug-08 | 131.935 | 141.054 | 143.154 | 138.447 | 143.247 | 139.878 | 143.177 | 144.497 | 140.123 | 137.545 | 143.208 | 142.779 | 141.398 |
| Nov-08 | 131.926 | 141.072 | 143.151 | 138.442 | 143.23 | 139.888 | 143.190 | 144.480 | 140.109 | 137.533 | 143.219 | 142.779 | 141.399 |
| Mar-09 | 131.918 | 141.049 | 143.161 | 138.448 | 143.219 | 139.861 | 143.175 | 144.472 | 140.111 | 137.519 | 143.217 | 142.770 | 141.400 |
| Jun-09 | 131.949 | 141.075 | 143.185 | 138.474 | 143.246 | 139.893 | 143.212 | | 140.147 | 137.548 | 143.263 | 142.811 | 141.451 |
| Oct-09 | 131.908 | 141.037 | 143.155 | 138.439 | 143.184 | 139.831 | 143.149 | 144.441 | 140.098 | 137.476 | 143.207 | 142.750 | 141.396 |
| Dec-09 | 131.919 | 141.052 | 143.18 | 138.452 | 143.201 | 139.853 | 143.185 | 144.470 | 140.127 | 137.498 | 143.250 | 142.781 | 141.437 |
| Mar-10 | 131.875 | 140.999 | 143.133 | 138.405 | 143.13 | 139.793 | 143.126 | 144.401 | 140.070 | | 143.188 | 142.712 | 141.369 |
| Jun-10 | 131.896 | 141.028 | 143.163 | 138.442 | 143.165 | 139.825 | 143.163 | 144.433 | 140.121 | 137.473 | 143.232 | 142.761 | 141.423 |
| Oct-10 | 131.931 | 141.052 | 143.195 | 138.471 | 143.187 | 139.864 | 143.207 | 144.468 | 140.158 | 137.502 | 143.283 | 142.794 | 141.462 |
| Lifetime Total Δ (ft) | -0.13400 | -0.21700 | -0.00300 | -0.07700 | -0.50500 | -0.36600 | -0.89300 | -1.41200 | -0.22200 | -1.56800 | 0.02400 | -0.16700 | 0.02000 |
| Average Quarterly Δ (ft) | -0.00462 | -0.00748 | -0.00010 | -0.00266 | -0.01741 | -0.00482 | -0.01130 | -0.02017 | -0.00296 | -0.02091 | 0.00083 | -0.00576 | 0.00069 |
| Maximum | 132.07 | 141.27 | 143.24 | 138.55 | 143.69 | 141.00 | 144.10 | 145.88 | 141.21 | 139.07 | 143.29 | 142.96 | 141.47 |
| Minimum | 131.88 | 141.00 | 143.06 | 138.41 | 143.13 | 139.79 | 143.13 | 144.40 | 140.07 | 137.47 | 143.19 | 142.71 | 141.37 |

* Surveyed by Virogroup. All previous elevations were surveyed by Mathis. Virogroup's control system is +0.12 above Mathis' last remaining benchmark on site. All five (5) settlement plates were replaced. The two (2) destroyed plates were reset to last known elevation. The three (3) bent plates were reset by measuring distance from ground to bend and bend to top of casing.

OUTLIERS REMOVED

| | | | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | row 57 is start of measurements | | | | | row 9 is start of measurements | | | | | row 57 is start of measurements | | |
| | 132.065 | 141.269 | 143.198 | 138.548 | 143.692 | 140.230 | 144.100 | 145.880 | 140.380 | 139.070 | 143.259 | 142.961 | 141.442 |
| | | | | | | row 21 was used previously | | | | | | | |
| | | | | | | 140.400 | 143.390 | 145.220 | 140.620 | 138.190 | | | |

TABLE 2.4-2
Summary of Projected Settlement
Section I Cover
Pinewood Landfill
Pinewood, South Carolina

**Section I Landfill**

| Cells | Cell A | | | | Cell B | | | Cell C | | | Cell D | | | Cell E | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| **Sumps** | 1A1P | 1A2P | 1A3P | 1A4P | 1B1P | 1B2P | 1B3P | 1C1P | 1C2P | 1C3P | 1D1P | 1D2P | 1D3P | 1E1P | 1E2P | 1E3P |
| **1996** | Note 1 | Note 1 | Note 1 | Note 1 | Note 1 | Note 1 | Note 1 | Note 1 | Note 1 | Note 1 | Note 2 | Note 2 | Note 2 | Note 1 | Note 1 | Note 1 |
| **1997** | Note 1 | Note 1 | Note 1 | Note 1 | Note 1 | Note 1 | Note 1 | Note 1 | Note 1 | Note 1 | 5,938 | 16,553 | 9,075 | Note 1 | Note 1 | Note 1 |
| **1998** | Note 1 | Note 1 | Note 1 | Note 1 | Note 1 | Note 1 | Note 1 | Note 1 | Note 1 | Note 1 | 3,231 | 25,712 | 10,633 | Note 1 | Note 1 | Note 1 |
| **1999** | Note 1 | Note 1 | Note 1 | Note 1 | Note 1 | Note 1 | Note 1 | Note 1 | Note 1 | Note 1 | 4,594 | 21,972 | 10,314 | Note 1 | Note 1 | Note 1 |
| **2000** | Note 1 | Note 1 | Note 1 | Note 1 | Note 1 | Note 1 | Note 1 | Note 1 | Note 1 | Note 1 | 3,150 | 29,350 | 10,612 | Note 1 | Note 1 | Note 1 |
| **2001** | Note 1 | Note 1 | Note 1 | Note 1 | Note 1 | Note 1 | Note 1 | Note 1 | Note 1 | Note 1 | 3,012 | 21,132 | 11,702 | Note 1 | Note 1 | Note 1 |
| **2002** | 3,626 | 5,814 | 2,804 | 3,331 | 2,972 | 4,593 | 3,233 | 17,877 | 10,573 | 8,012 | 1,472 | 15,641 | 13,068 | 6,451 | 7,235 | 3,102 |
| **2003** | 6,813 | 8,735 | 3,341 | 6,807 | 5,893 | 6,711 | 3,960 | 9,045 | 11,182 | 11,662 | 1,417 | 29,798 | 21,310 | 8,455 | 8,613 | 3,610 |
| **2004** | 4,128 | 5,039 | 2,495 | 3,631 | 3,865 | 3,787 | 2,722 | 7,189 | 8,923 | 8,576 | 1,418 | 14,317 | 24,855 | 3,554 | 5,045 | 4,441 |
| **2005** | 7,114 | 10,897 | 5,804 | 6,924 | 12,008 | 11,978 | 6,935 | 25,638 | 18,342 | 19,353 | 4,695 | 33,714 | 11,594 | 8,209 | 10,021 | 7,074 |
| **2006** | 9,830 | 11,293 | 9,503 | 8,575 | 15,065 | 11,591 | 7,992 | 16,930 | 18,541 | 22,190 | 4,757 | 28,425 | 8,141 | 9,140 | 10,967 | 7,044 |
| **2007** | 9,448 | 12,858 | 8,580 | 17,758 | 10,565 | 14,398 | 7,862 | 38,622 | 33,450 | 43,049 | 4,057 | 50,080 | 28,464 | 17,047 | 16,546 | 12,405 |
| **2008** | 12,995 | 19,651 | 8,082 | 13,678 | 11,524 | 14,221 | 8,846 | 30,554 | 32,054 | 37,087 | 2,476 | 46,478 | 23,148 | 13,464 | 18,343 | 8,330 |
| **2009** | 11,263 | 18,172 | 8,774 | 14,351 | 12,660 | 16,155 | 15,700 | 27,948 | 27,023 | 42,635 | 8,948 | 85,901 | 26,712 | 12,298 | 16,123 | 8,860 |
| **2010** | 9,267 | 21,657 | 7,549 | 11,564 | 18,046 | 14,088 | 8,351 | 27,143 | 35,985 | 41,814 | 13,083 | 121,769 | 24,565 | 10,892 | 14,670 | 7,848 |
| **Gallons Leachate Removed** | 74,484 | 114,117 | 56,932 | 86,620 | 92,598 | 97,521 | 65,601 | 200,945 | 196,072 | 234,376 | 62,248 | 540,843 | 234,193 | 89,511 | 107,563 | 62,714 |
| **Cubic Feet Removed** | 9,958 | 15,256 | 7,611 | 11,580 | 12,379 | 13,038 | 8,770 | 26,864 | 26,213 | 31,334 | 8,322 | 72,305 | 31,309 | 11,967 | 14,380 | 8,384 |
| **Surface Area Attributed to Sump (SF)** | 58,465 | 42,275 | 39,620 | 49,305 | 40,435 | 27,920 | 49,060 | 56,500 | 43,465 | 49,000 | 59,140 | 40,040 | 51,275 | 120,680 | 108,365 | 115,053 |
| **Average Projected Settlement (ft)** | 0.17 | 0.36 | 0.19 | 0.23 | 0.31 | 0.47 | 0.18 | 0.48 | 0.60 | 0.64 | 0.14 | 1.81 | 0.61 | 0.10 | 0.13 | 0.07 |
| **Cumulative Settlement at Near-by Marker (ft)** | NA | NA | NA | NA | NA | 0.22 | 0.08 | NA | 0.50 | NA | 0.38 | 0.60 | 0.62 | NA | 0.17 | NA |
| **Gallons Leachate Removed** | 332,153 | | | | 255,720 | | | 631,393 | | | 837,284 | | | 259,789 | | |
| **Cubic Feet Removed** | 44,405 | | | | 34,187 | | | 84,411 | | | 111,936 | | | 34,731 | | |
| **Surface Area Attributed to Cell (SF)** | 189,665 | | | | 117,415 | | | 148,965 | | | 150,455 | | | 344,098 | | |
| **Average Projected Settlement (ft)** | 0.23 | | | | 0.29 | | | 0.57 | | | 0.74 | | | 0.10 | | |
| **Average Cumulative Measured Settlement (ft)** | 0.13 | | | | 0.10 | | | 0.50 | | | 0.45 | | | 0.04 | | |

Note 1 - Leachate data not used because settlement data was not available for this time period
Note 2 - Leachate data not available for this time period

TABLE 2.5-1
Soil Gas Survey Analytical Results
GORE Standard Target VOCs/SVOCs (A1)
Section I Cover
Pinewood Landfill
Pinewood, South Carolina

| DATE ANALYZED | FIELD ID | SAMPLE NAME | TPH | BTEX | BENZ | TOL | EtBENZ | mpXYL | oXYL |
|---|---|---|---|---|---|---|---|---|---|
| | | MDL= | 0.02 | | 0.02 | 0.02 | 0.02 | 0.03 | 0.02 |
| 11/19/10 | BG-01 | 648027 | 16.45 | 0.26 | 0.13 | 0.07 | 0.02 | 0.04 | bdl |
| 11/19/10 | BG-02 | 648028 | 0.11 | nd | nd | nd | nd | nd | nd |
| 11/18/10 | SG-1A-01 | 648029 | 0.12 | 0.06 | 0.06 | nd | nd | nd | nd |
| 11/19/10 | SG-1A-02 | 648030 | 0.09 | nd | nd | nd | nd | nd | nd |
| 11/19/10 | SG-1A-03 | 648031 | 0.31 | nd | nd | nd | nd | nd | nd |
| 11/19/10 | SG-1A-04 | 648032 | 0.18 | 0.02 | 0.02 | nd | nd | nd | nd |
| 11/19/10 | SG-1A-06 | 648033 | 0.19 | nd | nd | nd | nd | nd | nd |
| 11/19/10 | SG-1A-05 | 648034 | 0.16 | 0.04 | 0.04 | nd | nd | nd | nd |
| 11/19/10 | SG-1A-07 | 648035 | 0.04 | nd | nd | nd | nd | nd | nd |
| 11/20/10 | SG-1A-09 | 648036 | 0.06 | bdl | bdl | nd | nd | nd | nd |
| 11/20/10 | SG-1A-08 | 648037 | 0.08 | nd | nd | nd | nd | nd | nd |
| 11/19/10 | SG-1B-10 | 648038 | 0.08 | 0.06 | 0.06 | nd | nd | nd | nd |
| 11/18/10 | SG-1C-20 | 648039 | 18.29 | 0.20 | 0.20 | bdl | nd | nd | nd |
| 11/19/10 | SG-1B-11 | 648041 | 0.20 | nd | nd | nd | nd | nd | nd |
| 11/19/10 | SG-1B-12 | 648042 | 0.02 | 0.05 | 0.05 | nd | nd | nd | nd |
| 11/18/10 | SG-1B-13 | 648043 | 0.02 | bdl | bdl | nd | nd | nd | nd |
| 11/19/10 | SG-1B-14 | 648044 | 0.12 | 0.05 | 0.05 | nd | nd | nd | nd |
| 11/18/10 | SG-1B-15 | 648045 | 0.05 | nd | nd | nd | nd | nd | nd |
| 11/18/10 | SG-1B-16 | 648046 | 0.05 | 0.09 | 0.09 | nd | nd | nd | nd |
| 11/19/10 | SG-1B-22 | 648047 | 0.55 | 0.02 | 0.02 | nd | nd | nd | nd |
| 11/19/10 | SG-1B-24 | 648048 | 0.05 | 0.04 | 0.04 | nd | nd | nd | nd |
| 11/20/10 | SG-1B-26 | 648049 | 0.59 | 0.05 | 0.05 | nd | nd | nd | nd |
| 11/19/10 | SG-1B-17 | 648050 | 0.31 | 0.03 | 0.03 | nd | nd | nd | nd |
| 11/18/10 | SG-1B-18 | 648051 | 0.10 | 0.04 | 0.04 | nd | nd | nd | nd |
| 11/19/10 | SG-1C-27 | 648053 | 0.08 | 0.13 | 0.13 | nd | nd | nd | nd |
| 11/18/10 | SG-1D-35 | 648054 | 49.09 | 0.70 | 0.42 | 0.14 | 0.05 | 0.05 | 0.04 |
| 11/19/10 | SG-1C-25 | 648055 | 0.09 | 0.02 | 0.02 | nd | nd | nd | nd |
| 11/19/10 | SG-1D-33 | 648056 | 0.91 | 0.08 | 0.05 | 0.02 | nd | nd | bdl |
| 11/19/10 | SG-1C-23 | 648057 | 2.63 | 0.13 | 0.10 | 0.03 | nd | nd | bdl |
| 11/19/10 | SG-1C-21 | 648058 | 0.23 | 0.05 | 0.05 | nd | nd | nd | nd |
| 11/19/10 | SG-1D-31 | 648059 | 1.58 | 0.04 | 0.04 | nd | nd | nd | nd |
| 11/18/10 | SG-1D-30 | 648060 | 0.18 | 0.06 | 0.06 | nd | nd | nd | nd |
| 11/19/10 | SG-1D-32 | 648061 | 0.47 | 0.09 | 0.09 | nd | nd | nd | nd |
| 11/19/10 | SG-1D-34 | 648062 | 0.03 | 0.03 | 0.03 | nd | nd | nd | nd |
| 11/18/10 | SG-1D-36 | 648063 | bdl | nd | nd | nd | nd | nd | nd |
| 11/19/10 | SG-1E-49 | 648064 | 1.25 | 0.96 | 0.16 | 0.36 | 0.10 | 0.19 | 0.14 |
| 11/19/10 | SG-1E-48 | 648065 | 0.47 | 0.07 | 0.05 | nd | 0.02 | bdl | nd |
| 11/19/10 | SG-1E-44 | 648066 | 8.13 | 0.73 | 0.70 | nd | nd | nd | 0.03 |
| 11/19/10 | SG-1E-42 | 648067 | 0.12 | 0.05 | 0.05 | nd | nd | nd | nd |
| 11/19/10 | SG-1E-40 | 648068 | 0.24 | nd | nd | nd | nd | nd | nd |
| 11/19/10 | SG-1E-39 | 648069 | 0.38 | 0.20 | 0.20 | nd | nd | nd | nd |
| 11/18/10 | SG-1E-37 | 648070 | 0.47 | 0.03 | 0.03 | nd | nd | nd | nd |
| 11/19/10 | SG-1E-41 | 648071 | 0.10 | 0.02 | 0.02 | nd | nd | nd | nd |
| 11/19/10 | SG-1E-43 | 648072 | 0.08 | 0.55 | 0.52 | 0.03 | nd | nd | nd |
| 11/19/10 | SG-1E-46 | 648073 | 0.71 | 1.90 | 1.58 | 0.20 | nd | 0.05 | 0.06 |
| 11/19/10 | SG-1E-45 | 648074 | 0.39 | 0.04 | 0.04 | nd | nd | nd | nd |
| 11/19/10 | SG-1E-47 | 648075 | 0.09 | 0.09 | nd | nd | nd | nd | 0.09 |
| 11/19/10 | SG-1E-50 | 648076 | bdl | 0.04 | 0.04 | nd | nd | nd | nd |
| 11/18/10 | SG-1E-38 | 648077 | 25.83 | 0.07 | 0.07 | nd | nd | bdl | bdl |
| 11/19/10 | SG-1D-28 | 648078 | 0.07 | nd | nd | nd | nd | nd | nd |
| 11/19/10 | SG-1D-29 | 648079 | 0.48 | 0.03 | 0.03 | nd | nd | nd | nd |
| 11/18/10 | SG-1C-19 | 648080 | 0.53 | 0.05 | 0.05 | nd | nd | nd | nd |
| | | | | | | | | | |
| 11/19/10 | TRIP BLANK-01 | 648040 | nd | nd | nd | nd | nd | nd | nd |
| 11/19/10 | TRIP BLANK-02 | 648052 | nd | nd | nd | nd | nd | nd | nd |
| 11/19/10 | TRIP BLANK-03 | 648081 | nd | nd | nd | nd | nd | nd | nd |
| 11/19/10 | TRIP BLANK-04 | 648082 | nd | nd | nd | nd | nd | nd | nd |
| | | | | | | | | | |
| 11/18/10 | method blank | method blank | nd | nd | nd | nd | nd | nd | nd |
| 11/19/10 | method blank | method blank | nd | nd | nd | nd | nd | nd | nd |

TABLE 2.5-1
Soil Gas Survey Analytical Results
GORE Standard Target VOCs/SVOCs (A1)
Section I Cover
Pinewood Landfill
Pinewood, South Carolina

| DATE ANALYZED | FIELD ID | SAMPLE NAME | C11, C13, &C15 | UNDEC | TRIDEC | PENTADEC | TMBs | 124TMB | 135TMB |
|---|---|---|---|---|---|---|---|---|---|
| | | MDL= | | 0.04 | 0.02 | 0.02 | | 0.02 | 0.03 |
| 11/19/10 | BG-01 | 648027 | 0.07 | 0.07 | nd | nd | bdl | bdl | nd |
| 11/19/10 | BG-02 | 648028 | nd | nd | nd | nd | nd | nd | nd |
| 11/18/10 | SG-1A-01 | 648029 | nd | nd | nd | nd | nd | nd | nd |
| 11/19/10 | SG-1A-02 | 648030 | nd | nd | nd | nd | nd | nd | nd |
| 11/19/10 | SG-1A-03 | 648031 | nd | nd | nd | nd | nd | nd | nd |
| 11/19/10 | SG-1A-04 | 648032 | nd | nd | nd | nd | nd | nd | nd |
| 11/19/10 | SG-1A-06 | 648033 | nd | nd | nd | nd | nd | nd | nd |
| 11/19/10 | SG-1A-05 | 648034 | nd | nd | nd | nd | nd | nd | nd |
| 11/19/10 | SG-1A-07 | 648035 | nd | nd | nd | nd | nd | nd | nd |
| 11/20/10 | SG-1A-09 | 648036 | nd | nd | nd | nd | nd | nd | nd |
| 11/20/10 | SG-1A-08 | 648037 | nd | nd | nd | nd | nd | nd | nd |
| 11/19/10 | SG-1B-10 | 648038 | nd | nd | nd | nd | nd | nd | nd |
| 11/18/10 | SG-1C-20 | 648039 | nd | nd | nd | nd | nd | nd | nd |
| 11/19/10 | SG-1B-11 | 648041 | nd | nd | nd | nd | nd | nd | nd |
| 11/19/10 | SG-1B-12 | 648042 | nd | nd | nd | nd | nd | nd | nd |
| 11/18/10 | SG-1B-13 | 648043 | nd | nd | nd | nd | nd | nd | nd |
| 11/19/10 | SG-1B-14 | 648044 | nd | nd | nd | nd | nd | nd | nd |
| 11/18/10 | SG-1B-15 | 648045 | nd | nd | nd | nd | nd | nd | nd |
| 11/18/10 | SG-1B-16 | 648046 | nd | nd | nd | nd | nd | nd | nd |
| 11/19/10 | SG-1B-22 | 648047 | nd | nd | nd | nd | nd | nd | nd |
| 11/19/10 | SG-1B-24 | 648048 | nd | nd | nd | nd | nd | nd | nd |
| 11/20/10 | SG-1B-26 | 648049 | nd | nd | nd | nd | bdl | nd | bdl |
| 11/19/10 | SG-1B-17 | 648050 | nd | nd | nd | nd | nd | nd | nd |
| 11/18/10 | SG-1B-18 | 648051 | nd | nd | nd | nd | nd | nd | nd |
| 11/19/10 | SG-1C-27 | 648053 | nd | nd | nd | nd | nd | nd | nd |
| 11/18/10 | SG-1D-35 | 648054 | 0.09 | 0.09 | nd | nd | 0.02 | 0.02 | bdl |
| 11/19/10 | SG-1C-25 | 648055 | nd | nd | nd | nd | nd | nd | nd |
| 11/19/10 | SG-1D-33 | 648056 | nd | nd | nd | nd | nd | nd | nd |
| 11/19/10 | SG-1C-23 | 648057 | bdl | bdl | nd | nd | bdl | bdl | bdl |
| 11/19/10 | SG-1C-21 | 648058 | nd | nd | nd | nd | nd | nd | nd |
| 11/19/10 | SG-1D-31 | 648059 | nd | nd | nd | nd | nd | nd | nd |
| 11/18/10 | SG-1D-30 | 648060 | nd | nd | nd | nd | nd | nd | nd |
| 11/19/10 | SG-1D-32 | 648061 | nd | nd | nd | nd | nd | nd | nd |
| 11/19/10 | SG-1D-34 | 648062 | nd | nd | nd | nd | nd | nd | nd |
| 11/18/10 | SG-1D-36 | 648063 | nd | nd | nd | nd | nd | nd | nd |
| 11/19/10 | SG-1E-49 | 648064 | nd | nd | nd | nd | bdl | nd | bdl |
| 11/19/10 | SG-1E-48 | 648065 | nd | nd | nd | nd | nd | nd | nd |
| 11/19/10 | SG-1E-44 | 648066 | bdl | bdl | nd | nd | nd | nd | nd |
| 11/19/10 | SG-1E-42 | 648067 | nd | nd | nd | nd | nd | nd | nd |
| 11/19/10 | SG-1E-40 | 648068 | nd | nd | nd | nd | nd | nd | nd |
| 11/19/10 | SG-1E-39 | 648069 | nd | nd | nd | nd | nd | nd | nd |
| 11/18/10 | SG-1E-37 | 648070 | nd | nd | nd | nd | nd | nd | nd |
| 11/19/10 | SG-1E-41 | 648071 | nd | nd | nd | nd | nd | nd | nd |
| 11/19/10 | SG-1E-43 | 648072 | nd | nd | nd | nd | nd | nd | nd |
| 11/19/10 | SG-1E-46 | 648073 | nd | nd | nd | nd | nd | nd | nd |
| 11/19/10 | SG-1E-45 | 648074 | nd | nd | nd | nd | nd | nd | nd |
| 11/19/10 | SG-1E-47 | 648075 | nd | nd | nd | nd | nd | nd | nd |
| 11/19/10 | SG-1E-50 | 648076 | nd | nd | nd | nd | nd | nd | nd |
| 11/18/10 | SG-1E-38 | 648077 | 0.02 | bdl | 0.02 | bdl | 0.04 | 0.04 | bdl |
| 11/19/10 | SG-1D-28 | 648078 | nd | nd | nd | nd | nd | nd | nd |
| 11/19/10 | SG-1D-29 | 648079 | nd | nd | nd | nd | nd | nd | nd |
| 11/18/10 | SG-1C-19 | 648080 | nd | nd | nd | nd | nd | nd | nd |
| | | | | | | | | | |
| 11/19/10 | TRIP BLANK-01 | 648040 | nd | nd | nd | nd | nd | nd | nd |
| 11/19/10 | TRIP BLANK-02 | 648052 | nd | nd | nd | nd | nd | nd | nd |
| 11/19/10 | TRIP BLANK-03 | 648081 | nd | nd | nd | nd | nd | nd | nd |
| 11/19/10 | TRIP BLANK-04 | 648082 | nd | nd | nd | nd | nd | nd | nd |
| | | | | | | | | | |
| 11/18/10 | method blank | method blank | nd | nd | nd | nd | nd | nd | nd |
| 11/19/10 | method blank | method blank | nd | nd | nd | nd | nd | nd | nd |

TABLE 2.5-1
Soil Gas Survey Analytical Results
GORE Standard Target VOCs/SVOCs (A1)
Section I Cover
Pinewood Landfill
Pinewood, South Carolina

| DATE ANALYZED | FIELD ID | SAMPLE NAME | ct12DCE | t12DCE | c12DCE | NAPH&2-MN | NAPH | 2MeNAPH | MTBE |
|---|---|---|---|---|---|---|---|---|---|
| | | MDL= | | 0.04 | 0.03 | | 0.02 | 0.02 | 0.03 |
| 11/19/10 | BG-01 | 648027 | nd | nd | nd | nd | nd | nd | nd |
| 11/19/10 | BG-02 | 648028 | nd | nd | nd | nd | nd | nd | nd |
| 11/18/10 | SG-1A-01 | 648029 | nd | nd | nd | nd | nd | nd | nd |
| 11/19/10 | SG-1A-02 | 648030 | nd | nd | nd | nd | nd | nd | nd |
| 11/19/10 | SG-1A-03 | 648031 | nd | nd | nd | nd | nd | nd | nd |
| 11/19/10 | SG-1A-04 | 648032 | nd | nd | nd | nd | nd | nd | nd |
| 11/19/10 | SG-1A-06 | 648033 | nd | nd | nd | nd | nd | nd | nd |
| 11/19/10 | SG-1A-05 | 648034 | nd | nd | nd | nd | nd | nd | nd |
| 11/19/10 | SG-1A-07 | 648035 | nd | nd | nd | nd | nd | nd | nd |
| 11/20/10 | SG-1A-09 | 648036 | nd | nd | nd | nd | nd | nd | nd |
| 11/20/10 | SG-1A-08 | 648037 | nd | nd | nd | nd | nd | nd | nd |
| 11/19/10 | SG-1B-10 | 648038 | nd | nd | nd | nd | nd | nd | nd |
| 11/18/10 | SG-1C-20 | 648039 | 26.33 | 4.00 | 22.33 | nd | nd | nd | nd |
| 11/19/10 | SG-1B-11 | 648041 | nd | nd | nd | nd | nd | nd | nd |
| 11/19/10 | SG-1B-12 | 648042 | nd | nd | nd | nd | nd | nd | nd |
| 11/18/10 | SG-1B-13 | 648043 | 0.22 | 0.06 | 0.16 | nd | nd | nd | nd |
| 11/19/10 | SG-1B-14 | 648044 | nd | nd | nd | nd | nd | nd | nd |
| 11/18/10 | SG-1B-15 | 648045 | bdl | bdl | nd | nd | nd | nd | nd |
| 11/18/10 | SG-1B-16 | 648046 | 1.43 | 0.68 | 0.75 | nd | nd | nd | nd |
| 11/19/10 | SG-1B-22 | 648047 | nd | nd | nd | nd | nd | nd | nd |
| 11/19/10 | SG-1B-24 | 648048 | nd | nd | nd | nd | nd | nd | nd |
| 11/20/10 | SG-1B-26 | 648049 | bdl | bdl | nd | nd | nd | nd | nd |
| 11/19/10 | SG-1B-17 | 648050 | nd | nd | nd | nd | nd | nd | nd |
| 11/18/10 | SG-1B-18 | 648051 | 0.35 | 0.14 | 0.21 | nd | nd | nd | nd |
| 11/19/10 | SG-1C-27 | 648053 | nd | nd | nd | nd | nd | nd | nd |
| 11/18/10 | SG-1D-35 | 648054 | nd | nd | nd | bdl | nd | bdl | nd |
| 11/19/10 | SG-1C-25 | 648055 | nd | nd | nd | nd | nd | nd | nd |
| 11/19/10 | SG-1D-33 | 648056 | nd | nd | nd | nd | nd | nd | nd |
| 11/19/10 | SG-1C-23 | 648057 | nd | nd | nd | nd | nd | nd | nd |
| 11/19/10 | SG-1C-21 | 648058 | nd | nd | nd | nd | nd | nd | nd |
| 11/19/10 | SG-1D-31 | 648059 | nd | nd | nd | nd | nd | nd | nd |
| 11/18/10 | SG-1D-30 | 648060 | 0.22 | 0.04 | 0.18 | nd | nd | nd | nd |
| 11/19/10 | SG-1D-32 | 648061 | 0.63 | nd | 0.63 | nd | nd | nd | nd |
| 11/19/10 | SG-1D-34 | 648062 | nd | nd | nd | nd | nd | nd | nd |
| 11/18/10 | SG-1D-36 | 648063 | 0.07 | bdl | 0.07 | nd | nd | nd | nd |
| 11/19/10 | SG-1E-49 | 648064 | 0.47 | 0.04 | 0.43 | nd | nd | nd | nd |
| 11/19/10 | SG-1E-48 | 648065 | bdl | nd | bdl | nd | nd | nd | bdl |
| 11/19/10 | SG-1E-44 | 648066 | 31.43 | 1.02 | 30.41 | nd | nd | nd | nd |
| 11/19/10 | SG-1E-42 | 648067 | 0.45 | 0.10 | 0.35 | nd | nd | nd | bdl |
| 11/19/10 | SG-1E-40 | 648068 | nd | nd | nd | nd | nd | nd | nd |
| 11/19/10 | SG-1E-39 | 648069 | 0.22 | nd | 0.22 | nd | nd | nd | nd |
| 11/18/10 | SG-1E-37 | 648070 | nd | nd | nd | nd | nd | nd | 0.04 |
| 11/19/10 | SG-1E-41 | 648071 | 0.60 | 0.20 | 0.39 | nd | nd | nd | nd |
| 11/19/10 | SG-1E-43 | 648072 | 14.04 | 1.08 | 12.95 | nd | nd | nd | nd |
| 11/19/10 | SG-1E-46 | 648073 | 5.48 | 0.90 | 4.57 | nd | nd | nd | nd |
| 11/19/10 | SG-1E-45 | 648074 | nd | nd | nd | nd | nd | nd | nd |
| 11/19/10 | SG-1E-47 | 648075 | 0.22 | bdl | 0.22 | nd | nd | nd | bdl |
| 11/19/10 | SG-1E-50 | 648076 | nd | nd | nd | nd | nd | nd | nd |
| 11/18/10 | SG-1E-38 | 648077 | nd | nd | nd | 0.16 | 0.07 | 0.10 | nd |
| 11/19/10 | SG-1D-28 | 648078 | bdl | nd | bdl | nd | nd | nd | nd |
| 11/19/10 | SG-1D-29 | 648079 | nd | nd | nd | nd | nd | nd | nd |
| 11/18/10 | SG-1C-19 | 648080 | nd | nd | nd | nd | nd | nd | nd |
| | | | | | | | | | |
| 11/19/10 | TRIP BLANK-01 | 648040 | nd | nd | nd | nd | nd | nd | nd |
| 11/19/10 | TRIP BLANK-02 | 648052 | nd | nd | nd | nd | nd | nd | nd |
| 11/19/10 | TRIP BLANK-03 | 648081 | nd | nd | nd | nd | nd | nd | nd |
| 11/19/10 | TRIP BLANK-04 | 648082 | nd | nd | nd | nd | nd | nd | nd |
| | | | | | | | | | |
| 11/18/10 | method blank | method blank | nd | nd | nd | nd | nd | nd | nd |
| 11/19/10 | method blank | method blank | nd | nd | nd | nd | nd | nd | nd |

TABLE 2.5-1
Soil Gas Survey Analytical Results
GORE Standard Target VOCs/SVOCs (A1)
Section I Cover
Pinewood Landfill
Pinewood, South Carolina

| DATE ANALYZED | FIELD ID | SAMPLE NAME | 11DCE | 11DCA | 111TCA | 12DCA | TCE | OCT | PCE | 14DCB |
|---|---|---|---|---|---|---|---|---|---|---|
| | | MDL= | 0.02 | 0.02 | 0.03 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 11/19/10 | BG-01 | 648027 | nd | nd | nd | nd | nd | bdl | nd | nd |
| 11/19/10 | BG-02 | 648028 | nd | nd | nd | nd | nd | nd | nd | nd |
| 11/18/10 | SG-1A-01 | 648029 | 0.82 | 13.44 | nd | nd | nd | nd | 0.23 | nd |
| 11/19/10 | SG-1A-02 | 648030 | nd | 0.09 | nd | nd | nd | nd | nd | nd |
| 11/19/10 | SG-1A-03 | 648031 | nd | nd | nd | nd | nd | nd | nd | nd |
| 11/19/10 | SG-1A-04 | 648032 | nd | 0.07 | nd | nd | nd | nd | nd | nd |
| 11/19/10 | SG-1A-06 | 648033 | nd | 0.12 | nd | nd | nd | nd | nd | nd |
| 11/19/10 | SG-1A-05 | 648034 | nd | nd | nd | nd | nd | nd | nd | nd |
| 11/19/10 | SG-1A-07 | 648035 | nd | nd | nd | nd | nd | nd | nd | nd |
| 11/20/10 | SG-1A-09 | 648036 | 0.24 | 1.13 | nd | nd | nd | nd | nd | nd |
| 11/20/10 | SG-1A-08 | 648037 | bdl | 0.05 | nd | nd | nd | nd | nd | nd |
| 11/19/10 | SG-1B-10 | 648038 | 0.31 | 3.72 | nd | nd | nd | nd | 0.15 | nd |
| 11/18/10 | SG-1C-20 | 648039 | 7.74 | 20.80 | 0.04 | nd | 10.57 | nd | 0.91 | nd |
| 11/19/10 | SG-1B-11 | 648041 | 0.06 | 1.51 | nd | 0.08 | bdl | nd | 0.03 | nd |
| 11/19/10 | SG-1B-12 | 648042 | 0.10 | 1.33 | nd | nd | nd | nd | nd | nd |
| 11/18/10 | SG-1B-13 | 648043 | 0.02 | 0.37 | nd | nd | 1.17 | nd | nd | nd |
| 11/19/10 | SG-1B-14 | 648044 | nd | nd | nd | nd | nd | nd | nd | nd |
| 11/18/10 | SG-1B-15 | 648045 | 0.15 | 1.56 | nd | nd | 0.02 | nd | 0.56 | nd |
| 11/18/10 | SG-1B-16 | 648046 | 0.50 | 5.70 | bdl | 0.32 | 8.76 | nd | 14.66 | nd |
| 11/19/10 | SG-1B-22 | 648047 | nd | nd | nd | nd | nd | nd | nd | nd |
| 11/19/10 | SG-1B-24 | 648048 | nd | nd | nd | nd | nd | nd | nd | nd |
| 11/20/10 | SG-1B-26 | 648049 | 1.67 | 9.19 | bdl | 0.91 | 0.10 | nd | 1.55 | nd |
| 11/19/10 | SG-1B-17 | 648050 | nd | nd | nd | nd | nd | nd | nd | nd |
| 11/18/10 | SG-1B-18 | 648051 | 0.05 | 1.35 | nd | 0.37 | 0.59 | nd | 0.16 | nd |
| 11/19/10 | SG-1C-27 | 648053 | nd | 0.05 | nd | nd | nd | nd | nd | nd |
| 11/18/10 | SG-1D-35 | 648054 | nd | nd | nd | nd | nd | 0.25 | 0.03 | nd |
| 11/19/10 | SG-1C-25 | 648055 | nd | nd | nd | nd | nd | nd | 0.04 | nd |
| 11/19/10 | SG-1D-33 | 648056 | 0.03 | 0.31 | nd | nd | nd | nd | nd | nd |
| 11/19/10 | SG-1C-23 | 648057 | nd | nd | nd | nd | nd | bdl | nd | nd |
| 11/19/10 | SG-1C-21 | 648058 | nd | nd | nd | nd | nd | nd | nd | nd |
| 11/19/10 | SG-1D-31 | 648059 | nd | nd | nd | nd | nd | nd | nd | nd |
| 11/18/10 | SG-1D-30 | 648060 | 0.17 | 6.00 | nd | nd | nd | nd | nd | nd |
| 11/19/10 | SG-1D-32 | 648061 | nd | 35.81 | nd | 0.23 | 7.06 | nd | 0.52 | nd |
| 11/19/10 | SG-1D-34 | 648062 | 0.75 | 2.67 | nd | nd | 0.02 | nd | nd | nd |
| 11/18/10 | SG-1D-36 | 648063 | 0.26 | 2.47 | nd | nd | 0.02 | nd | nd | nd |
| 11/19/10 | SG-1E-49 | 648064 | 3.45 | 3.07 | 11.35 | 0.45 | 3.61 | bdl | 2.24 | bdl |
| 11/19/10 | SG-1E-48 | 648065 | 0.18 | 0.22 | nd | nd | bdl | nd | 0.08 | nd |
| 11/19/10 | SG-1E-44 | 648066 | 8.30 | 35.44 | 1.35 | nd | 28.10 | 0.03 | 31.33 | 0.11 |
| 11/19/10 | SG-1E-42 | 648067 | 0.24 | 7.36 | nd | nd | 1.60 | nd | 1.01 | nd |
| 11/19/10 | SG-1E-40 | 648068 | 0.34 | 1.51 | nd | nd | nd | nd | 0.41 | nd |
| 11/19/10 | SG-1E-39 | 648069 | nd | nd | nd | nd | bdl | nd | nd | nd |
| 11/18/10 | SG-1E-37 | 648070 | 0.07 | 0.87 | nd | nd | nd | nd | nd | nd |
| 11/19/10 | SG-1E-41 | 648071 | 0.68 | 15.25 | 0.06 | nd | 1.92 | nd | 11.30 | nd |
| 11/19/10 | SG-1E-43 | 648072 | 1.23 | 20.93 | nd | 4.78 | 27.87 | nd | 3.08 | nd |
| 11/19/10 | SG-1E-46 | 648073 | 2.33 | 22.12 | 0.07 | 0.23 | 7.58 | nd | 3.77 | nd |
| 11/19/10 | SG-1E-45 | 648074 | bdl | 0.75 | nd | nd | nd | nd | 0.04 | nd |
| 11/19/10 | SG-1E-47 | 648075 | 0.04 | 2.43 | bdl | nd | 0.15 | nd | 0.16 | nd |
| 11/19/10 | SG-1E-50 | 648076 | nd | 0.19 | nd | nd | nd | nd | 0.03 | nd |
| 11/18/10 | SG-1E-38 | 648077 | nd | nd | nd | nd | nd | nd | nd | nd |
| 11/19/10 | SG-1D-28 | 648078 | nd | 0.54 | nd | nd | nd | nd | nd | nd |
| 11/19/10 | SG-1D-29 | 648079 | 0.02 | 0.89 | nd | nd | nd | nd | nd | nd |
| 11/18/10 | SG-1C-19 | 648080 | nd | nd | nd | nd | nd | nd | nd | nd |
| | | | | | | | | | | |
| 11/19/10 | TRIP BLANK-01 | 648040 | nd | nd | nd | nd | nd | nd | nd | nd |
| 11/19/10 | TRIP BLANK-02 | 648052 | nd | nd | nd | nd | nd | nd | nd | nd |
| 11/19/10 | TRIP BLANK-03 | 648081 | nd | nd | nd | nd | nd | nd | nd | nd |
| 11/19/10 | TRIP BLANK-04 | 648082 | nd | nd | nd | nd | nd | nd | nd | nd |
| | | | | | | | | | | |
| 11/18/10 | method blank | method blank | nd | nd | nd | nd | nd | nd | nd | nd |
| 11/19/10 | method blank | method blank | nd | nd | nd | nd | nd | nd | nd | nd |

TABLE 2.5-1
Soil Gas Survey Analytical Results
GORE Standard Target VOCs/SVOCs (A1)
Section I Cover
Pinewood Landfill
Pinewood, South Carolina

| DATE ANALYZED | FIELD ID | SAMPLE NAME | CHCl3 | CCl4 | 112TCA | ClBENZ | 1112TetCA | 1122TetCA | 13DCB | 12DCB |
|---|---|---|---|---|---|---|---|---|---|---|
| | | MDL= | 0.02 | 0.03 | 0.02 | 0.02 | 0.03 | 0.02 | 0.02 | 0.02 |
| 11/19/10 | BG-01 | 648027 | nd | nd | nd | nd | nd | nd | nd | nd |
| 11/19/10 | BG-02 | 648028 | nd | nd | nd | nd | nd | nd | nd | nd |
| 11/18/10 | SG-1A-01 | 648029 | 0.03 | nd | nd | nd | nd | nd | nd | nd |
| 11/19/10 | SG-1A-02 | 648030 | nd | nd | nd | nd | nd | nd | nd | nd |
| 11/19/10 | SG-1A-03 | 648031 | bdl | nd | nd | nd | nd | nd | nd | nd |
| 11/19/10 | SG-1A-04 | 648032 | nd | nd | nd | nd | nd | nd | nd | nd |
| 11/19/10 | SG-1A-06 | 648033 | nd | nd | nd | nd | nd | nd | nd | nd |
| 11/19/10 | SG-1A-05 | 648034 | nd | nd | nd | nd | nd | nd | nd | nd |
| 11/19/10 | SG-1A-07 | 648035 | 0.04 | nd | nd | nd | nd | nd | nd | nd |
| 11/20/10 | SG-1A-09 | 648036 | nd | nd | nd | nd | nd | nd | nd | nd |
| 11/20/10 | SG-1A-08 | 648037 | 0.03 | nd | nd | nd | nd | nd | nd | nd |
| 11/19/10 | SG-1B-10 | 648038 | nd | nd | nd | nd | nd | nd | nd | nd |
| 11/18/10 | SG-1C-20 | 648039 | nd | nd | nd | nd | nd | nd | nd | nd |
| 11/19/10 | SG-1B-11 | 648041 | nd | nd | nd | nd | nd | nd | nd | nd |
| 11/19/10 | SG-1B-12 | 648042 | 0.03 | nd | nd | nd | nd | nd | nd | nd |
| 11/18/10 | SG-1B-13 | 648043 | nd | nd | nd | nd | nd | nd | nd | nd |
| 11/19/10 | SG-1B-14 | 648044 | nd | nd | nd | nd | nd | nd | nd | nd |
| 11/18/10 | SG-1B-15 | 648045 | 0.04 | nd | 0.15 | nd | nd | nd | nd | nd |
| 11/18/10 | SG-1B-16 | 648046 | 0.35 | nd | 0.66 | nd | nd | nd | nd | nd |
| 11/19/10 | SG-1B-22 | 648047 | nd | nd | nd | nd | nd | nd | nd | nd |
| 11/19/10 | SG-1B-24 | 648048 | nd | nd | nd | nd | nd | nd | nd | nd |
| 11/20/10 | SG-1B-26 | 648049 | nd | nd | nd | nd | nd | nd | nd | nd |
| 11/19/10 | SG-1B-17 | 648050 | nd | nd | nd | nd | nd | nd | nd | nd |
| 11/18/10 | SG-1B-18 | 648051 | 0.03 | nd | nd | nd | nd | nd | nd | nd |
| 11/19/10 | SG-1C-27 | 648053 | 0.05 | nd | nd | nd | nd | nd | nd | nd |
| 11/18/10 | SG-1D-35 | 648054 | nd | nd | nd | nd | nd | nd | nd | nd |
| 11/19/10 | SG-1C-25 | 648055 | 0.05 | nd | nd | nd | nd | nd | nd | nd |
| 11/19/10 | SG-1D-33 | 648056 | nd | nd | nd | nd | nd | nd | nd | nd |
| 11/19/10 | SG-1C-23 | 648057 | nd | nd | nd | nd | nd | nd | nd | nd |
| 11/19/10 | SG-1C-21 | 648058 | nd | nd | nd | nd | nd | nd | nd | nd |
| 11/19/10 | SG-1D-31 | 648059 | nd | nd | nd | nd | nd | nd | nd | nd |
| 11/18/10 | SG-1D-30 | 648060 | nd | nd | nd | nd | nd | nd | nd | nd |
| 11/19/10 | SG-1D-32 | 648061 | 0.10 | nd | 0.78 | nd | nd | nd | nd | nd |
| 11/19/10 | SG-1D-34 | 648062 | nd | nd | nd | nd | nd | nd | nd | nd |
| 11/18/10 | SG-1D-36 | 648063 | 0.04 | nd | nd | nd | nd | nd | nd | nd |
| 11/19/10 | SG-1E-49 | 648064 | 0.81 | nd | 0.37 | nd | nd | nd | nd | 0.05 |
| 11/19/10 | SG-1E-48 | 648065 | 0.02 | nd | nd | nd | nd | nd | nd | nd |
| 11/19/10 | SG-1E-44 | 648066 | 7.67 | nd | 19.62 | 0.12 | nd | 2.44 | 0.03 | 0.10 |
| 11/19/10 | SG-1E-42 | 648067 | 0.04 | nd | nd | 0.05 | nd | nd | nd | nd |
| 11/19/10 | SG-1E-40 | 648068 | 0.47 | nd | nd | 0.02 | nd | nd | nd | 0.06 |
| 11/19/10 | SG-1E-39 | 648069 | nd | nd | nd | nd | nd | nd | nd | nd |
| 11/18/10 | SG-1E-37 | 648070 | nd | nd | nd | nd | nd | nd | nd | nd |
| 11/19/10 | SG-1E-41 | 648071 | 0.10 | nd | nd | nd | nd | nd | nd | nd |
| 11/19/10 | SG-1E-43 | 648072 | 0.08 | nd | nd | 0.47 | nd | nd | nd | 0.03 |
| 11/19/10 | SG-1E-46 | 648073 | 2.72 | nd | 3.26 | bdl | nd | 0.60 | nd | nd |
| 11/19/10 | SG-1E-45 | 648074 | nd | nd | nd | nd | nd | nd | nd | nd |
| 11/19/10 | SG-1E-47 | 648075 | 1.00 | nd | nd | 0.10 | nd | nd | nd | 0.09 |
| 11/19/10 | SG-1E-50 | 648076 | nd | nd | nd | nd | nd | nd | nd | nd |
| 11/18/10 | SG-1E-38 | 648077 | nd | nd | nd | nd | nd | nd | nd | nd |
| 11/19/10 | SG-1D-28 | 648078 | nd | nd | nd | nd | nd | nd | nd | nd |
| 11/19/10 | SG-1D-29 | 648079 | nd | nd | nd | nd | nd | nd | nd | nd |
| 11/18/10 | SG-1C-19 | 648080 | nd | nd | nd | nd | nd | nd | nd | nd |
| | | | | | | | | | | |
| 11/19/10 | TRIP BLANK-01 | 648040 | nd | nd | nd | nd | nd | nd | nd | nd |
| 11/19/10 | TRIP BLANK-02 | 648052 | nd | nd | nd | nd | nd | nd | nd | nd |
| 11/19/10 | TRIP BLANK-03 | 648081 | nd | nd | nd | nd | nd | nd | nd | nd |
| 11/19/10 | TRIP BLANK-04 | 648082 | nd | nd | nd | nd | nd | nd | nd | nd |
| | | | | | | | | | | |
| 11/18/10 | method blank | method blank | nd | nd | nd | nd | nd | nd | nd | nd |
| 11/19/10 | method blank | method blank | nd | nd | nd | nd | nd | nd | nd | nd |

Notes:
No mdl is available for summed combinations of analytes. In summed columns (eg., BTEX), the reported values should be considered ESTIMATED if any of the individual compounds were reported as bdl.
All units are in micrograms (ug), relative mass value.

TABLE 2.5-1
Soil Gas Survey Analytical Results
GORE Standard Target VOCs/SVOCs (A1)
Section I Cover
Pinewood Landfill
Pinewood, South Carolina

**KEY TO DATA TABLE**

| | |
|---|---|
| **UNITS** | |
| ug | micrograms, relative mass value |
| MDL | method detection limit |
| bdl | below detection limit; compound was observed at level below the MDL |
| nd | non-detect, compound was not detected at any level |
| **ANALYTES** | |
| TPH | total petroleum hydrocarbons |
| BTEX | combined masses of benzene, toluene, ethylbenzene and total xylenes (Gasoline Range Aromatics) |
| BENZ | benzene |
| TOL | toluene |
| EtBENZ | ethylbenzene |
| mpXYL | m-, p-xylene |
| oXYL | o-xylene |
| C11,C13&C15 | combined masses of undecane, tridecane, and pentadecane (C11+C13+C15) (Diesel Range Alkanes) |
| UNDEC | undecane |
| TRIDEC | tridecane |
| PENTADEC | pentadecane |
| TMBs | combined masses of 1,3,5-trimethylbenzene and 1,2,4-trimethylbenzene |
| 135TMB | 1,3,5-trimethylbenzene |
| 124TMB | 1,2,4-trimethylbenzene |
| MTBE | methyl t-butyl ether |
| NAPH | naphthalene |
| 2MeNAPH | 2-methyl naphthalene |
| MTBE | methyl t-butyl ether |
| OCT | octane |
| ct12DCE | cis- & trans-1,2-dichloroethene |
| t12DCE | trans-1,2-dichloroethene |
| c12DCE | cis-1,2-dichloroethene |
| 11DCA | 1,1-dichloroethane |
| CHC13 | chloroform |
| 111TCA | 1,1,1-trichloroethane |
| 12DCA | 1,2-dichloroethane |
| CC14 | carbon tetrachloride |
| TCE | trichloroethene |
| PCE | tetrachloroethene |
| ClBENZ | chlorobenzene |
| 14DCB | 1,4-dichlorobenzene |
| 11DCE | 1,1-dichloroethene |
| 112TCA | 1,1,2-trichloroethane |
| 1112TetCA | 1,1,1,2-tetrachloroethane |
| 1122TetCA | 1,1,2,2-tetrachloroethane |
| 13DCB | 1,3-dichlorobenzene |
| 12DCB | 1,2-dichlorobenzene |
| **BLANKS** | |
| method blank | QA/QC module, documents analytical conditions during analysis |

TABLE 2.6-1
Section I Shallow Cover Wells Analytical Data
Pinewood Landfill
Pinewood, South Carolina

| DATE | MAY 29, 2009 | | | | | OCTOBER 22, 2009 | | | | | NOVEMBER 10 - 11, 2010 | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| CONSITITUENT / WELL ID | SILC-1 | SILC-2 | SILC-3 | SILC-4 | SILC-5 | SILC-1 | SILC-2 | SILC-3 | SILC-4 | SILC-5 | SILC-1 | SILC-2 | SILC-3 | SILC-4 | SILC-5 |
| ***Volatile Organic Compounds (ug/l)*** | | | | | | | | | | | | | | | |
| 1,1,1 - Trichloroethane | ND | 5.22 | 149 | ND | ND | NA | NA | 248 | NA | NA | ND | ND | NA | ND | ND |
| 1,1,2,2 - Tetrachloroethane | ND | 15.1 | 43.1 | ND | ND | NA | NA | 43.1 | NA | NA | ND | 0.63 | NA | ND | ND |
| 1,1,2 - Trichloroethane | ND | 947 | 229 | ND | 1.51 | NA | NA | 245 | NA | NA | ND | 307 | NA | ND | ND |
| 1,1 - Dichloroethane | 3.52 | 2210 | 884 | 46.7 | 1860 | NA | NA | 1070 | NA | NA | 14.7 | 305 | NA | 12.3 | 286 |
| 1,1 - Dichloroethylene | ND | 74.3 | 49.3 | 2.04 | ND | NA | NA | 55.7 | NA | NA | ND | 7.35 | NA | 0.66 | 1.35 |
| cis-1,2-Dichloroethylene | 4.41 | 11.9 | 130 | 17.4 | 803 | NA | NA | 275 | NA | NA | ND | NA | NA | NA | NA |
| 1,2 - Dichloroethane | ND | 7.98 | 27.9 | ND | 71.9 | NA | NA | 3.02 | NA | NA | ND | 11.1 | NA | ND | 6.3 |
| 1,2 - Dichloropropane | ND | ND | 2.65 | ND | 6.82 | NA | NA | 3.24 | NA | NA | ND | ND | NA | ND | 0.41 |
| 2-Chloroethylvinyl ether | ND | ND | ND | ND | ND | NA | NA | NA | NA | NA | ND | ND | NA | ND | ND |
| Acrolein | ND | ND | ND | ND | ND | NA | NA | NA | NA | NA | ND | ND | NA | ND | ND |
| Acrylonitrile | ND | ND | ND | ND | ND | NA | NA | NA | NA | NA | ND | ND | NA | ND | ND |
| Benzene | ND | 2.14 | 14.4 | 6.97 | 18.1 | NA | NA | 19 | NA | NA | 1.19 | 0.32 | NA | ND | ND |
| Bromodichloromethane | ND | ND | ND | ND | ND | NA | NA | NA | NA | NA | ND | ND | NA | ND | ND |
| Bromoform | ND | ND | ND | ND | ND | NA | NA | NA | NA | NA | ND | ND | NA | ND | ND |
| Bromomethane | ND | ND | ND | ND | ND | NA | NA | NA | NA | NA | ND | ND | NA | ND | ND |
| Carbon Tetrachloride | ND | ND | ND | ND | ND | NA | NA | NA | NA | NA | ND | ND | NA | ND | ND |
| Chlorobenzene | ND | ND | 20.7 | ND | 4.39 | NA | NA | 16.2 | NA | NA | ND | ND | NA | ND | ND |
| Chloroethane | ND | ND | 1.92 | 0.49 | 3.14 | NA | NA | NA | NA | NA | ND | ND | NA | 2.08 | ND |
| Chloroform | ND | 18.9 | 1440 | 0.38 | 2.27 | NA | NA | 1710 | NA | NA | ND | 0.26 | NA | ND | ND |
| Chloromethane | ND | ND | ND | ND | ND | NA | NA | NA | NA | NA | ND | ND | NA | ND | ND |
| Dibromochloromethane | ND | ND | ND | ND | ND | NA | NA | NA | NA | NA | ND | ND | NA | ND | ND |
| Ethylbenzene | ND | ND | 2.77 | 0.31 | 1.82 | NA | NA | 0.37 | NA | NA | ND | ND | NA | ND | ND |
| Methylene Chloride | ND | 774 | 4030 | ND | 213 | NA | NA | 6.59 | NA | NA | ND | ND | NA | ND | ND |
| Tetrachoroethylene | ND | 8.98 | 133 | 0.62 | 8.82 | NA | NA | 253 | NA | NA | ND | 1.39 | NA | ND | 1.11 |
| Toluene | ND | 3.72 | 61.8 | 9.06 | 86.3 | NA | NA | 5.46 | NA | NA | 0.26 | ND | NA | ND | ND |
| Trichlorethylene | ND | 60.8 | 661 | 1.92 | 55.6 | NA | NA | 986 | NA | NA | ND | 7.05 | NA | ND | 2.42 |
| Vinyl Chloride | 4.36 | 27.8 | 23 | 20.4 | 17.8 | NA | NA | 12.1 | NA | NA | 31.8 | 5.13 | NA | 6.29 | ND |
| cis-1,3-Dichloropropylene | ND | ND | ND | ND | ND | NA | NA | NA | NA | NA | ND | ND | NA | ND | ND |
| trans - 1,2 Dichloroethylene | 0.33 | 0.98 | 3.47 | ND | 11.5 | NA | NA | 4.58 | NA | NA | 2.2 | ND | NA | ND | 0.75 |
| trans - 1,3 Dichloropropylene | ND | ND | ND | ND | ND | NA | NA | NA | NA | NA | ND | ND | NA | ND | ND |
| ***Semi-Volatile Organic Compounds (ug/l)*** | | | | | | | | | | | | | | | |
| 1, 4 Dioxane | NA | NA | NA | NA | NA | NA | NA | 53.9 | NA | NA | NA | NA | NA | NA | NA |
| m,p-Cresols | NA | NA | NA | NA | NA | NA | NA | 8.1 | NA | NA | NA | NA | NA | NA | NA |

TABLE 2.6-1
Section I Shallow Cover Wells Analytical Data
Pinewood Landfill
Pinewood, South Carolina

| DATE | MAY 29, 2009 | | | | | OCTOBER 22, 2009 | | | | | NOVEMBER 10 - 11, 2010 | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| CONSITITUENT / WELL ID | SILC-1 | SILC-2 | SILC-3 | SILC-4 | SILC-5 | SILC-1 | SILC-2 | SILC-3 | SILC-4 | SILC-5 | SILC-1 | SILC-2 | SILC-3 | SILC-4 | SILC-5 |
| ***Metals (ug/l)*** | | | | | | | | | | | | | | | |
| Arsenic | NA | NA | NA | NA | NA | NA | NA | 5.77 | NA | NA | NA | NA | NA | NA | NA |
| Barium | NA | NA | NA | NA | NA | NA | NA | 99.7 | NA | NA | NA | NA | NA | NA | NA |
| Beryllium | NA | NA | NA | NA | NA | NA | NA | < 1 | NA | NA | NA | NA | NA | NA | NA |
| Cadmium | NA | NA | NA | NA | NA | NA | NA | < 1 | NA | NA | NA | NA | NA | NA | NA |
| Chromium | NA | NA | NA | NA | NA | NA | NA | 5.3 | NA | NA | NA | NA | NA | NA | NA |
| Cobalt | NA | NA | NA | NA | NA | NA | NA | 16.8 | NA | NA | NA | NA | NA | NA | NA |
| Copper | NA | NA | NA | NA | NA | NA | NA | 6.1 | NA | NA | NA | NA | NA | NA | NA |
| Lead | NA | NA | NA | NA | NA | NA | NA | 3.6 | NA | NA | NA | NA | NA | NA | NA |
| Nickel | NA | NA | NA | NA | NA | NA | NA | 8.6 | NA | NA | NA | NA | NA | NA | NA |
| Selenium | NA | NA | NA | NA | NA | NA | NA | 1.6 | NA | NA | NA | NA | NA | NA | NA |
| Thallium | NA | NA | NA | NA | NA | NA | NA | < 1 | NA | NA | NA | NA | NA | NA | NA |
| Vanadium | NA | NA | NA | NA | NA | NA | NA | 4.2 | NA | NA | NA | NA | NA | NA | NA |
| Zinc | NA | NA | NA | NA | NA | NA | NA | 31 | NA | NA | NA | NA | NA | NA | NA |

Notes:
ND - Not Detected
NA - Not Analyzed
ug/l - micrograms per liter

Table 2.6-2
Summary of Section I Shallow Cover Wells Analytical Data
Pinewood Landfill
Pinewood, South Carolina

| DATE | MAY 29, 2009 | | | | | OCTOBER 22, 2009 | | | | | NOVEMBER 10 - 11, 2010 | | | | | AVERAGE VALUE | MAXIMUM VALUE | ORDER OF HIGHEST CONCENTRATION |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| CONSITITUENT WELL ID | SILC-1 | SILC-2 | SILC-3 | SILC-4 | SILC-5 | SILC-1 | SILC-2 | SILC-3 | SILC-4 | SILC-5 | SILC-1 | SILC-2 | SILC-3 | SILC-4 | SILC-5 | | | |
| ***Volatile Organic Compounds (ug/l)*** | | | | | | | | | | | | | | | | | | |
| Methylene Chloride | ND | 774 | 4030 | ND | 213 | NA | NA | 6.59 | NA | NA | ND | ND | NA | ND | ND | 1256 | 4030 | 1 |
| 1,1 - Dichloroethane | 3.52 | 2210 | 884 | 46.7 | 1860 | NA | NA | 1070 | NA | NA | 14.7 | 305 | NA | 12.3 | 286 | 669 | 2210 | 2 |
| Chloroform | ND | 18.9 | 1440 | 0.38 | 2.27 | NA | NA | 1710 | NA | NA | ND | 0.26 | NA | ND | ND | 529 | 1710 | 3 |
| 1,1,2 - Trichloroethane | ND | 947 | 229 | ND | 1.51 | NA | NA | 245 | NA | NA | ND | 307 | NA | ND | ND | 346 | 947 | 4 |
| Trichlorethylene | ND | 60.8 | 661 | 1.92 | 55.6 | NA | NA | 986 | NA | NA | ND | 7.05 | NA | ND | 2.42 | 254 | 986 | 5 |
| cis-1,2-Dichloroethylene | 4.41 | 11.9 | 130 | 17.4 | 803 | NA | NA | 275 | NA | NA | NA | NA | NA | NA | NA | 207 | 803 | 6 |
| Tetrachoroethylene | ND | 8.98 | 133 | 0.62 | 8.82 | NA | NA | 253 | NA | NA | ND | 1.39 | NA | ND | 1.11 | 58 | 253 | 7 |
| 1,1,1 - Trichloroethane | ND | 5.22 | 149 | ND | ND | NA | NA | 248 | NA | NA | ND | ND | NA | ND | ND | 134 | 248 | 8 |

Notes:
All concentrations reported in ug/l (micrograms per liter).
ND - Not Detected
NA - Not Analyzed

TABLE 2.6-3
Summary of Sections II and III Shallow Cover Wells Analytical Data
Pinewood Landfill
Pinewood, South Carolina

| Date | MCL | 7/25/2009 | 10/26/2009 | 12/15/2009 | 12/29/2009 | 12/15/2009 | 12/29/2009 | 12/29/2009 | 7/25/2009 | 10/5/2009 | 10/26/2009 |
|---|---|---|---|---|---|---|---|---|---|---|---|
| Sample ID | | IIC Cover | S2-LC-03 | 2C-SW-Ditch | S2-LC-03 | 2D-SW-Trench | S2-LC-04 | S2-LC-06 | IIG Cover | S2-LC-07 | S2-LC-07 |
| ***Indicator Parameters*** | | | | | | | | | | | |
| pH (s.u.) | | NA | 6.83 | NA | 6.34 | NA | 5.51 | 6.01 | NA | 5.2 | 5.5 |
| Conductivity (uS/cm) | | NA | 211 | NA | 156 | NA | 52.5 | 70.2 | NA | 55.7 | 152 |
| ***Volatile Organic Compounds (ug/l)*** | | | | | | | | | | | |
| 1,1,1-Trichloroethane | 200 | ND | ND | ND | ND | ND | 1.31 | ND | ND | ND | ND |
| 1,1-Dichloroethane | none | 7.5 | 1.86 | 0.953 J | 3.58 | 0.660 J | 10.8 | ND | 0.952 J | ND | ND |
| cis-1,2-Dichloroethylene | 70 | 3.17 | 0.540 J | 0.577 J | 2.81 | 2.76 | 5.44 | ND | ND | ND | ND |
| trans-1,2-Dichloroethylene | 100 | ND | ND | ND | ND | ND | ND | ND | ND | ND | ND |
| 1,2-Dichloroethane | 5 | 0.452 J | ND | ND | ND | ND | 0.680 J | ND | ND | ND | ND |
| 1,4-Dichlorobenzene | 75 | ND | ND | ND | ND | ND | 2.16 | ND | ND | ND | ND |
| Acetone | none | ND | ND | ND | ND | 2.46 J | ND | ND | ND | 1.71 J | ND |
| Benzene | 5 | ND | ND | ND | ND | ND | ND | ND | ND | ND | ND |
| Carbon disulfide | none | ND | ND | ND | ND | ND | ND | ND | ND | ND | ND |
| Carbon tetrachloride | 5 | ND | ND | ND | 0.320 J | ND | ND | ND | ND | ND | ND |
| Chloroform | none | 0.720 J | ND | ND | 0.820 J | ND | 0.450 J | ND | ND | ND | ND |
| Methylene Chloride | none | ND | ND | ND | ND | ND | 11.4 | ND | ND | ND | ND |
| Tetrachloroethylene | 5 | 1.44 | 0.770 J | ND | 0.370 J | 0.799 J | **24.3** | ND | ND | ND | ND |
| Trichloroethylene | 5 | 4.93 | 2.54 | 0.495 J | 4.55 | 0.784 J | **9.01** | ND | ND | ND | ND |
| Vinyl chloride | 2 | ND | ND | ND | 0.790 J | ND | 0.820 J | ND | ND | ND | ND |
| Xylenes (total) | 10,000 | ND | ND | ND | ND | ND | 0.330 J | ND | ND | ND | ND |

TABLE 2.6-3
Summary of Sections II and III Shallow Cover Wells Analytical Data
Pinewood Landfill
Pinewood, South Carolina

| Date / Sample ID | MCL | 12/29/2009 S2-LC-07 | 10/26/2009 S2-LC-08 | 12/29/2009 S2-LC-08 | 10/5/2009 S2-LC-09 | 12/29/2009 S2-LC-09 | 12/29/2009 S3-LC-02 | 12/29/2009 S3-LC-04 | 10/26/2009 S3-LC-06 | 12/29/2009 S3-LC-06 |
|---|---|---|---|---|---|---|---|---|---|---|
| ***Indicator Parameters*** | | | | | | | | | | |
| pH (s.u.) | | 5.95 | 5.73 | 6.24 | 6.0 | 6.03 | 5.99 | 5.64 | 5.98 | 5.64 |
| Conductivity (uS/cm) | | 181 | 281 | 161 | 218 | 85.4 | 132 | 47.3 | 55.1 | 30.1 |
| ***Volatile Organic Compounds (ug/l)*** | | | | | | | | | | |
| 1,1,1-Trichloroethane | 200 | ND | ND | ND | ND | ND | ND | ND | ND | ND |
| 1,1-Dichloroethane | none | ND | 4.58 | 2.64 | ND | 3.27 | ND | ND | ND | ND |
| cis-1,2-Dichloroethylene | 70 | ND | 1.03 | 0.690 J | ND | 4.24 | ND | ND | ND | ND |
| trans-1,2-Dichloroethylene | 100 | ND | ND | ND | ND | 1.14 | ND | ND | ND | ND |
| 1,2-Dichloroethane | 5 | ND | ND | ND | ND | **13.9** | ND | ND | ND | ND |
| 1,4-Dichlorobenzene | 75 | ND | ND | ND | ND | ND | ND | ND | ND | ND |
| Acetone | none | ND | ND | ND | 1.74 J | ND | ND | ND | ND | ND |
| Benzene | 5 | ND | 1.52 | 0.790 J | ND | ND | ND | ND | ND | ND |
| Carbon disulfide | none | ND | ND | ND | 1.91 J | ND | ND | ND | ND | ND |
| Carbon tetrachloride | 5 | ND | ND | ND | ND | ND | ND | ND | ND | ND |
| Chloroform | none | ND | ND | ND | ND | ND | ND | ND | ND | ND |
| Methylene Chloride | none | ND | ND | ND | ND | ND | ND | ND | ND | ND |
| Tetrachloroethylene | 5 | ND | ND | ND | ND | 0.590 J | ND | ND | ND | ND |
| Trichloroethylene | 5 | ND | ND | ND | ND | 2.55 | ND | ND | ND | ND |
| Vinyl chloride | 2 | ND | ND | ND | ND | 0.680 J | ND | ND | ND | ND |
| Xylenes (total) | 10,000 | ND | ND | ND | ND | ND | ND | ND | ND | ND |

Notes:
All concentrations reported in ug/l (micrograms per liter), unless otherwise noted.
J - estimated concentration
MCL - USEPA Maximum Contaminant Level
NA - Not Analyzed
ND - Not Detected
Bold - exceeds MCL
IIC Cover sample collected from the same area as S2-LC-03
IIG Cover sample collected from the same area as S2-LC-07

TABLE 2.7-1
French Drain Analytical Data - November 2010
Pinewood Landfill
Pinewood, South Carolina

| | SAMPLING LOCATION | | |
|---|---|---|---|
| | Perimeter French Drain | | Section I French Drain |
| Discharge Point | Pond A | Pond B | Pond A |
| ***Volatile Organic Compounds (ug/l)*** | | | |
| 1,1,1 - Trichloroethane | ND | ND | ND |
| 1,1,2,2 - Tetrachloroethane | ND | ND | ND |
| 1,1,2 - Trichloroethane | ND | ND | ND |
| 1,1 - Dichloroethane | ND | ND | ND |
| 1,1 - Dichloroethylene | ND | ND | ND |
| cis-1,2-Dichloroethylene | ND | ND | ND |
| 1,2 - Dichloroethane | ND | ND | ND |
| 1,2 - Dichloropropane | ND | ND | ND |
| 2-Chloroethylvinyl ether | ND | ND | ND |
| Acrolein | ND | ND | ND |
| Acrylonitrile | ND | ND | ND |
| Benzene | ND | ND | ND |
| Bromodichloromethane | ND | ND | ND |
| Bromoform | ND | ND | ND |
| Bromomethane | ND | ND | ND |
| Carbon Tetrachloride | ND | ND | ND |
| Chlorobenzene | ND | ND | ND |
| Chloroethane | ND | ND | ND |
| Chloroform | ND | ND | ND |
| Chloromethane | ND | ND | ND |
| Dibromochloromethane | ND | ND | ND |
| Ethylbenzene | ND | ND | ND |
| Methylene Chloride | ND | ND | ND |
| Tetrachoroethylene | ND | ND | ND |
| Toluene | ND | ND | ND |
| Trichlorethylene | ND | ND | ND |
| Vinyl Chloride | ND | ND | ND |
| cis-1,3-Dichloropropylene | ND | ND | ND |
| trans - 1,2 Dichloroethylene | ND | ND | ND |
| trans - 1,3 Dichloropropylene | ND | ND | ND |

Notes:
ND - Not Detected
ug/l - micrograms per liter

TABLE 2.7-2
Summary of Historic French Drain Analytical Data
Pinewood Landfill
Pinewood, South Carolina

| | SAMPLING LOCATION | DATE | CONSTITUENT | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|
| | | | Methylene Chloride | 1,1 Dichloro-ethane | Tetrachloro-ethylene | Chloromethane | Cadmium | Arsenic | Lead | Silver |
| **Perimeter French Drain** | Discharge To Pond A | 2/27/2008 | 2.37 | | | | 0.3 | | | |
| | | 5/2/2008 | | | | | 0.2 | | | |
| | | 8/8/2008 | | | | | 0.2 | | | |
| | | 11/13/2008 | | | | | 0.2 | | | |
| | | 2/10/2009 | | | | | 0.2 | | | |
| | | 5/8/2009 | | | | | 0.9 | 0.06 | 0.01 | 0.009 |
| | | 8/3/2009 | | | | | 0.2 | | | |
| | | 11/5/2009 | | | | | 0.2 | | | |
| | | 2/12/2010 | | | | | 0.3 | | | |
| | Discharge to Pond B | 2/27/2008 | | | | | 0.7 | | | |
| | | 5/2/2008 | | | | | 0.5 | | | |
| | | 8/8/2008 | | | | | 0.4 | | | |
| | | 11/13/2008 | | | | | 0.4 | | | |
| | | 2/10/2009 | | | | | 0.6 | | | |
| | | 5/8/2009 | | | | | 0.5 | 0.4 | 0.06 | 0.004 |
| | | 8/3/2009 | | | | | 0.4 | | | |
| | | 11/5/2009 | | | | | 0.4 | | | |
| | | 2/12/2010 | | | | < 1 | 0.7 | | | |
| **Section I French Drain** | Discharge to Pond A | 2/27/2008 | 2.41 | | | | 0.9 | | | |
| | | 5/2/2008 | | | | | 0.7 | | | |
| | | 8/8/2008 | | | | | 0.8 | | | |
| | | 11/13/2008 | | | | | 0.6 | | | |
| | | 2/10/2009 | | | | | 0.6 | | | |
| | | 5/8/2009 | | | | | 0.2 | 0.4 | 0.08 | 0.006 |
| | | 8/3/2009 | | | | | 0.7 | | | |
| | | 11/5/2009 | | | | | 0.5 | | | |
| | | 2/12/2010 | | | | | 1.23 | | | |
| | Discharge to Pond A - MH2 | 2/12/2010 | | | | < 1 | | | | |
| | Discharge to Pond A - MH3 | 8/3/2009 | | | < 1 | | | | | |
| | | 2/12/2010 | | | | < 1 | | | | |
| | Discharge to Pond A - MH4 | 2/27/2008 | 2.13 | < 1 | | | | | | |
| | | 11/13/2008 | | | | | | | | |
| | Discharge to Pond A - MH5 | 2/27/2008 | | < 1 | | | | | | |
| | | 5/2/2008 | | | | | | | | |
| | | 8/8/2008 | | 1.74 | | | | | | |
| | | 11/13/2008 | | < 1 | | | | | | |
| | | 2/10/2009 | | < 1 | | | | | | |
| | | 5/8/2009 | | 2.94 | | | | | | |
| | | 8/3/2009 | | 2.58 | | | | | | |
| | | 11/5/2009 | | < 1 | | | | | | |
| | | 1/25/2010 | | < 1 | | | | | | |
| | | 2/12/2010 | | < 1 | | | | | | |

Notes:
All concentrations reported in ug/L (micrograms per liter).
MH - man hole

TABLE 2.8-1
Summary of First Flush Basin French Drain Analytical Data
Pinewood Landfill
Pinewood, South Carolina

| SAMPLING LOCATION | DATE | CONSTITUENT | | | | | | |
|---|---|---|---|---|---|---|---|---|
| | | 1,1,2,2-Tetrachloroethane | 1,1-Dichloroethane | Tetrachloroethylene | 1,1,2-Trichloroethane | cis-1,2 Dichloroethylene | Trichloroethylene | 1,1-Dichloroethylene |
| SB#1 - French Drain Discharge @ First Flush Basin | 2/27/2008 | ND | 1.04 | 140 | ND | 37 | 18.7 | NA |
| | 5/6/2008 | ND | < 1 | 98.6 | ND | 34.7 | 16.7 | NA |
| | 9/8/2008 | ND | 1.4 | 159 | ND | 46.6 | 24.1 | NA |
| | 11/13/2008 | NA | NA | 106 | NA | 34.7 | 19.6 | NA |
| | 5/8/2009 | 2.59 | 2.54 | 52.7 | 6.45 | 33.7 | 18.7 | NA |
| | 8/3/2009 | 1.25 | 1.56 | 104 | 2.93 | 29.6 | 18.5 | 1.28 |
| | 11/5/2009 | ND | 1.12 | 74.2 | < 1 | 24.3 | 13.6 | < 1 |
| | 2/12/2010 | 1.06 | 1.38 | 64.7 | 2.96 | 17 | 11.3 | 1.53 |
| SB#2 - French Drain Discharge @ First Flush Basin | 2/27/2008 | ND | ND | 25 | ND | 16.7 | 6.75 | NA |
| | 5/6/2008 | ND | < 1 | 64.9 | ND | 41.1 | 20.9 | NA |
| | 9/8/2008 | ND | ND | 42.8 | ND | 29.1 | 13.9 | NA |
| | 11/13/2008 | ND | ND | 14.6 | ND | 10.9 | 5.88 | NA |
| | 5/8/2009 | ND | ND | 35.1 | ND | 24 | 11.5 | NA |
| | 8/3/2009 | ND | < 1 | 43.1 | ND | 31.4 | 16.7 | < 1 |
| | 11/5/2009 | ND | ND | 26 | ND | 19.5 | 10.2 | < 1 |
| | 2/12/2010 | ND | ND | 7.93 | ND | 5.12 | 2.02 | ND |

Notes:
All concentrations reported in ug/l (micrograms per liter).
NA - Not Analyzed
ND - Not Detected

TABLE 2.8-2
Summary of Outfall 01A (North and South Basin) Analytical Data
Pinewood Landfill
Pinewood, South Carolina

| SAMPLING LOCATION | DATE | Tetrachloroethylene |
|---|---|---|
| North Basin | 3/11/2008 | < 1 |
| | 7/21/2008 | ND |
| | 2/18/2009 | ND |
| | 5/13/2009 | ND |
| | 12/13/2009 | ND |
| | 2/20/2010 | ND |
| | | |
| South Basin | 1/31/2008 | ND |
| | 5/14/2008 | ND |
| | 10/21/2008 | ND |
| | 12/28/2008 | ND |
| | 3/31/2009 | ND |
| | 6/26/2009 | ND |
| | 11/11/2009 | ND |
| | 1/18/2009 | < 1 |

Notes:
All concentrations reported in ug/l (micrograms per liter).
NA - Not Analyzed
ND - Not Detected

TABLE 2.8-3
Storm Water Analytical Data - December 18, 2009
Section I
Pinewood Landfill
Pinewood, South Carolina

| CONSTITUENT | SAMPLING LOCATION | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| | SI-SW-1 | SI-SW-2 | SI-SW-3 | SI-SW-4 | SI-SW-5 | SI-SW-6 | SI-SW-7 | SI-SW-8 | SI-SW-9 |
| ***Volatile Organic Compounds (ug/l)*** | | | | | | | | | |
| 1,1,1,2 - Tetrachloroethane | NA | ND | ND | ND | ND | ND | ND | ND | ND |
| 1,1,1 - Trichloroethane | NA | ND | ND | ND | ND | ND | ND | ND | ND |
| 1,1,2,2 - Tetrachloroethane | NA | ND | ND | ND | ND | ND | ND | ND | ND |
| 1,1,2 - Trichloroethane | NA | ND | ND | ND | ND | ND | ND | ND | ND |
| 1,1 - Dichloroethane | NA | ND | ND | ND | ND | ND | ND | ND | ND |
| 1,1 - Dichloroethylene | NA | ND | ND | ND | ND | ND | ND | ND | ND |
| 1,2,3 - Trichloropropane | NA | ND | ND | ND | ND | ND | ND | ND | ND |
| 1,2 - Dibromo-3-chloropropane | NA | ND | ND | ND | ND | ND | ND | ND | ND |
| 1,2 - Dibromomethane | NA | ND | ND | ND | ND | ND | ND | ND | ND |
| 1,2 - Dichloroethane | NA | ND | ND | ND | ND | ND | ND | ND | ND |
| 1,2 - Dichloropropane | NA | ND | ND | ND | ND | ND | ND | ND | ND |
| 1,4 - Dioxane | NA | ND | ND | ND | ND | ND | ND | ND | ND |
| 2 - Butanone | NA | ND | ND | ND | ND | ND | ND | ND | ND |
| 2 - Chloro-1,3-butadiene | NA | ND | ND | ND | ND | ND | ND | ND | ND |
| 2 - Hexanone | NA | ND | ND | ND | ND | ND | ND | ND | ND |
| 4 - Methyl-2-Pentanone | NA | ND | ND | ND | ND | ND | ND | ND | ND |
| Acetone | NA | ND | ND | ND | 1.96 | ND | 1.74 | ND | ND |
| Acetonitrile | NA | ND | ND | ND | ND | ND | ND | ND | ND |
| Acrolein | NA | ND | ND | ND | ND | ND | ND | ND | ND |
| Acrylonitrile | NA | ND | ND | ND | ND | ND | ND | ND | ND |
| Allyl chloride | NA | ND | ND | ND | ND | ND | ND | ND | ND |
| Benzene | NA | ND | ND | ND | ND | ND | ND | ND | ND |
| Bromodichloromethane | NA | ND | ND | ND | ND | ND | ND | ND | ND |
| Bromoform | NA | ND | ND | ND | ND | ND | ND | ND | ND |
| Bromomethane | NA | ND | ND | ND | ND | ND | ND | ND | ND |
| Carbon disulfide | NA | ND | ND | ND | ND | ND | ND | ND | ND |
| Carbon Tetrachloride | NA | ND | ND | ND | ND | ND | ND | ND | ND |
| Chlorobenzene | NA | ND | ND | ND | ND | ND | ND | ND | ND |
| Chloroethane | NA | ND | ND | ND | ND | ND | ND | ND | ND |
| Chloroform | NA | ND | ND | ND | ND | ND | ND | ND | ND |
| Chloromethane | NA | ND | ND | ND | ND | 0.48 | ND | ND | ND |
| Dibromochloromethane | NA | ND | ND | ND | ND | ND | ND | ND | ND |
| Dibromomethane | NA | ND | ND | ND | ND | ND | ND | ND | ND |
| Dichlorodifluoromethane | NA | ND | ND | ND | ND | ND | ND | ND | ND |
| Ethylbenzene | NA | ND | ND | ND | ND | ND | ND | ND | ND |
| Idomethane | NA | ND | ND | ND | ND | ND | ND | ND | ND |
| Isobutyl alcohol | NA | ND | ND | ND | ND | ND | ND | ND | ND |
| Methacrylonitrile | NA | ND | ND | ND | ND | ND | ND | ND | ND |
| Methylene Chloride | NA | ND | ND | ND | ND | ND | ND | ND | ND |
| Propionitrile | NA | ND | ND | ND | ND | ND | ND | ND | ND |
| Styrene | NA | ND | ND | ND | ND | ND | ND | ND | ND |
| Tetrachoroethylene | NA | ND | ND | ND | ND | ND | ND | ND | ND |
| Toluene | NA | ND | ND | ND | ND | ND | ND | ND | ND |
| Trichlorethylene | NA | ND | ND | ND | ND | ND | ND | ND | ND |
| Trichlorofluoromethane | NA | ND | ND | ND | ND | ND | ND | ND | ND |
| Vinyl Acetate | NA | ND | ND | ND | ND | ND | ND | ND | ND |
| Vinyl Chloride | NA | ND | ND | ND | ND | ND | ND | ND | ND |
| Xylenes (total) | NA | ND | ND | ND | ND | ND | ND | ND | ND |
| bis(2-Chloroisopropyl) ether | NA | ND | ND | ND | ND | ND | ND | ND | ND |
| cis-1,2-Dichloroethylene | NA | ND | ND | ND | ND | ND | ND | ND | ND |
| cis-1,3-Dichloropropylene | NA | ND | ND | ND | ND | ND | ND | ND | ND |
| trans - 1,2 Dichloroethylene | NA | ND | ND | ND | ND | ND | ND | ND | ND |
| trans - 1,3 Dichloropropylene | NA | ND | ND | ND | ND | ND | ND | ND | ND |
| trans - 1,4 Dichloro-2-butene | NA | ND | ND | ND | ND | ND | ND | ND | ND |

Notes:
All concentrations reported in ug/l (micrograms per liter).
Shaded - Detected concentration
ND - Not Detected
NA - Not Analyzed

TABLE 2.8-4
Summary of Pond A (Outfall 001) and Pond B (Outfall 002) Analytical Data
Pinewood Landfill
Pinewood, South Carolina

| | METALS | | | | | | | | | | PESTICIDES / HERBICIDES | | | | VOLATILE ORGANIC COMPOUNDS | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| Constituent | Cadmium (ug/l) | | Lead (ug/L) | | Silver (ug/l) | | Mercury (ug/l) | | Arsenic (ug/l) | | Heptachlor (ug/l) | | 2,4,5-TP (ug/l) | | Acetone (ug/l) | | Acrolein (ug/l) | | Chloromethane (ug/l) | |
| Date | Outfall 001 | Outfall 002 | Outfall 001 | Outfall 002 | Outfall 001 | Outfall 002 | Outfall 001 | Outfall 002 | Outfall 001 | Outfall 002 | Outfall 001 | Outfall 002 | Outfall 001 | Outfall 002 | Outfall 001 | Outfall 002 | Outfall 001 | Outfall 002 | Outfall 001 | Outfall 002 |
| 1/10/2008 | 0.39 | 0.55 | | | 0.023 | 0.087 | 0.0031 | 0.0019 | | | | | | | | | | | | |
| 1/21/2008 | 0.45 | | | | | | | | | | | | | | | | | | | |
| 1/31/2008 | 0.25 | | | | | | | | | | | | | | | | | | | |
| 2/13/2008 | 0.84 | 0.66 | | | 0.088 | 0.15 | 0.0015 | 0.0009 | | | | | | | | | | | | |
| 2/27/2008 | 0.34 | | | | | | | | | | | | | | | | | | | |
| 2/28/2008 | 0.44 | | | | | | | | | | | | | | | | | | | |
| 3/14/2008 | 0.54 | 1.12 | 0.73 | | 0.011 | 0.073 | 0.0039 | 0.0015 | | | | | | | | | | | | |
| 3/25/2008 | 0.7 | | | | | | | | | | | | | | | | | | | |
| 3/27/2008 | 0.53 | | | | | | | | | | | | | | | | | | | |
| 4/15/2008 | 0.2 | 1.08 | | | 0.011 | 0.28 | 0.0022 | 0.0018 | | | | | | | | | | | | |
| 5/14/2008 | 0.18 | 0.29 | 0.58 | 0.59 | 0.011 | 0.07 | 0.0043 | 0.0043 | | | | | | | | | | | | |
| 6/18/2008 | 0.43 | 0.19 | | | 0.011 | 0.011 | 0.0037 | 0.0025 | | | | | | | | | | | | |
| 6/30/2008 | 0.16 | | | | | | | | | | | | | | | | | | | |
| 7/17/2008 | 0.37 | 0.15 | | | 0.011 | 0.011 | 0.0035 | 0.001 | | | | | | | | | | | | |
| 7/31/2008 | 0.15 | | | | | | | | | | | | | | | | | | | |
| 8/20/2008 | 0.07 | 0.04 | | | 0.011 | 0.011 | 0.0021 | 0.001 | | | | | | | | | | | | |
| 9/18/2008 | 0.08 | 0.07 | | | 0.011 | 0.011 | 0.0009 | 0.0009 | | | | | | | | | | | | |
| 10/21/2009 | 0.07 | 0.07 | | | 0.011 | 0.011 | 0.0015 | 0.0015 | | | | | | | | | | | | |
| 11/18/2008 | 0.29 | 0.22 | 0.66 | 0.79 | 0.048 | 0.07 | 0.0048 | 0.0041 | | | | | | | | | | | | |
| 12/18/2008 | 0.28 | 0.49 | | | 0.012 | 0.011 | 0.0444 | 0.0013 | | | | | | | | | | | | |
| 1/15/2009 | 0.89 | 0.52 | | | | | 0.0016 | 0.0009 | | | | | | | | | | | | |
| 2/10/2009 | 0.19 | 0.7 | | | | | 0.0023 | 0.0007 | | | | | | | | | | | | |
| 3/17/2009 | 0.61 | 0.68 | | | | | 0.0025 | 0.0018 | | | | | | | | | | | | |
| 4/9/2009 | 0.33 | 0.33 | 0.67 | | | | 0.0049 | 0.0021 | | | | | | | | | | 2.34 | | |
| 5/13/2009 | 0.14 | 0.39 | 0.16 | 0.06 | 0.023 | 0.003 | 0.0027 | 0.0017 | 0.46 | 0.24 | | | | | | | | | | |
| 6/11/2009 | 0.12 | 0.27 | | | | | 0.0042 | 0.0042 | | | | | | | | | | | | |
| 7/21/2009 | 0.16 | 0.18 | | | | | 0.0038 | 0.0029 | | | | | | | | | | | | |
| 8/17/2009 | 0.4 | 0.29 | | | | | 0.0023 | 0.0008 | 1.7 | | | | | | | | | | | |
| 9/22/2009 | 0.25 | 0.2 | | | | | 0.0013 | 0.0007 | | | | | | | | | | | | |
| 10/15/2009 | 0.27 | 0.18 | 0.93 | 0.88 | | | 0.0049 | 0.0049 | | | | | | | | | | | | |
| 11/6/2009 | 0.16 | 0.25 | | | | | 0.0002 | 0.0009 | | | | | | | | | | | | |
| 12/14/2009 | 0.27 | 0.39 | 0.7 | | | | 0.0058 | 0.0023 | | | 0.0833 | | | | | | | | | |
| 1/25/2010 | 0.64 | 0.79 | 0.85 | 1.05 | | | 0.0056 | 0.0039 | | | | | | | | 1.56 | | | < 1 | < 1 |
| 2/2/2010 | | | | | | | | | | | | | | | | 2.28 | | | | |
| 2/11/2010 | 0.81 | 1.4 | | | | | 0.0042 | 0.0014 | | | | | 0.0318 | | | | | | | |
| 2/25/2010 | | | | | | | | | | | | | | | | 4.16 | | | | |
| 3/4/2010 | | | | | | | | | | | | | | | 2.26 | 6.56 | | | | |
| 3/11/2010 | | | | | | | | | | | | | | | 5.47 | 2.49 | | | | |

TABLE 3.2-1
Existing Storm Water Conveyance Components
Section I Cover
Pinewood Landfill
Pinewood, South Carolina

**Culverts on Section I Cover**

| Culvert ID | 10 year 24 hr Flow to Culvert (cfs) | 25 year 24 hr Flow to Culvert (cfs) | Head on Inlet (feet) | Culvert Capacity (cfs) | Number of Pipes | Pipe Diameter (inches) | Pipe Material | 10 year Culvert Capacity Acceptable? | 25 year Culvert Capacity Acceptable? |
|---|---|---|---|---|---|---|---|---|---|
| J-13 | 2.2 | 2.68 | 1.25 | 3.59 | 1 | 15 | CPP | ok | ok |
| J-17 | 0.68 | 0.83 | 1.25 | 3.59 | 1 | 15 | CPP | ok | ok |
| J-19 | 1.44 | 1.76 | 1.25 | 3.59 | 1 | 15 | CPP | ok | ok |
| J-21 | 12.55 | 15.28 | 3.14 | 12.95 | 1 | 18 | RCP | ok | CULVERT DEFICIENT |
| J-27 | 1.2 | 1.47 | 1.25 | 3.59 | 1 | 15 | CPP | ok | ok |
| J-31 | 1.23 | 1.49 | 1.25 | 3.59 | 1 | 15 | CPP | ok | ok |
| J-33 | 6.71 | 8.19 | 1.0 | 4.11 | 2 | 12 | CPP | CULVERT DEFICIENT | CULVERT DEFICIENT |
| J-36 | 3.98 | 4.86 | 2.0 | 2.9 | 1 | 12 | CMP | CULVERT DEFICIENT | CULVERT DEFICIENT |
| J-41 | 3.27 | 3.98 | | Pipe sloped Backwards | 1 | 15 | CPP | --- | --- |
| J-43 | 22.22 | 27.05 | 1 | 4.11 | 2 | 12 | CPP | CULVERT DEFICIENT | CULVERT DEFICIENT |
| J-60 | 7.64 | 9.31 | 1.5 | 5.66 | 1 | 18 | RCP | CULVERT DEFICIENT | CULVERT DEFICIENT |
| J-64 | 2.53 | 3.08 | 1.5 | 5.66 | 1 | 18 | RCP | ok | ok |

**Open Channels on Section I Cover**

| Channel ID | 25 year 24 hr Flow to Channel (cfs) | 25 year 24 hr Max Water Depth (feet) | Bottom Width (feet) | Side Slope | Slope (feet/foot) |
|---|---|---|---|---|---|
| J-39 | 9.75 | 0.9 | 0 | 3 | 0.019 |
| J-59 | 9.35 | 0.4 | 3 | 3 | 0.045 |
| J-129 | 19.96 | 1.2 | 0 | 3 | 0.019 |

Notes:
CMP - Corrugated Metal Pipe
CPP - Corrugated Plastic Pipe
RCP - Reinforced Concrete Pipe
cfs - cubic feet per second

TABLE 4.9-1
Recommended Improvements to Storm Water Culverts
Section I Cover
Pinewood Landfill
Pinewood, South Carolina

| Recommended Improvements to Storm Water Culverts | | | | | | | | |
|---|---|---|---|---|---|---|---|---|
| Culvert ID | 10 year 24 hr Flow to Culvert (cfs) | 25 year 24 hr Flow to Culvert (cfs) | New Modeled Head on Inlet (feet) | New Culvert Capacity (cfs) | Number of Pipes | Current Pipe Diameter (inches) | Recommended Pipe Diameter (inches) | Pipe Material |
| J-21 | 12.55 | 15.28 | 2.5 | 16.54 | 1 | 18 | 24 | RCP |
| J-33 | 6.71 | 8.19 | 1.5 | 11.33 | 2 | 12 | 18 | CPP |
| J-36 | 3.98 | 4.86 | 2.0 | 6.61 | 1 | 12 | 18 | CMP |
| J-41 | 3.27 | 3.98 | 1.5 | 5.75 | 1 | 15 | 18 | CPP |
| J-43 | 22.22 | 27.05 | 2.5 | 40.62 | 2 | 12 | 30 | CPP |
| J-60 | 7.64 | 9.31 | 2.0 | 11.63 | 1 | 18 | 24 | RCP |

Notes:
CMP - Corrugated Metal Pipe
CPP - Corrugated Plastic Pipe
RCP - Reinforced Concrete Pipe
cfs - cubic feet per second

# FIGURES

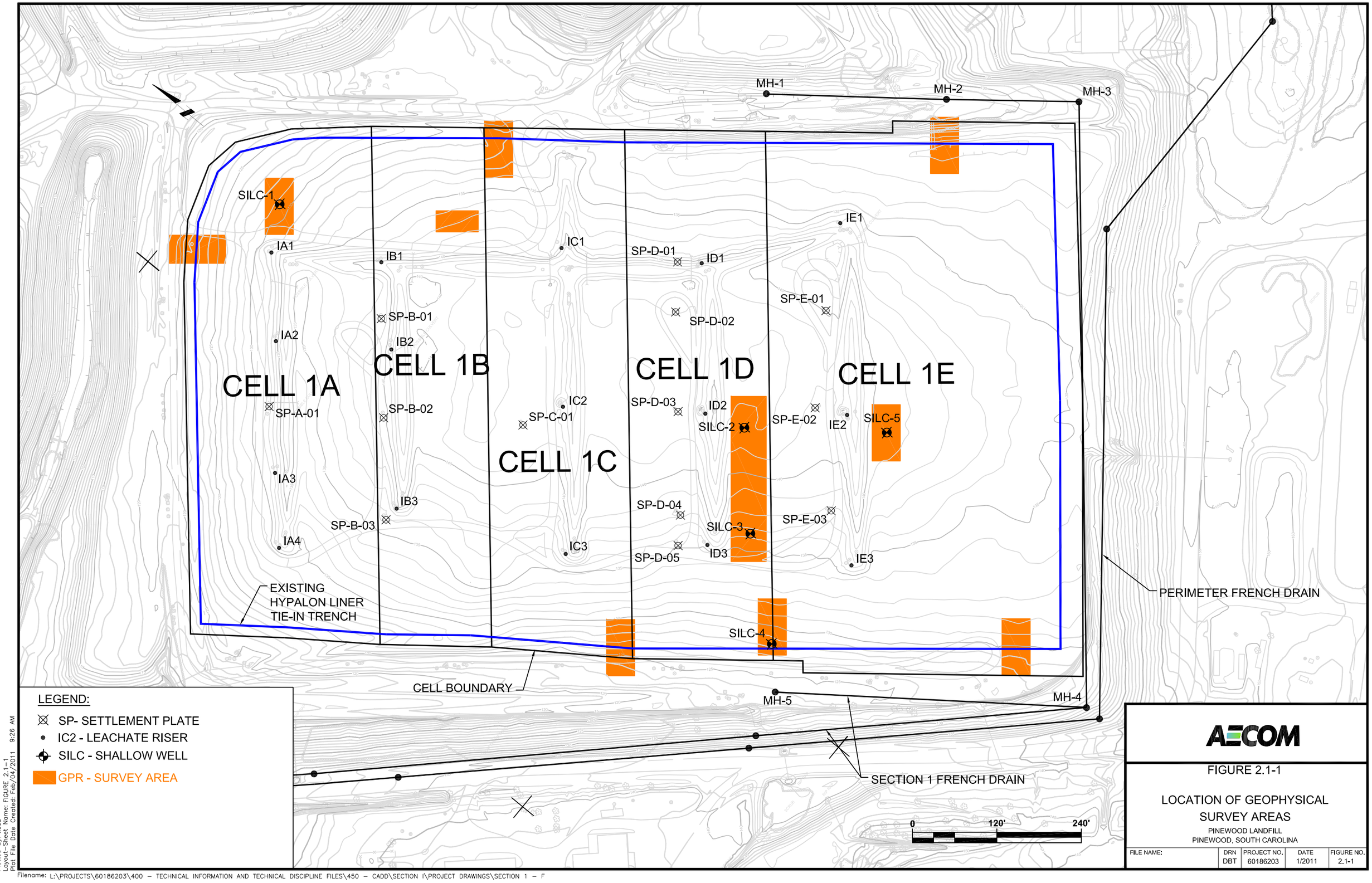



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FIGURE 2.1-1

LOCATION OF GEOPHYSICAL SURVEY AREAS

PINEWOOD LANDFILL
PINEWOOD, SOUTH CAROLINA

| FILE NAME: | DRN | PROJECT NO. | DATE | FIGURE NO. |
|---|---|---|---|---|
| | DBT | 60186203 | 1/2011 | 2.1-1 |

Plotted By: ticed
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Plot File Date Created: Feb/04/2011 9:26 AM

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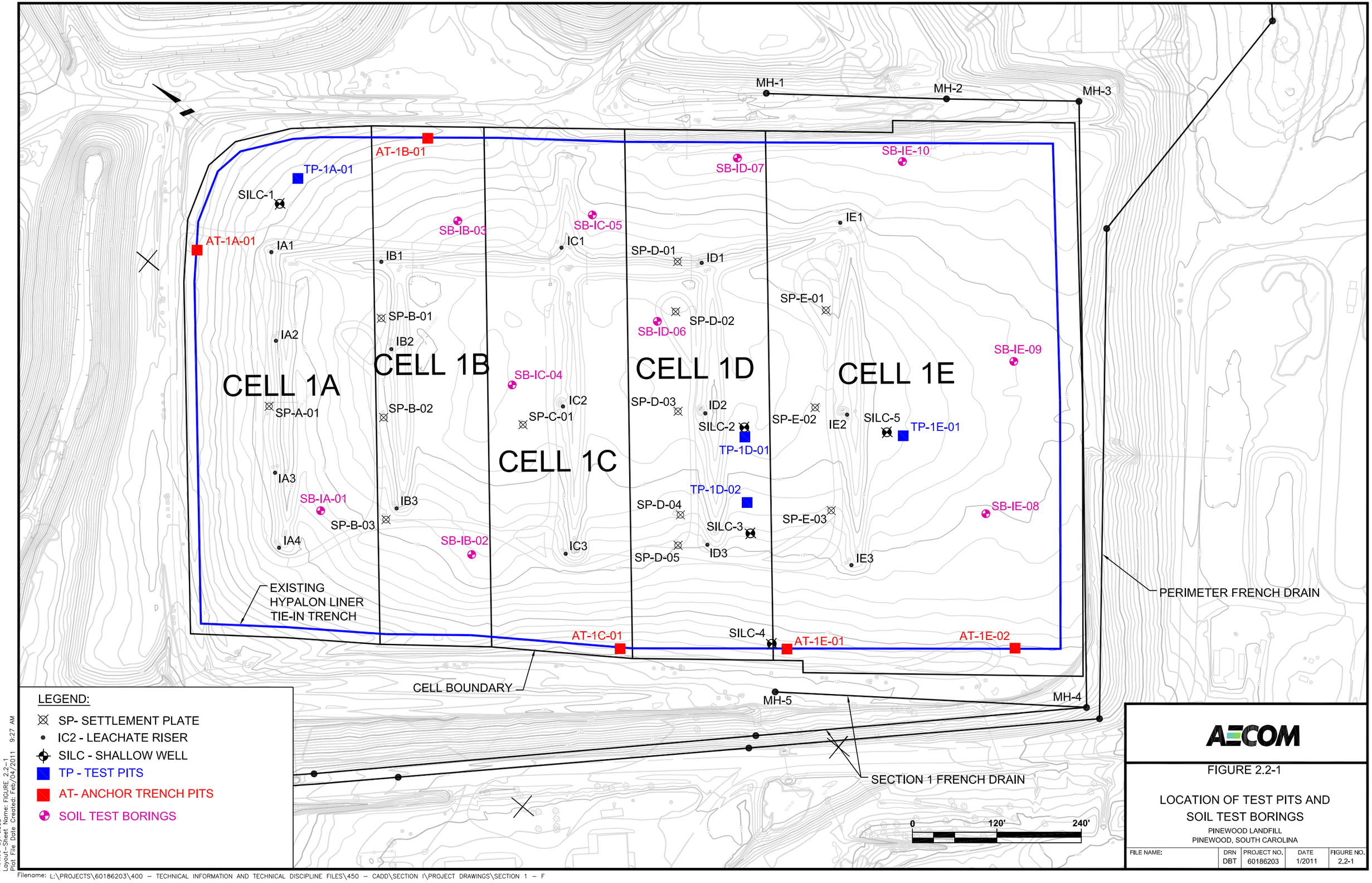


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FIGURE 2.2-1

LOCATION OF TEST PITS AND SOIL TEST BORINGS

PINEWOOD LANDFILL
PINEWOOD, SOUTH CAROLINA

| FILE NAME: | DRN | PROJECT NO. | DATE | FIGURE NO. |
|---|---|---|---|---|
| | DBT | 60186203 | 1/2011 | 2.2-1 |

Plotted By: ticed
Layout-Sheet Name: FIGURE 2.2-1
Plot File Date Created: Feb/04/2011 9:27 AM

Filename: L:\PROJECTS\60186203\400 – TECHNICAL INFORMATION AND TECHNICAL DISCIPLINE FILES\450 – CADD\SECTION I\PROJECT DRAWINGS\SECTION 1 – F

MH-1
MH-2
MH-3
EXISTING TOE OF SLOPE
SP-D-01
SP-B-01
SP-D-02
SP-E-01
CELL 1A
CELL 1B
CELL 1D
CELL 1E
SP-D-03
SP-A-01
SP-B-02
SP-C-01
SP-E-02
EXISTING INTER CELL
SEPARATION BERM
CELL 1C
SP-D-04
SP-B-03
SP-E-03
SP-D-05
EXISTING
HYPALON LINER
TIE-IN TRENCH
PERIMETER FRENCH DRAIN
CELL BOUNDARY
MH-5
MH-4
SECTION 1 FRENCH DRAIN
0
120'
240'

| CUMULATIVE SETTLEMENT DATA | |
|---|---|
| PLATE NUMBER | LIFETIME TOTAL Δ (ft) |
| A-1 | -0.134 |
| B-1 | -0.217 |
| B-2 | -0.003 |
| B-3 | -0.077 |
| C-1 | -0.505 |
| D-1 | -0.366 |
| D-2 | -0.893 |
| D-3 | -1.412 |
| D-4 | -0.222 |
| D-5 | -1.568 |
| E-1 | 0.024 |
| E-2 | -0.167 |
| E-3 | 0.020 |

LEGEND:

⊠ SP- SETTLEMENT PLATE (EXISTING)

AECOM

FIGURE 2.4-1
LOCATION OF EXISTING
SETTLEMENT PLATES
AND CUMULATIVE SETTLEMENT

PINEWOOD LANDFILL
PINEWOOD, SOUTH CAROLINA

| FILE NAME: | DRN | PROJECT NO. | DATE | FIGURE NO. |
|---|---|---|---|---|
| | DBT | 60186203 | 1/2011 | 2.4-1 |

Plotted By: TICED
Layout-Sheet Name: FIGURE 2.4-1
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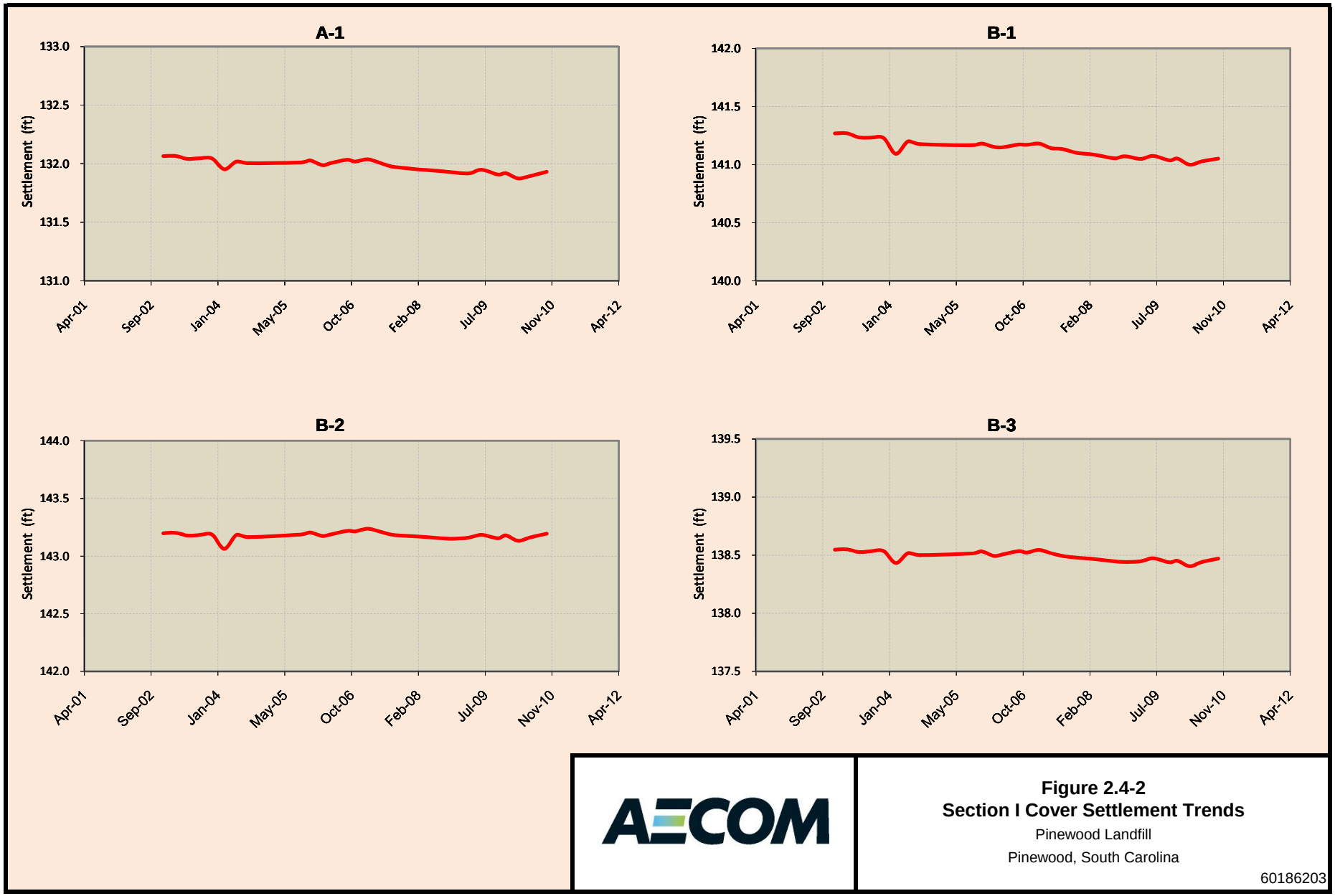


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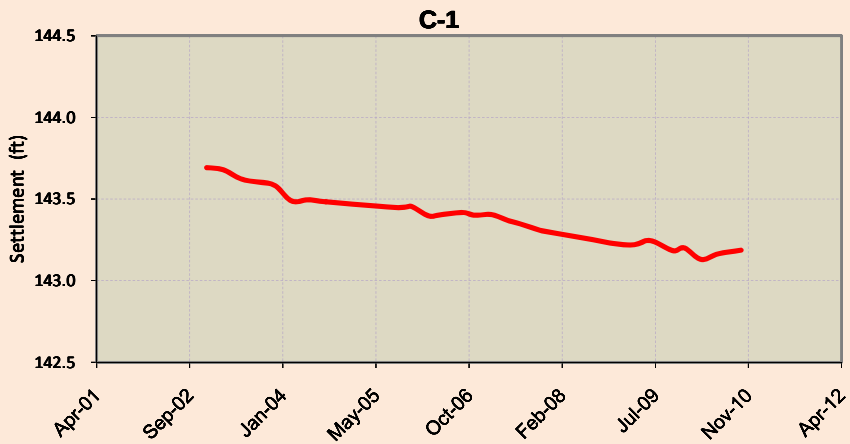
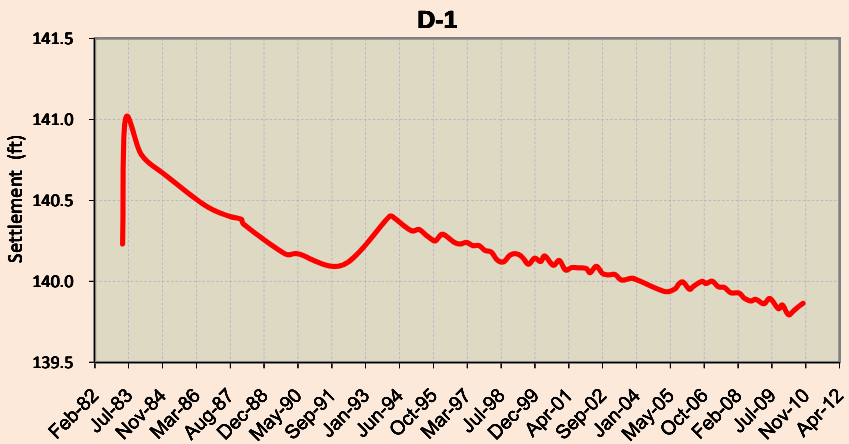
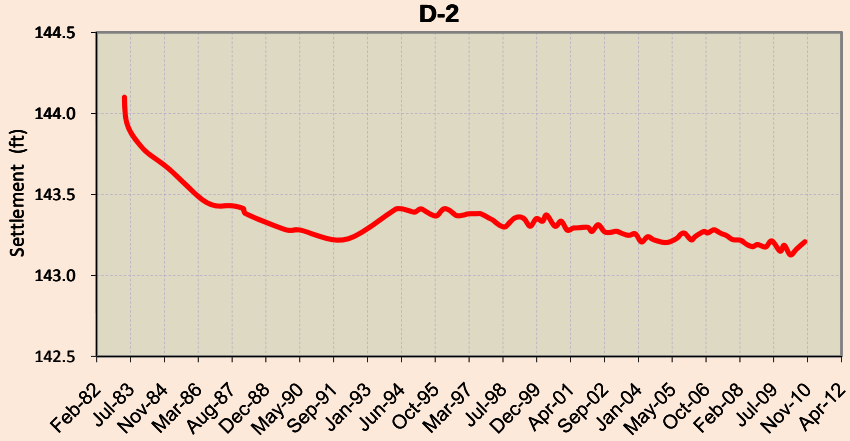
**Figure 2.4-2**
**Section I Cover Settlement Trends**
Pinewood Landfill
Pinewood, South Carolina
60186203



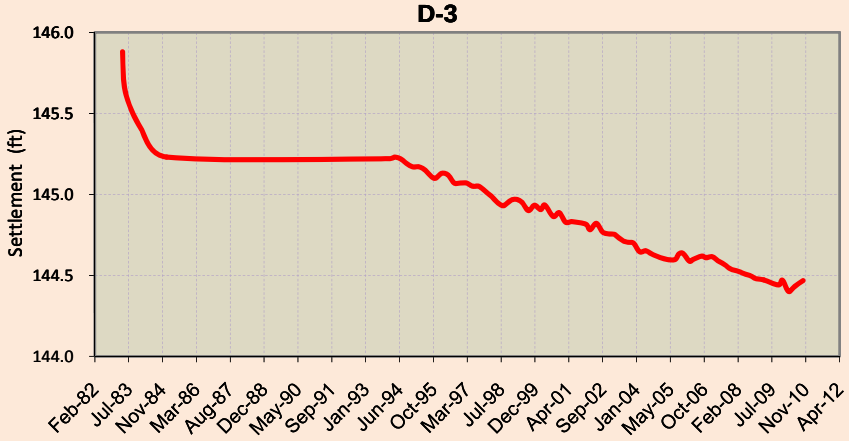




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**Figure 2.4-2**
**Section I Cover Settlement Trends**
Pinewood Landfill
Pinewood, South Carolina
60186203

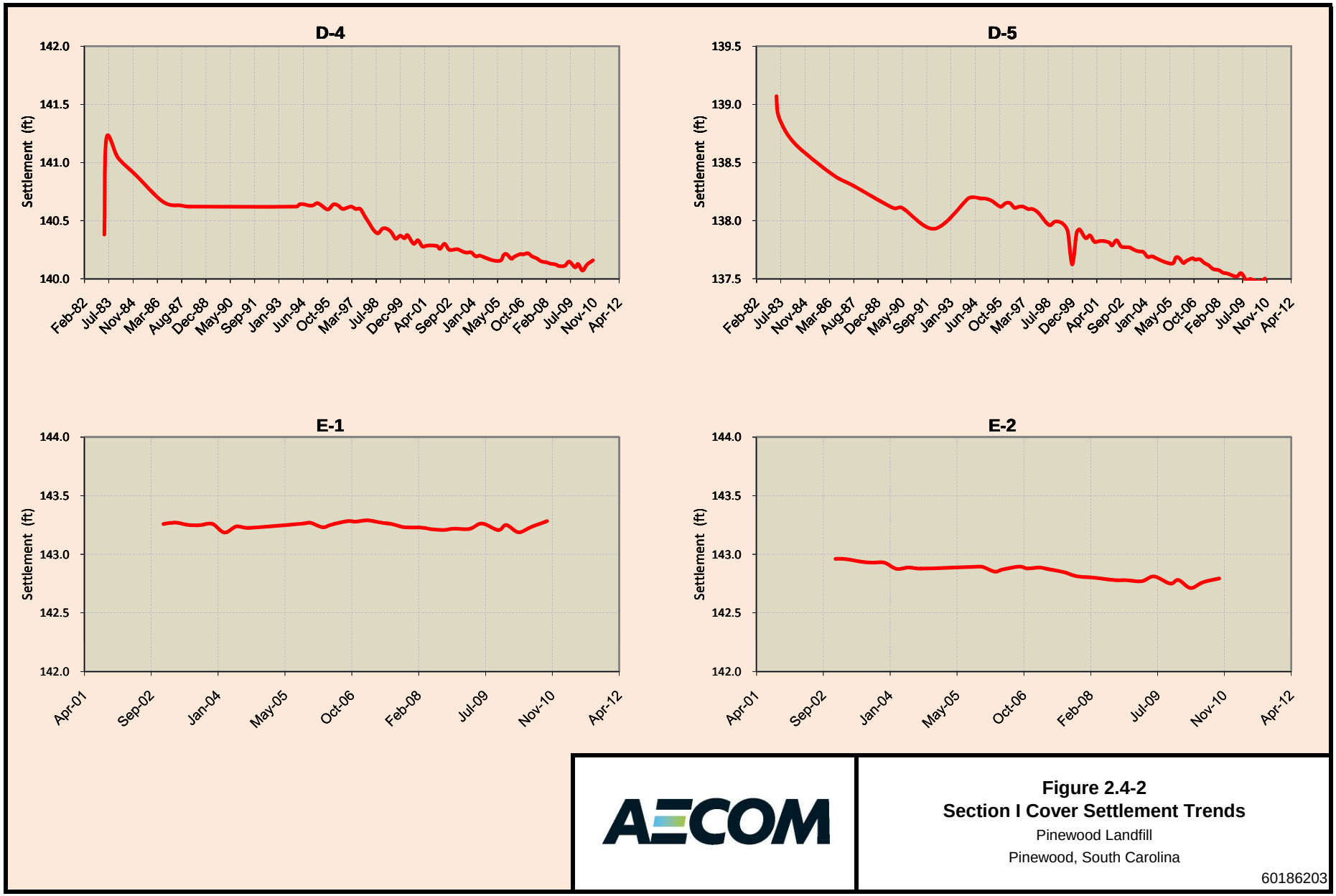


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**Figure 2.4-2**
**Section I Cover Settlement Trends**
Pinewood Landfill
Pinewood, South Carolina
60186203

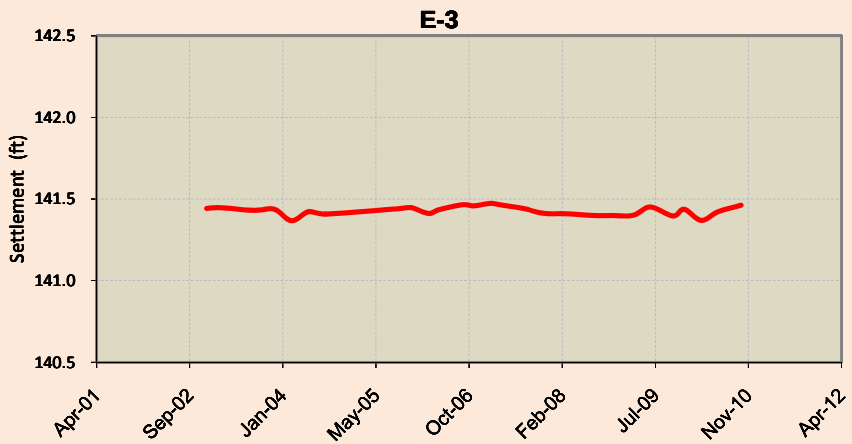
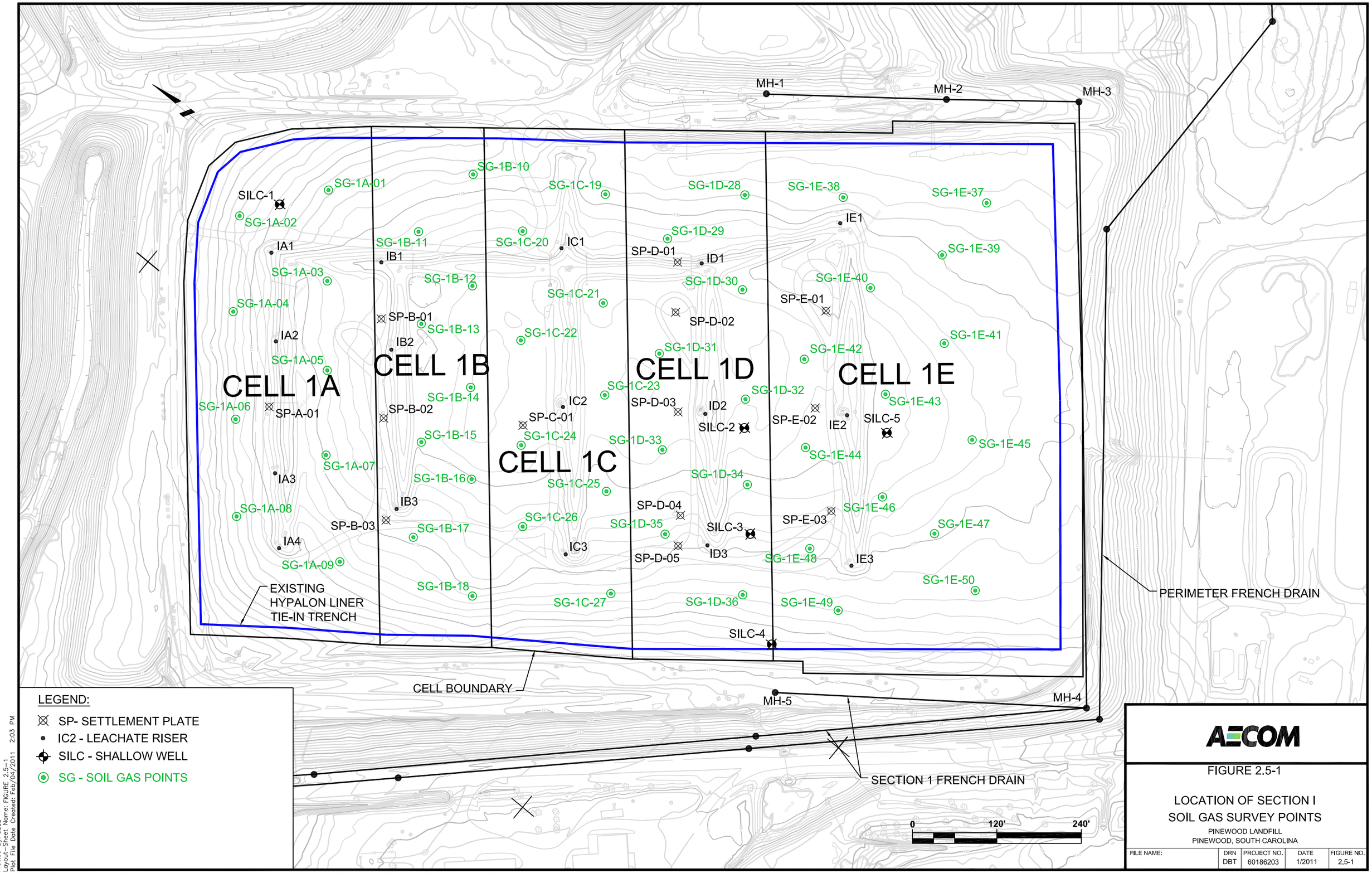



**Figure 2.4-2**
**Section I Cover Settlement Trends**
Pinewood Landfill
Pinewood, South Carolina
60186203




LEGEND:

- SP- SETTLEMENT PLATE
- IC2 - LEACHATE RISER
- SILC - SHALLOW WELL
- SG - SOIL GAS POINTS

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FIGURE 2.5-1

LOCATION OF SECTION I
SOIL GAS SURVEY POINTS

PINEWOOD LANDFILL
PINEWOOD, SOUTH CAROLINA

| FILE NAME: | DRN | PROJECT NO. | DATE | FIGURE NO. |
|---|---|---|---|---|
| | DBT | 60186203 | 1/2011 | 2.5-1 |

Plotted By: ticed
Layout--Sheet Name: FIGURE 2.5-1
Plot File Date Created: Feb/04/2011 2:03 PM

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POND B

SECTION II

SECTION III

BG-02

BG-01

POND A

SECTION I

0' 350' 700'

LEGEND

BG-01 BACKGROUND SOIL GAS LOCATION

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FIGURE 2.5-2

BACKGROUND SOIL GAS SURVEY LOCATIONS

PINEWOOD LANDFILL
PINEWOOD, SOUTH CAROLINA

| FILE NAME: | DRN | PROJECT NO. | DATE | FIGURE NO. |
|---|---|---|---|---|
| | CFF | 60186203 | 1/2011 | 2.5-2 |

Plotted By:Furmanskic
Layout-Sheet Name: MODEL
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L:\PROJECTS\60186203\400 - TECHNICAL INFORMATION AND TECHNICAL DISCIPLINE FILES\450 - CADD\CADD for 475-Projects 1&2\Figure 2.5-2.dgn

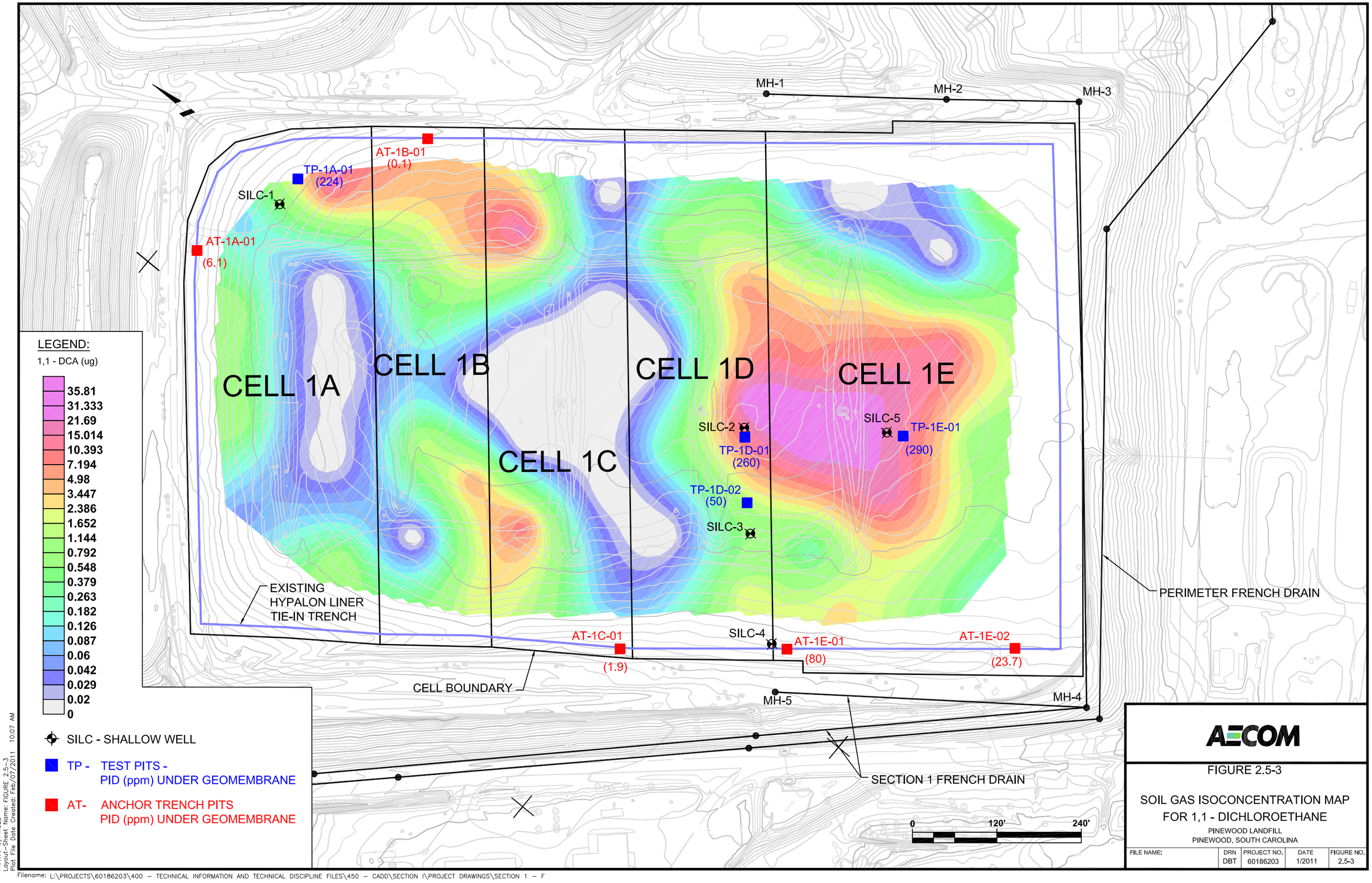


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FIGURE 2.5-3

SOIL GAS ISOCONCENTRATION MAP
FOR 1,1 - DICHLOROETHANE

PINEWOOD LANDFILL
PINEWOOD, SOUTH CAROLINA

| FILE NAME: | DRN | PROJECT NO. | DATE | FIGURE NO. |
|---|---|---|---|---|
| | DBT | 60186203 | 1/2011 | 2.5-3 |

Plotted By: TICED
Layout--Sheet Name: FIGURE 2.5-3
Plot File Date Created: Feb/07/2011 10:07 AM

Filename: L:\PROJECTS\60186203\400 – TECHNICAL INFORMATION AND TECHNICAL DISCIPLINE FILES\450 – CADD\SECTION I\PROJECT DRAWINGS\SECTION 1 – F

SILC-1

SECTION 1

SILC-2

SILC-3

SILC-5

SILC-4

0' 100' 200' 400'

LEGEND

SILC-4 SHALLOW COVER WELL

AECOM

FIGURE 2.6-1

SECTION I
SHALLOW COVER WELL LOCATIONS

PINEWOOD LANDFILL
PINEWOOD, SOUTH CAROLINA

| FILE NAME: | DRN | PROJECT NO. | DATE | FIGURE NO. |
|---|---|---|---|---|
| | CFF | 60186203 | 1/2011 | 2.6-1 |

Plotted By:Furmanskic
Layout-Sheet Name: MODEL
Plot File Date Created:Feb/07/2011 7:53 AM

L:\PROJECTS\60186203\400 - TECHNICAL INFORMATION AND TECHNICAL DISCIPLINE FILES\450 - CADD\CADD for 475-Projects 1&2\Figure 2.6-1.dgn

| POINT | DESCRIPTION |
|---|---|
| FDsec1MH 1 | FRENCH DRAIN MANHOLE |
| FDsec1MH 2 | FRENCH DRAIN MANHOLE |
| FDsec1MH 3 | FRENCH DRAIN MANHOLE |
| FDsec1MH 4 | FRENCH DRAIN MANHOLE |
| FDsec1MH 5 | FRENCH DRAIN MANHOLE |
| FDSEC1 | OUTLET PIPE |
| FDPondA | OUTLET PIPE |
| FDPondB | OUTLET PIPE |
| SBD#1 | SUMP |
| SBD#2 | SUMP |

FDPondB
POND B
OUTFALL 002
SECTION II
SECTION III
SBD#1
BREAKPOINT
OUTFALL 001A
SBD#2
OUTFALL 001
FDPondA
POND A
FDSecI
FDSecIMH 1
SECTION I
FDSecIMH 2
FDSecIMH 3
FDSecIMH 5
FDSecIMH 4

0' 350' 700'

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FIGURE 2.7-1

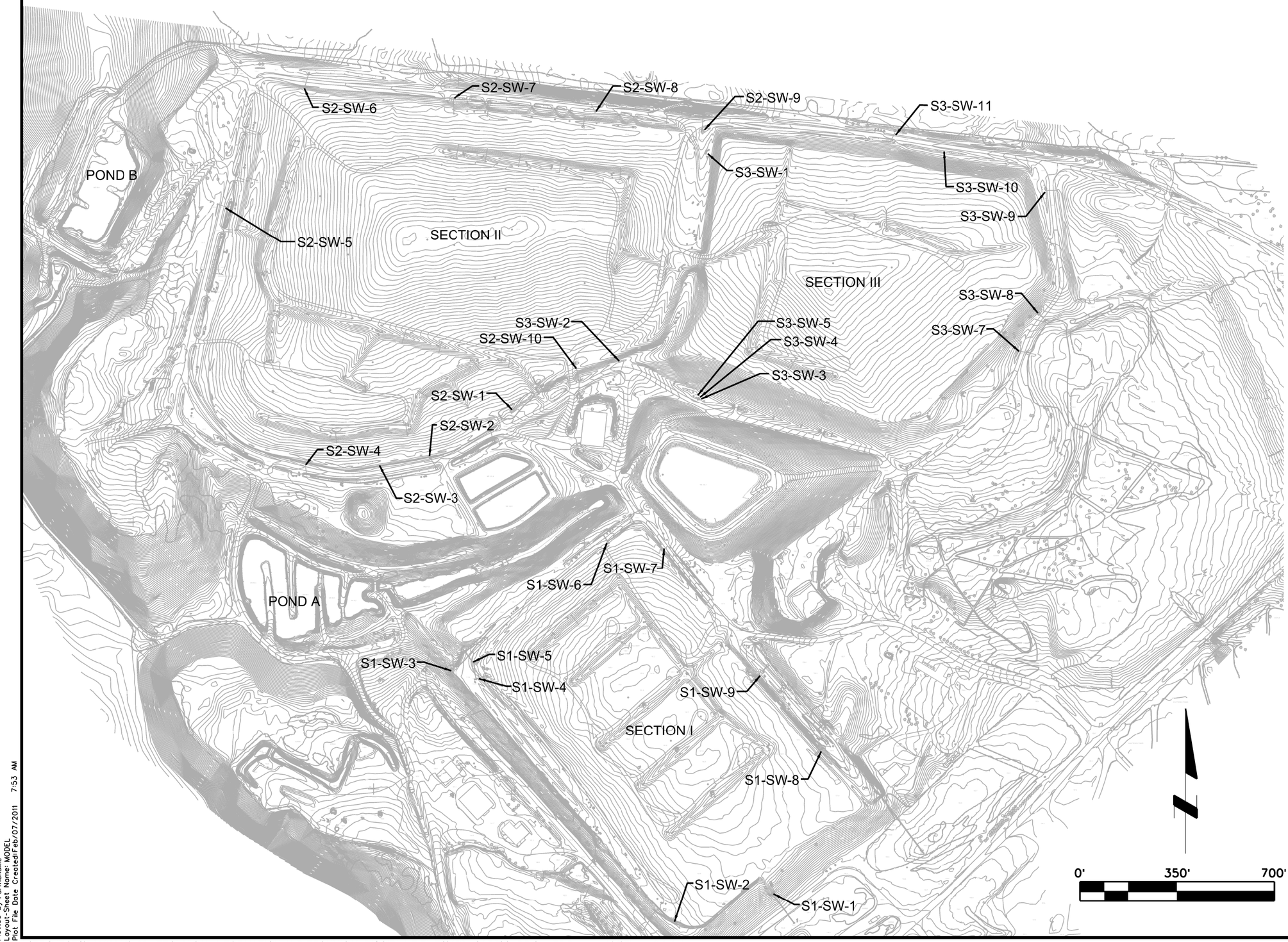
FRENCH DRAIN WATER QUALITY SAMPLING LOCATIONS

PINEWOOD LANDFILL
PINEWOOD, SOUTH CAROLINA

| FILE NAME: | DRN | PROJECT NO. | DATE | FIGURE NO. |
|---|---|---|---|---|
| | CFF | 60186203 | 1/2011 | 2.7-1 |

Plotted By: turmanskic
Layout-Sheet Name: MODEL
Plot File Date Created:Feb/07/2011 10:44 AM

L:\PROJECTS\60186203\400 - TECHNICAL INFORMATION AND TECHNICAL DISCIPLINE FILES\450 - CADD\CADD for 475-Projects 1&2\Figure 2.7-1.dgn




SECTION 1

| POINT | DESCRIPTION |
|---|---|
| S1-SW-1 | PIPE OUTLET |
| S1-SW-2 | DITCH LINE |
| S1-SW-3 | DITCH LINE |
| S1-SW-4 | DITCH LINE |
| S1-SW-5 | DROP INLET |
| S1-SW-6 | PIPE OUTLET |
| S1-SW-7 | DITCH LINE |
| S1-SW-8 | PIPE OUTLET |
| S1-SW-9 | PIPE OUTLET |

SECTION 2

| POINT | DESCRIPTION |
|---|---|
| S2-SW-1 | DROP INLET |
| S2-SW-2 | PIPE INLET |
| S2-SW-3 | PIPE INLET |
| S2-SW-4 | PIPE INLET |
| S2-SW-5 | PIPE INLET |
| S2-SW-6 | DROP INLET |
| S2-SW-7 | PIPE INLET |
| S2-SW-8 | PIPE INLET |
| S2-SW-9 | PIPE INLET |
| S2-SW-10 | PIPE OUTLOT |

SECTION 3

| POINT | DESCRIPTION |
|---|---|
| | SURFACE DRAINAGE FROM |
| S3-SW-1 | EXPOSED GEONET |
| S3-SW-2 | DITCH LINE |
| S3-SW-3 | DITCH LINE AT DROP INLET |
| S3-SW-4 | SECTION 3 TOE DRAIN WEST |
| S3-SW-5 | SECTION 3 TOE DRAIN EAST |
| S3-SW-6 | PIPE INLET |
| S3-SW-7 | PIPE INLET |
| S3-SW-8 | PIPE INLET |
| S3-SW-9 | PIPE INLET |
| S3-SW-10 | PIPE INLET |
| S3-SW-11 | PIPE INLET |

AECOM

FIGURE 2.8-1

EXISTING STORM WATER SAMPLING LOCATIONS

PINEWOOD LANDFILL
PINEWOOD, SOUTH CAROLINA

| FILE NAME: | DRN | PROJECT NO. | DATE | FIGURE NO. |
|---|---|---|---|---|
| | CFF | 60186203 | 1/2011 | 2.8-1 |

Plotted By:Furmanskic
Layout-Sheet Name: MODEL
Plot File Date Created:Feb/07/2011 7:53 AM

L:\PROJECTS\60186203\400 - TECHNICAL INFORMATION AND TECHNICAL DISCIPLINE FILES\450 - CADD\CADD for 475-Projects 1&2\Figure 2.8-1.dgn

J-21
J-36
J-66
J-13
J-39
J-17
J-64
J-4
J-60
J-19
J-27
J-33
J-31
J-59
SECTION I
J-41
J-43
J-129

0' 100' 200' 400'

LEGEND

CULVERT

CHANNEL

STORM WATER FLOW DIRECTION

AECOM

FIGURE 3.1-1

CULVERT AND CHANNEL LOCATIONS

PINEWOOD LANDFILL
PINEWOOD, SOUTH CAROLINA

| FILE NAME: | DRN | PROJECT NO. | DATE | FIGURE NO. |
|---|---|---|---|---|
| | CFF | 60186203 | 1/2011 | 3.1-1 |

Plotted By:Furmanskic
Layout-Sheet Name: MODEL
Plot File Date Created:Feb/07/2011 7:53 AM

L:\PROJECTS\60186203\400 - TECHNICAL INFORMATION AND TECHNICAL DISCIPLINE FILES\450 - CADD\CADD for 475-Projects 1&2\Figure 3.1-1.dgn

J-21
J-36
CM-12
CM-11
J-66
CM-17
J-13
CM-7
J-39
CM-3
J-17
CM-21
CM-16
J-64
J-4
CM-5
CM-18
J-19
J-60
CM-6
J-27
J-33
CM-10
CM-8
CM-19
J-59
J-31
CM-9
SECTION I
CM-13
J-41
J-43
CM-14
J-129
CM-29

0' 100' 200' 400'

## LEGEND

| | |
|---|---|
| CM-14 | DRAINAGE AREAS |
| | CULVERT |
| | CHANNEL |
| | STORM WATER FLOW DIRECTION |

AECOM

FIGURE 3.2-1

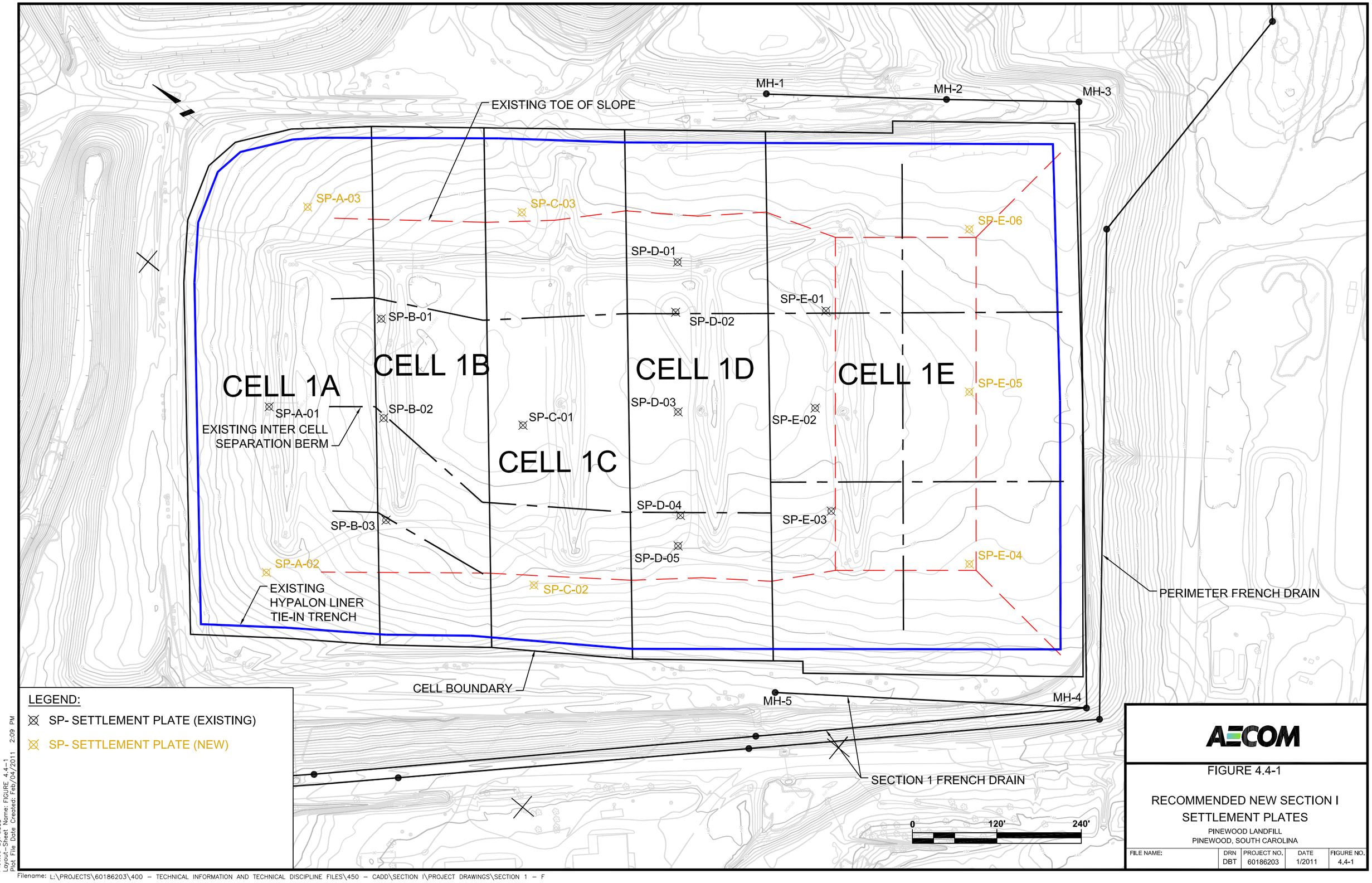
STORM WATER MODEL INPUTS

PINEWOOD LANDFILL
PINEWOOD, SOUTH CAROLINA

| FILE NAME: | DRN | PROJECT NO. | DATE | FIGURE NO. |
|---|---|---|---|---|
| | CFF | 60186203 | 1/2011 | 3.2-1 |

Plotted By:Furmanskic
Layout-Sheet Name: MODEL
Plot File Date Created:Feb/07/2011 7:53 AM

L:\PROJECTS\60186203\400 - TECHNICAL INFORMATION AND TECHNICAL DISCIPLINE FILES\450 - CADD\CADD for 475-Projects 1&2\Appendix Figure 3.2-1.dgn




LEGEND:

- SP- SETTLEMENT PLATE (EXISTING)
- SP- SETTLEMENT PLATE (NEW)

AECOM

FIGURE 4.4-1

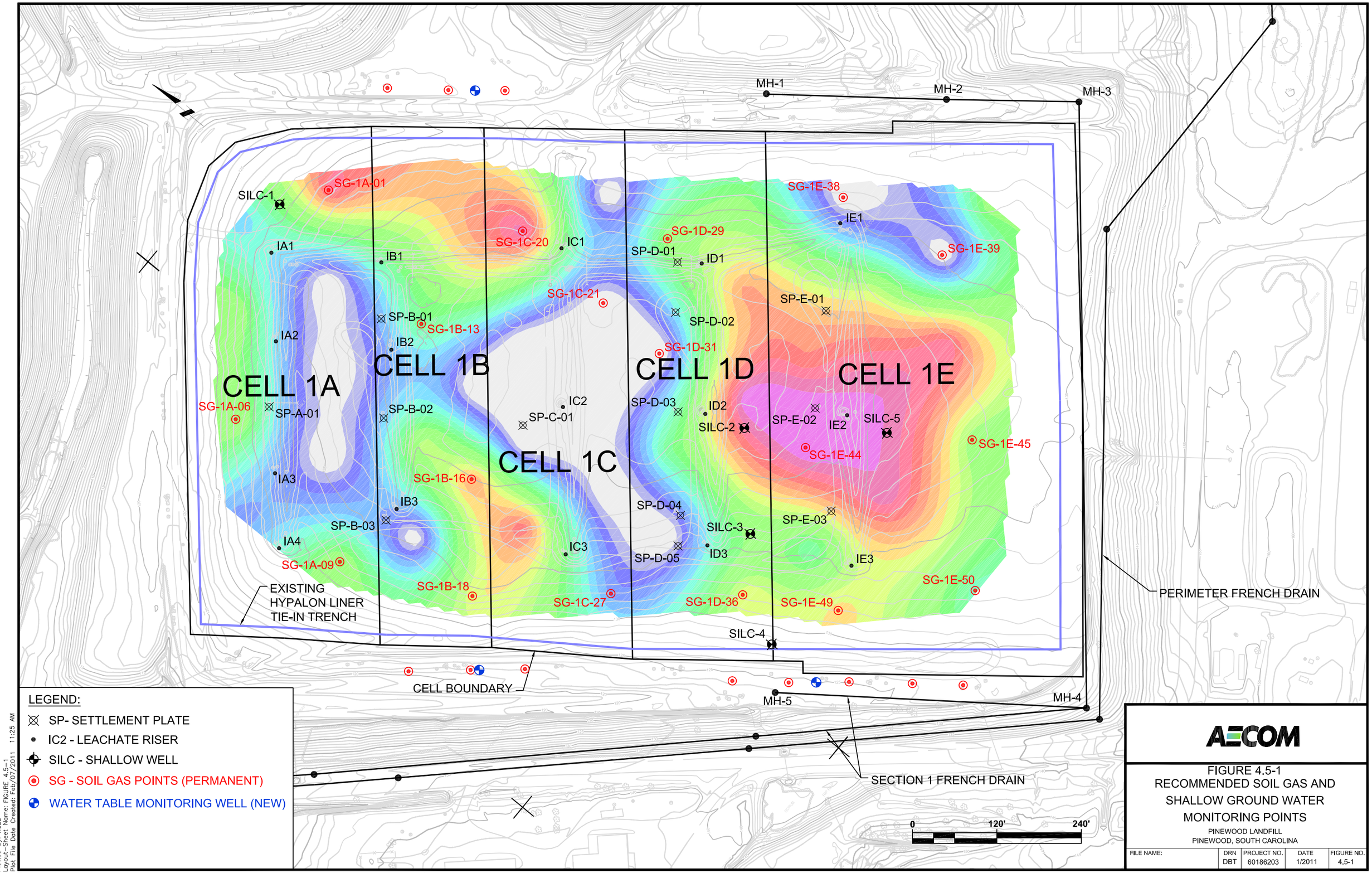
RECOMMENDED NEW SECTION I
SETTLEMENT PLATES

PINEWOOD LANDFILL
PINEWOOD, SOUTH CAROLINA

| FILE NAME: | DRN | PROJECT NO. | DATE | FIGURE NO. |
|---|---|---|---|---|
| | DBT | 60186203 | 1/2011 | 4.4-1 |

Plotted By: ticed
Layout-Sheet Name: FIGURE 4.4-1
Plot File Date Created: Feb/04/2011 2:09 PM

Filename: L:\PROJECTS\60186203\400 – TECHNICAL INFORMATION AND TECHNICAL DISCIPLINE FILES\450 – CADD\SECTION I\PROJECT DRAWINGS\SECTION 1 – F




LEGEND:

- SP- SETTLEMENT PLATE
- IC2 - LEACHATE RISER
- SILC - SHALLOW WELL
- SG - SOIL GAS POINTS (PERMANENT)
- WATER TABLE MONITORING WELL (NEW)

AECOM

FIGURE 4.5-1
RECOMMENDED SOIL GAS AND SHALLOW GROUND WATER MONITORING POINTS

PINEWOOD LANDFILL
PINEWOOD, SOUTH CAROLINA

| FILE NAME: | DRN | PROJECT NO. | DATE | FIGURE NO. |
|---|---|---|---|---|
| | DBT | 60186203 | 1/2011 | 4.5-1 |

Plotted By: TICED
Layout-Sheet Name: FIGURE 4.5-1
Plot File Date Created: Feb/07/2011 11:25 AM

Filename: L:\PROJECTS\60186203\400 – TECHNICAL INFORMATION AND TECHNICAL DISCIPLINE FILES\450 – CADD\SECTION I\PROJECT DRAWINGS\SECTION 1 – F


LEGEND

| | |
|---|---|
| SILC-4 | SHALLOW COVER WELL |
| WT-032 | PROPOSED BACKGROUND WELL FOR SECTION I (EXISTING) |

AECOM

FIGURE 4.6-1

RECOMMENDED BACKGROUND WELL FOR SECTION I COVER WELLS

PINEWOOD LANDFILL
PINEWOOD, SOUTH CAROLINA

| FILE NAME: | DRN | PROJECT NO. | DATE | FIGURE NO. |
|---|---|---|---|---|
| | CFF | 60186203 | 1/2011 | 4.6-1 |

Plotted By: furmanskic
Layout-Sheet Name: MODEL
Plot File Date Created: Feb/07/2011 10:44 AM

L:\PROJECTS\60186203\400 - TECHNICAL INFORMATION AND TECHNICAL DISCIPLINE FILES\450 - CADD\CADD for 475-Projects 1&2\Figure 4.6-1.dgn

| POINT | DESCRIPTION |
|---|---|
| FDPondA | PIPE OUTLET |
| FDPondB | PIPE OUTLET |
| FDSec1 | PIPE OUTLET |

FDPondB

POND B

SECTION II

SECTION III

BREAKPOINT

FDPondA

FDSec1

POND A

SECTION I

0' 350' 700'

LEGEND

- FRENCH DRAIN MANHOLE
- NON-PERFORATED DRAINAGE PIPE
- PERFORATED DRAINAGE PIPE

AECOM

FIGURE 4.7-1

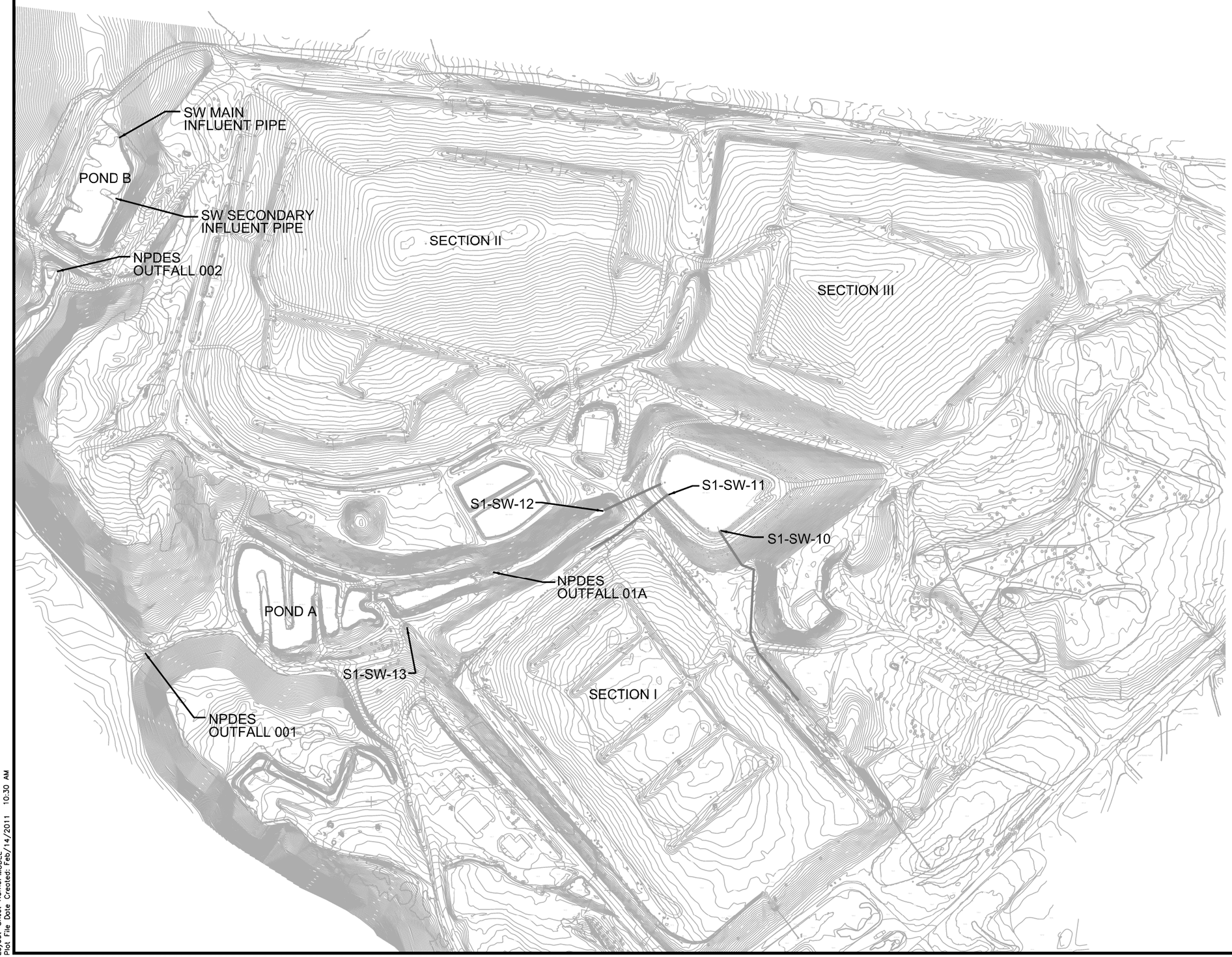
RECOMMENDED FRENCH DRAIN SAMPLING LOCATIONS

PINEWOOD LANDFILL
PINEWOOD, SOUTH CAROLINA

| FILE NAME: | DRN | PROJECT NO. | DATE | FIGURE NO. |
|---|---|---|---|---|
| | CFF | 60186203 | 1/2011 | 4.7-1 |

Plotted By:furmanskic
Layout-Sheet Name: MODEL
Plot File Date Created:Feb/07/2011 7:53 AM

L:\PROJECTS\60186203\400 - TECHNICAL INFORMATION AND TECHNICAL DISCIPLINE FILES\450 - CADD\CADD for 475-Projects 1&2\Figure 4.7-1.dgn




SECTION I

| POINT | DESCRIPTION |
|---|---|
| S1-SW-10 | PIPE OUTLET |
| S1-SW-11 | PIPE OUTLET |
| S1-SW-12 | PIPE OUTLET |
| S1-SW-13 | PIPE INLET |

SECTION II & III

| POINT | DESCRIPTION |
|---|---|
| SW MAIN INFLUENT PIPE | INLET PIPE |
| SW SECONDARY INFLUENT PIPE | INLET PIPE |

NPDES OUTFALLS

| POINT | DESCRIPTION |
|---|---|
| OUTFALL 001 | OUTFALL STRUCTURE |
| OUTFALL 002 | OUTFALL STRUCTURE |
| OUTFALL 01A | OUTFALL STRUCTURE |

0' 350' 700'

AECOM

FIGURE 4.8-1
RECOMMENDED SECTION I, II & III
STORM WATER SAMPLING LOCATIONS
AND NPDES PERMIT
SAMPLING LOCATIONS

PINEWOOD LANDFILL
PINEWOOD, SOUTH CAROLINA

| FILE NAME: | DRN | PROJECT NO. | DATE | FIGURE NO. |
|---|---|---|---|---|
| | CFF | 60186203 | 1/2011 | 4.8-1 |

Plotted By: Furmanskic
Layout-Sheet Name: MODEL
Plot File Date Created: Feb/14/2011 10.30 AM

L:\PROJECTS\60186203\400 - TECHNICAL INFORMATION AND TECHNICAL DISCIPLINE FILES\450 - CADD\CADD for 475-Projects 1&2\Figure 4.8-1.dgn

J-21

J-36

REPLACE EXISTING CULVERT

REPLACE EXISTING CULVERT

J-60

REPLACE EXISTING CULVERT

J-33

SECTION I

PROPOSED \ RELOCATED CULVERT J-23

REPLACE EXISTING CULVERT

J-41

PROPOSED BERM

CM-14

CM-29

PROPOSED 18" RCP

0' 100' 200' 400'

LEGEND

ACREAGE PROPOSED FOR REMOVAL FROM CAP DRAINAGE AREA

STORM WATER FLOW DIRECTION

CM-14 DRAINAGE AREA

AECOM

FIGURE 4.9-1

RECOMMENDED STORM WATER CONVEYANCE SYSTEM IMPROVEMENTS

PINEWOOD LANDFILL
PINEWOOD, SOUTH CAROLINA

| FILE NAME: | DRN | PROJECT NO. | DATE | FIGURE NO. |
|---|---|---|---|---|
| | CFF | 60186203 | 1/2011 | 4.9-1 |

Plotted By: Furmanskic
Layout-Sheet Name: MODEL
Plot File Date Created: Feb/08/2011 1:21 PM

L:\PROJECTS\60186203\400 - TECHNICAL INFORMATION AND TECHNICAL DISCIPLINE FILES\450 - CADD\CADD for 475-Projects 1&2\Figure 4.9-1.dgn

# APPENDICES

# Appendix 2.1-1

GEL Geophysics Report

GEL Geophysics LLC

a member of **The GEL Group** INC

PO Box 30712 Charleston, SC 29417
2040 Savage Road Charleston, SC 29407
P 843.769.7379 F 843.766.9182

www.gel.com

December 6, 2010

Mr. Walter Gerald, P.G.
AECOM
10 Patewood Drive
Building VI, Suite 500
Greenville, South Carolina 29615

Re: Ground Penetrating Radar Investigation
Pinewood Landfill
Pinewood, South Carolina

Dear Mr. Gerald:

GEL Geophysics, LLC performed a ground penetrating radar (GPR) investigation at the referenced site on November 19, 2010, under the direction of Chuck Suddeth, P.G. of AECOM. The investigation was conducted as a pilot study to determine the effectiveness of GPR at the site. AECOM wished to determine whether or not GPR technology could effectively detect and differentiate the various layers of materials overlying the synthetic liner of the landfill, as well as detect the synthetic liner/waste interface. The field procedures and results of our investigation are discussed below.

Field Procedures

The GPR investigation was performed using a RAMAC GPR system configured with a 250 MHz antenna array. A brief overview of GPR technology is included as Attachment I. The core study areas consisted of 11 discrete areas selected by AECOM within Cells 1A, 1B, 1C, 1D, and 1E. The individual study areas are listed for each cell below:

- Cell 1A: GPR-1A-01 and AT-1A-01
- Cell 1B: SB-1B-03
- Cell 1C: AT-1C-01 and AT-1B-01
- Cell 1D: GPR-1D-02, GPR-1D-03, and GPR-1D-04
- Cell 1E: GPR-1E-05, GPR-1E-06, and AT-1E-01

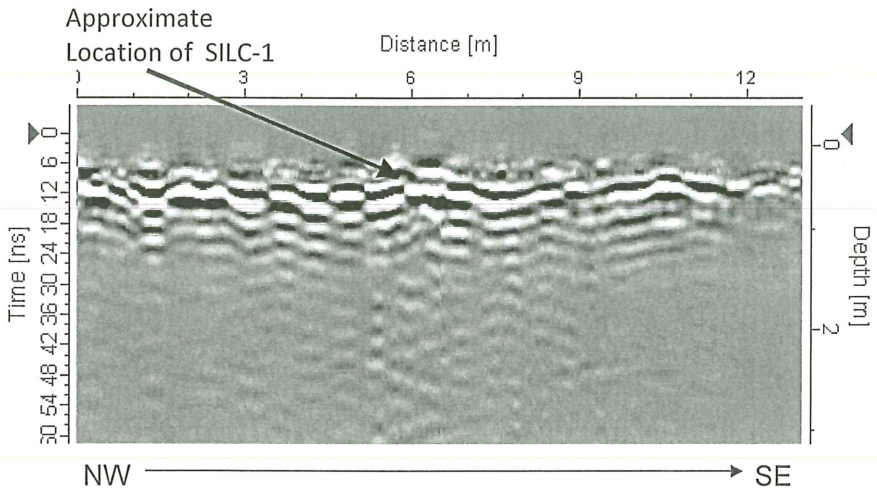
The GPR survey of each consisted of multiple parallel profiles collected in a grid pattern appropriate for the size of the area. The data were processed and interpreted in the field, and also collected for post-processing and analysis. The data were processed using MALA Geoscience's Groundvision software.

Results of Investigation

Based on the results of both the field interpretation of data and a review of the post-processed data profiles, it was determined that the subsurface conditions on all five cells investigated are not conducive for GPR. The maximum effective depth of penetration ranged from 1-2 feet below land surface, and only gross differences between the topsoil layer and the first underlying clay layer could be seen in some data profiles. It is understood that some study areas were selected by AECOM because depths of material

layers were known as a result of prior excavations and well installations. As an example, Figure 1 below is a cross-section of a GPR profile in Cell 1A (Area GPR-1A-01) immediately adjacent to well SILC-1, which had been installed in a trench.

**FIGURE 1**
**Example GPR Cross-Section**




Profile Dat0009.rd3 - Area GPR-1A-01
Direction: NW-SE directly adjacent to SILC-1

Had GPR been effective, a clearly defined trench feature would have been detectable at the location of SILC-1, which corresponds to the 6-meter distance position on the radargram shown above. However, it is apparent in the data above that GPR did not detect this known feature. Based on a review of all GPR data collected at the site, GPR is not a viable technology for differentiating between overlying soil layers within the landfill cells. Furthermore, GPR technology is not recommended as a method to determine the depth of the synthetic liner overlying the landfill cells.

GEL Geophysics appreciates the opportunity to have assisted AECOM with this investigation. If you have questions regarding this report, please do not hesitate to call me at (843) 769-7379, extension 4415.

Yours very truly,

Scott T. Smith
Senior Project Manager

enclosures

fc: aeco00210.120610.rpt.doc

# ATTACHMENT I

# EQUIPMENT AND METHODOLOGY

## Ground Penetrating Radar

GPR is an electromagnetic method that detects interfaces between subsurface materials with differing dielectric constants. The GPR system consists of: an antenna, which houses a transmitter and receiver; a profiling recorder, which processes the received signal and produces a graphic display of the data; and a video display unit, which processes and transmits the GPR signal to a color video display and recording device.

The transmitter radiates repetitive short-duration EM signals into the earth from an antenna moving across the ground surface. Electromagnetic waves are reflected back to the receiver by interfaces between materials with differing dielectric constants. The intensity of the reflected signal is a function of the contrast in the dielectric constant at the interface, the conductivity of the material that the wave is traveling through, and the frequency of the signal. Subsurface features which may cause such reflections are: 1) natural geologic conditions such as changes in sediment composition, bedding and cementation horizons, voids, and water content; or 2) man-introduced materials or changes to the subsurface such as soil backfill, buried debris, tanks, pipelines, and utilities. The profiling recorder receives the signal from the antenna and produces a continuous cross section of the subsurface interface reflections, referred to as "reflectors" or "reflection events."

Depth of investigation of the GPR signal is highly site specific, and is limited by signal attenuation (absorption) of the subsurface materials. Signal attenuation is dependent upon the electrical conductivity of the subsurface materials. Signal attenuation is greatest in materials with relatively high electrical conductivities such as clays and brackish groundwater, and lowest in relatively low conductivity materials such as unsaturated sand or rock. In addition, the presence of reinforcement bar in concrete structures may severely attenuate the GPR signal such that objects below the slab may be undetectable. Depth of investigation is also dependent on antenna frequency and generally increases with decreasing frequency; however, the ability to identify smaller subsurface features is diminished with decreasing frequency.

GEL Geophysics uses GPR antennas that are internally shielded from above-ground interference sources. Accordingly, the GPR signal is not affected by nearby aboveground conductive objects such as metal fences, overhead power lines, and vehicles. Therefore, no spurious reflection events are generated on the GPR data by aboveground features, which could lead to false interpretation of subsurface anomalies.

# Appendix 2.2-1

## Photo Log of Extruded Liner Clay Samples, PVC Geomembrane and Test Pits

Photographic Log

Section I Cover Evaluation
Undisturbed Samples of Liner Clay
From Test Pits

TP-1A-01
TP-1D-01
TP-1D-02
TP-1E-01


## PHOTOGRAPHIC LOG

**Project Name:**
Pinewood Landfill
Section I Cover Evaluation

**Location:**
Pinewood, South Carolina

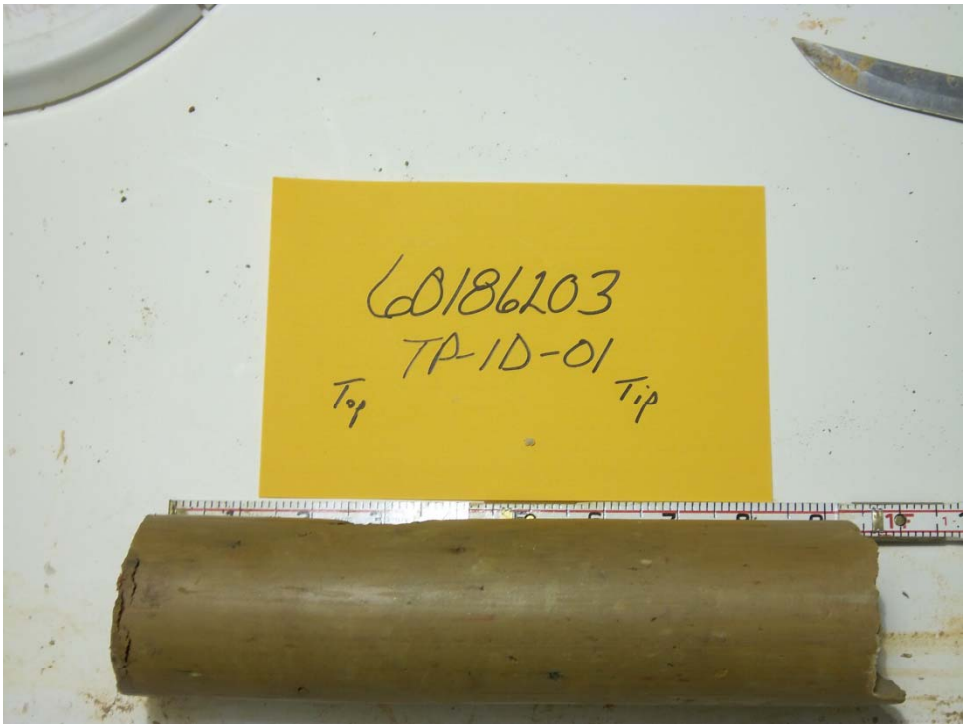
**Date Taken:**

**Picture Number:**

**Photograph by:** AECOM

**Project Number:** 60186203

**Description:**
Test Pit TP-1A-01
Liner Clay




## PHOTOGRAPHIC LOG

**Project Name:**
Pinewood Landfill
Section I Cover Evaluation

**Location:**
Pinewood, South Carolina

**Date Taken:**

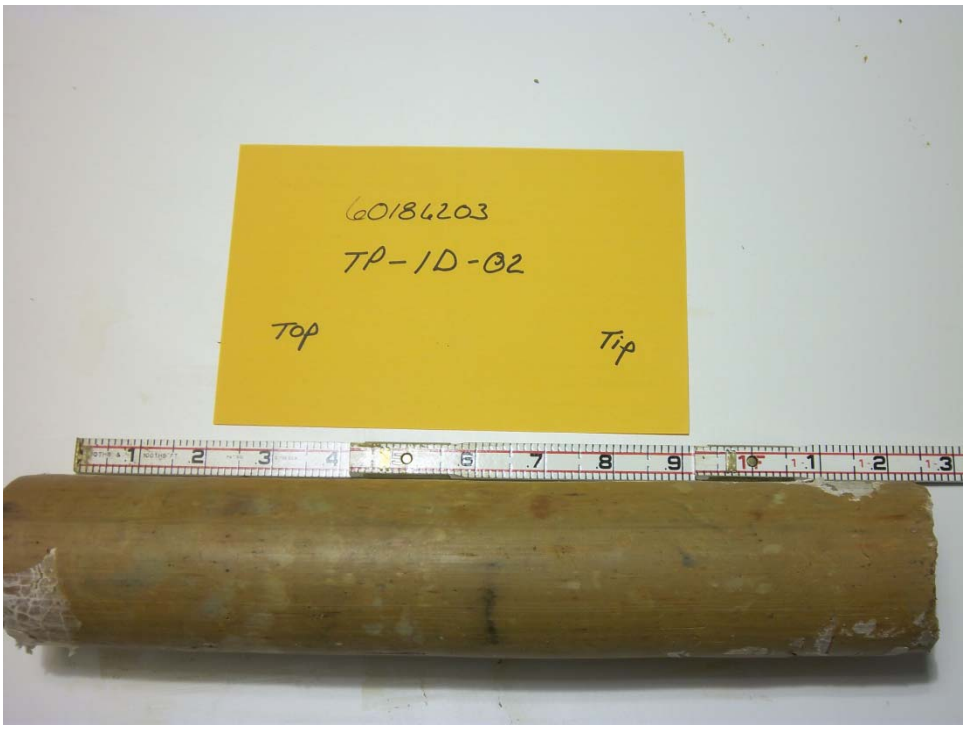
**Picture Number:**

**Photograph by:** AECOM

**Project Number:** 60186203

**Description:**
Test Pit TP-1D-01
Liner Clay

AECOM




## PHOTOGRAPHIC LOG

**Project Name:**
Pinewood Landfill
Section I Cover Evaluation

**Location:**
Pinewood, South Carolina

**Date Taken:**

**Picture Number:**

**Photograph by:** AECOM

**Project Number:** 60186203

**Description:**
Test Pit TP-1D-02
Liner Clay


## PHOTOGRAPHIC LOG

**Project Name:**
Pinewood Landfill
Section I Cover Evaluation

**Location:**
Pinewood, South Carolina

**Date Taken:**

**Picture Number:**

**Photograph by:** AECOM

**Project Number:** 60186203

**Description:**
Test Pit TP-1E-01
Liner Clay

AECOM


PHOTOGRAPHIC LOG

Project Name:
Pinewood Landfill
Section I Cover Evaluation

Location:
Pinewood, South Carolina

Date Taken:

Picture Number:

Photograph by: AECOM

Project Number: 60186203

Description:
Test Pit TP-1E-01
Liner Clay

PHOTOGRAPHIC LOG

Project Name:
Pinewood Landfill
Section I Cover Evaluation

Location:
Pinewood, South Carolina

Date Taken:

Picture Number:

Photograph by: AECOM

Project Number: 60186203

Description:

AECOM

Photographic Log

Section I Cover Evaluation
Undisturbed Samples of Liner Clay
From Soil Test Borings

SB-1A-01
SB-1B-02
SB-1B-03
SB-1C-04
SB-1C-05
SB-1D-06
SB-1D-07
SB-1E-08
SB-1E-09
SB-1E-10


## PHOTOGRAPHIC LOG

**Project Name:**
Pinewood Landfill
Section I Cover Evaluation

**Location:**
Pinewood, South Carolina

**Date Taken:**

**Picture Number:**

**Photograph by:** AECOM

**Project Number:** 60186203

**Description:**
Soil Boring SB-1A-01
Liner Clay


## PHOTOGRAPHIC LOG

**Project Name:**
Pinewood Landfill
Section I Cover Evaluation

**Location:**
Pinewood, South Carolina

**Date Taken:**

**Picture Number:**

**Photograph by:** AECOM

**Project Number:** 60186203

**Description:**
Soil Boring SB-1B-02
Liner Clay

AECOM


## PHOTOGRAPHIC LOG

**Project Name:**
Pinewood Landfill
Section I Cover Evaluation

**Location:**
Pinewood, South Carolina

**Date Taken:**

**Picture Number:**

**Photograph by:** AECOM

**Project Number:** 60186203

**Description:**
Soil Boring SB-1B-03
Liner Clay


## PHOTOGRAPHIC LOG

**Project Name:**
Pinewood Landfill
Section I Cover Evaluation

**Location:**
Pinewood, South Carolina

**Date Taken:**

**Picture Number:**

**Photograph by:** AECOM

**Project Number:** 60186203

**Description:**
Soil Boring SB-1C-04
Liner Clay

AECOM


## PHOTOGRAPHIC LOG

**Project Name:**
Pinewood Landfill
Section I Cover Evaluation

**Location:**
Pinewood, South Carolina

**Date Taken:**

**Picture Number:**

**Photograph by:** AECOM

**Project Number:** 60186203

**Description:**
Soil Boring SB-1C-05
Liner Clay


## PHOTOGRAPHIC LOG

**Project Name:**
Pinewood Landfill
Section I Cover Evaluation

**Location:**
Pinewood, South Carolina

**Date Taken:**

**Picture Number:**

**Photograph by:** AECOM

**Project Number:** 60186203

**Description:**
Soil Boring SB-1D-06
Liner Clay

AECOM


## PHOTOGRAPHIC LOG

**Project Name:**
Pinewood Landfill
Section I Cover Evaluation

**Location:**
Pinewood, South Carolina

**Date Taken:**

**Picture Number:**

**Photograph by:** AECOM

**Project Number:** 60186203

**Description:**
Soil Boring SB-1D-07
Liner Clay


## PHOTOGRAPHIC LOG

**Project Name:**
Pinewood Landfill
Section I Cover Evaluation

**Location:**
Pinewood, South Carolina

**Date Taken:**

**Picture Number:**

**Photograph by:** AECOM

**Project Number:** 60186203

**Description:**
Soil Boring SB-1E-08
Liner Clay

AECOM


PHOTOGRAPHIC LOG

Project Name:
Pinewood Landfill
Section I Cover Evaluation

Location:
Pinewood, South Carolina

Date Taken:

Picture Number:

Photograph by: AECOM

Project Number: 60186203

Description:
Soil Boring SB-1E-09
Liner Clay


PHOTOGRAPHIC LOG

Project Name:
Pinewood Landfill
Section I Cover Evaluation

Location:
Pinewood, South Carolina

Date Taken:

Picture Number:

Photograph by: AECOM

Project Number: 60186203

Description:
Soil Boring SB-1E-09
Liner Clay

AECOM


## PHOTOGRAPHIC LOG

**Project Name:**
Pinewood Landfill
Section I Cover Evaluation

**Location:**
Pinewood, South Carolina

**Date Taken:**

**Picture Number:**

**Photograph by:** AECOM

**Project Number:** 60186203

**Description:**
Soil Boring SB-1E-10
Liner Clay

## PHOTOGRAPHIC LOG

**Project Name:**
Pinewood Landfill
Section I Cover Evaluation

**Location:**
Pinewood, South Carolina

**Date Taken:**

**Picture Number:**

**Photograph by:** AECOM

**Project Number:** 60186203

**Description:**

Photographic Log

Section I Cover Evaluation
Coupon Samples of
PVC Geomembrane Liner
From Test Pits

AT-1A-01
AT-1B-01
AT-1C-01
AT-1E-01
AT-1E-02
TP-1A-01
TP-1D-01
TP-1D-02
TP-1E-01

PHOTOGRAPHIC LOG

Project Name:
Pinewood Landfill
Section I Cover Evaluation

Location:
Pinewood, South Carolina

Date Taken:

Picture Number:

Photograph by: AECOM

Project Number: 60186203

Description:
PVC Geomembrane
Test Pit AT-1A-01

PHOTOGRAPHIC LOG

Project Name:
Pinewood Landfill
Section I Cover Evaluation

Location:
Pinewood, South Carolina

Date Taken:

Picture Number:

Photograph by: AECOM

Project Number: 60186203

Description:
PVC Geomembrane
Test Pit AT-1B-01

AECOM

PHOTOGRAPHIC LOG

Project Name:
Pinewood Landfill
Section I Cover Evaluation

Location:
Pinewood, South Carolina

Date Taken:

Picture Number:

Photograph by: AECOM

Project Number: 60186203

Description:
PVC Geomembrane
Test Pit AT-1C-01

PHOTOGRAPHIC LOG

Project Name:
Pinewood Landfill
Section I Cover Evaluation

Location:
Pinewood, South Carolina

Date Taken:

Picture Number:

Photograph by: AECOM

Project Number: 60186203

Description:
PVC Geomembrane
Test Pit AT-1E-01

AECOM


PHOTOGRAPHIC LOG

Project Name:
Pinewood Landfill
Section I Cover Evaluation

Location:
Pinewood, South Carolina

Date Taken:

Picture Number:

Photograph by: AECOM

Project Number: 60186203

Description:
PVC Geomembrane
Test Pit AT-1E-02


PHOTOGRAPHIC LOG

Project Name:
Pinewood Landfill
Section I Cover Evaluation

Location:
Pinewood, South Carolina

Date Taken:

Picture Number:

Photograph by: AECOM

Project Number: 60186203

Description:
PVC Geomembrane
Test Pit TP-1A-01 Lower Panel

AECOM

## PHOTOGRAPHIC LOG

**Project Name:**
Pinewood Landfill
Section I Cover Evaluation

**Location:**
Pinewood, South Carolina

**Date Taken:**

**Picture Number:**

**Photograph by:** AECOM

**Project Number:** 60186203

**Description:**
PVC Geomembrane
Test Pit TP-1A-01 Upper Panel

## PHOTOGRAPHIC LOG

**Project Name:**
Pinewood Landfill
Section I Cover Evaluation

**Location:**
Pinewood, South Carolina

**Date Taken:**

**Picture Number:**

**Photograph by:** AECOM

**Project Number:** 60186203

**Description:**
PVC Geomembrane
Test Pit TP-1D-01

AECOM


PHOTOGRAPHIC LOG

**Project Name:**
Pinewood Landfill
Section I Cover Evaluation

**Location:**
Pinewood, South Carolina

**Date Taken:**

**Picture Number:**

**Photograph by:** AECOM

**Project Number:** 60186203

**Description:**
PVC Geomembrane
Test Pit TP-1D-02


PHOTOGRAPHIC LOG

**Project Name:**
Pinewood Landfill
Section I Cover Evaluation

**Location:**
Pinewood, South Carolina

**Date Taken:**

**Picture Number:**

**Photograph by:** AECOM

**Project Number:** 60186203

**Description:**
PVC Geomembrane
Test Pit TP-1E-01

AECOM

# Photographic Log

## Section I Cover Evaluation
## Representative Anchor Trenches
## and Test Pit

AT-1A-01
AT-1B-01
AT-1C-01
TP-1D-01

## PHOTOGRAPHIC LOG

**Project Name:**
Pinewood Landfill
Section I Cover Evaluation

**Location:**
Pinewood, South Carolina

**Date Taken:**

**Picture Number:**

**Photograph by:** AECOM

**Project Number:** 60186203

**Description:**
Anchor Trench Test Pit
AT-1A-01
Note PVC Geomembrane Patch

## PHOTOGRAPHIC LOG

**Project Name:**
Pinewood Landfill
Section I Cover Evaluation

**Location:**
Pinewood, South Carolina

**Date Taken:**

**Picture Number:**

**Photograph by:** AECOM

**Project Number:** 60186203

**Description:**
Anchor Trench Test Pit
AT-1B-01
Note PVC Geomembrane Patch

AECOM

## PHOTOGRAPHIC LOG

**Project Name:**
Pinewood Landfill
Section I Cover Evaluation

**Location:**
Pinewood, South Carolina

**Date Taken:**

**Picture Number:**

**Photograph by:** AECOM

**Project Number:** 60186203

**Description:**
Anchor Trench Test Pit
AT-1C-01
Note PVC Geomembrane Patch


## PHOTOGRAPHIC LOG

**Project Name:**
Pinewood Landfill
Section I Cover Evaluation

**Location:**
Pinewood, South Carolina

**Date Taken:**

**Picture Number:**

**Photograph by:** AECOM

**Project Number:** 60186203

**Description:**
Cover Soil Test Pit
TP-1D-01
Note PVC Geomembrane Patch

AECOM

# Appendix 2.2-2

Soil Test Boring Reports

# Test Boring Report

AECOM

BORING NO. SB-1A-01
PAGE 1 OF 1

| | | | |
|---|---|---|---|
| PROJECT: | Pinewood Landfill Section 1 Cover Evaluation | PROJECT NO: | 60186203 |
| CLIENT: | Pinewood Site Custodial Trust | LOCATION: | Pinewood, SC |
| CONTRACTOR: | Earth Con | ELEVATION: | |
| EQUIPMENT: | Mobile B-53 | NORTHING: | |
| | | EASTING: | |
| | | DATE START: | 12/01/10 |
| | | DATE FINISH: | 12/01/10 |
| | | DRILLER: | B. Brodie |
| | | OVERSIGHT: | S. Ross |

| GROUNDWATER | | | DRILLING INFORMATION | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| DATE | HRS AFTER COMP | WATER | DRILL METHOD | HSA | CASING INSTALL | N/A | TEMP / PERM | N/A |
| | | N/A | HOLE DIA. | 6.25" | CASING DIA. | N/A | CASING TYPE | N/A |
| | | | TOTAL DEPTH | 8.0' | CASING DEPTH | N/A | GROUT TYPE | N/A |
| | | | SAMPLING | SS | HAMMER WT | N/A | HAMMER FALL | N/A |

| DEPTH IN FEET | ORGANIC VAPOR SCREENING (PPM) | SAMPLER BLOWS PER 6 INCHES | SAMPLE NUMBER | SAMPLE DEPTH RANGE | FIELD CLASSIFICATION AND REMARKS (SOIL CLASSIFICATION: USCS) |
|---|---|---|---|---|---|
| | | | 1 | 0 - 2 | Topsoil |
| | 0.0 | | | | CLAYEY SAND (SC), reddish brown, mostly medium sand, some clay, stiff, dry. |
| | | | 2 | 2 - 4 | POORLY GRADED SAND (SP), yellowish brown, mostly fine sand, dense, dry (Chunks of claystone imbedded in this interval). |
| | 0.0 | | 3 | 4 - 6 | SANDY CLAY (CL), yellowish red, mostly clay, some medium to coarse sand, few silt, very stiff, dry. |
| 5.0 | | | | | CLAYSTONE, dark gray to black, dense, dry. |
| | 0.0 | | 4 | 6 - 8 | LEAN CLAY (CL), yellowish brown to light brown, mostly clay, few fine sand, medium stiff, moist. |
| 10.0 | | | | | Boring terminated at 8.0 ft.<br>Pushed Shelby tube from 6.0 - 8.0 ft in adjacent boring. |
| 15.0 | | | | | |
| 20.0 | | | | | |

| BLOWS/FT. | DENSITY |
|---|---|
| 0-4 | VERY LOOSE |
| 5-10 | LOOSE |
| 11-30 | MEDIUM DENSE |
| 31-50 | DENSE |
| 50+ | VERY DENSE |

| BLOWS/FT. | CONSISTENCY |
|---|---|
| 0-2 | VERY SOFT |
| 3-4 | SOFT |
| 5-8 | MEDIUM STIFF |
| 9-15 | STIFF |
| 16-30 | VERY STIFF |
| 31+ | HARD |

| SAMPLER ID. | |
|---|---|
| SS | SPLIT SPOON |
| ST | SHELBY TUBE |
| G | GRAB SAMPLE |
| MC | MACRO-CORE |

| DESCRIPTIONS | |
|---|---|
| MOSTLY | 50-100% |
| SOME | 30-45% |
| LITTLE | 15-25% |
| FEW | 5-10% |
| TRACE | <5% |

| NOTES | |
|---|---|
| WD | WHILE DRILLING |
| NE | NOT ENCOUNTERED |
| UR | NOT READ |
| NR | NO RECOVERY |

AECOM

# Test Boring Report

BORING NO. SB-1B-02
PAGE 1 OF 1

PROJECT: Pinewood Landfill Section 1 Cover Evaluation
CLIENT: Pinewood Site Custodial Trust
CONTRACTOR: Earth Con
EQUIPMENT: Mobile B-53

PROJECT NO: 60186203
LOCATION: Pinewood, SC
ELEVATION:
NORTHING:
EASTING:
DATE START: 12/01/10
DATE FINISH: 12/01/10
DRILLER: B. Brodie
OVERSIGHT: S. Ross

| GROUNDWATER | | | DRILLING INFORMATION | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| DATE | HRS AFTER COMP | WATER | DRILL METHOD | HSA | CASING INSTALL | N/A | TEMP / PERM | N/A |
| | | N/A | HOLE DIA. | 6.25" | CASING DIA. | N/A | CASING TYPE | N/A |
| | | | TOTAL DEPTH | 7.0' | CASING DEPTH | N/A | GROUT TYPE | N/A |
| | | | SAMPLING | SS | HAMMER WT | N/A | HAMMER FALL | N/A |

| DEPTH IN FEET | ORGANIC VAPOR SCREENING (PPM) | SAMPLER BLOWS PER 6 INCHES | SAMPLE NUMBER | SAMPLE DEPTH RANGE | FIELD CLASSIFICATION AND REMARKS (SOIL CLASSIFICATION: USCS) |
|---|---|---|---|---|---|
| | | | | | Topsoil |
| | | | 1 | 0 - 2 | SANDY CLAY (CL), reddish brown, mostly clay, little medium to coarse sand, few silt, dense, dry. |
| | | | 2 | 2 - 4 | CLAYEY SAND (SC) to LEAN CLAY (CL), reddish brown, mostly clay, few medium to coarse sand, few silt, stiff, dry to slightly moist. |
| 5.0 | | | 3 | 4 - 6 | HIGHLY PLASTIC CLAY (OH), pale brown to yellowish brown, mottled, mostly clay, few medium to fine sand, medium stiff, moist. |
| | | | 4 | 6 - 7 | |
| 10.0 | | | | | Boring terminated at 7.0 ft.<br>Encountered PVC geomembrane at 6.8 ft.<br>Pushed Shelby tube from 4.5 - 6.5 ft in adjacent boring. |
| 15.0 | | | | | |
| 20.0 | | | | | |

| BLOWS/FT. | DENSITY |
|---|---|
| 0-4 | VERY LOOSE |
| 5-10 | LOOSE |
| 11-30 | MEDIUM DENSE |
| 31-50 | DENSE |
| 50+ | VERY DENSE |

| BLOWS/FT. | CONSISTENCY |
|---|---|
| 0-2 | VERY SOFT |
| 3-4 | SOFT |
| 5-8 | MEDIUM STIFF |
| 9-15 | STIFF |
| 16-30 | VERY STIFF |
| 31+ | HARD |

| SAMPLER ID. | |
|---|---|
| SS | SPLIT SPOON |
| ST | SHELBY TUBE |
| G | GRAB SAMPLE |
| MC | MACRO-CORE |

| DESCRIPTIONS | |
|---|---|
| MOSTLY | 50-100% |
| SOME | 30-45% |
| LITTLE | 15-25% |
| FEW | 5-10% |
| TRACE | <5% |

| NOTES | |
|---|---|
| WD | WHILE DRILLING |
| NE | NOT ENCOUNTERED |
| UR | NOT READ |
| NR | NO RECOVERY |

# Test Boring Report

AECOM

BORING NO. SB-1B-03
PAGE 1 OF 1

| | | | |
|---|---|---|---|
| PROJECT: | Pinewood Landfill Section 1 Cover Evaluation | PROJECT NO: | 60186203 |
| CLIENT: | Pinewood Site Custodial Trust | LOCATION: | Pinewood, SC |
| CONTRACTOR: | Earth Con | ELEVATION: | |
| EQUIPMENT: | Mobile B-53 | NORTHING: | |
| | | EASTING: | |
| | | DATE START: | 12/01/10 |
| | | DATE FINISH: | 12/01/10 |
| | | DRILLER: | B. Brodie |
| | | OVERSIGHT: | S. Ross |

| GROUNDWATER | | | DRILLING INFORMATION | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| DATE | HRS AFTER COMP | WATER | DRILL METHOD | HSA | | CASING INSTALL | N/A | TEMP / PERM | N/A |
| | | N/A | HOLE DIA. | 6.25" | | CASING DIA. | N/A | CASING TYPE | N/A |
| | | | TOTAL DEPTH | 6.0' | | CASING DEPTH | N/A | GROUT TYPE | N/A |
| | | | SAMPLING | SS | | HAMMER WT | N/A | HAMMER FALL | N/A |

| DEPTH IN FEET | ORGANIC VAPOR SCREENING (PPM) | SAMPLER BLOWS PER 6 INCHES | SAMPLE NUMBER | SAMPLE DEPTH RANGE | FIELD CLASSIFICATION AND REMARKS (SOIL CLASSIFICATION: USCS) |
|---|---|---|---|---|---|
| | | | | | Topsoil |
| | 0.0 | | 1 | 0 - 2 | CLAYEY SAND (SC), yellowish brown, mostly medium sand, little clay, few silt, trace gravel, dense, dry. |
| | 0.0 | | 2 | 2 - 4 | Similar to above except yellowish brown to yellowish red, (mottled). Grades to reddish brown in color at 3.0'. |
| 5.0 | 0.1<br>2.6 | | 3 | 4 - 6 | LEAN CLAY (CL), yellowish brown to gray, (mottled), mostly clay, few to trace fine sand, medium stiff, moist.<br>Chemical odor in lower 4" of sample. |
| 10.0 | | | | | Boring terminated at 6.0 ft.<br>Pushed Shelby tube from 4.0 - 5.5 ft in adjacent boring. |
| 15.0 | | | | | |
| 20.0 | | | | | |

| BLOWS/FT. | DENSITY |
|---|---|
| 0-4 | VERY LOOSE |
| 5-10 | LOOSE |
| 11-30 | MEDIUM DENSE |
| 31-50 | DENSE |
| 50+ | VERY DENSE |

| BLOWS/FT. | CONSISTENCY |
|---|---|
| 0-2 | VERY SOFT |
| 3-4 | SOFT |
| 5-8 | MEDIUM STIFF |
| 9-15 | STIFF |
| 16-30 | VERY STIFF |
| 31+ | HARD |

| SAMPLER ID. | |
|---|---|
| SS | SPLIT SPOON |
| ST | SHELBY TUBE |
| G | GRAB SAMPLE |
| MC | MACRO-CORE |

| DESCRIPTIONS | |
|---|---|
| MOSTLY | 50-100% |
| SOME | 30-45% |
| LITTLE | 15-25% |
| FEW | 5-10% |
| TRACE | <5% |

| NOTES | |
|---|---|
| WD | WHILE DRILLING |
| NE | NOT ENCOUNTERED |
| UR | NOT READ |
| NR | NO RECOVERY |

# Test Boring Report

AECOM

BORING NO. SB-1C-04
PAGE 1 OF 1

| | | | |
|---|---|---|---|
| PROJECT: | Pinewood Landfill Section 1 Cover Evaluation | PROJECT NO: | 60186203 |
| CLIENT: | Pinewood Site Custodial Trust | LOCATION: | Pinewood, SC |
| CONTRACTOR: | Earth Con | ELEVATION: | |
| EQUIPMENT: | Mobile B-53 | NORTHING: | |
| | | EASTING: | |
| | | DATE START: | 12/01/10 |
| | | DATE FINISH: | 12/01/10 |
| | | DRILLER: | B. Brodie |
| | | OVERSIGHT: | S. Ross |

| GROUNDWATER | | | DRILLING INFORMATION | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| DATE | HRS AFTER COMP | WATER | DRILL METHOD | HSA | | CASING INSTALL | N/A | TEMP / PERM | N/A |
| | | N/A | HOLE DIA. | 6.25" | | CASING DIA. | N/A | CASING TYPE | N/A |
| | | | TOTAL DEPTH | 6.0' | | CASING DEPTH | N/A | GROUT TYPE | N/A |
| | | | SAMPLING | SS | | HAMMER WT | N/A | HAMMER FALL | N/A |

| DEPTH IN FEET | ORGANIC VAPOR SCREENING (PPM) | SAMPLER BLOWS PER 6 INCHES | SAMPLE NUMBER | SAMPLE DEPTH RANGE | FIELD CLASSIFICATION AND REMARKS<br>SOIL CLASSIFICATION: USCS |
|---|---|---|---|---|---|
| | | | 1 | 0 - 2 | Topsoil<br>SLIGHTLY SILTY SAND (SP-SM), pale brown to reddish brown, mostly sand, little gravel, few clay, dense, dry; increasing silt/clay content with depth. |
| | | | 2 | 2 - 4 | SILTY SAND (SM) similar to above, reddish brown, few clay, trace gravel. |
| 5.0 | | | 3 | 4 - 6 | CLAYEY SAND (SC), reddish brown to to brown, (mottled), mostly clay, few silt, few medium sand, stiff, dry. |
| 10.0 | | | | | Boring terminated at 6.0 ft.<br>Pushed Shelby tube from 3.0 - 5.0 ft in adjacent boring. |
| 15.0 | | | | | |
| 20.0 | | | | | |

| BLOWS/FT. | DENSITY |
|---|---|
| 0-4 | VERY LOOSE |
| 5-10 | LOOSE |
| 11-30 | MEDIUM DENSE |
| 31-50 | DENSE |
| 50+ | VERY DENSE |

| BLOWS/FT. | CONSISTENCY |
|---|---|
| 0-2 | VERY SOFT |
| 3-4 | SOFT |
| 5-8 | MEDIUM STIFF |
| 9-15 | STIFF |
| 16-30 | VERY STIFF |
| 31+ | HARD |

| SAMPLER ID. | |
|---|---|
| SS | SPLIT SPOON |
| ST | SHELBY TUBE |
| G | GRAB SAMPLE |
| MC | MACRO-CORE |

| DESCRIPTIONS | |
|---|---|
| MOSTLY | 50-100% |
| SOME | 30-45% |
| LITTLE | 15-25% |
| FEW | 5-10% |
| TRACE | <5% |

| NOTES | |
|---|---|
| WD | WHILE DRILLING |
| NE | NOT ENCOUNTERED |
| UR | NOT READ |
| NR | NO RECOVERY |

# Test Boring Report

AECOM

BORING NO. SB-1C-05
PAGE 1 OF 1

| | | | |
|---|---|---|---|
| PROJECT: | Pinewood Landfill Section 1 Cover Evaluation | PROJECT NO: | 60186203 |
| CLIENT: | Pinewood Site Custodial Trust | LOCATION: | Pinewood, SC |
| CONTRACTOR: | Earth Con | ELEVATION: | |
| EQUIPMENT: | Mobile B-53 | NORTHING: | |
| | | EASTING: | |
| | | DATE START: | 11/30/10 |
| | | DATE FINISH: | 11/30/10 |
| | | DRILLER: | B. Brodie |
| | | OVERSIGHT: | S. Ross |

| GROUNDWATER | | | DRILLING INFORMATION | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| DATE | HRS AFTER COMP | WATER | DRILL METHOD | HSA | | CASING INSTALL | N/A | TEMP / PERM | N/A |
| | | N/A | HOLE DIA. | 6.25" | | CASING DIA. | N/A | CASING TYPE | N/A |
| | | | TOTAL DEPTH | 8.0' | | CASING DEPTH | N/A | GROUT TYPE | N/A |
| | | | SAMPLING | SS | | HAMMER WT | N/A | HAMMER FALL | N/A |

| DEPTH IN FEET | ORGANIC VAPOR SCREENING (PPM) | SAMPLER BLOWS PER 6 INCHES | SAMPLE NUMBER | SAMPLE DEPTH RANGE | FIELD CLASSIFICATION AND REMARKS<br>SOIL CLASSIFICATION: USCS |
|---|---|---|---|---|---|
| | 0.2 | | 1 | 0 - 2 | Topsoil<br>SILTY SAND (SM), light reddish brown, mostly silt, little medium to coarse sand, few to trace clay, medium dense, dry. |
| | 0.2 | | 2 | 2 - 4 | Similar to above (SC-SM), grades to yellowish red, mostly silt, little clay, few coarse sand, trace gravel. |
| 5.0 | 0.2 | | 3 | 4 - 6 | Similar to above, dense, dry. |
| | | | 4 | 6 - 8 | CLAYEY SAND (SC), dark red to red, mostly lean clay, little to few coarse sand, few silt, stiff, moist. |
| 10.0 | | | | | Boring terminated at 8.0 ft.<br>Pushed Shelby tube from 6.0 - 8.0 ft in adjacent boring. |
| 15.0 | | | | | |
| 20.0 | | | | | |

| BLOWS/FT. | DENSITY |
|---|---|
| 0-4 | VERY LOOSE |
| 5-10 | LOOSE |
| 11-30 | MEDIUM DENSE |
| 31-50 | DENSE |
| 50+ | VERY DENSE |

| BLOWS/FT. | CONSISTENCY |
|---|---|
| 0-2 | VERY SOFT |
| 3-4 | SOFT |
| 5-8 | MEDIUM STIFF |
| 9-15 | STIFF |
| 16-30 | VERY STIFF |
| 31+ | HARD |

| SAMPLER ID. | |
|---|---|
| SS | SPLIT SPOON |
| ST | SHELBY TUBE |
| G | GRAB SAMPLE |
| MC | MACRO-CORE |

| DESCRIPTIONS | |
|---|---|
| MOSTLY | 50-100% |
| SOME | 30-45% |
| LITTLE | 15-25% |
| FEW | 5-10% |
| TRACE | <5% |

| NOTES | |
|---|---|
| WD | WHILE DRILLING |
| NE | NOT ENCOUNTERED |
| UR | NOT READ |
| NR | NO RECOVERY |

# Test Boring Report

AECOM

BORING NO. SB-1D-06
PAGE 1 OF 1

| | | | |
|---|---|---|---|
| PROJECT: | Pinewood Landfill Section 1 Cover Evaluation | PROJECT NO: | 60186203 |
| CLIENT: | Pinewood Site Custodial Trust | LOCATION: | Pinewood, SC |
| CONTRACTOR: | Earth Con | ELEVATION: | |
| EQUIPMENT: | Mobile B-53 | NORTHING: | |
| | | EASTING: | |
| | | DATE START: | 12/01/10 |
| | | DATE FINISH: | 12/01/10 |
| | | DRILLER: | B. Brodie |
| | | OVERSIGHT: | S. Ross |

| GROUNDWATER | | | DRILLING INFORMATION | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| DATE | HRS AFTER COMP | WATER | DRILL METHOD | HSA | CASING INSTALL | N/A | TEMP / PERM | N/A |
| | | N/A | HOLE DIA. | 6.25" | CASING DIA. | N/A | CASING TYPE | N/A |
| | | | TOTAL DEPTH | 7.0' | CASING DEPTH | N/A | GROUT TYPE | N/A |
| | | | SAMPLING | SS | HAMMER WT | N/A | HAMMER FALL | N/A |

| DEPTH IN FEET | ORGANIC VAPOR SCREENING (PPM) | SAMPLER BLOWS PER 6 INCHES | SAMPLE NUMBER | SAMPLE DEPTH RANGE | FIELD CLASSIFICATION AND REMARKS (SOIL CLASSIFICATION: USCS) |
|---|---|---|---|---|---|
| | | | | | Topsoil |
| | | | 1 | 0 - 2 | SLIGHTLY CLAYEY SAND (SP-SC), reddish brown, mostly medium to fine sand, little clay, dense, dry. |
| | 0.0 | | 2 | 2 - 4 | Similar to above, SILTY SAND (SM). |
| | 0.2 | | | | |
| 5.0 | | | 3 | 4 - 6 | CLAYEY SAND (SC) to SANDY LEAN CLAY (CL), dark reddish brown, mostly clay, few fine sand, stiff, moist. |
| | | | 4 | 6 - 7 | Encountered PVC geomembrane at 6.5' and stopped sampling. |
| | | | | | Boring terminated at 7.0 ft.<br>Pushed Shelby tube from 4.0 - 6.0 ft in adjacent boring. |
| 10.0 | | | | | |
| 15.0 | | | | | |
| 20.0 | | | | | |

| BLOWS/FT. | DENSITY |
|---|---|
| 0-4 | VERY LOOSE |
| 5-10 | LOOSE |
| 11-30 | MEDIUM DENSE |
| 31-50 | DENSE |
| 50+ | VERY DENSE |

| BLOWS/FT. | CONSISTENCY |
|---|---|
| 0-2 | VERY SOFT |
| 3-4 | SOFT |
| 5-8 | MEDIUM STIFF |
| 9-15 | STIFF |
| 16-30 | VERY STIFF |
| 31+ | HARD |

| SAMPLER ID. | |
|---|---|
| SS | SPLIT SPOON |
| ST | SHELBY TUBE |
| G | GRAB SAMPLE |
| MC | MACRO-CORE |

| DESCRIPTIONS | |
|---|---|
| MOSTLY | 50-100% |
| SOME | 30-45% |
| LITTLE | 15-25% |
| FEW | 5-10% |
| TRACE | <5% |

| NOTES | |
|---|---|
| WD | WHILE DRILLING |
| NE | NOT ENCOUNTERED |
| UR | NOT READ |
| NR | NO RECOVERY |

# Test Boring Report

AECOM

BORING NO. SB-1D-07
PAGE 1 OF 1

PROJECT: Pinewood Landfill Section 1 Cover Evaluation
CLIENT: Pinewood Site Custodial Trust
CONTRACTOR: Earth Con
EQUIPMENT: Mobile B-53

PROJECT NO: 60186203
LOCATION: Pinewood, SC
ELEVATION:
NORTHING:
EASTING:
DATE START: 11/30/10
DATE FINISH: 11/30/10
DRILLER: B. Brodie
OVERSIGHT: S. Ross

| GROUNDWATER | | | DRILLING INFORMATION | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| DATE | HRS AFTER COMP | WATER | DRILL METHOD | HSA | | CASING INSTALL | N/A | TEMP / PERM | N/A |
| | | N/A | HOLE DIA. | 6.25" | | CASING DIA. | N/A | CASING TYPE | N/A |
| | | | TOTAL DEPTH | 7.5' | | CASING DEPTH | N/A | GROUT TYPE | N/A |
| | | | SAMPLING | SS | | HAMMER WT | N/A | HAMMER FALL | N/A |

| DEPTH IN FEET | ORGANIC VAPOR SCREENING (PPM) | SAMPLER BLOWS PER 6 INCHES | SAMPLE NUMBER | SAMPLE DEPTH RANGE | FIELD CLASSIFICATION AND REMARKS (SOIL CLASSIFICATION: USCS) |
|---|---|---|---|---|---|
| | | | 1 | 0 - 2 | Topsoil<br>SILTY SAND (SM), brown to pale brown, mostly medium sand, poorly graded, trace coarse sand, trace fine gravel, loose, dry. |
| | | | 2 | 2 - 4 | Similar to above except grayish-reddish-brown. |
| 5.0 | | | 3 | 4 - 6 | CLAYEY SAND (SC), reddish brown to yellowish red, mostly medium to coarse sand, few clay, trace medium to coarse gravel, medium dense, dry. |
| | | | 4 | 6 - 7.5 | HIGHLY PLASTIC CLAY (CH), pale brown to reddish brown (mottled), mostly clay, few to trace medium to fine sand, medium stiff, moist. |
| 10.0 | | | | | Boring terminated at 7.5 ft.<br>Pushed Shelby tube from 7.0 -9.0 ft in adjacent boring.<br>Encountered PVC geomembrane at 8.0 ft. |
| 15.0 | | | | | |
| 20.0 | | | | | |

| BLOWS/FT. | DENSITY |
|---|---|
| 0-4 | VERY LOOSE |
| 5-10 | LOOSE |
| 11-30 | MEDIUM DENSE |
| 31-50 | DENSE |
| 50+ | VERY DENSE |

| BLOWS/FT. | CONSISTENCY |
|---|---|
| 0-2 | VERY SOFT |
| 3-4 | SOFT |
| 5-8 | MEDIUM STIFF |
| 9-15 | STIFF |
| 16-30 | VERY STIFF |
| 31+ | HARD |

| SAMPLER ID. | |
|---|---|
| SS | SPLIT SPOON |
| ST | SHELBY TUBE |
| G | GRAB SAMPLE |
| MC | MACRO-CORE |

| DESCRIPTIONS | |
|---|---|
| MOSTLY | 50-100% |
| SOME | 30-45% |
| LITTLE | 15-25% |
| FEW | 5-10% |
| TRACE | <5% |

| NOTES | |
|---|---|
| WD | WHILE DRILLING |
| NE | NOT ENCOUNTERED |
| UR | NOT READ |
| NR | NO RECOVERY |

# Test Boring Report

AECOM

BORING NO. SB-1E-08
PAGE 1 OF 1

| | | | |
|---|---|---|---|
| PROJECT: | Pinewood Landfill Section 1 Cover Evaluation | PROJECT NO: | 60186203 |
| CLIENT: | Pinewood Site Custodial Trust | LOCATION: | Pinewood, SC |
| CONTRACTOR: | Earth Con | ELEVATION: | |
| EQUIPMENT: | Mobile B-53 | NORTHING: | |
| | | EASTING: | |
| | | DATE START: | 11/30/10 |
| | | DATE FINISH: | 11/30/10 |
| | | DRILLER: | B. Brodie |
| | | OVERSIGHT: | S. Ross |

| GROUNDWATER | | | DRILLING INFORMATION | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| DATE | HRS AFTER COMP | WATER | DRILL METHOD | HSA | | CASING INSTALL | N/A | TEMP / PERM | N/A |
| | | N/A | HOLE DIA. | 6.25" | | CASING DIA. | N/A | CASING TYPE | N/A |
| | | | TOTAL DEPTH | 3.5' | | CASING DEPTH | N/A | GROUT TYPE | N/A |
| | | | SAMPLING | SS | | HAMMER WT | N/A | HAMMER FALL | N/A |

| DEPTH IN FEET | ORGANIC VAPOR SCREENING (PPM) | SAMPLER BLOWS PER 6 INCHES | SAMPLE NUMBER | SAMPLE DEPTH RANGE | FIELD CLASSIFICATION AND REMARKS<br>SOIL CLASSIFICATION: USCS |
|---|---|---|---|---|---|
| | | | 1 | 0 - 2 | Topsoil<br>CLAYEY SAND (SC), reddish brown, mostly medium to coarse sand, little clay, few silt, medium dense, dry. |
| | 0.4 | | 2 | 2 - 3.5 | HIGHLY PLASTIC CLAY (CH), pale brown to reddish brown (mottled), mostly clay, few fine sand, medium stiff, moist. |
| 5.0 | | | | | Encountered PVC geomembrane at 3.4 ft.<br>Boring terminated at 3.5 ft.<br>Pushed Shelby tube from 1.5 -3.5 ft in adjacent boring. |
| 10.0 | | | | | |
| 15.0 | | | | | |
| 20.0 | | | | | |

| BLOWS/FT. | DENSITY |
|---|---|
| 0-4 | VERY LOOSE |
| 5-10 | LOOSE |
| 11-30 | MEDIUM DENSE |
| 31-50 | DENSE |
| 50+ | VERY DENSE |

| BLOWS/FT. | CONSISTENCY |
|---|---|
| 0-2 | VERY SOFT |
| 3-4 | SOFT |
| 5-8 | MEDIUM STIFF |
| 9-15 | STIFF |
| 16-30 | VERY STIFF |
| 31+ | HARD |

| SAMPLER ID. | |
|---|---|
| SS | SPLIT SPOON |
| ST | SHELBY TUBE |
| G | GRAB SAMPLE |
| MC | MACRO-CORE |

| DESCRIPTIONS | |
|---|---|
| MOSTLY | 50-100% |
| SOME | 30-45% |
| LITTLE | 15-25% |
| FEW | 5-10% |
| TRACE | <5% |

| NOTES | |
|---|---|
| WD | WHILE DRILLING |
| NE | NOT ENCOUNTERED |
| UR | NOT READ |
| NR | NO RECOVERY |

# Test Boring Report

AECOM

BORING NO. SB-1E-09
PAGE 1 OF 1

| | | | |
|---|---|---|---|
| PROJECT: | Pinewood Landfill Section 1 Cover Evaluation | PROJECT NO: | 60186203 |
| CLIENT: | Pinewood Site Custodial Trust | LOCATION: | Pinewood, SC |
| CONTRACTOR: | Earth Con | ELEVATION: | |
| EQUIPMENT: | Mobile B-53 | NORTHING: | |
| | | EASTING: | |
| | | DATE START: | 11/30/10 |
| | | DATE FINISH: | 11/30/10 |
| | | DRILLER: | B. Brodie |
| | | OVERSIGHT: | S. Ross |

| GROUNDWATER | | | DRILLING INFORMATION | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| DATE | HRS AFTER COMP | WATER | DRILL METHOD | HSA | | CASING INSTALL | N/A | TEMP / PERM | N/A |
| | | N/A | HOLE DIA. | 6.25" | | CASING DIA. | N/A | CASING TYPE | N/A |
| | | | TOTAL DEPTH | 5.0' | | CASING DEPTH | N/A | GROUT TYPE | N/A |
| | | | SAMPLING | SS | | HAMMER WT | N/A | HAMMER FALL | N/A |

| DEPTH IN FEET | ORGANIC VAPOR SCREENING (PPM) | SAMPLER BLOWS PER 6 INCHES | SAMPLE NUMBER | SAMPLE DEPTH RANGE | FIELD CLASSIFICATION AND REMARKS<br>SOIL CLASSIFICATION: USCS |
|---|---|---|---|---|---|
| | | | 1 | 0 - 2 | Topsoil<br>CLAYEY SAND (SC), yellowish red to reddish brown, mostly medium sand, few clay, few silt, few fine sand, trace gravel, medium dense, dry. |
| | 0.4 | | 2 | 2 - 4 | HIGHLY PLASTIC CLAY (CH), yellowish brown, mostly clay, few fine sand, medium stiff, moist. |
| | | | 2 | 4 - 5 | |
| 5.0 | | | | | Boring terminated at 5.0 ft.<br>Pushed Shelby tube from 2.5 - 4.5 ft in adjacent boring. |
| 10.0 | | | | | |
| 15.0 | | | | | |
| 20.0 | | | | | |

| BLOWS/FT. | DENSITY |
|---|---|
| 0-4 | VERY LOOSE |
| 5-10 | LOOSE |
| 11-30 | MEDIUM DENSE |
| 31-50 | DENSE |
| 50+ | VERY DENSE |

| BLOWS/FT. | CONSISTENCY |
|---|---|
| 0-2 | VERY SOFT |
| 3-4 | SOFT |
| 5-8 | MEDIUM STIFF |
| 9-15 | STIFF |
| 16-30 | VERY STIFF |
| 31+ | HARD |

| SAMPLER ID. | |
|---|---|
| SS | SPLIT SPOON |
| ST | SHELBY TUBE |
| G | GRAB SAMPLE |
| MC | MACRO-CORE |

| DESCRIPTIONS | |
|---|---|
| MOSTLY | 50-100% |
| SOME | 30-45% |
| LITTLE | 15-25% |
| FEW | 5-10% |
| TRACE | <5% |

| NOTES | |
|---|---|
| WD | WHILE DRILLING |
| NE | NOT ENCOUNTERED |
| UR | NOT READ |
| NR | NO RECOVERY |

# Test Boring Report

AECOM

BORING NO. SB-1E-10
PAGE 1 OF 1

PROJECT: Pinewood Landfill Section 1 Cover Evaluation
CLIENT: Pinewood Site Custodial Trust
CONTRACTOR: Earth Con
EQUIPMENT: Mobile B-53

PROJECT NO: 60186203
LOCATION: Pinewood, SC
ELEVATION:
NORTHING:
EASTING:
DATE START: 11/30/10
DATE FINISH: 11/30/10
DRILLER: B. Brodie
OVERSIGHT: S. Ross

| GROUNDWATER | | | DRILLING INFORMATION | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| DATE | HRS AFTER COMP | WATER | DRILL METHOD | HSA | | CASING INSTALL | N/A | TEMP / PERM | N/A |
| | | N/A | HOLE DIA. | 6.25" | | CASING DIA. | N/A | CASING TYPE | N/A |
| | | | TOTAL DEPTH | 5.0' | | CASING DEPTH | N/A | GROUT TYPE | N/A |
| | | | SAMPLING | SS | | HAMMER WT | N/A | HAMMER FALL | N/A |

| DEPTH IN FEET | ORGANIC VAPOR SCREENING (PPM) | SAMPLER BLOWS PER 6 INCHES | SAMPLE NUMBER | SAMPLE DEPTH RANGE | FIELD CLASSIFICATION AND REMARKS<br>SOIL CLASSIFICATION: USCS |
|---|---|---|---|---|---|
| | | | | | Topsoil |
| | | | 1 | 0 - 2 | CLAYEY SAND (SC), reddish brown, mostly medium sand, few clay, few silt, trace medium gravel, dense, dry. |
| | | | 2 | 2 - 4 | HIGHLY PLASTIC CLAY (CH), pale brown, mostly clay, few to trace fine sand, stiff, moist. |
| | | | 3 | 4 - 5 | |
| 5.0 | | | | | Encountered PVC geomembrane at 5.0 ft.<br>Boring terminated at 5.0 ft.<br>Pushed Shelby tube from 2.0 - 4.0 ft in adjacent boring. |
| 10.0 | | | | | |
| 15.0 | | | | | |
| 20.0 | | | | | |

| BLOWS/FT. | DENSITY |
|---|---|
| 0-4 | VERY LOOSE |
| 5-10 | LOOSE |
| 11-30 | MEDIUM DENSE |
| 31-50 | DENSE |
| 50+ | VERY DENSE |

| BLOWS/FT. | CONSISTENCY |
|---|---|
| 0-2 | VERY SOFT |
| 3-4 | SOFT |
| 5-8 | MEDIUM STIFF |
| 9-15 | STIFF |
| 16-30 | VERY STIFF |
| 31+ | HARD |

| SAMPLER ID. | |
|---|---|
| SS | SPLIT SPOON |
| ST | SHELBY TUBE |
| G | GRAB SAMPLE |
| MC | MACRO-CORE |

| DESCRIPTIONS | |
|---|---|
| MOSTLY | 50-100% |
| SOME | 30-45% |
| LITTLE | 15-25% |
| FEW | 5-10% |
| TRACE | <5% |

| NOTES | |
|---|---|
| WD | WHILE DRILLING |
| NE | NOT ENCOUNTERED |
| UR | NOT READ |
| NR | NO RECOVERY |

# Appendix 2.2-3
# Geotechnical Testing Reports

AECOM Technical Services, Inc.

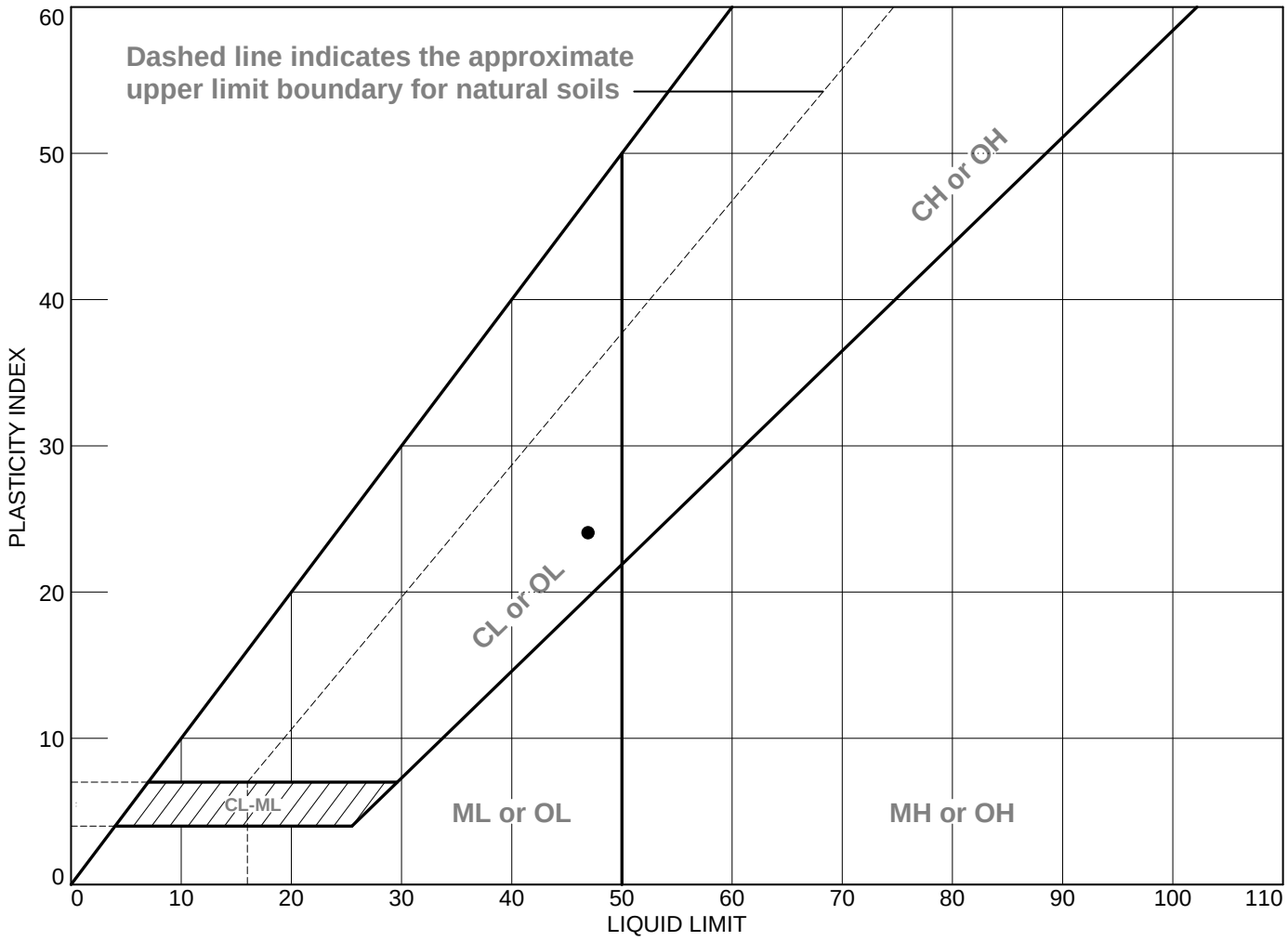
TRI / Environmental, Inc.

# AECOM Technical Services, Inc.

## Undisturbed Soil Samples

## Liquid and Plastic Limits Testing
## Particle Size Distribution Testing

# LIQUID AND PLASTIC LIMITS TEST REPORT




| SOIL DATA | | | | | | | | |
|---|---|---|---|---|---|---|---|---|
| SYMBOL | SOURCE | SAMPLE NO. | DEPTH | NATURAL WATER CONTENT (%) | PLASTIC LIMIT (%) | LIQUID LIMIT (%) | PLASTICITY INDEX (%) | USCS |
| ● | ON SITE | SB-1A-1A | | 33.4 | 23 | 47 | 24 | CL |

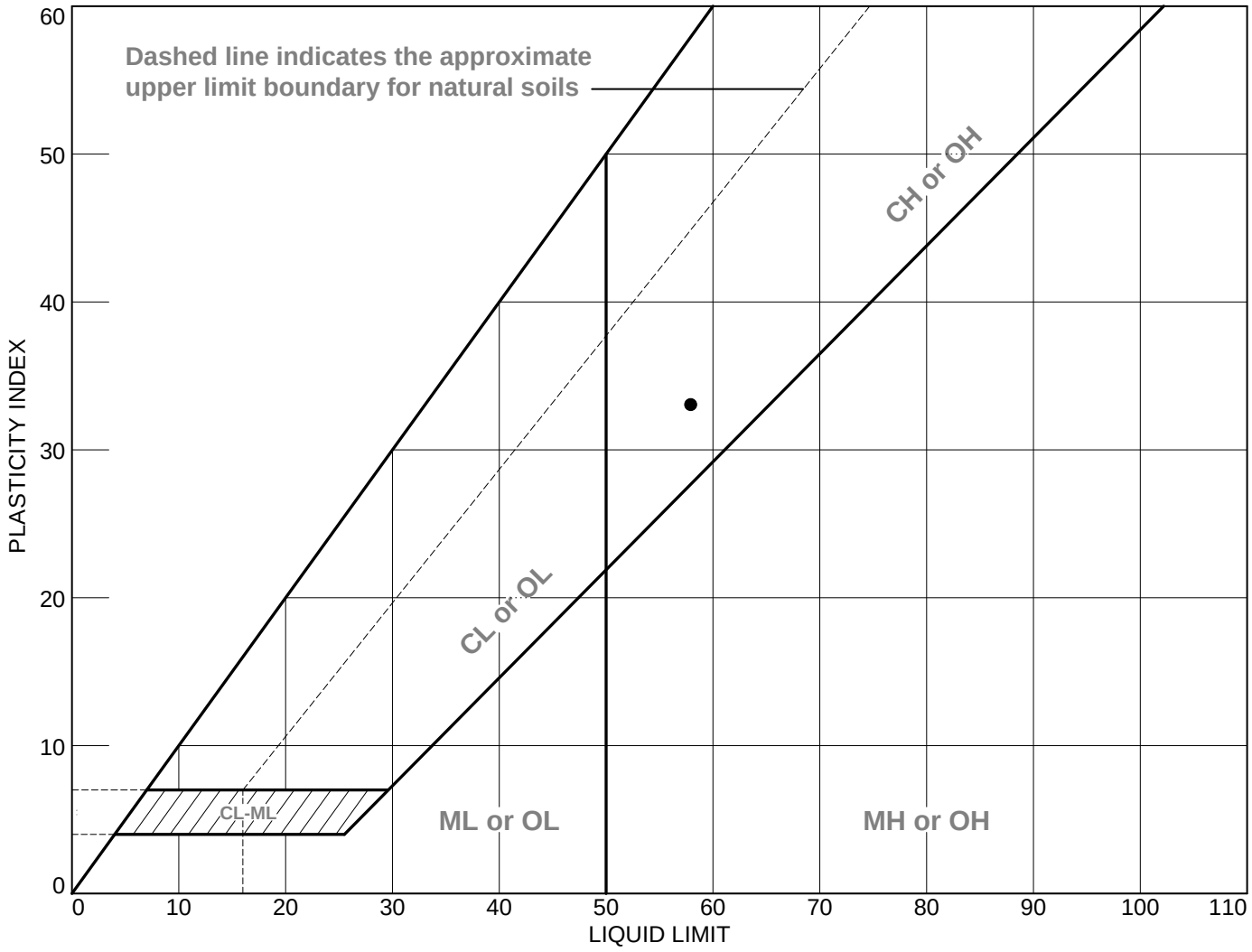
AECOM

**Client:** KESTREL HORIZONS LLC
**Project:** PINEWOOD SITE IMPROVEMENT

**Project No.:** 60186203 **Figure**

**Tested By:** BOB PEETERS

# LIQUID AND PLASTIC LIMITS TEST REPORT




**SOIL DATA**

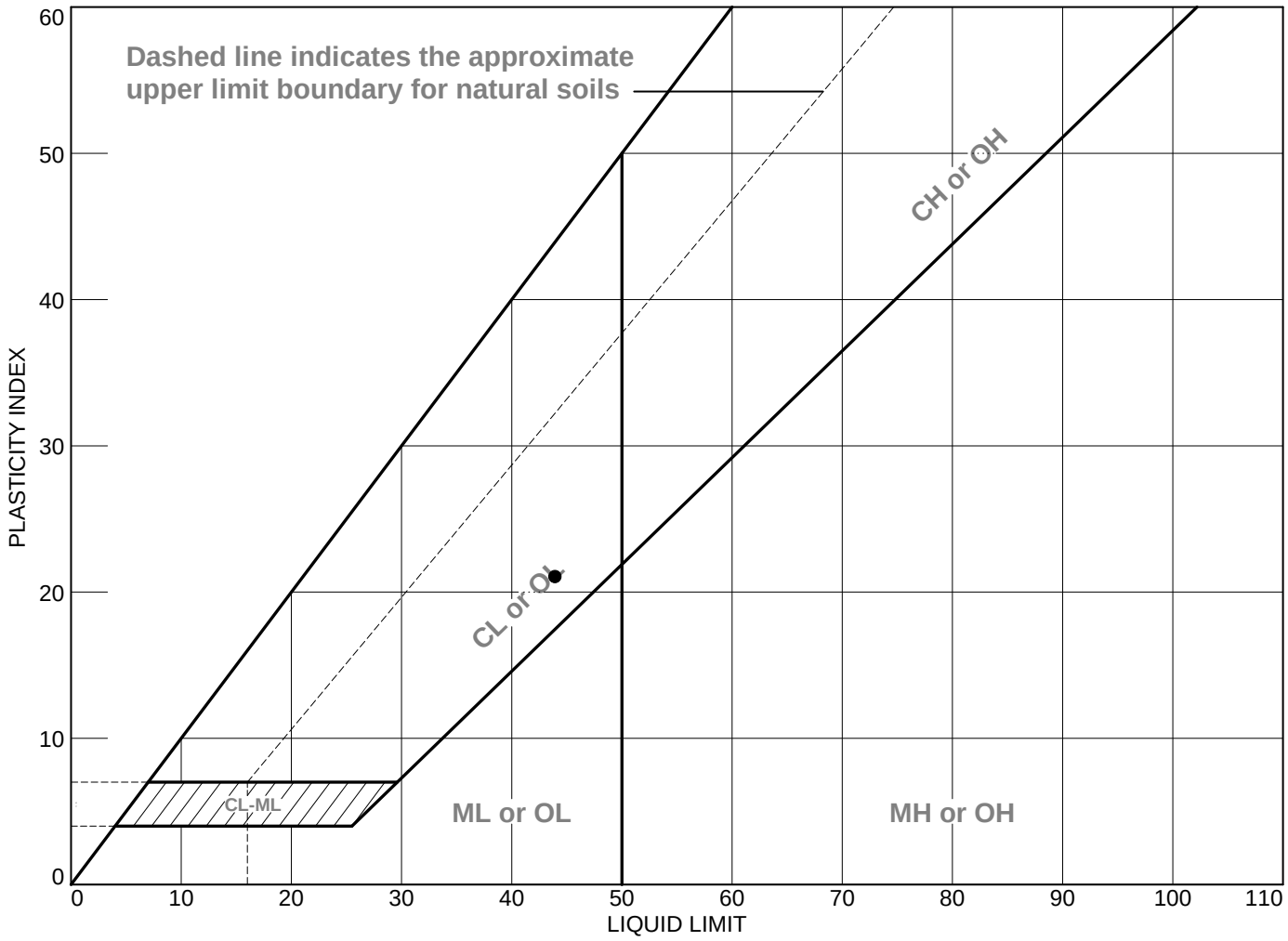
| SYMBOL | SOURCE | SAMPLE NO. | DEPTH | NATURAL WATER CONTENT (%) | PLASTIC LIMIT (%) | LIQUID LIMIT (%) | PLASTICITY INDEX (%) | USCS |
|---|---|---|---|---|---|---|---|---|
| ● | ON SITE | SB-1B-2A | | 30.2 | 25 | 58 | 33 | CH |

AECOM

**Client:** KESTREL HORIZONS LLC
**Project:** PINEWOOD SITE IMPROVEMENT

**Project No.:** 60186203 **Figure**

# LIQUID AND PLASTIC LIMITS TEST REPORT




**SOIL DATA**

| SYMBOL | SOURCE | SAMPLE NO. | DEPTH | NATURAL WATER CONTENT (%) | PLASTIC LIMIT (%) | LIQUID LIMIT (%) | PLASTICITY INDEX (%) | USCS |
|---|---|---|---|---|---|---|---|---|
| ● | ON SITE | SB-1B-3 | | 27.9 | 23 | 44 | 21 | CL |

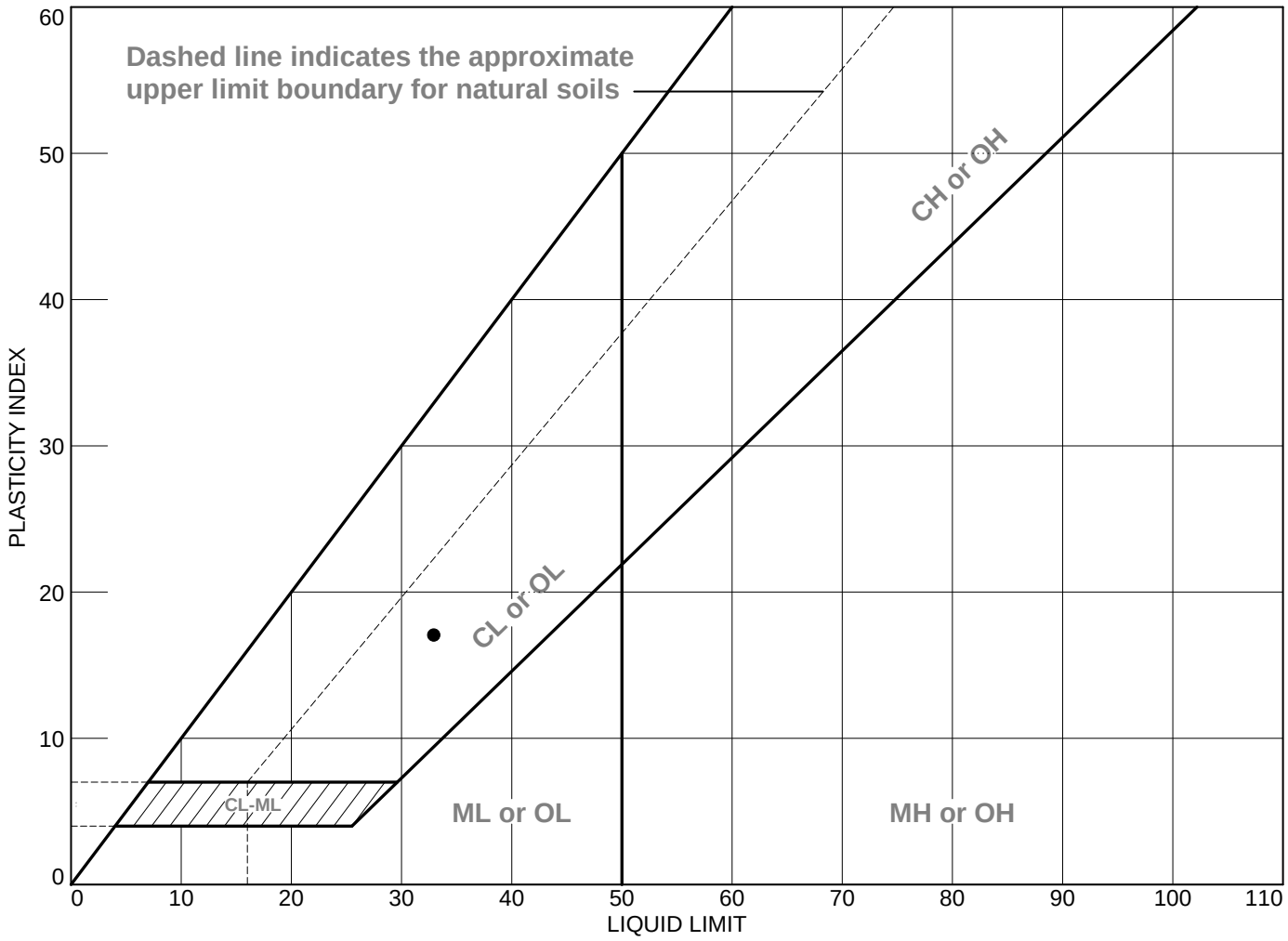
AECOM

**Client:** KESTREL HORIZONS LLC
**Project:** PINEWOOD SITE IMPROVEMENT

**Project No.:** 60186203 **Figure**

**Tested By:** BOB PEETERS

# LIQUID AND PLASTIC LIMITS TEST REPORT




| SOIL DATA | | | | | | | | |
|---|---|---|---|---|---|---|---|---|
| SYMBOL | SOURCE | SAMPLE NO. | DEPTH | NATURAL WATER CONTENT (%) | PLASTIC LIMIT (%) | LIQUID LIMIT (%) | PLASTICITY INDEX (%) | USCS |
| ● | ON SITE | SB-1C-4A | | 16.7 | 16 | 33 | 17 | SC |

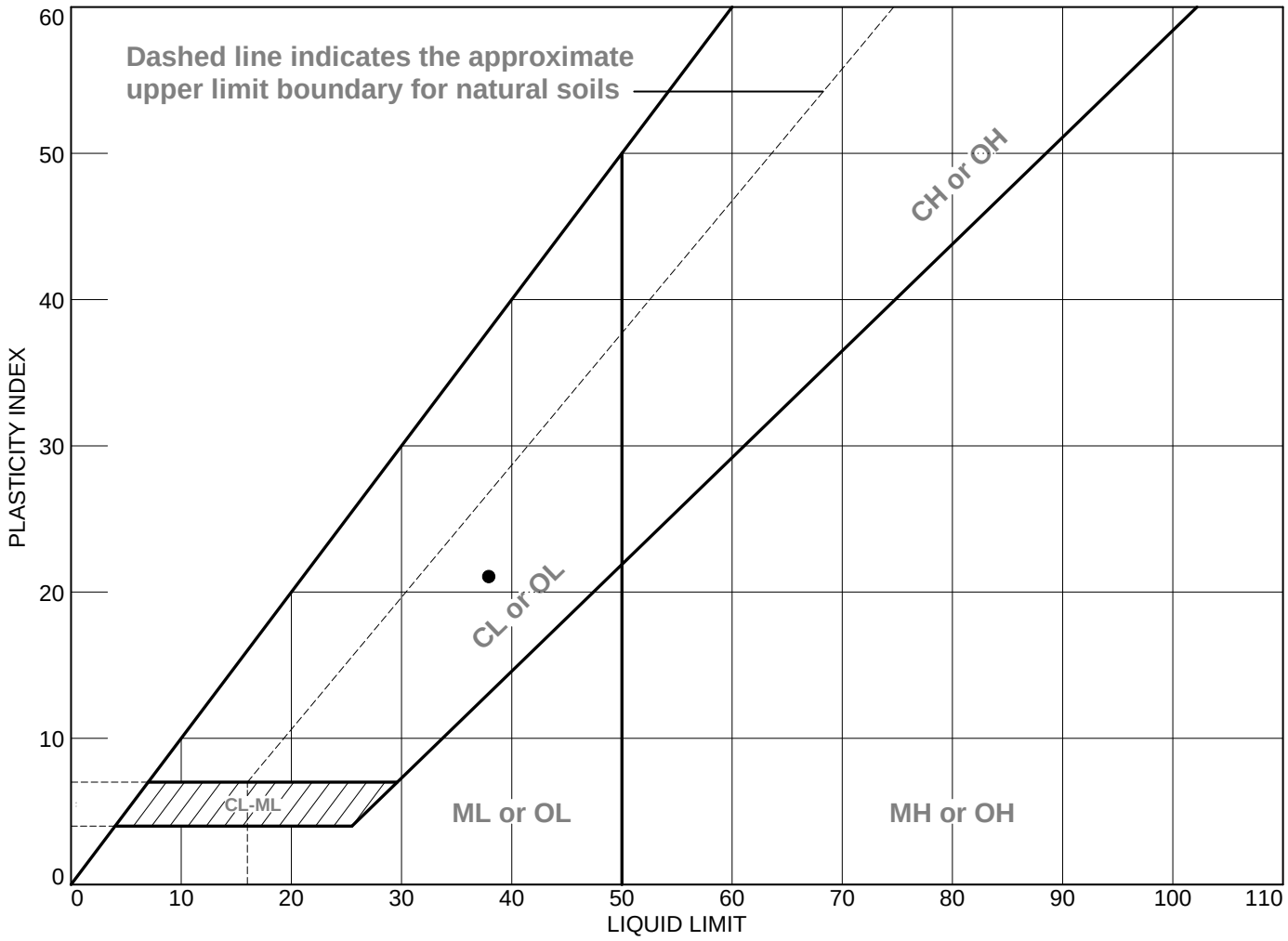
AECOM

**Client:** KESTREL HORIZONS LLC
**Project:** PINEWOOD SITE IMPROVEMENT

**Project No.:** 60186203 **Figure**

**Tested By:** BOB PEETERS

# LIQUID AND PLASTIC LIMITS TEST REPORT




| SOIL DATA | | | | | | | | |
|---|---|---|---|---|---|---|---|---|
| SYMBOL | SOURCE | SAMPLE NO. | DEPTH | NATURAL WATER CONTENT (%) | PLASTIC LIMIT (%) | LIQUID LIMIT (%) | PLASTICITY INDEX (%) | USCS |
| ● | ON SITE | SB-1C-5A | | | 17 | 38 | 21 | SC |

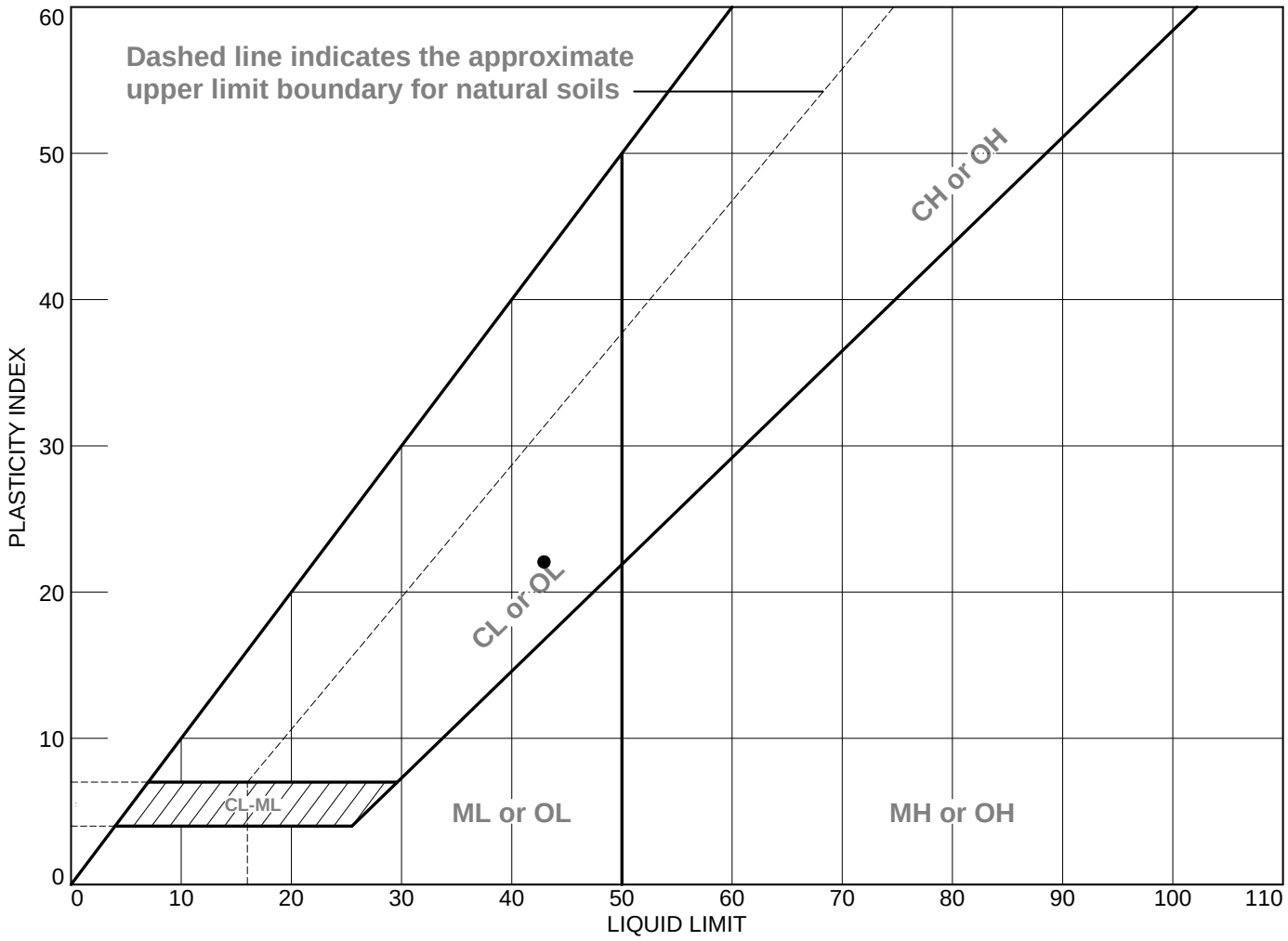
AECOM

**Client:** KESTREL HORIZONS LLC
**Project:** PINEWOOD SITE IMPROVEMENT

**Project No.:** 60186203 **Figure**

**Tested By:** BOB PEETERS

# LIQUID AND PLASTIC LIMITS TEST REPORT




**SOIL DATA**

| SYMBOL | SOURCE | SAMPLE NO. | DEPTH | NATURAL WATER CONTENT (%) | PLASTIC LIMIT (%) | LIQUID LIMIT (%) | PLASTICITY INDEX (%) | USCS |
|---|---|---|---|---|---|---|---|---|
| ● | ON SITE | SB-1D-6 | | 16.9 | 21 | 43 | 22 | SC |

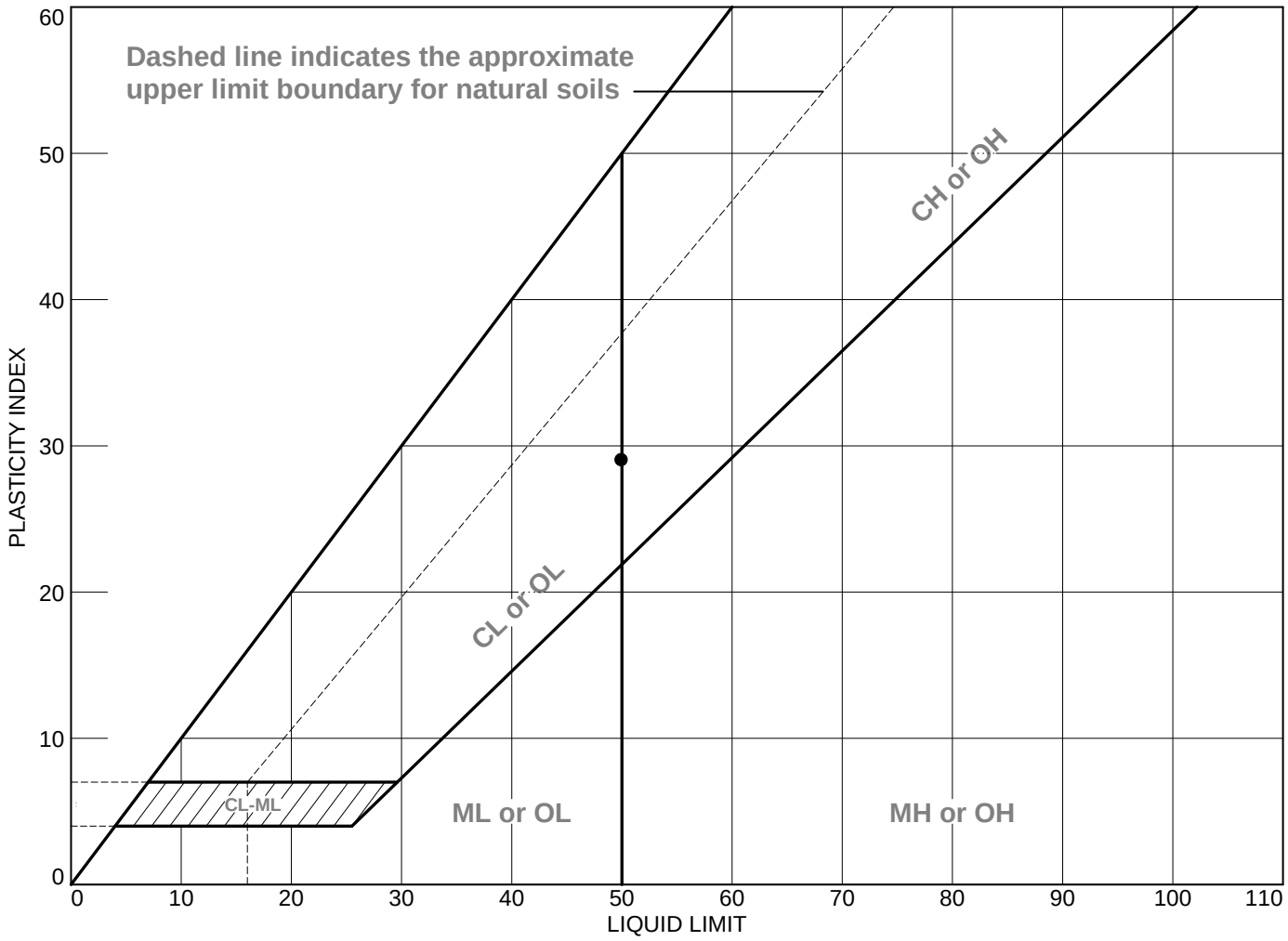
AECOM

**Client:** KESTREL HORIZONS LLC
**Project:** PINEWOOD SITE IMPROVEMENT

**Project No.:** 60186203 **Figure**

**Tested By:** BOB PEETERS

# LIQUID AND PLASTIC LIMITS TEST REPORT




| SOIL DATA | | | | | | | | |
|---|---|---|---|---|---|---|---|---|
| SYMBOL | SOURCE | SAMPLE NO. | DEPTH | NATURAL WATER CONTENT (%) | PLASTIC LIMIT (%) | LIQUID LIMIT (%) | PLASTICITY INDEX (%) | USCS |
| ● | ON SITE | SB-1D-7 | | 26.1 | 21 | 50 | 29 | CH |

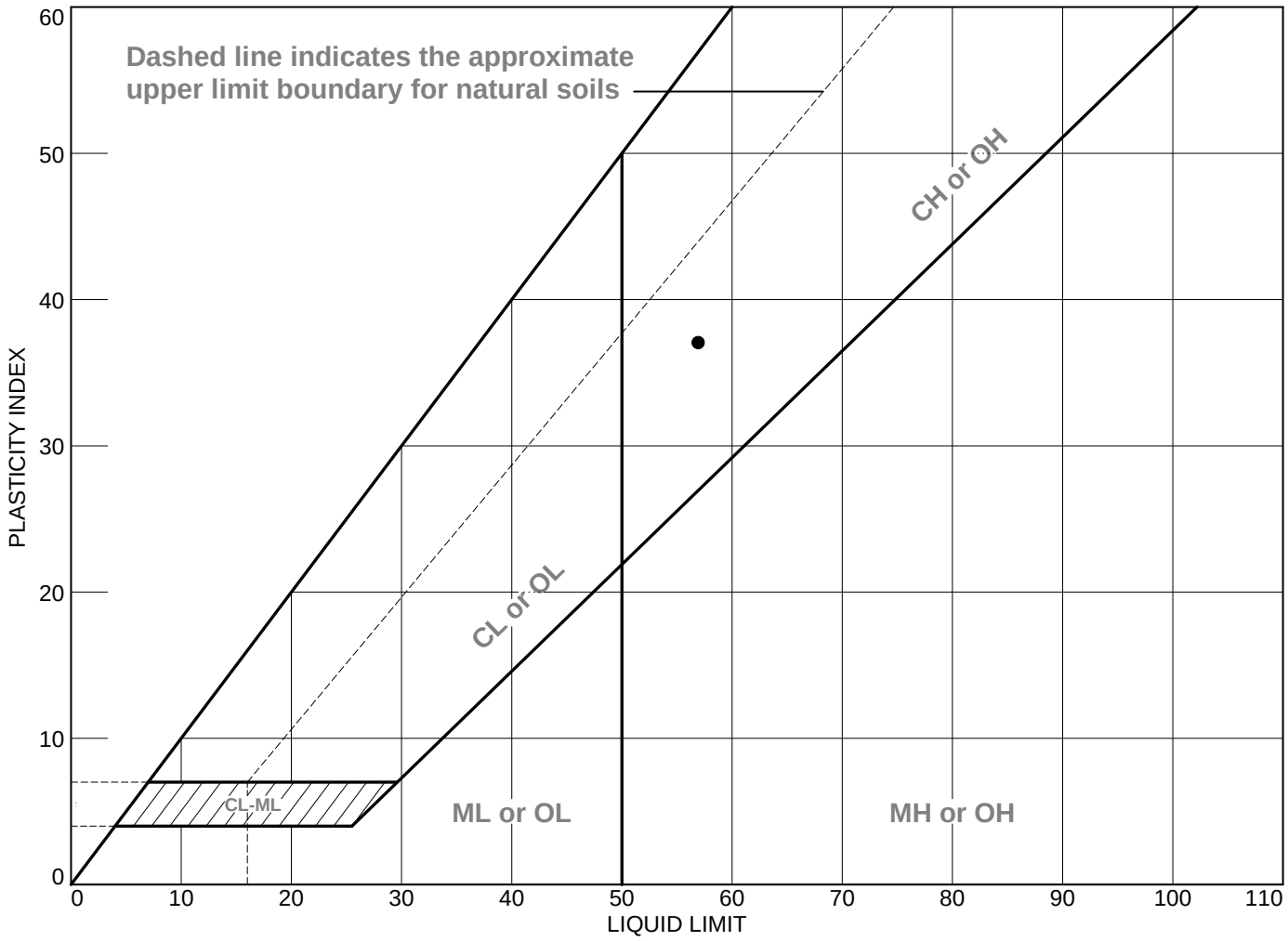
AECOM

**Client:** KESTREL HORIZONS LLC
**Project:** PINEWOOD SITE IMPROVEMENT

**Project No.:** 60186203 **Figure**

**Tested By:** BOB PEETERS

# LIQUID AND PLASTIC LIMITS TEST REPORT




| SOIL DATA | | | | | | | | |
|---|---|---|---|---|---|---|---|---|
| SYMBOL | SOURCE | SAMPLE NO. | DEPTH | NATURAL WATER CONTENT (%) | PLASTIC LIMIT (%) | LIQUID LIMIT (%) | PLASTICITY INDEX (%) | USCS |
| ● | ON SITE | SB-1E-8 | | 22.8 | 20 | 57 | 37 | CH |

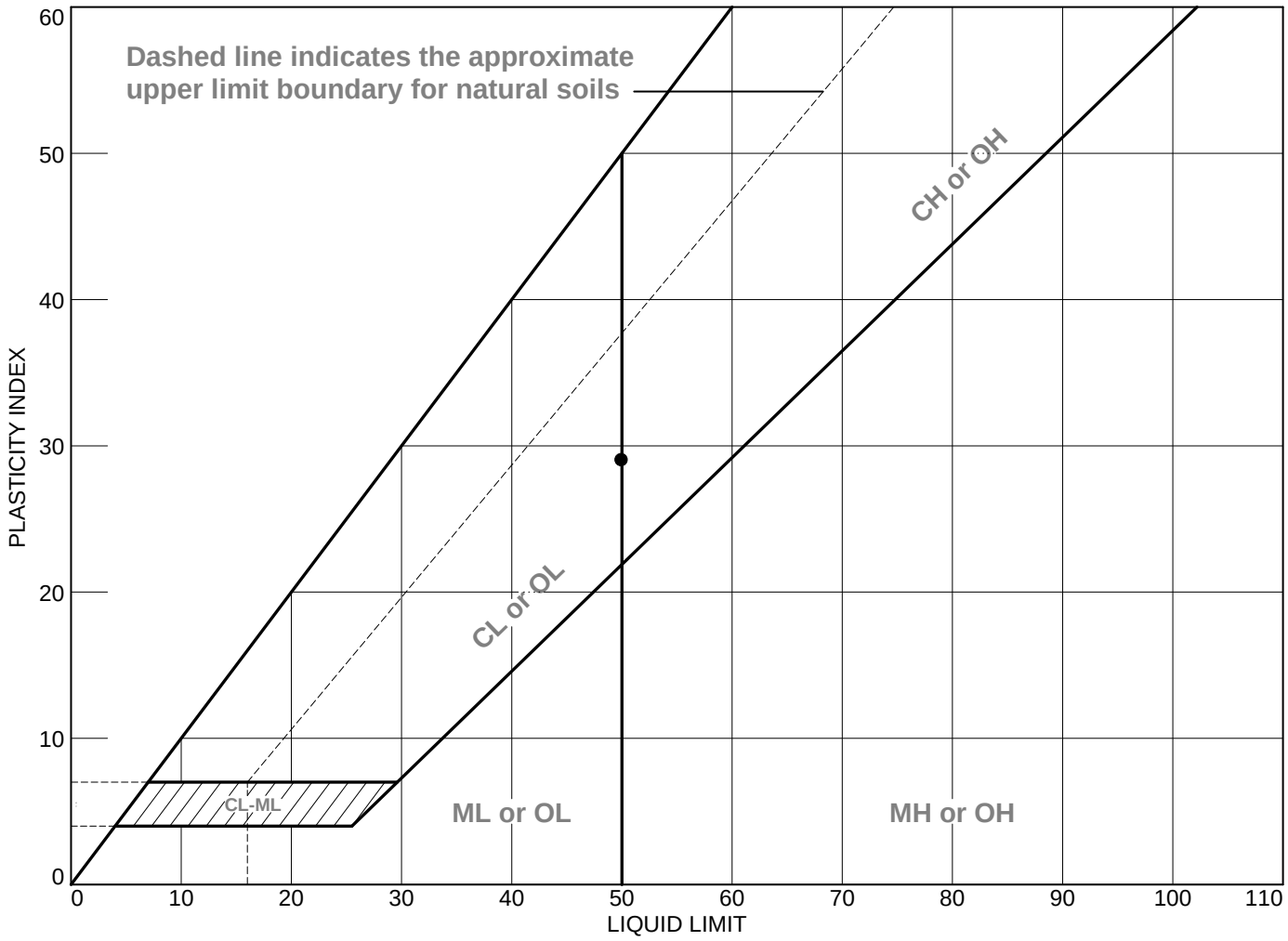
AECOM

**Client:** KESTREL HORIZONS LLC
**Project:** PINEWOOD SITE IMPROVEMENT

**Project No.:** 60186203 **Figure**

**Tested By:** BOB PEETERS

# LIQUID AND PLASTIC LIMITS TEST REPORT




| SOIL DATA | | | | | | | | |
|---|---|---|---|---|---|---|---|---|
| SYMBOL | SOURCE | SAMPLE NO. | DEPTH | NATURAL WATER CONTENT (%) | PLASTIC LIMIT (%) | LIQUID LIMIT (%) | PLASTICITY INDEX (%) | USCS |
| ● | ON SITE | SB-1E-9A | | 25.2 | 21 | 50 | 29 | |

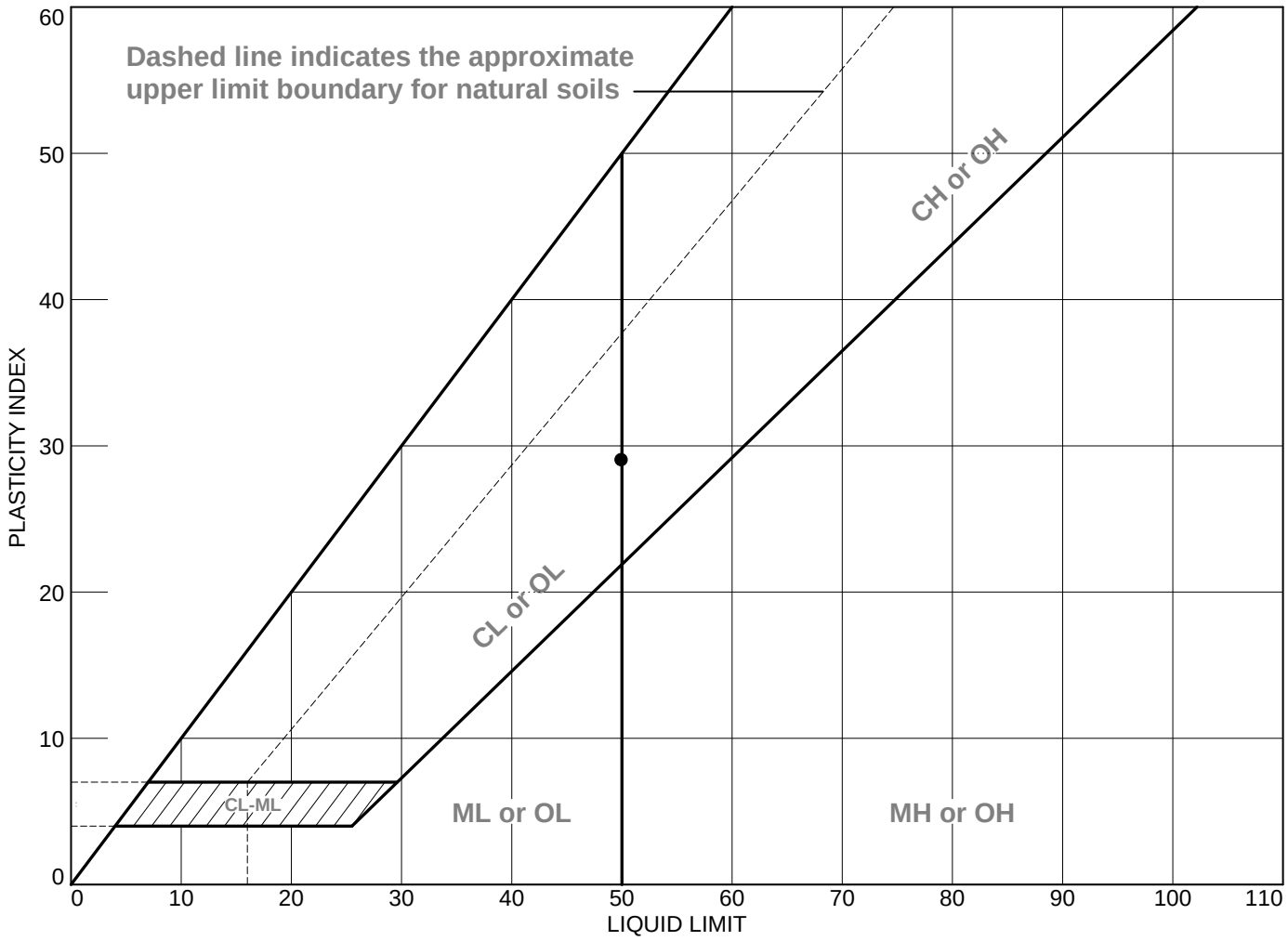
AECOM

**Client:** KESTREL HORIZONS LLC
**Project:** PINEWOOD SITE IMPROVEMENT

**Project No.:** 60186203 **Figure**

**Tested By:** BOB PEETERS

# LIQUID AND PLASTIC LIMITS TEST REPORT




| SOIL DATA | | | | | | | | |
|---|---|---|---|---|---|---|---|---|
| SYMBOL | SOURCE | SAMPLE NO. | DEPTH | NATURAL WATER CONTENT (%) | PLASTIC LIMIT (%) | LIQUID LIMIT (%) | PLASTICITY INDEX (%) | USCS |
| ● | ON SITE | SB-1E-10A | | 22.1 | 21 | 50 | 29 | CH |

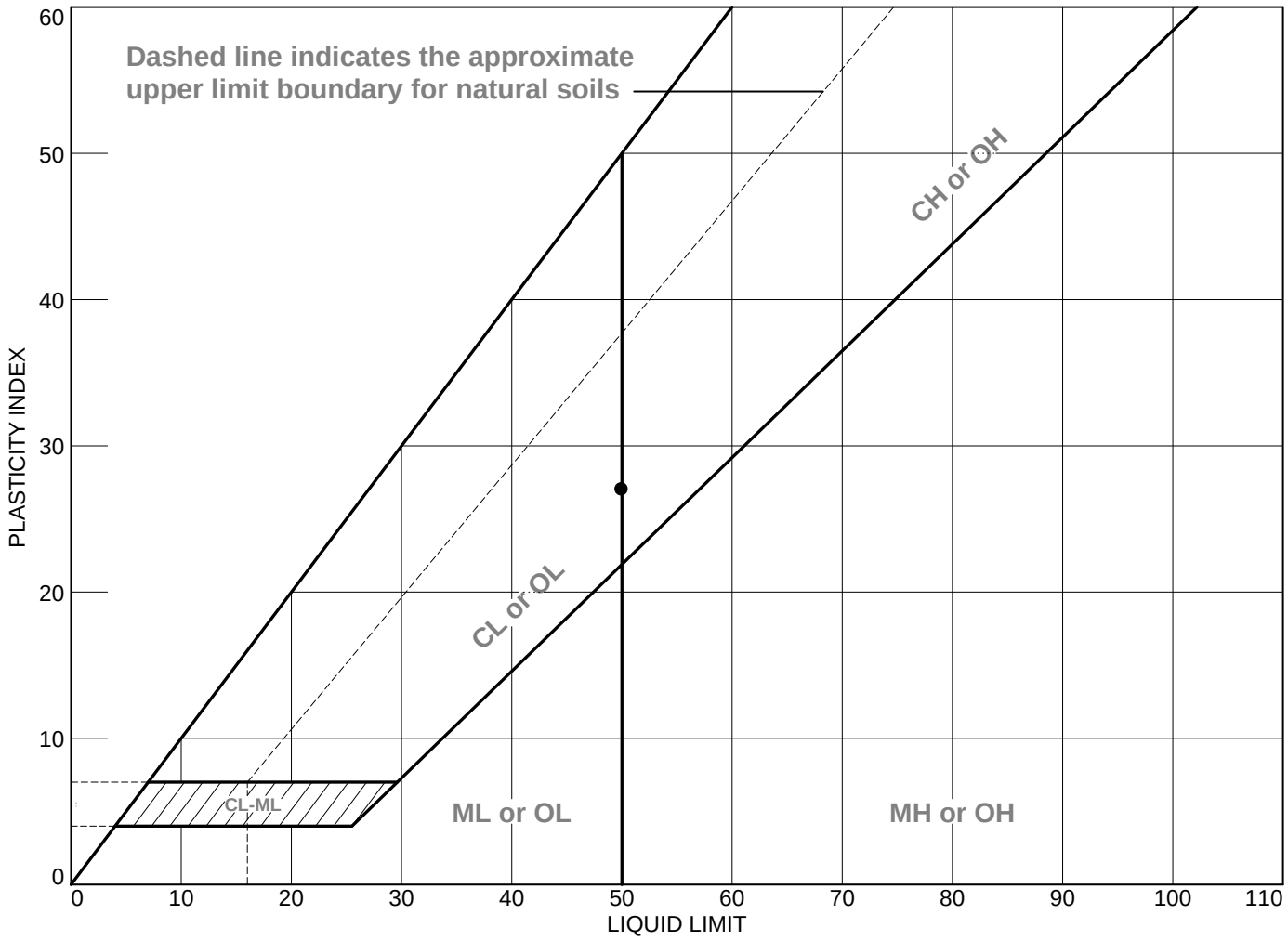
AECOM

**Client:** KESTREL HORIZONS LLC
**Project:** PINEWOOD SITE IMPROVEMENT

**Project No.:** 60186203 **Figure**

**Tested By:** BOB PEETERS

# LIQUID AND PLASTIC LIMITS TEST REPORT




| SOIL DATA | | | | | | | | |
|---|---|---|---|---|---|---|---|---|
| SYMBOL | SOURCE | SAMPLE NO. | DEPTH | NATURAL WATER CONTENT (%) | PLASTIC LIMIT (%) | LIQUID LIMIT (%) | PLASTICITY INDEX (%) | USCS |
| ● | ON SITE | TP-1A-01 | | 29.2 | 23 | 50 | 27 | CH |

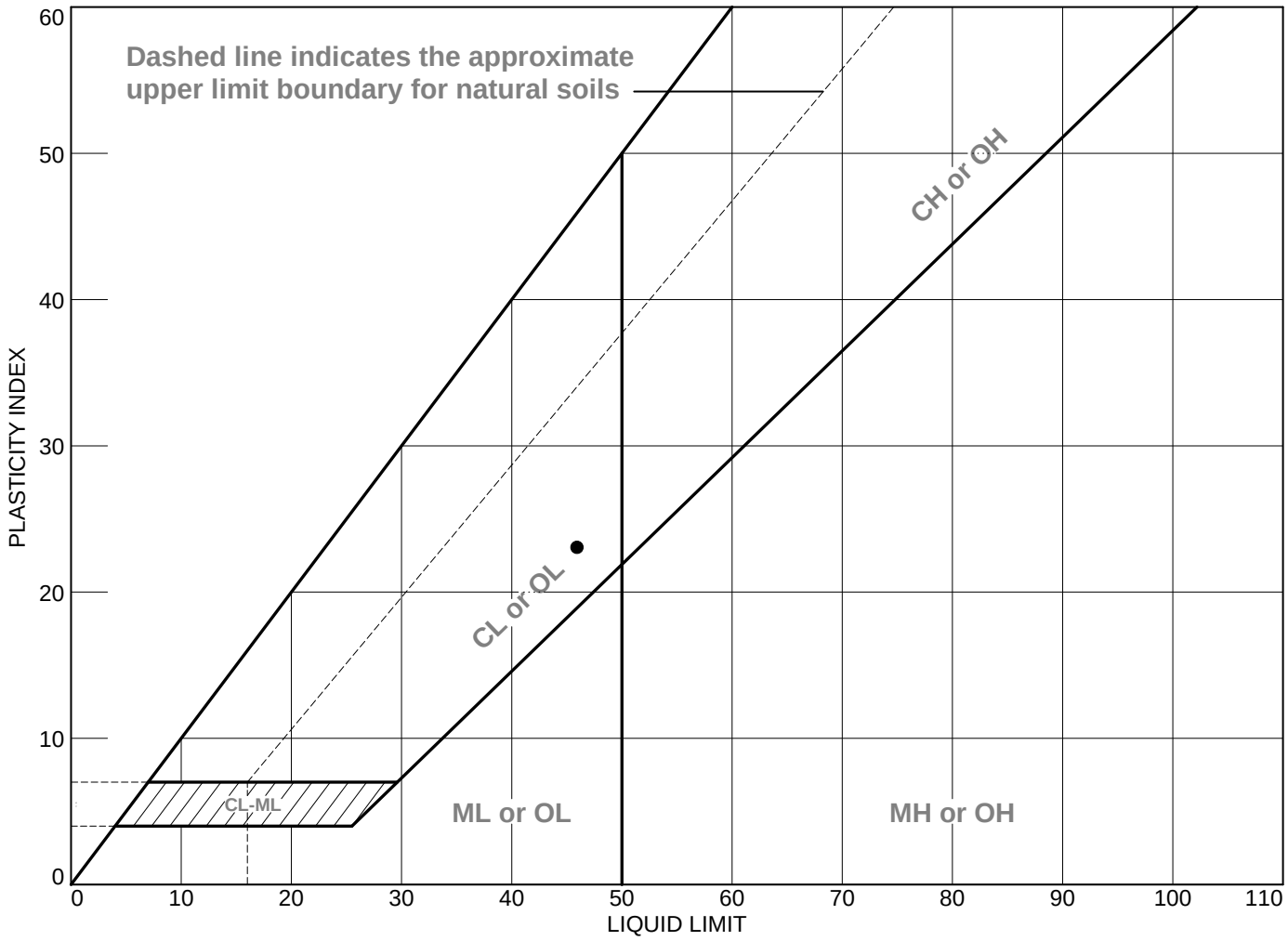
AECOM

**Client:** KESTREL HORIZONS LLC
**Project:** PINEWOOD SITE IMPROVEMENT

**Project No.:** 60186203 **Figure**

**Tested By:** BOB PEETERS

# LIQUID AND PLASTIC LIMITS TEST REPORT




**SOIL DATA**

| SYMBOL | SOURCE | SAMPLE NO. | DEPTH | NATURAL WATER CONTENT (%) | PLASTIC LIMIT (%) | LIQUID LIMIT (%) | PLASTICITY INDEX (%) | USCS |
|---|---|---|---|---|---|---|---|---|
| ● | ON SITE | TP-1D-01 | | 21.5 | 23 | 46 | 23 | CL |

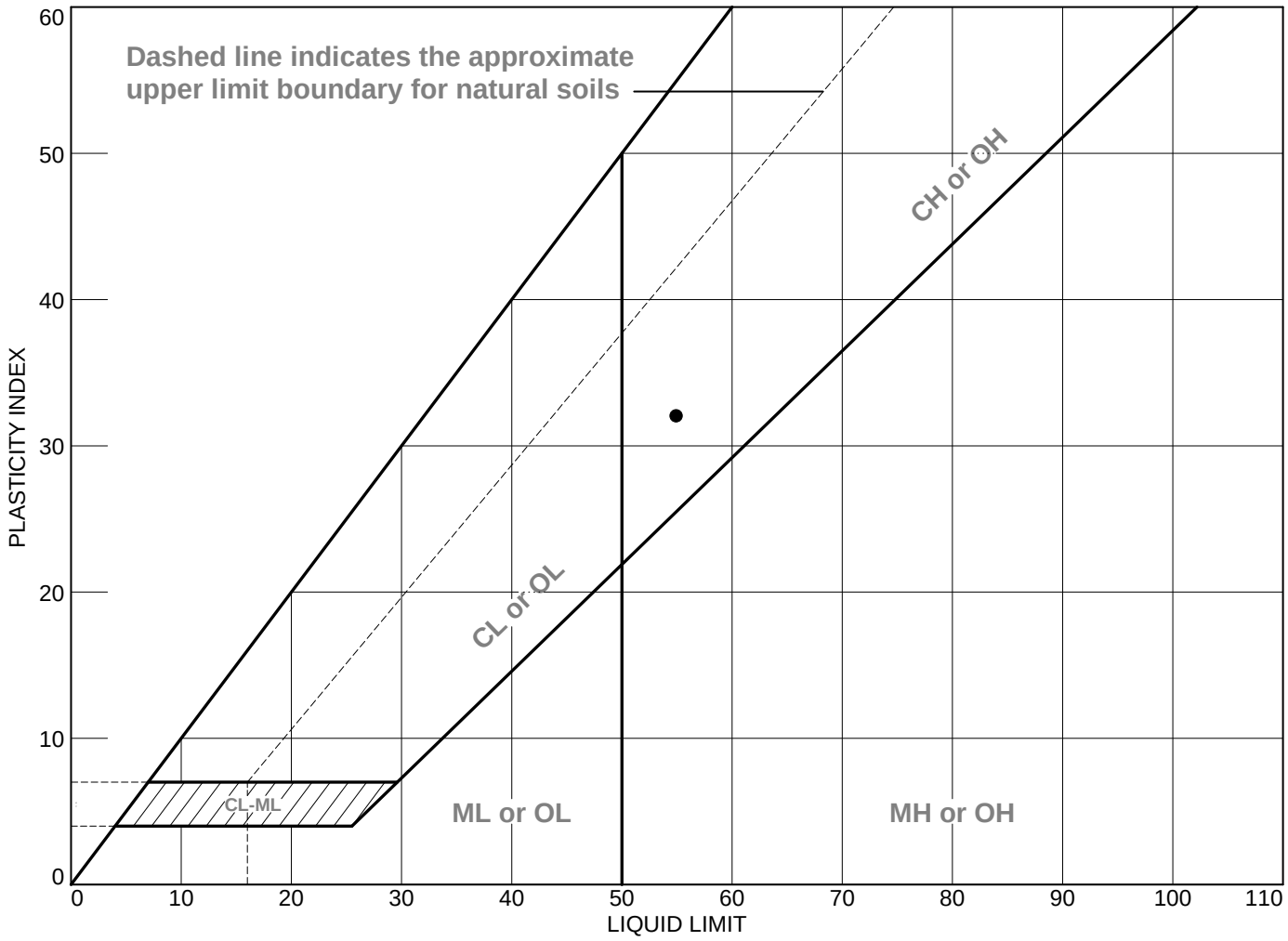
AECOM

**Client:** KESTREL HORIZONS LLC
**Project:** PINEWOOD SITE IMPROVEMENT

**Project No.:** 60186203 **Figure**

**Tested By:** BOB PEETERS

# LIQUID AND PLASTIC LIMITS TEST REPORT




| SOIL DATA | | | | | | | | |
|---|---|---|---|---|---|---|---|---|
| SYMBOL | SOURCE | SAMPLE NO. | DEPTH | NATURAL WATER CONTENT (%) | PLASTIC LIMIT (%) | LIQUID LIMIT (%) | PLASTICITY INDEX (%) | USCS |
| ● | ON SITE | TP-1D-02 | | 22.8 | 23 | 55 | 32 | CH |

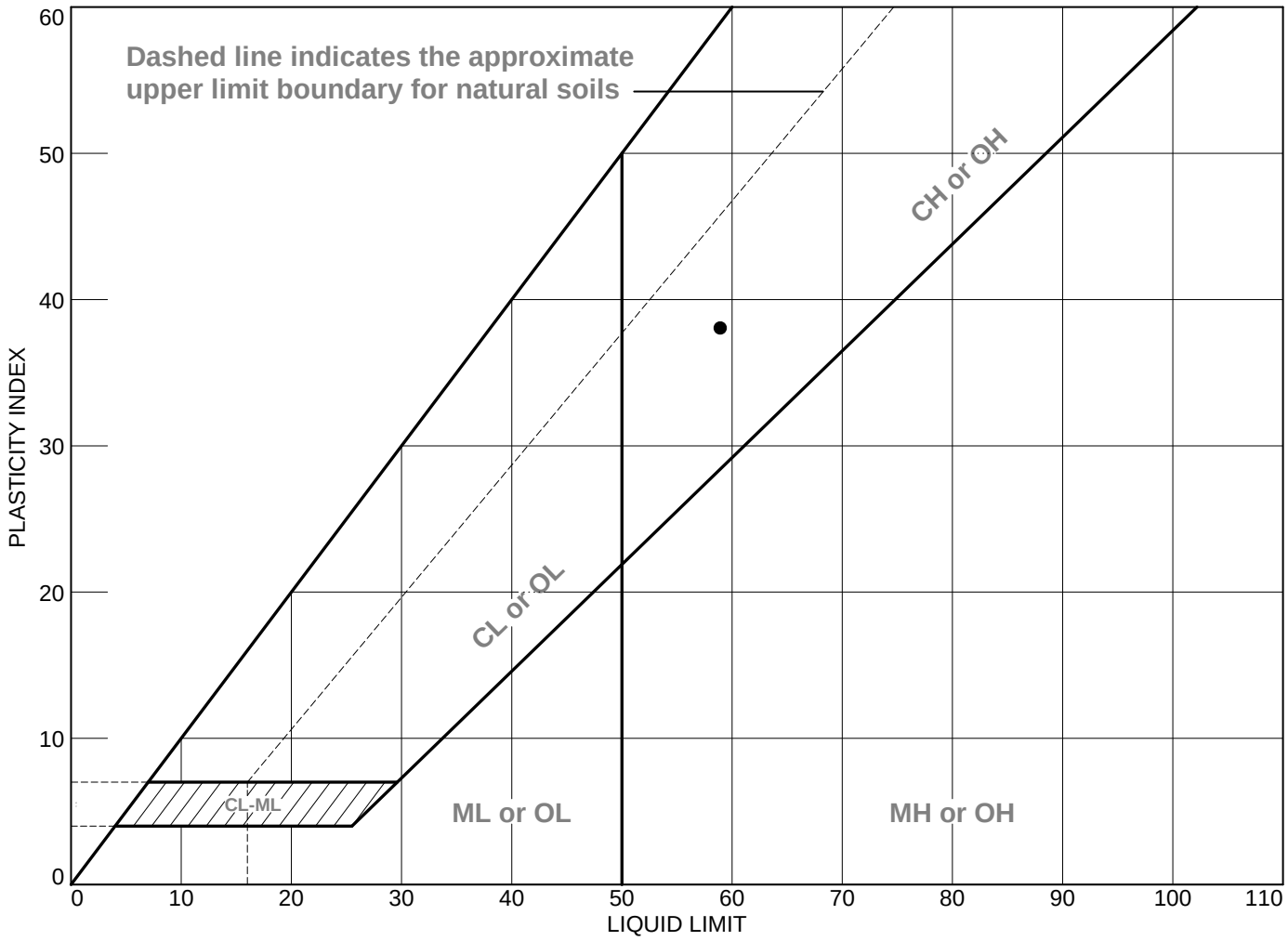
AECOM

**Client:** KESTREL HORIZONS LLC
**Project:** PINEWOOD SITE IMPROVEMENT

**Project No.:** 60186203 **Figure**

**Tested By:** BOB PEETERS

# LIQUID AND PLASTIC LIMITS TEST REPORT




| SOIL DATA | | | | | | | | |
|---|---|---|---|---|---|---|---|---|
| SYMBOL | SOURCE | SAMPLE NO. | DEPTH | NATURAL WATER CONTENT (%) | PLASTIC LIMIT (%) | LIQUID LIMIT (%) | PLASTICITY INDEX (%) | USCS |
| ● | ON SITE | TP-1E-01A | | 27.6 | 21 | 59 | 38 | CH |

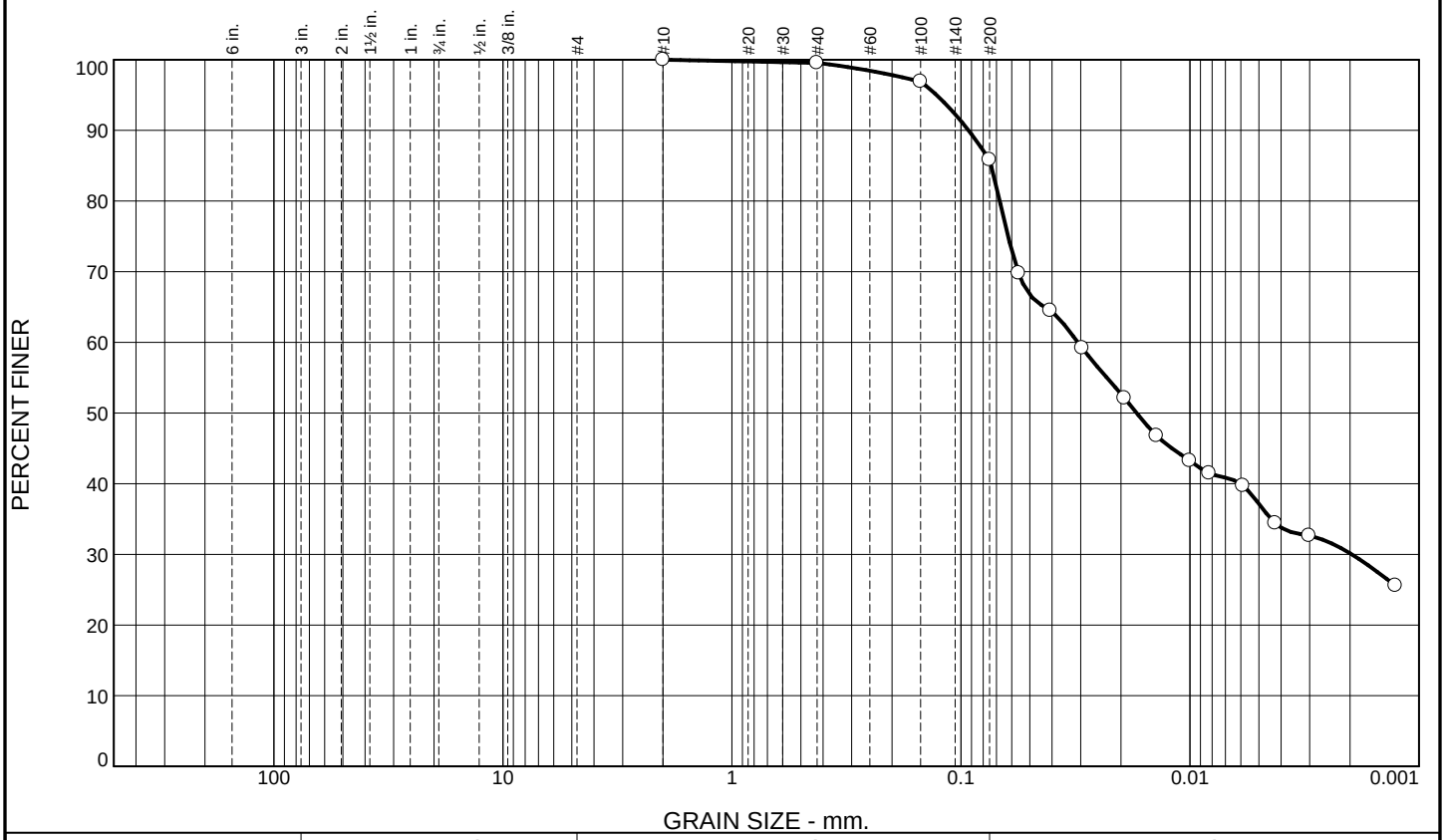
AECOM

**Client:** KESTREL HORIZONS LLC
**Project:** PINEWOOD SITE IMPROVEMENT

**Project No.:** 60186203 **Figure**

**Tested By:** BOB PEETERS

# Particle Size Distribution Report




| % +3" | % Gravel | | % Sand | | | % Fines | |
|---|---|---|---|---|---|---|---|
| | Coarse | Fine | Coarse | Medium | Fine | Silt | Clay |
| 0.0 | 0.0 | 0.0 | 0.0 | 0.4 | 13.8 | 48.7 | 37.1 |

| SIEVE SIZE | PERCENT FINER | SPEC.* PERCENT | PASS? (X=NO) |
|---|---|---|---|
| #10 | 100.0 | | |
| #40 | 99.6 | | |
| #100 | 96.9 | | |
| #200 | 85.8 | | |

* (no specification provided)

**Material Description**

LIGHT BROWN SILTY CLAY, LITTLE SAND

**Atterberg Limits**

PL= 23 LL= 47 PI= 24

**Coefficients**

$D_{90}$= 0.0927 $D_{85}$= 0.0738 $D_{60}$= 0.0309
$D_{50}$= 0.0171 $D_{30}$= 0.0020 $D_{15}$=
$D_{10}$= $C_u$= $C_c$=

**Classification**

USCS= CL AASHTO= A-7-6(22)

**Remarks**

**Source of Sample:** ON SITE
**Sample Number:** SB-1A-1A

**Date:** 01/11/11

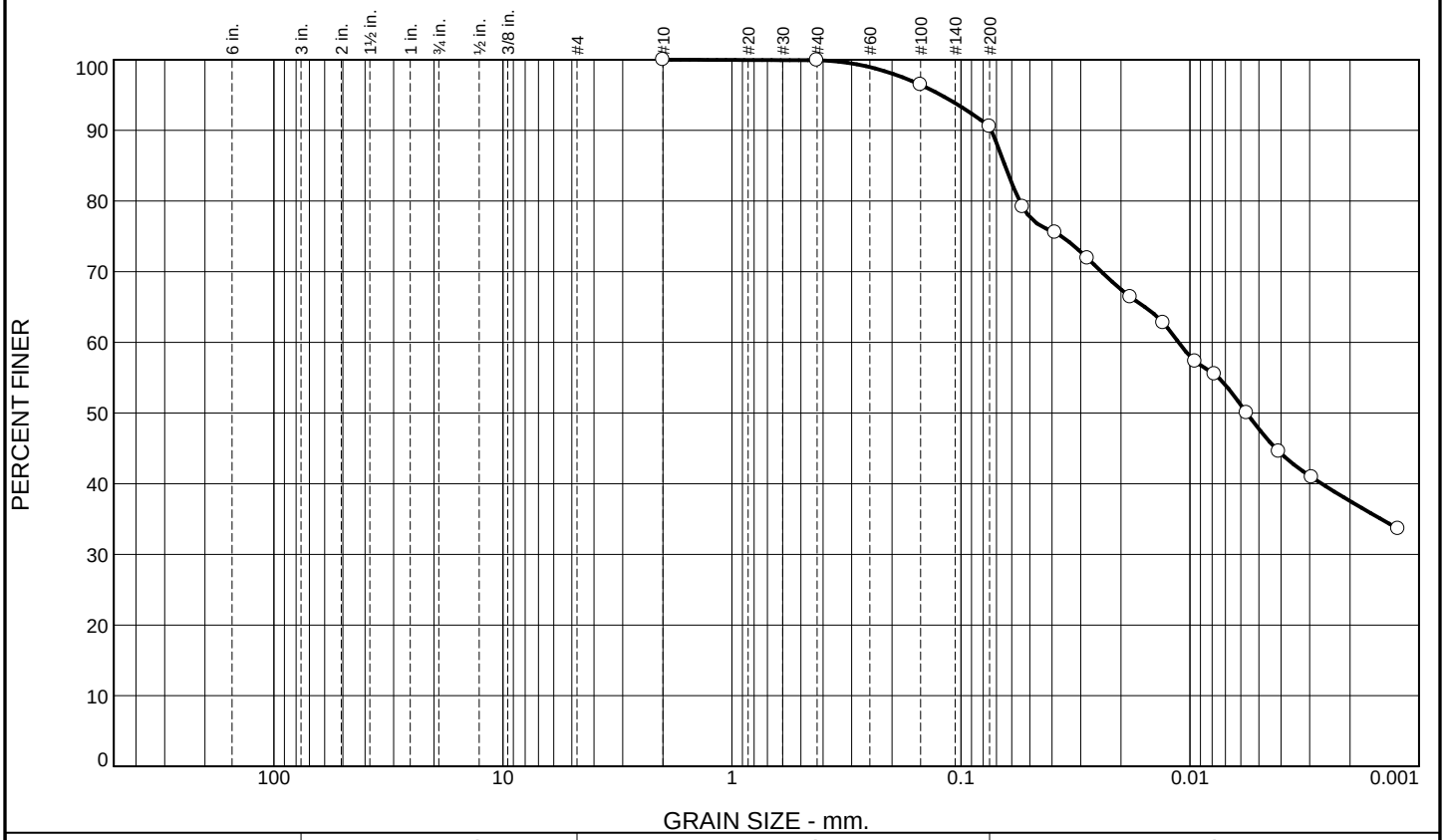
AECOM

**Client:** KESTREL HORIZONS LLC
**Project:** PINEWOOD SITE IMPROVEMENT

**Project No:** 60186203 **Figure**

**Tested By:** BOB PEETERS

# Particle Size Distribution Report




| % +3" | % Gravel | | % Sand | | | % Fines | |
|---|---|---|---|---|---|---|---|
| | Coarse | Fine | Coarse | Medium | Fine | Silt | Clay |
| 0.0 | 0.0 | 0.0 | 0.0 | 0.1 | 9.3 | 42.9 | 47.7 |

| SIEVE SIZE | PERCENT FINER | SPEC.* PERCENT | PASS? (X=NO) |
|---|---|---|---|
| #10 | 100.0 | | |
| #40 | 99.9 | | |
| #100 | 96.4 | | |
| #200 | 90.6 | | |

* (no specification provided)

**Material Description**

LIGHT BROWN SILTY CLAY, TRACE SAND

**Atterberg Limits**

PL= 25 LL= 58 PI= 33

**Coefficients**

$D_{90}$= 0.0737 $D_{85}$= 0.0642 $D_{60}$= 0.0112
$D_{50}$= 0.0057 $D_{30}$= $D_{15}$=
$D_{10}$= $C_u$= $C_c$=

**Classification**

USCS= CH AASHTO= A-7-6(34)

**Remarks**

**Source of Sample:** ON SITE
**Sample Number:** SB-1B-2A

**Date:** 01/11/11

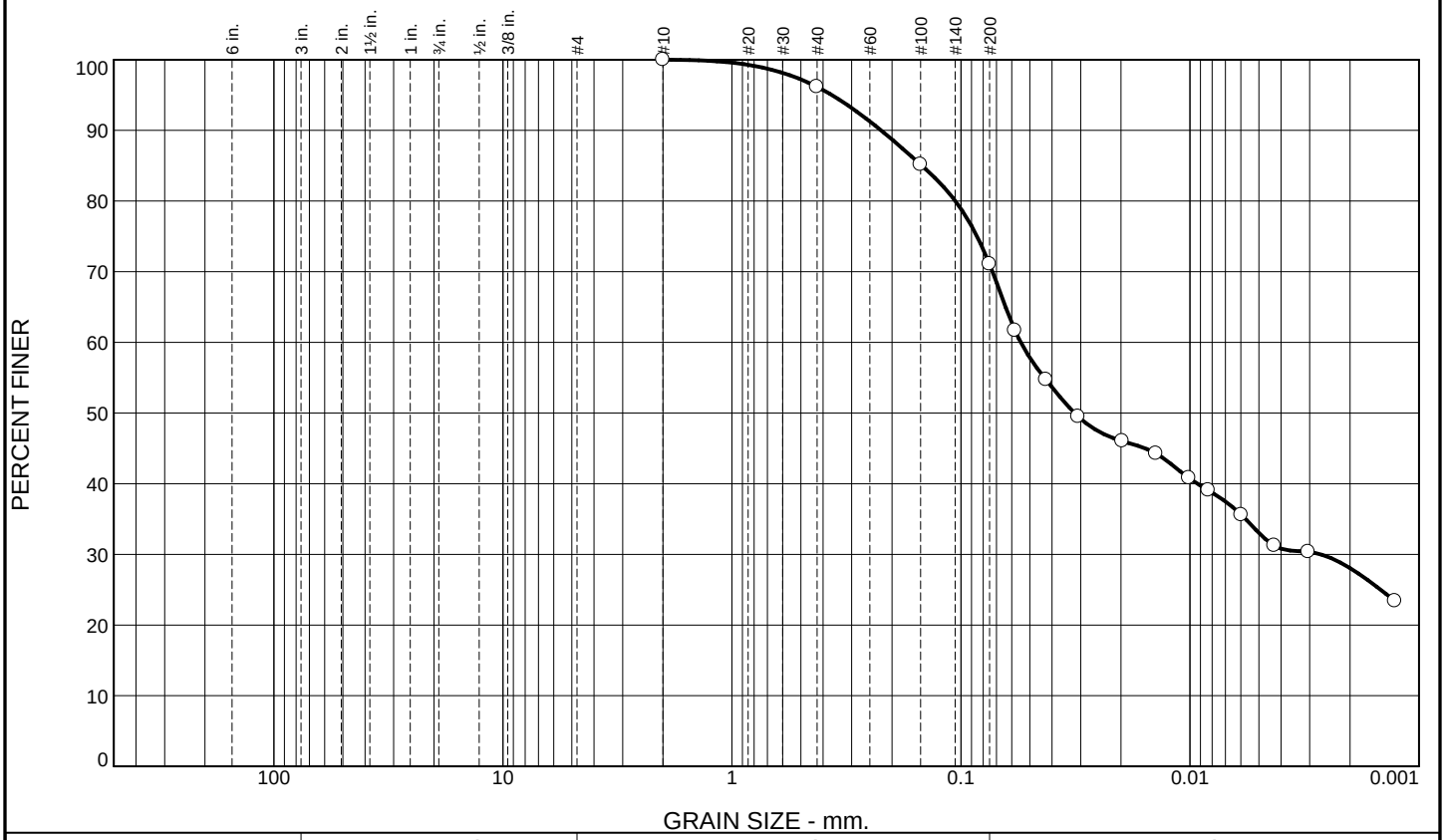
AECOM

**Client:** KESTREL HORIZONS LLC
**Project:** PINEWOOD SITE IMPROVEMENT

**Project No:** 60186203 **Figure**

**Tested By:** BOB PEETERS

# Particle Size Distribution Report




| % +3" | % Gravel | | % Sand | | | % Fines | |
|---|---|---|---|---|---|---|---|
| | Coarse | Fine | Coarse | Medium | Fine | Silt | Clay |
| 0.0 | 0.0 | 0.0 | 0.0 | 3.8 | 25.1 | 38.1 | 33.0 |

| SIEVE SIZE | PERCENT FINER | SPEC.* PERCENT | PASS? (X=NO) |
|---|---|---|---|
| #10 | 100.0 | | |
| #40 | 96.2 | | |
| #100 | 85.2 | | |
| #200 | 71.1 | | |

* (no specification provided)

**Material Description**

LIGHT REDDISH BROWN SILTY CLAY, SOME SAND

**Atterberg Limits**

PL= 23 LL= 44 PI= 21

**Coefficients**

$D_{90}$= 0.2233 $D_{85}$= 0.1482 $D_{60}$= 0.0548
$D_{50}$= 0.0319 $D_{30}$= 0.0027 $D_{15}$=
$D_{10}$= $C_u$= $C_c$=

**Classification**

USCS= CL AASHTO= A-7-6(14)

**Remarks**

**Source of Sample:** ON SITE
**Sample Number:** SB-1B-3

**Date:** 01/11/11

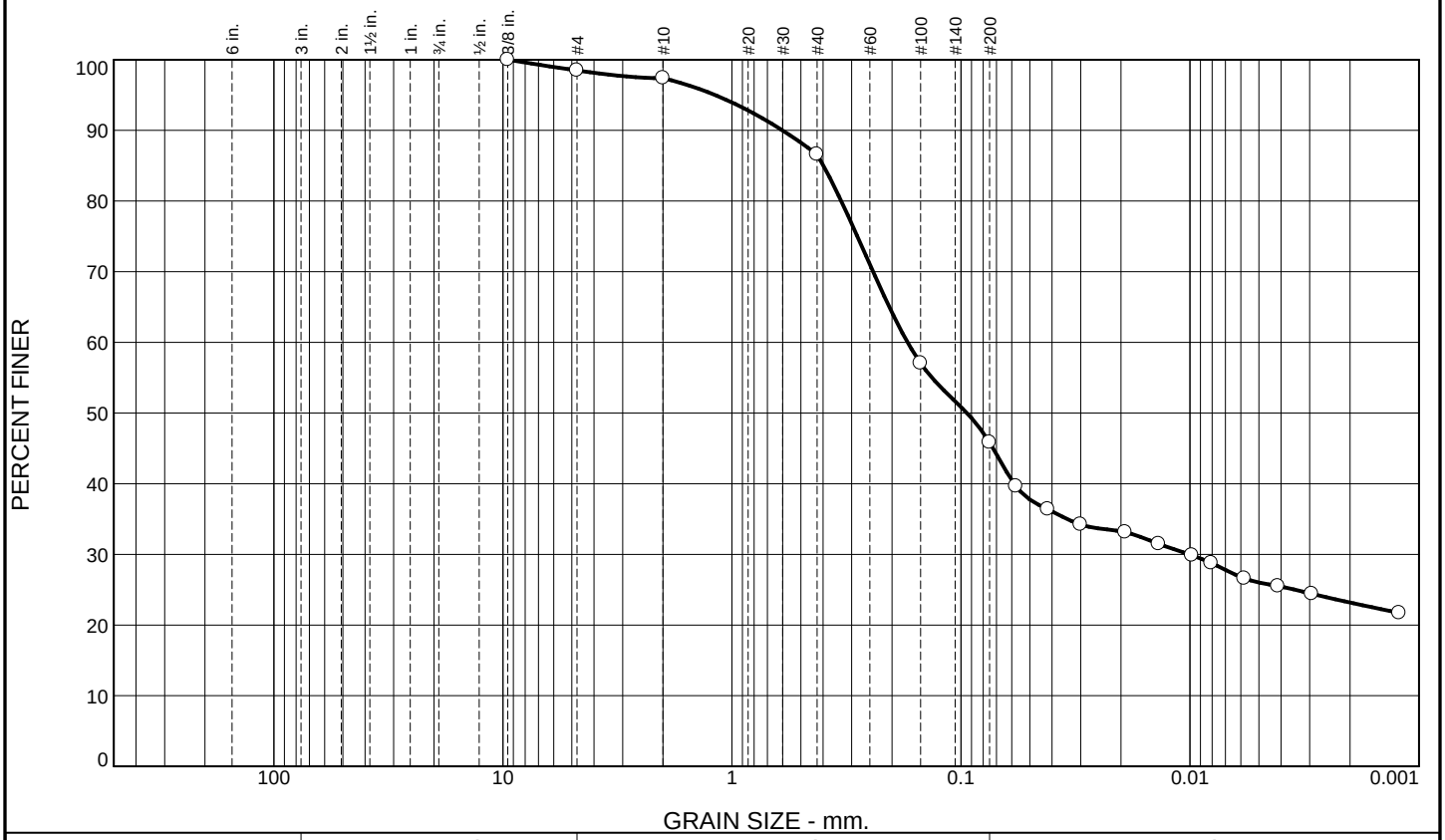
AECOM

**Client:** KESTREL HORIZONS LLC
**Project:** PINEWOOD SITE IMPROVEMENT

**Project No:** 60186203 **Figure**

**Tested By:** BOB PEETERS

# Particle Size Distribution Report




| % +3" | % Gravel | | % Sand | | | % Fines | |
|---|---|---|---|---|---|---|---|
| | Coarse | Fine | Coarse | Medium | Fine | Silt | Clay |
| 0.0 | 0.0 | 1.5 | 1.1 | 10.8 | 40.8 | 19.8 | 26.0 |

| SIEVE SIZE | PERCENT FINER | SPEC.* PERCENT | PASS? (X=NO) |
|---|---|---|---|
| .375 | 100.0 | | |
| #4 | 98.5 | | |
| #10 | 97.4 | | |
| #40 | 86.6 | | |
| #100 | 57.0 | | |
| #200 | 45.8 | | |

* (no specification provided)

**Material Description**

RED BROWN SANDY CLAY

**Atterberg Limits**

PL= 16 LL= 33 PI= 17

**Coefficients**

$D_{90}$= 0.6016 $D_{85}$= 0.3984 $D_{60}$= 0.1710
$D_{50}$= 0.0942 $D_{30}$= 0.0101 $D_{15}$=
$D_{10}$= $C_u$= $C_c$=

**Classification**

USCS= SC AASHTO= A-6(4)

**Remarks**

**Source of Sample:** ON SITE
**Sample Number:** SB-1C-4A

**Date:** 01/11/11

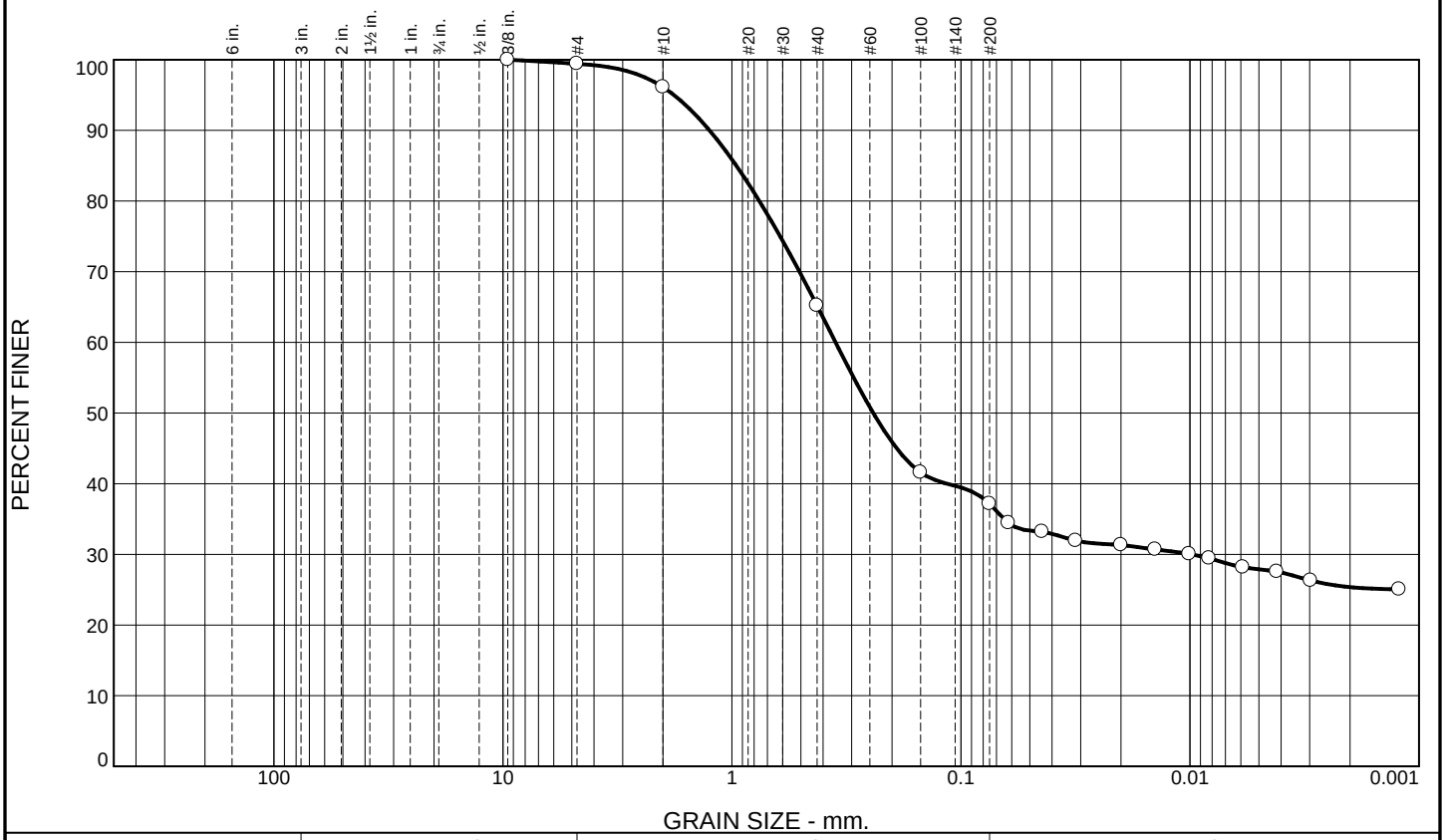
AECOM

**Client:** KESTREL HORIZONS LLC
**Project:** PINEWOOD SITE IMPROVEMENT

**Project No:** 60186203 **Figure**

**Tested By:** BOB PEETERS

# Particle Size Distribution Report




| % +3" | % Gravel | | % Sand | | | % Fines | |
|---|---|---|---|---|---|---|---|
| | Coarse | Fine | Coarse | Medium | Fine | Silt | Clay |
| 0.0 | 0.0 | 0.6 | 3.3 | 30.9 | 28.0 | 9.3 | 27.9 |

| SIEVE SIZE | PERCENT FINER | SPEC.* PERCENT | PASS? (X=NO) |
|---|---|---|---|
| .375 | 100.0 | | |
| #4 | 99.4 | | |
| #10 | 96.1 | | |
| #40 | 65.2 | | |
| #100 | 41.6 | | |
| #200 | 37.2 | | |

* (no specification provided)

**Material Description**

REDDISH BROWN SILTY CLAYEY SAND

**Atterberg Limits**

PL= 17 LL= 38 PI= 21

**Coefficients**

$D_{90}$= 1.2522 $D_{85}$= 0.9564 $D_{60}$= 0.3526
$D_{50}$= 0.2416 $D_{30}$= 0.0098 $D_{15}$=
$D_{10}$= $C_u$= $C_c$=

**Classification**

USCS= SC AASHTO= A-6(3)

**Remarks**

**Source of Sample:** ON SITE
**Sample Number:** SB-1C-5A

**Date:** 01/11/11

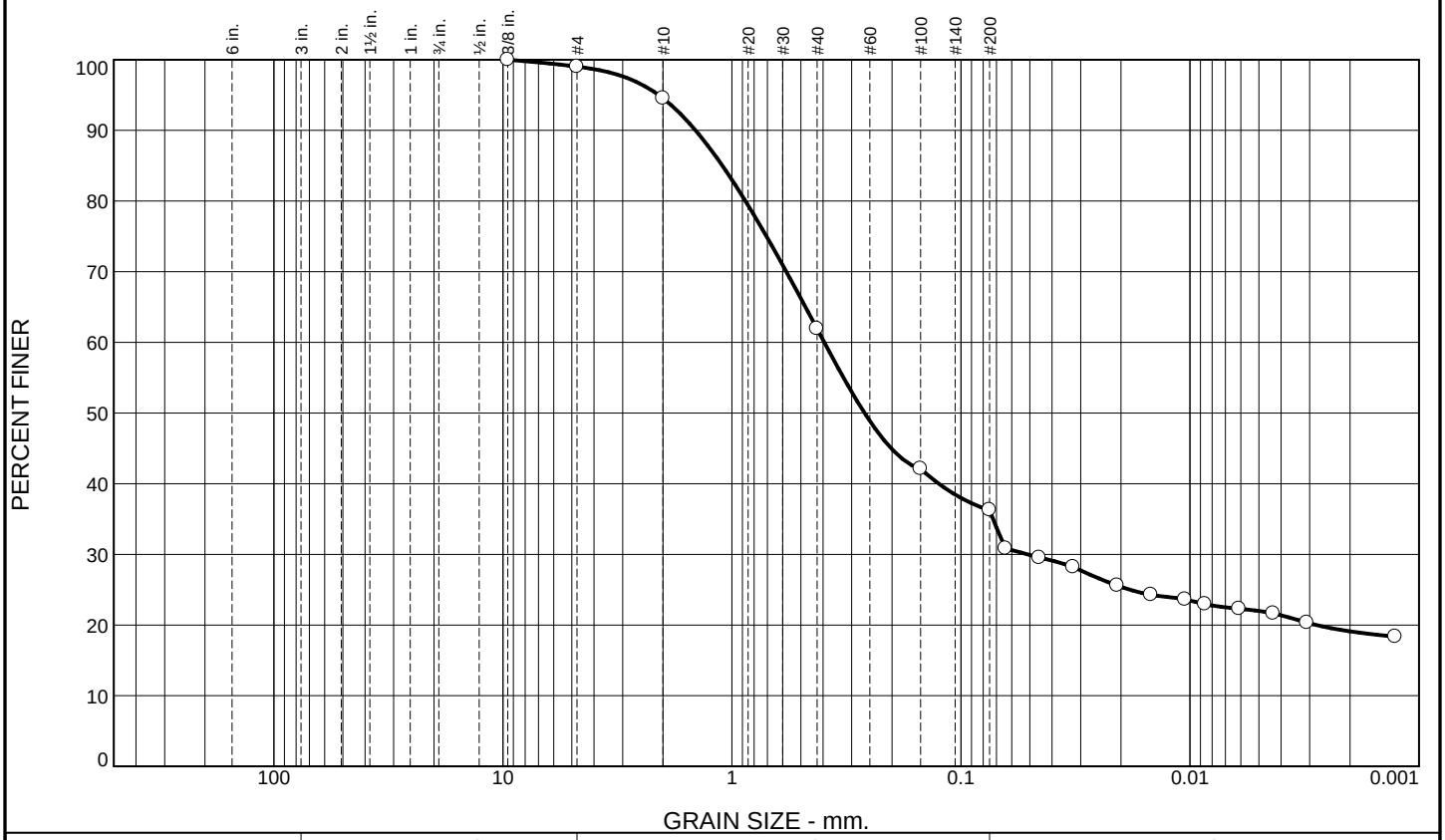
AECOM

**Client:** KESTREL HORIZONS LLC
**Project:** PINEWOOD SITE IMPROVEMENT

**Project No:** 60186203 **Figure**

**Tested By:** BOB PEETERS

# Particle Size Distribution Report




| % +3" | % Gravel | | % Sand | | | % Fines | |
|---|---|---|---|---|---|---|---|
| | Coarse | Fine | Coarse | Medium | Fine | Silt | Clay |
| 0.0 | 0.0 | 1.0 | 4.5 | 32.6 | 25.6 | 14.3 | 22.0 |

| SIEVE SIZE | PERCENT FINER | SPEC.* PERCENT | PASS? (X=NO) |
|---|---|---|---|
| .375 | 100.0 | | |
| #4 | 99.0 | | |
| #10 | 94.5 | | |
| #40 | 61.9 | | |
| #100 | 42.1 | | |
| #200 | 36.3 | | |

* (no specification provided)

**Material Description**

REDDISH BROWN CLAYEY SAND

**Atterberg Limits**

PL= 21 LL= 43 PI= 22

**Coefficients**

$D_{90}$= 1.4417 $D_{85}$= 1.1004 $D_{60}$= 0.3950
$D_{50}$= 0.2635 $D_{30}$= 0.0513 $D_{15}$=
$D_{10}$= $C_u$= $C_c$=

**Classification**

USCS= SC AASHTO= A-7-6(3)

**Remarks**

**Source of Sample:** ON SITE
**Sample Number:** SB-1D-6

**Date:** 01/11/11

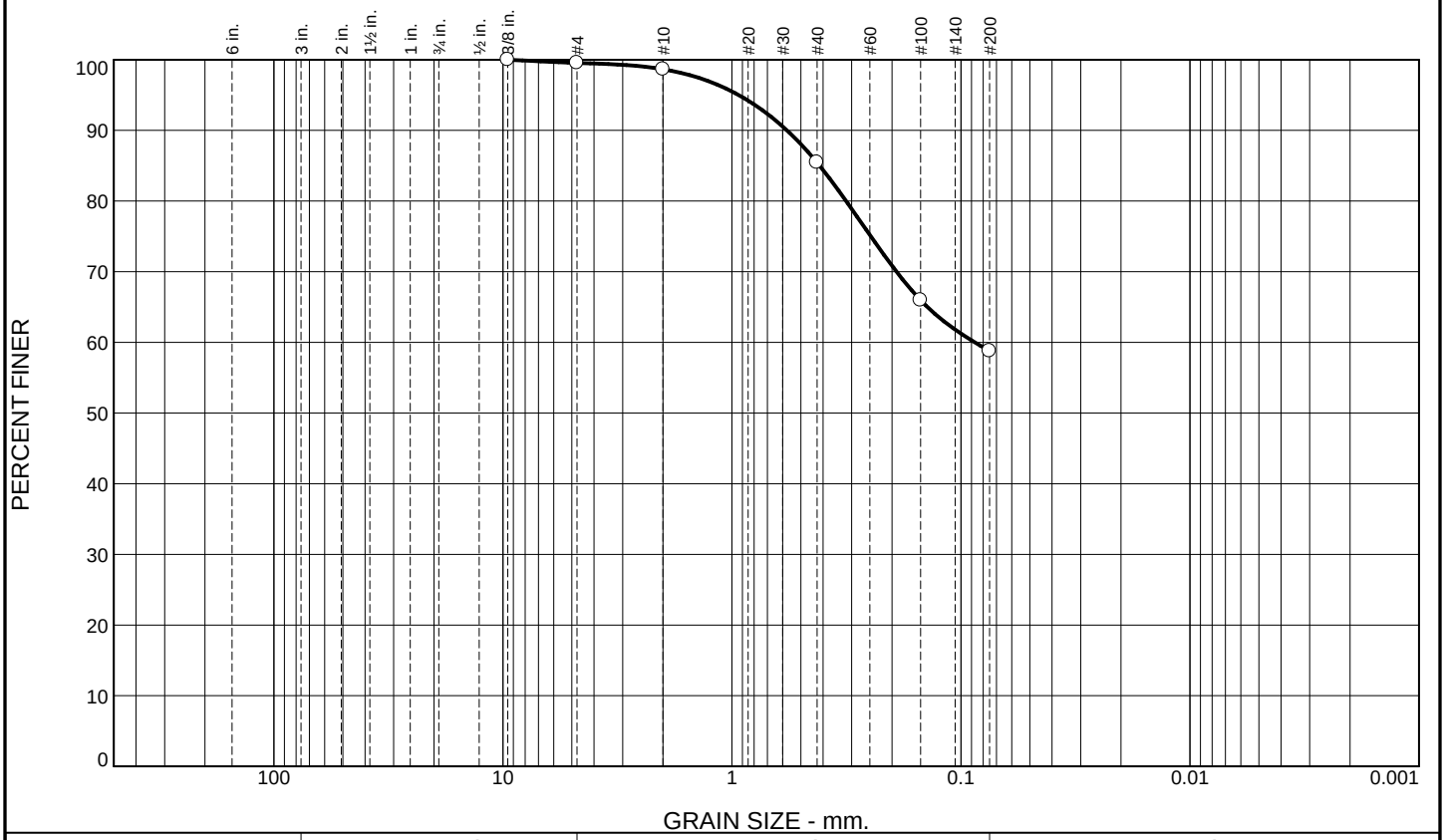
AECOM

**Client:** KESTREL HORIZONS LLC
**Project:** PINEWOOD SITE IMPROVEMENT

**Project No:** 60186203 **Figure**

**Tested By:** BOB PEETERS

# Particle Size Distribution Report




| % +3" | % Gravel | | % Sand | | | % Fines | |
|---|---|---|---|---|---|---|---|
| | Coarse | Fine | Coarse | Medium | Fine | Silt | Clay |
| 0.0 | 0.0 | 0.4 | 0.9 | 13.2 | 26.7 | 58.8 | |

| SIEVE SIZE | PERCENT FINER | SPEC.* PERCENT | PASS? (X=NO) |
|---|---|---|---|
| .375 | 100.0 | | |
| #4 | 99.6 | | |
| #10 | 98.7 | | |
| #40 | 85.5 | | |
| #100 | 66.0 | | |
| #200 | 58.8 | | |

* (no specification provided)

**Material Description**

REDDISH BROWN SILTY SANDY CLAY

**Atterberg Limits**

PL= LL= PI=

**Coefficients**

$D_{90}$= 0.5752 $D_{85}$= 0.4139 $D_{60}$= 0.0869
$D_{50}$= $D_{30}$= $D_{15}$=
$D_{10}$= $C_u$= $C_c$=

**Classification**

USCS= AASHTO=

**Remarks**

**Source of Sample:** ON SITE
**Sample Number:** SB-1D-06 (A)

**Date:** 01/13/11

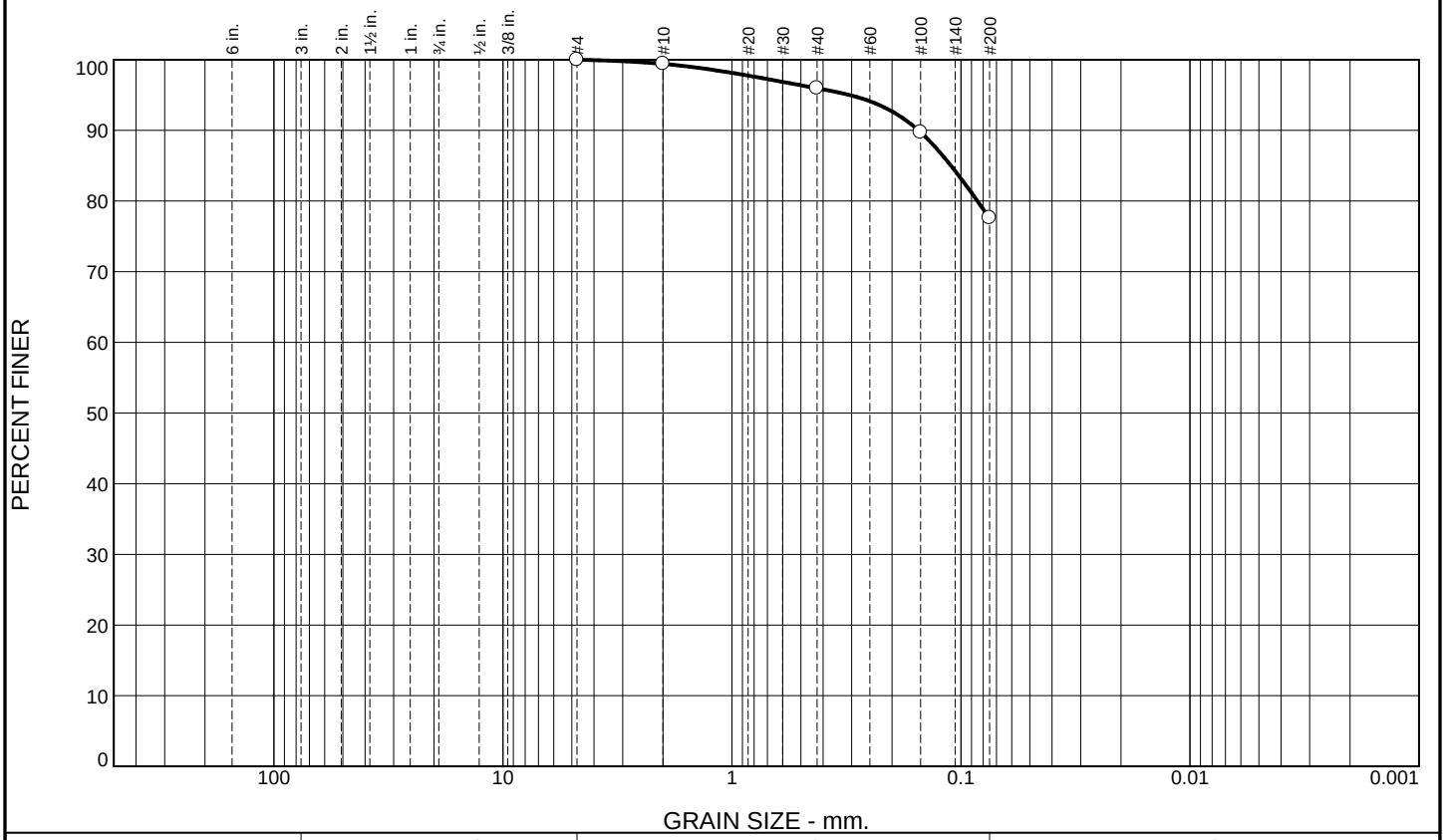
AECOM

**Client:** KESTREL HORIZONS LLC
**Project:** PINEWOOD SITE IMPROVEMENT

**Project No:** 60186203 **Figure**

**Tested By:** BOB PEETERS

# Particle Size Distribution Report




| % +3" | % Gravel | | % Sand | | | % Fines | |
|---|---|---|---|---|---|---|---|
| | Coarse | Fine | Coarse | Medium | Fine | Silt | Clay |
| 0.0 | 0.0 | 0.0 | 0.6 | 3.4 | 18.4 | 77.6 | |

| SIEVE SIZE | PERCENT FINER | SPEC.* PERCENT | PASS? (X=NO) |
|---|---|---|---|
| #4 | 100.0 | | |
| #10 | 99.4 | | |
| #40 | 96.0 | | |
| #100 | 89.7 | | |
| #200 | 77.6 | | |

* (no specification provided)

**Material Description**

LIGHT BROWN SILTY CLAY, SOME SAND

**Atterberg Limits**

PL= 21 LL= 50 PI= 29

**Coefficients**

$D_{90}$= 0.1531 $D_{85}$= 0.1105 $D_{60}$=
$D_{50}$= $D_{30}$= $D_{15}$=
$D_{10}$= $C_u$= $C_c$=

**Classification**

USCS= CH AASHTO= A-7-6(23)

**Remarks**

**Source of Sample:** ON SITE
**Sample Number:** SB-1D-7

**Date:** 01/11/11

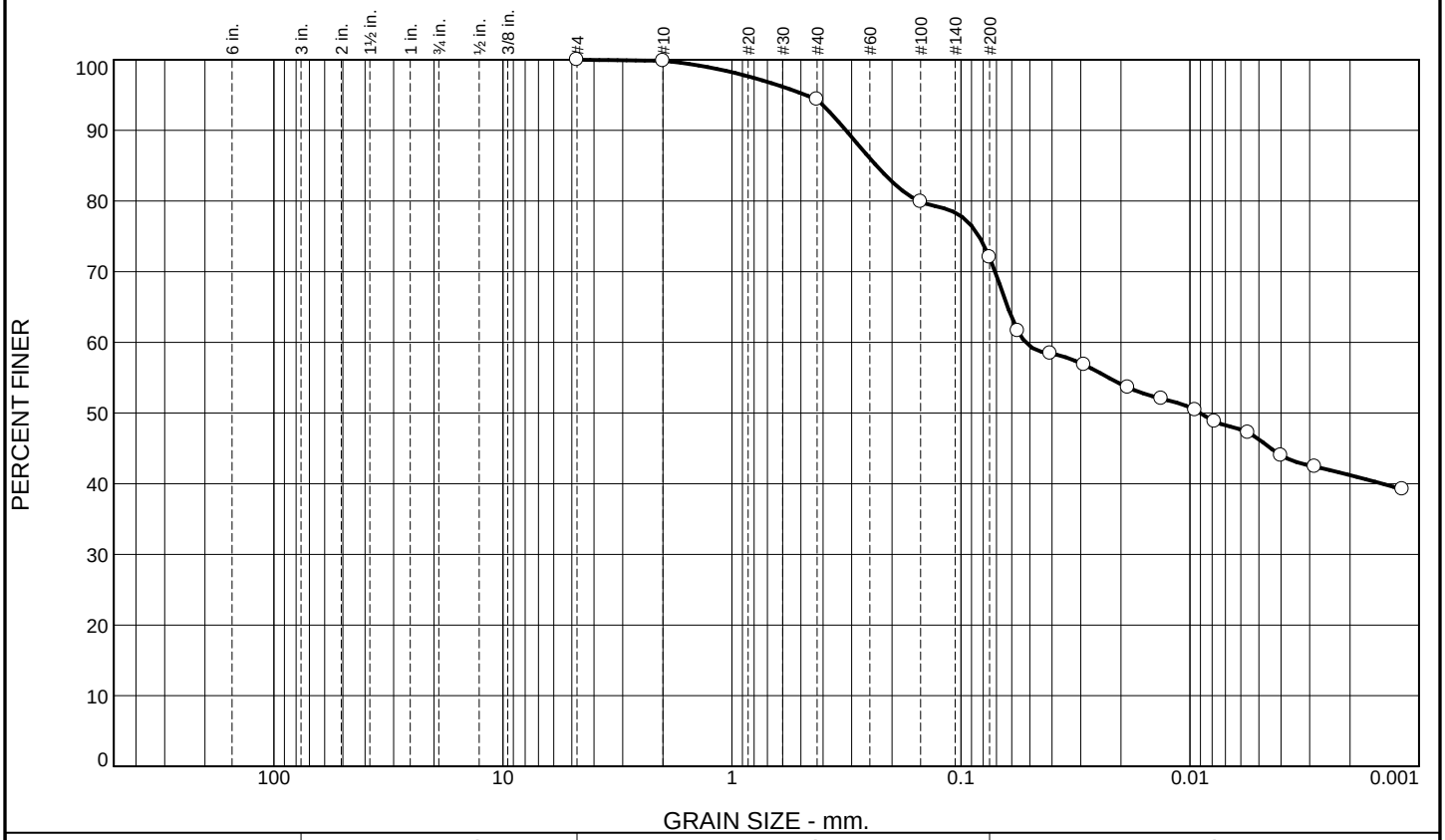
AECOM

**Client:** KESTREL HORIZONS LLC
**Project:** PINEWOOD SITE IMPROVEMENT

**Project No:** 60186203 **Figure**

**Tested By:** BOB PEETERS

# Particle Size Distribution Report




| % +3" | % Gravel | | % Sand | | | % Fines | |
|---|---|---|---|---|---|---|---|
| | Coarse | Fine | Coarse | Medium | Fine | Silt | Clay |
| 0.0 | 0.0 | 0.0 | 0.1 | 5.5 | 22.4 | 25.7 | 46.3 |

| SIEVE SIZE | PERCENT FINER | SPEC.* PERCENT | PASS? (X=NO) |
|---|---|---|---|
| #4 | 100.0 | | |
| #10 | 99.9 | | |
| #40 | 94.4 | | |
| #100 | 79.9 | | |
| #200 | 72.0 | | |

* (no specification provided)

**Material Description**

LIGHT BROWN SILTY CLAY, SOME SAND

**Atterberg Limits**

PL= 20 LL= 57 PI= 37

**Coefficients**

$D_{90}$= 0.3176 $D_{85}$= 0.2338 $D_{60}$= 0.0522
$D_{50}$= 0.0090 $D_{30}$= $D_{15}$=
$D_{10}$= $C_u$= $C_c$=

**Classification**

USCS= CH AASHTO= A-7-6(26)

**Remarks**

**Source of Sample:** ON SITE
**Sample Number:** SB-1E-8

**Date:** 01/11/11

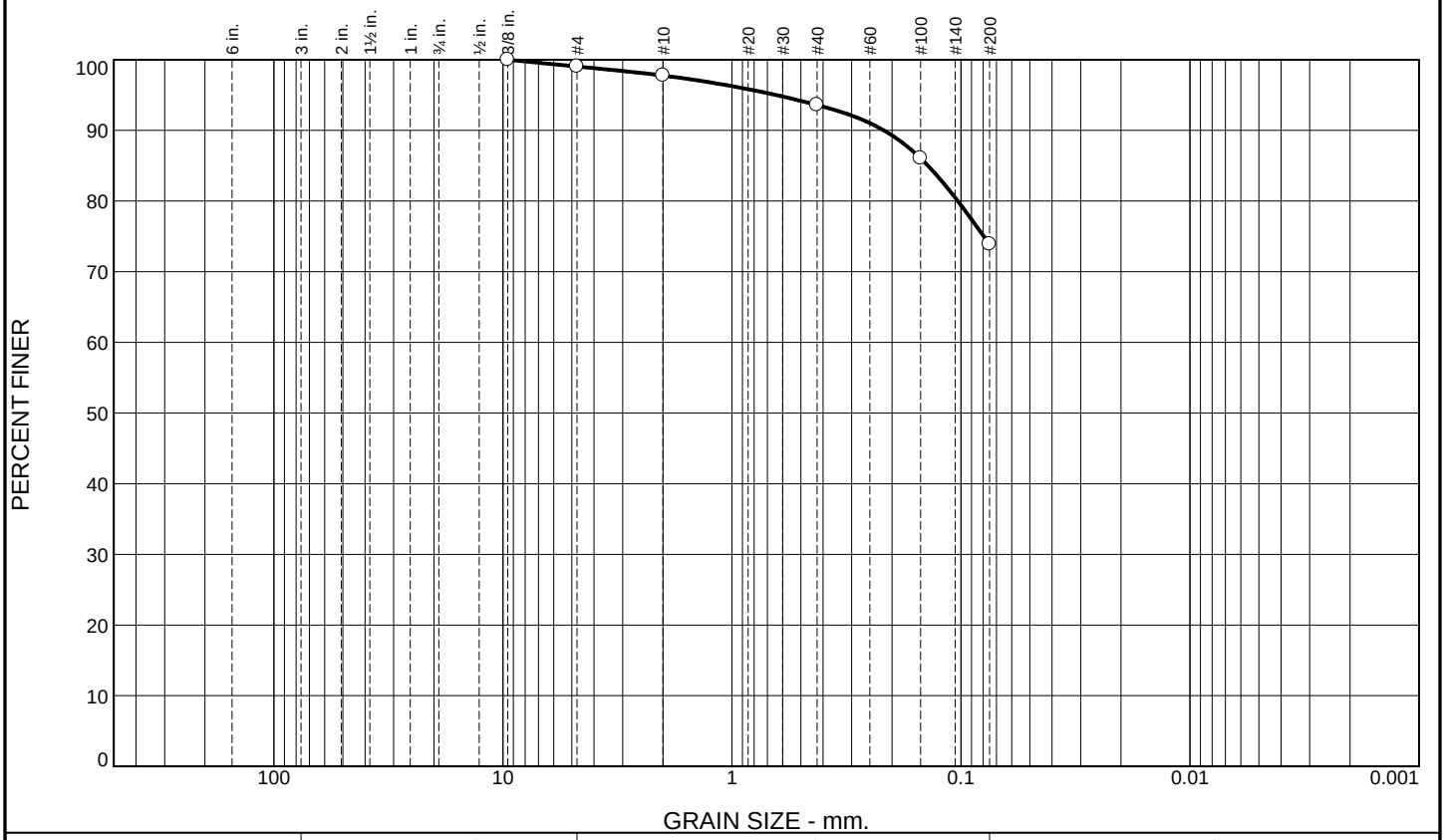
AECOM

**Client:** KESTREL HORIZONS LLC
**Project:** PINEWOOD SITE IMPROVEMENT

**Project No:** 60186203 **Figure**

**Tested By:** BOB PEETERS

# Particle Size Distribution Report




| % +3" | % Gravel | | % Sand | | | % Fines | |
|---|---|---|---|---|---|---|---|
| | Coarse | Fine | Coarse | Medium | Fine | Silt | Clay |
| 0.0 | 0.0 | 1.0 | 1.2 | 4.2 | 19.7 | 73.9 | |

| SIEVE SIZE | PERCENT FINER | SPEC.* PERCENT | PASS? (X=NO) |
|---|---|---|---|
| .375 | 100.0 | | |
| #4 | 99.0 | | |
| #10 | 97.8 | | |
| #40 | 93.6 | | |
| #100 | 86.1 | | |
| #200 | 73.9 | | |

* (no specification provided)

**Material Description**

LIGHT BROWN SILTY CLAY, SOME SAND

**Atterberg Limits**

PL= 21 LL= 50 PI= 29

**Coefficients**

$D_{90}$= 0.2171 $D_{85}$= 0.1392 $D_{60}$=
$D_{50}$= $D_{30}$= $D_{15}$=
$D_{10}$= $C_u$= $C_c$=

**Classification**

USCS= CH AASHTO= A-7-6(21)

**Remarks**

**Source of Sample:** ON SITE
**Sample Number:** SB-1E-10A

**Date:** 01/11/11

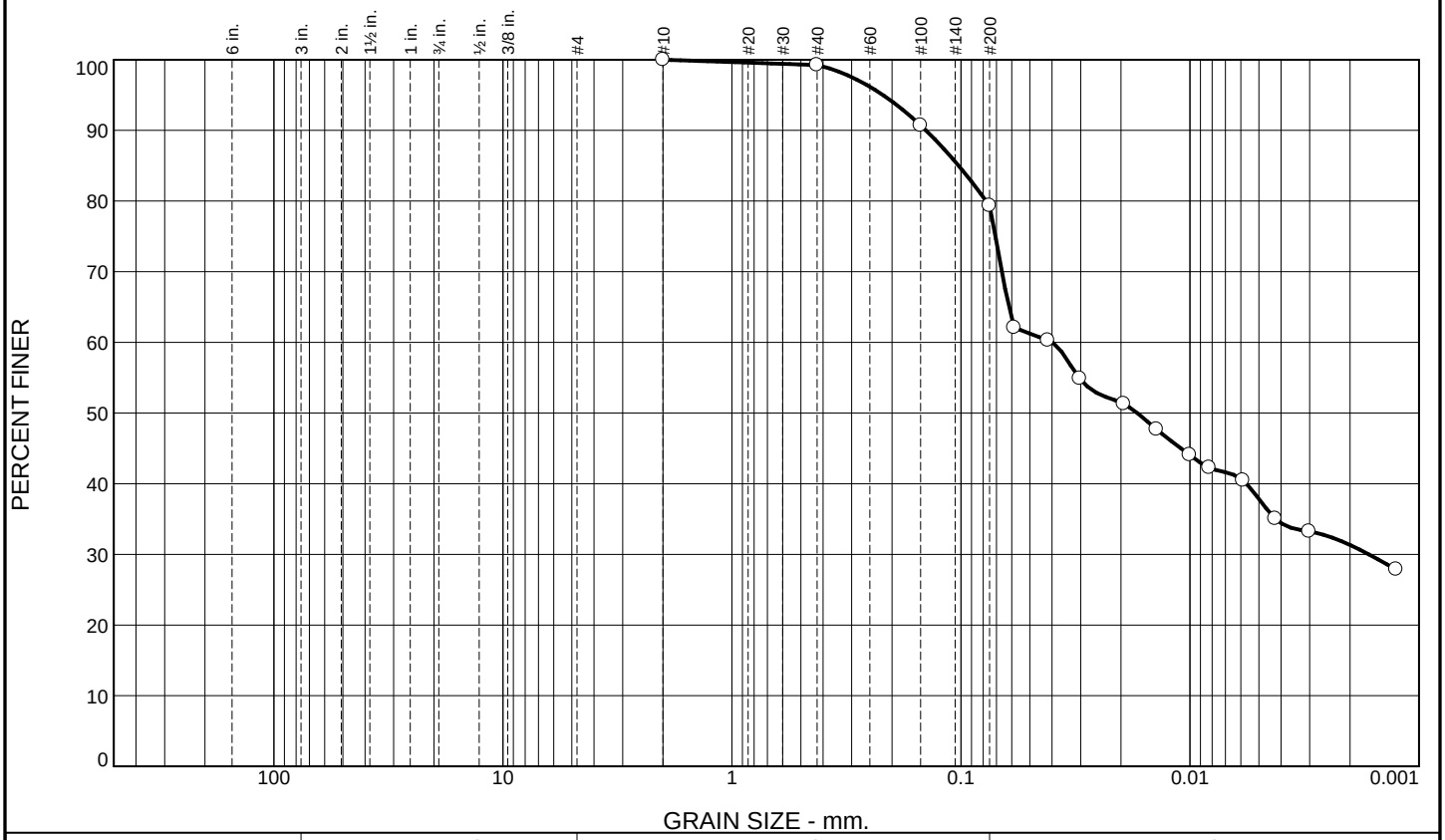
AECOM

**Client:** KESTREL HORIZONS LLC
**Project:** PINEWOOD SITE IMPROVEMENT

**Project No:** 60186203 **Figure**

**Tested By:** BOB PEETERS

# Particle Size Distribution Report




| % +3" | % Gravel | | % Sand | | | % Fines | |
|---|---|---|---|---|---|---|---|
| | Coarse | Fine | Coarse | Medium | Fine | Silt | Clay |
| 0.0 | 0.0 | 0.0 | 0.0 | 0.7 | 20.0 | 41.5 | 37.8 |

| SIEVE SIZE | PERCENT FINER | SPEC.* PERCENT | PASS? (X=NO) |
|---|---|---|---|
| #10 | 100.0 | | |
| #40 | 99.3 | | |
| #100 | 90.7 | | |
| #200 | 79.3 | | |

* (no specification provided)

**Material Description**

LIGHT BROWN SILTY CLAY, SOME FINE SAND

**Atterberg Limits**

PL= 23 LL= 50 PI= 27

**Coefficients**

$D_{90}$= 0.1423 $D_{85}$= 0.1024 $D_{60}$= 0.0397
$D_{50}$= 0.0170 $D_{30}$= 0.0017 $D_{15}$=
$D_{10}$= $C_u$= $C_c$=

**Classification**

USCS= CH AASHTO= A-7-6(22)

**Remarks**

**Source of Sample:** ON SITE
**Sample Number:** TP-1A-01

**Date:** 01/11/11

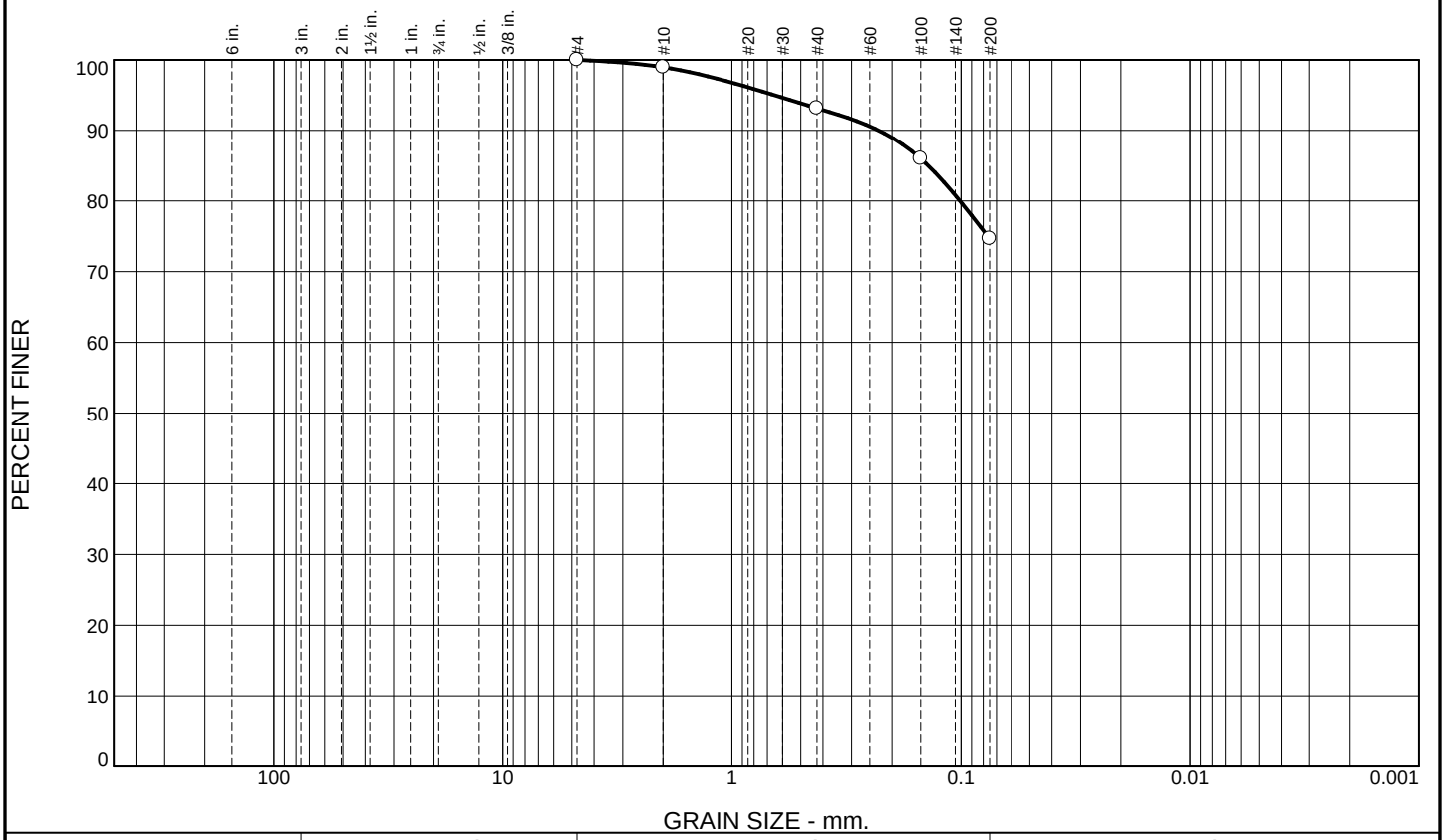
AECOM

**Client:** KESTREL HORIZONS LLC
**Project:** PINEWOOD SITE IMPROVEMENT

**Project No:** 60186203 **Figure**

**Tested By:** BOB PEETERS

# Particle Size Distribution Report




| % +3" | % Gravel | | % Sand | | | % Fines | |
|---|---|---|---|---|---|---|---|
| | Coarse | Fine | Coarse | Medium | Fine | Silt | Clay |
| 0.0 | 0.0 | 0.0 | 1.0 | 5.9 | 18.4 | 74.7 | |

| SIEVE SIZE | PERCENT FINER | SPEC.* PERCENT | PASS? (X=NO) |
|---|---|---|---|
| #4 | 100.0 | | |
| #10 | 99.0 | | |
| #40 | 93.1 | | |
| #100 | 86.0 | | |
| #200 | 74.7 | | |

* (no specification provided)

**Material Description**

LIGHT BROWN SILTY CLAY, SOME SAND, TRACE FINE GRAVEL

**Atterberg Limits**

PL= 23 LL= 46 PI= 23

**Coefficients**

$D_{90}$= 0.2288 $D_{85}$= 0.1391 $D_{60}$=
$D_{50}$= $D_{30}$= $D_{15}$=
$D_{10}$= $C_u$= $C_c$=

**Classification**

USCS= CL AASHTO= A-7-6(17)

**Remarks**

**Source of Sample:** ON SITE
**Sample Number:** TP-1D-01

**Date:** 01/11/11

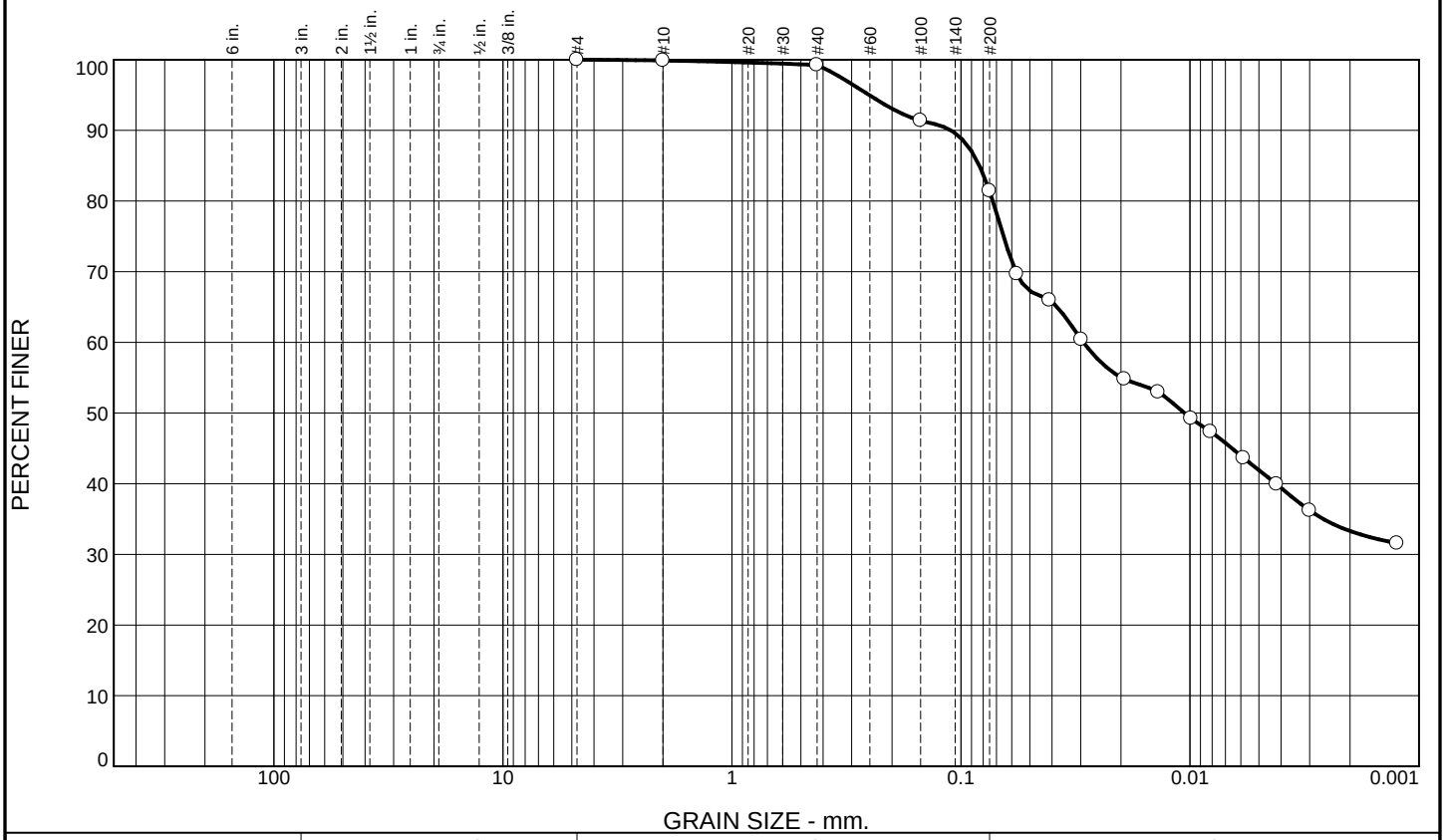
AECOM

**Client:** KESTREL HORIZONS LLC
**Project:** PINEWOOD SITE IMPROVEMENT

**Project No:** 60186203 **Figure**

**Tested By:** BOB PEETERS

# Particle Size Distribution Report




| % +3" | % Gravel | | % Sand | | | % Fines | |
|---|---|---|---|---|---|---|---|
| | Coarse | Fine | Coarse | Medium | Fine | Silt | Clay |
| 0.0 | 0.0 | 0.0 | 0.1 | 0.6 | 17.9 | 39.5 | 41.9 |

| SIEVE SIZE | PERCENT FINER | SPEC.* PERCENT | PASS? (X=NO) |
|---|---|---|---|
| #4 | 100.0 | | |
| #10 | 99.9 | | |
| #40 | 99.3 | | |
| #100 | 91.4 | | |
| #200 | 81.4 | | |

* (no specification provided)

**Material Description**

LIGHT BROWN SILTY CLAY, LITTLE SAND

**Atterberg Limits**

PL= 23 LL= 55 PI= 32

**Coefficients**

$D_{90}$= 0.1105 $D_{85}$= 0.0830 $D_{60}$= 0.0292
$D_{50}$= 0.0106 $D_{30}$= $D_{15}$=
$D_{10}$= $C_u$= $C_c$=

**Classification**

USCS= CH AASHTO= A-7-6(27)

**Remarks**

**Source of Sample:** ON SITE
**Sample Number:** TP-1D-02

**Date:** 01/11/11

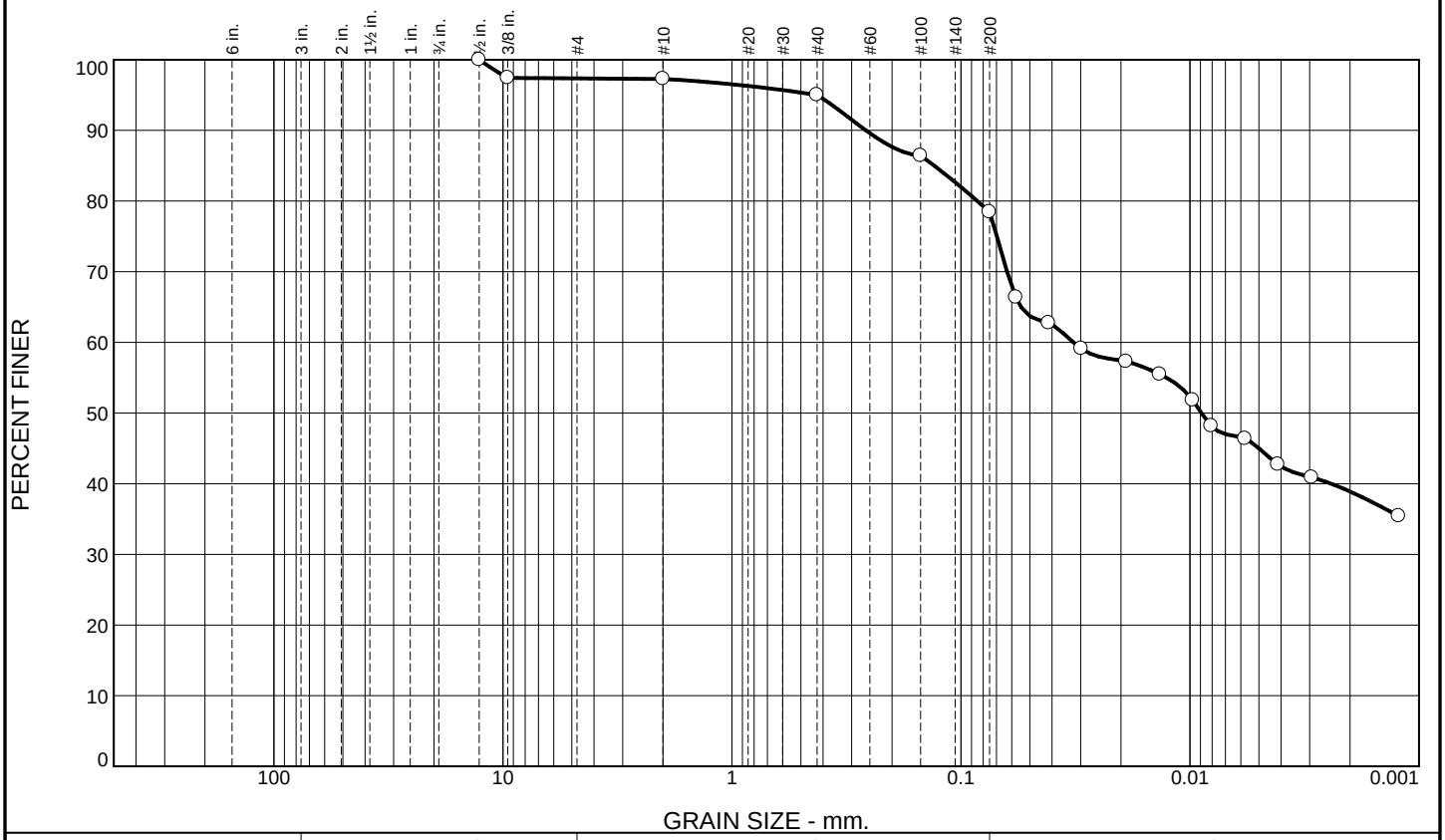
AECOM

**Client:** KESTREL HORIZONS LLC
**Project:** PINEWOOD SITE IMPROVEMENT

**Project No:** 60186203 **Figure**

**Tested By:** BOB PEETERS

# Particle Size Distribution Report




| % +3" | % Gravel | | % Sand | | | % Fines | |
|---|---|---|---|---|---|---|---|
| | Coarse | Fine | Coarse | Medium | Fine | Silt | Clay |
| 0.0 | 0.0 | 2.6 | 0.1 | 2.3 | 16.5 | 33.5 | 45.0 |

| SIEVE SIZE | PERCENT FINER | SPEC.* PERCENT | PASS? (X=NO) |
|---|---|---|---|
| .5 | 100.0 | | |
| .375 | 97.4 | | |
| #10 | 97.3 | | |
| #40 | 95.0 | | |
| #100 | 86.4 | | |
| #200 | 78.5 | | |

* (no specification provided)

**Material Description**

LIGHT BROWN SILTY CLAY, LITTLE SAND, TRACE GRAVEL

**Atterberg Limits**

PL= 21 LL= 59 PI= 38

**Coefficients**

$D_{90}$= 0.2599 $D_{85}$= 0.1308 $D_{60}$= 0.0323
$D_{50}$= 0.0089 $D_{30}$= $D_{15}$=
$D_{10}$= $C_u$= $C_c$=

**Classification**

USCS= CH AASHTO= A-7-6(30)

**Remarks**

**Source of Sample:** ON SITE
**Sample Number:** TP-1E-01A

**Date:** 01/11/11

AECOM

**Client:** KESTREL HORIZONS LLC
**Project:** PINEWOOD SITE IMPROVEMENT

**Project No:** 60186203 **Figure**

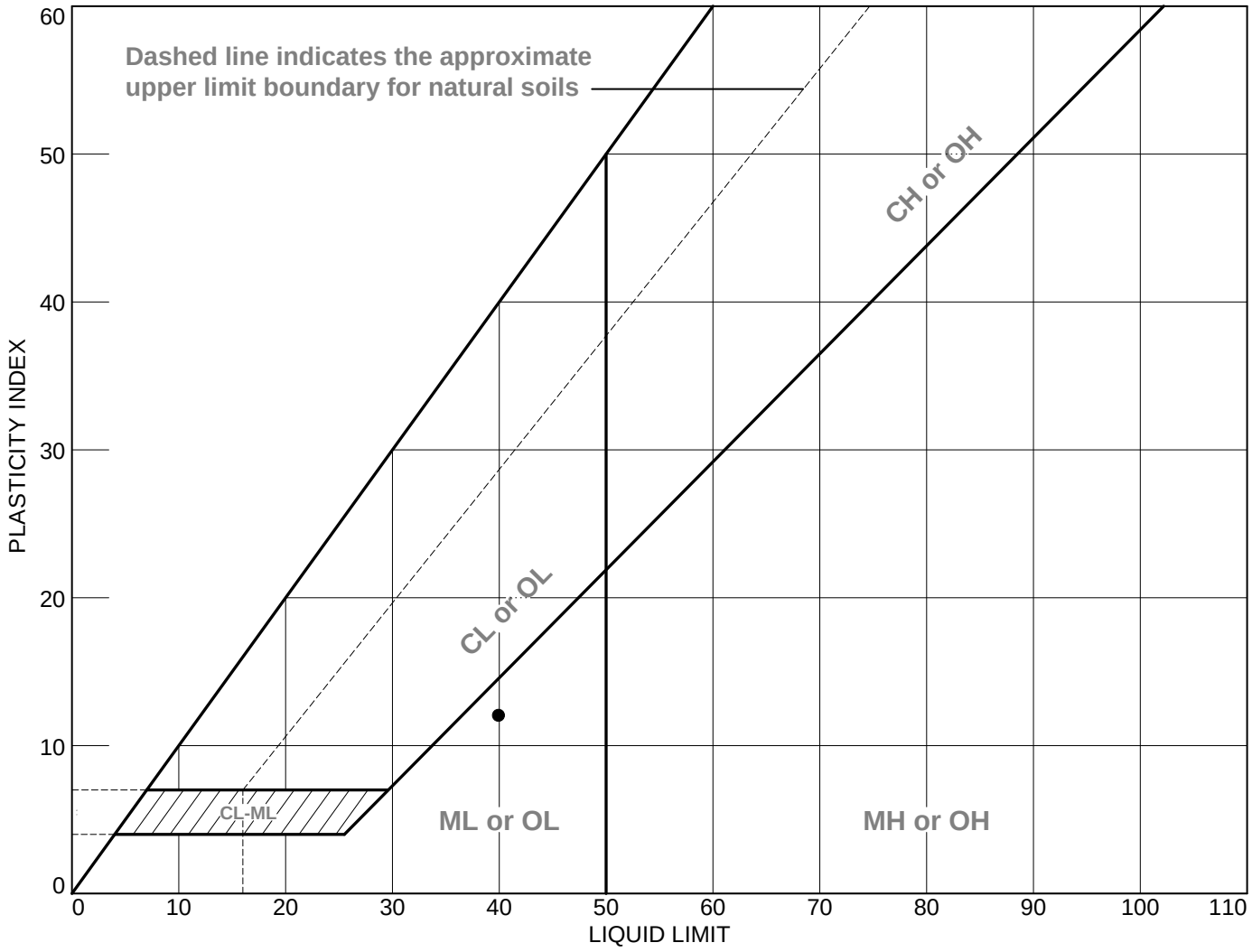
**Tested By:** BOB PEETERS

# AECOM Technical Services, Inc.

## Bulk Soil Samples

## Liquid and Plastic Limits Testing
## Particle Size Distribution Testing

# LIQUID AND PLASTIC LIMITS TEST REPORT




**SOIL DATA**

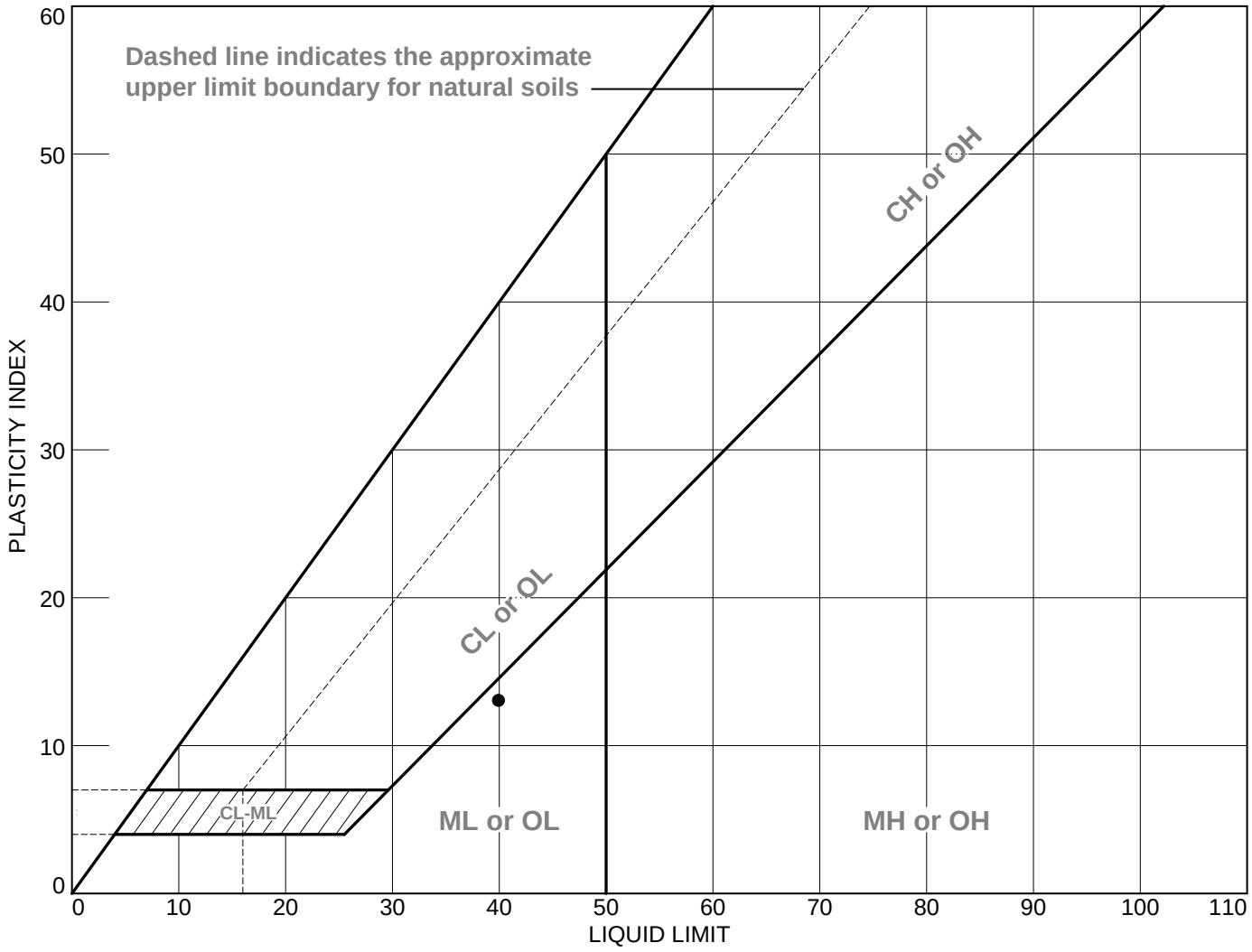
| SYMBOL | SOURCE | SAMPLE NO. | DEPTH | NATURAL WATER CONTENT (%) | PLASTIC LIMIT (%) | LIQUID LIMIT (%) | PLASTICITY INDEX (%) | USCS |
|---|---|---|---|---|---|---|---|---|
| ● | BULK SAMPLES | AT-1B-01 | | | 28 | 40 | 12 | ML |

AECOM

**Client:** KESTREL HORIZONS LLC
**Project:** PINEWOOD SITE IMPROVEMENT

**Project No.:** 60186203 **Figure**

# LIQUID AND PLASTIC LIMITS TEST REPORT



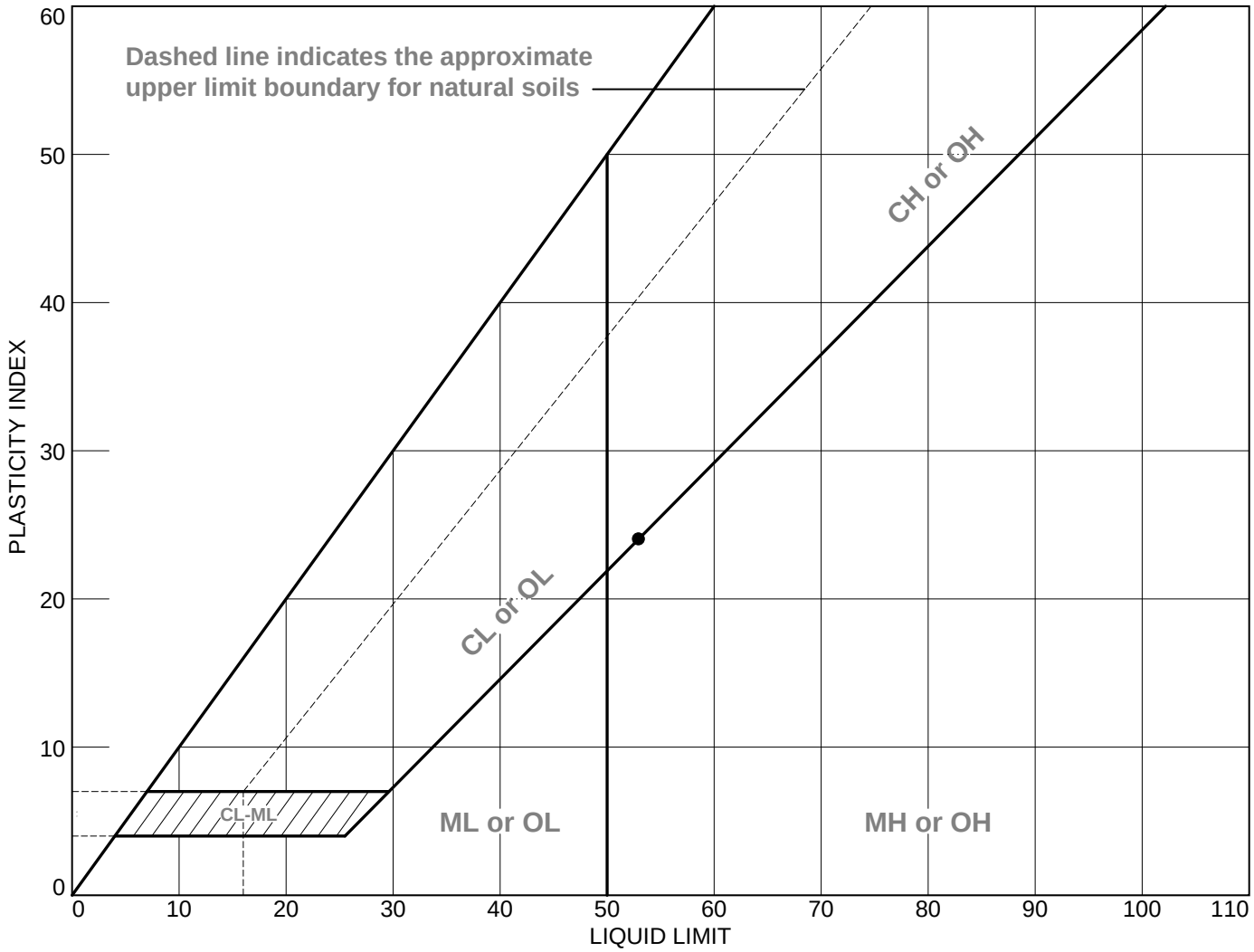

| SOIL DATA | | | | | | | | |
|---|---|---|---|---|---|---|---|---|
| SYMBOL | SOURCE | SAMPLE NO. | DEPTH | NATURAL WATER CONTENT (%) | PLASTIC LIMIT (%) | LIQUID LIMIT (%) | PLASTICITY INDEX (%) | USCS |
| ● | BULK SAMPLES | AT-1C-01 | | | 27 | 40 | 13 | SM |

AECOM

**Client:** KESTREL HORIZONS LLC
**Project:** PINEWOOD SITE IMPROVEMENT

**Project No.:** 60186203 **Figure**

# LIQUID AND PLASTIC LIMITS TEST REPORT




**SOIL DATA**

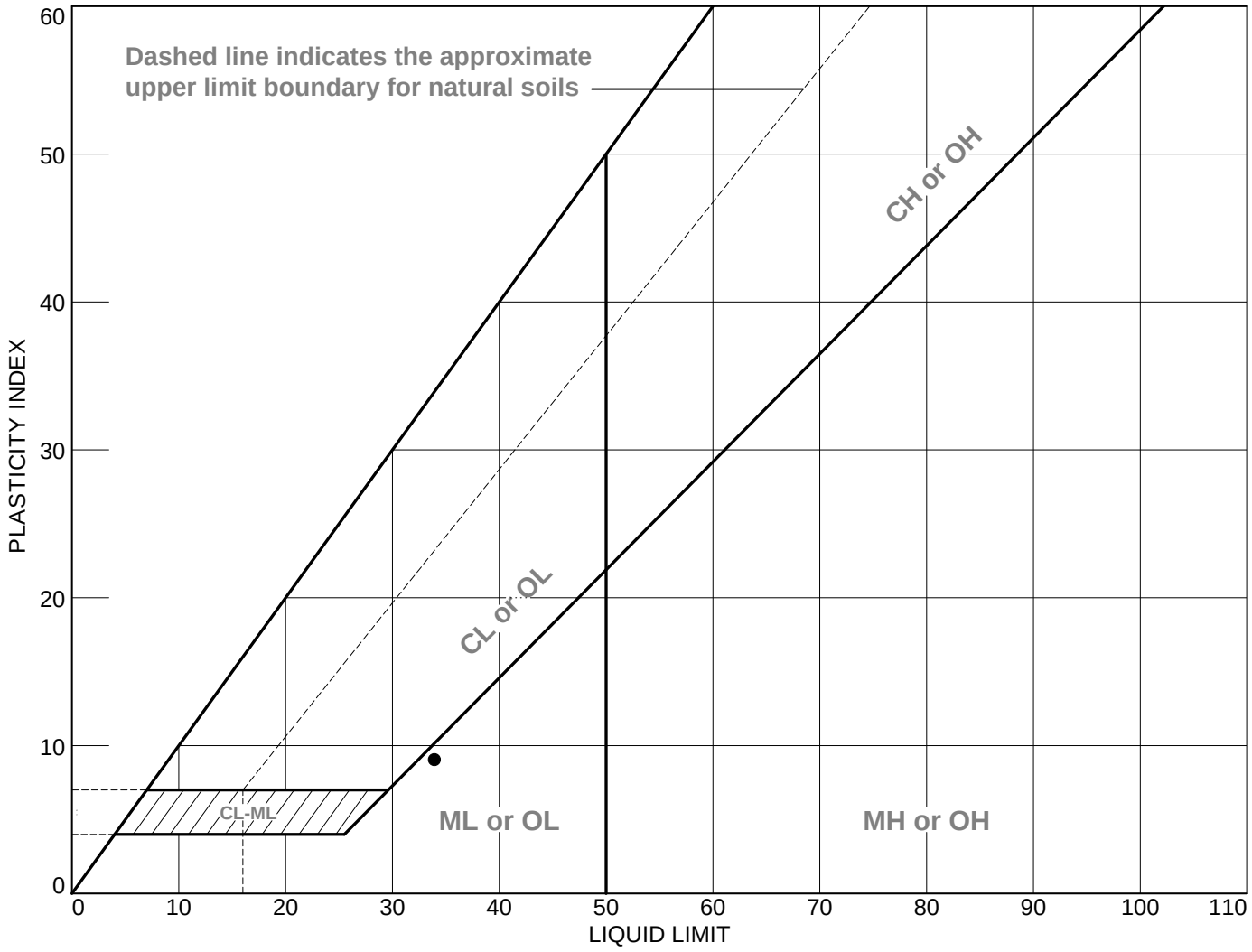
| SYMBOL | SOURCE | SAMPLE NO. | DEPTH | NATURAL WATER CONTENT (%) | PLASTIC LIMIT (%) | LIQUID LIMIT (%) | PLASTICITY INDEX (%) | USCS |
|---|---|---|---|---|---|---|---|---|
| ● | BULK SAMPLES | AT-1E-01 | | | 29 | 53 | 24 | CH |

AECOM

**Client:** KESTREL HORIZONS LLC
**Project:** PINEWOOD SITE IMPROVEMENT

**Project No.:** 60186203 **Figure**

# LIQUID AND PLASTIC LIMITS TEST REPORT




**SOIL DATA**

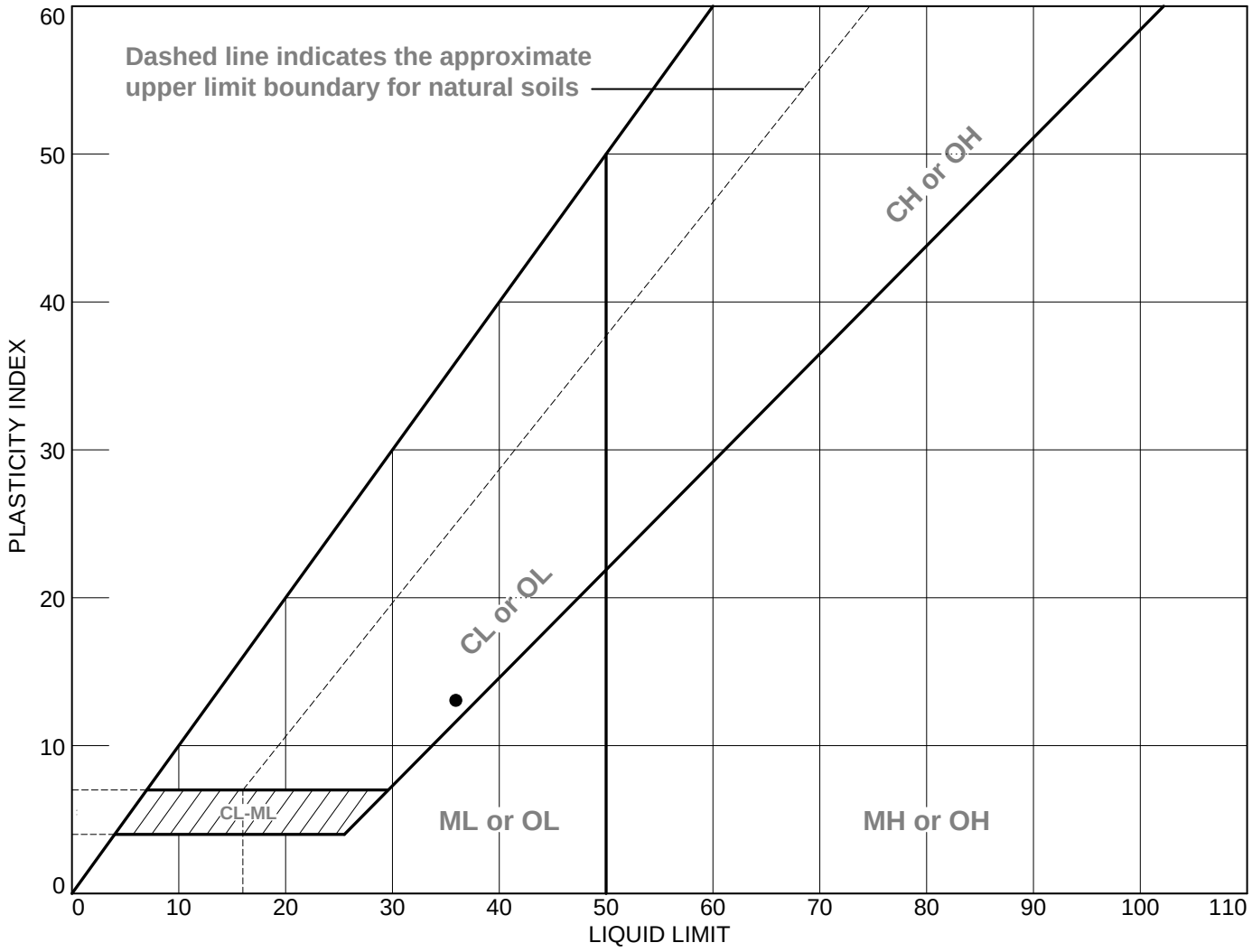
| SYMBOL | SOURCE | SAMPLE NO. | DEPTH | NATURAL WATER CONTENT (%) | PLASTIC LIMIT (%) | LIQUID LIMIT (%) | PLASTICITY INDEX (%) | USCS |
|---|---|---|---|---|---|---|---|---|
| ● | BULK SAMPLES | SB-1A-01 | 0.0'-2.0' | | 25 | 34 | 9 | ML |

AECOM

**Client:** KESTREL HORIZONS LLC
**Project:** PINEWOOD SITE IMPROVEMENT

**Project No.:** 60186203 **Figure**

# LIQUID AND PLASTIC LIMITS TEST REPORT



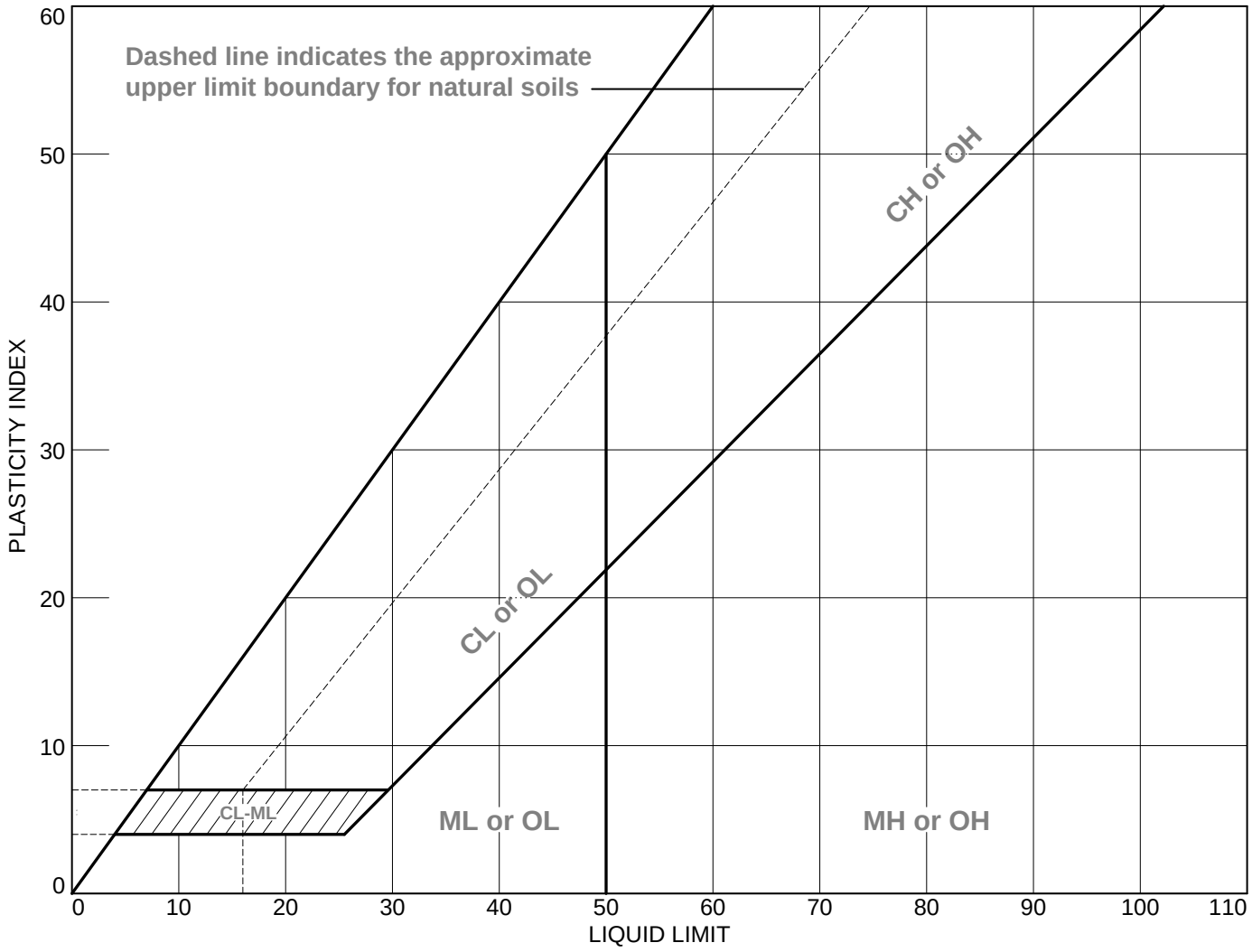

| SOIL DATA | | | | | | | | |
|---|---|---|---|---|---|---|---|---|
| SYMBOL | SOURCE | SAMPLE NO. | DEPTH | NATURAL WATER CONTENT (%) | PLASTIC LIMIT (%) | LIQUID LIMIT (%) | PLASTICITY INDEX (%) | USCS |
| ● | BULK SAMPLES | SB-1B-02 | 2.0'-4.0' | | 23 | 36 | 13 | SC |

AECOM

**Client:** KESTREL HORIZONS LLC
**Project:** PINEWOOD SITE IMPROVEMENT

**Project No.:** 60186203 **Figure**

# LIQUID AND PLASTIC LIMITS TEST REPORT



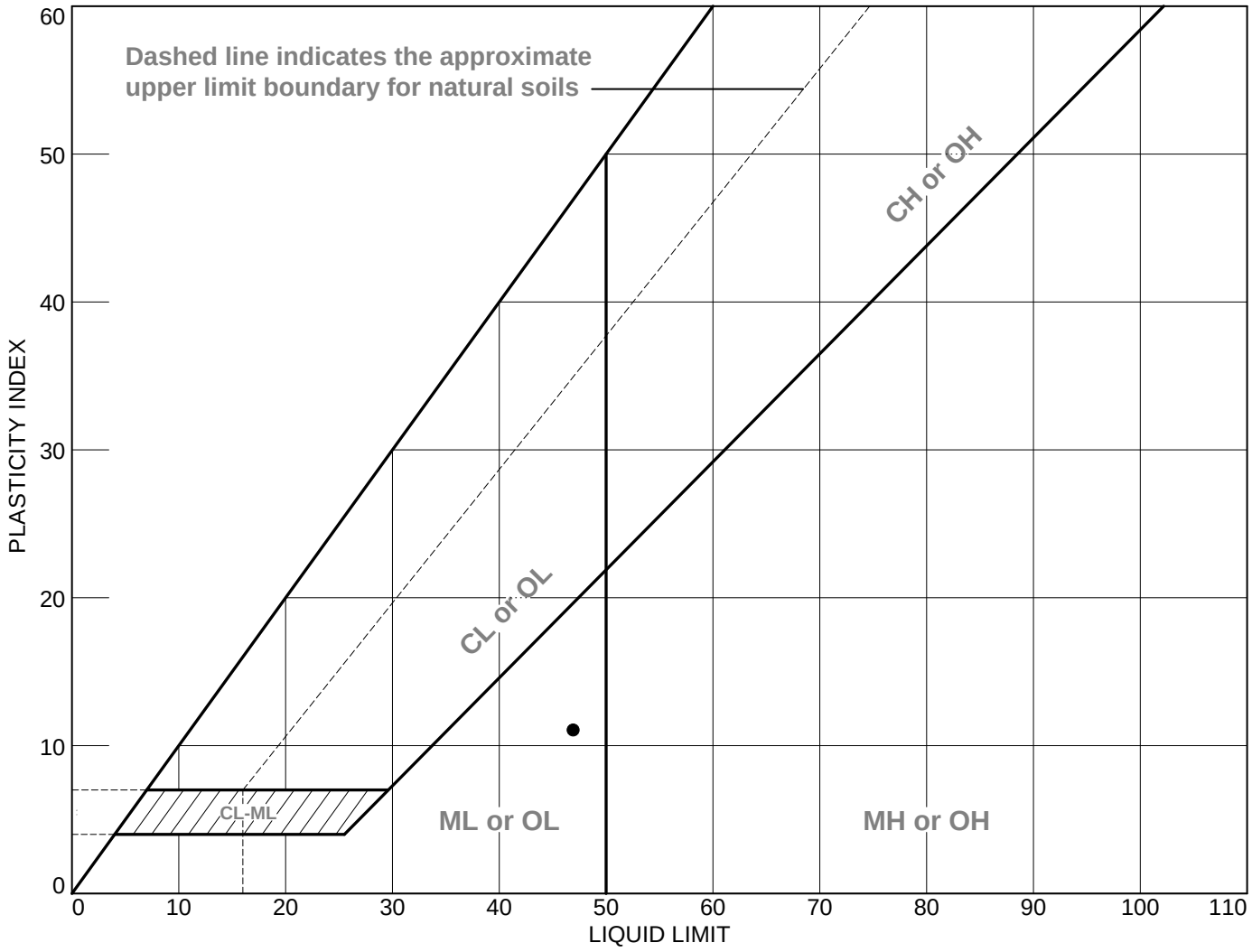

| SOIL DATA | | | | | | | | |
|---|---|---|---|---|---|---|---|---|
| SYMBOL | SOURCE | SAMPLE NO. | DEPTH | NATURAL WATER CONTENT (%) | PLASTIC LIMIT (%) | LIQUID LIMIT (%) | PLASTICITY INDEX (%) | USCS |
| ● | BULK SAMPLES | SB-1C-04 | | | NP | 22 | NP | |

AECOM

**Client:** KESTREL HORIZONS LLC
**Project:** PINEWOOD SITE IMPROVEMENT

**Project No.:** 60186203 **Figure**

# LIQUID AND PLASTIC LIMITS TEST REPORT




**SOIL DATA**

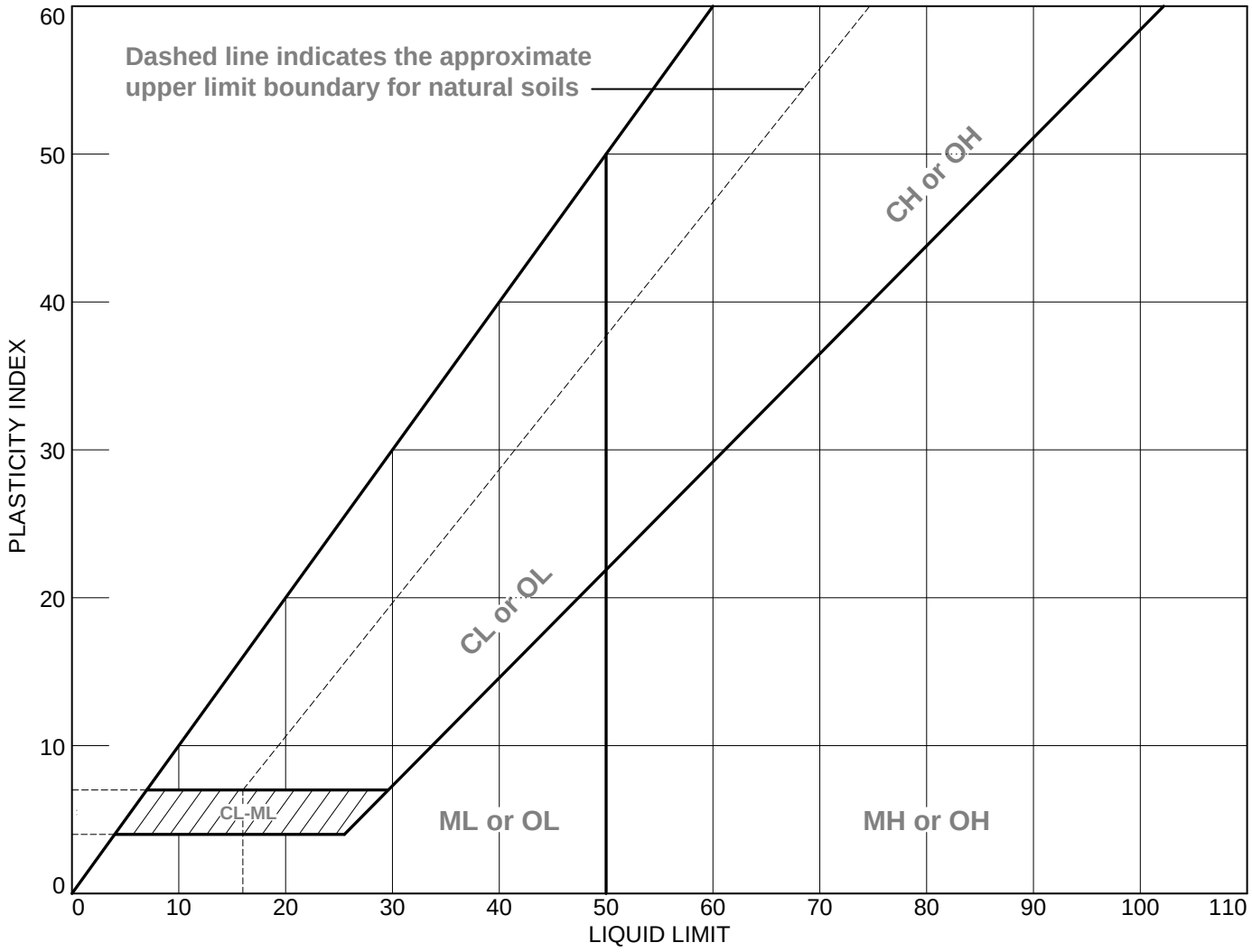
| SYMBOL | SOURCE | SAMPLE NO. | DEPTH | NATURAL WATER CONTENT (%) | PLASTIC LIMIT (%) | LIQUID LIMIT (%) | PLASTICITY INDEX (%) | USCS |
|---|---|---|---|---|---|---|---|---|
| ● | BULK SAMPLES | SB-1D-06 | 2.0'-4.0' | | 36 | 47 | 11 | ML |

AECOM

**Client:** KESTREL HORIZONS LLC
**Project:** PINEWOOD SITE IMPROVEMENT

**Project No.:** 60186203 **Figure**

# LIQUID AND PLASTIC LIMITS TEST REPORT



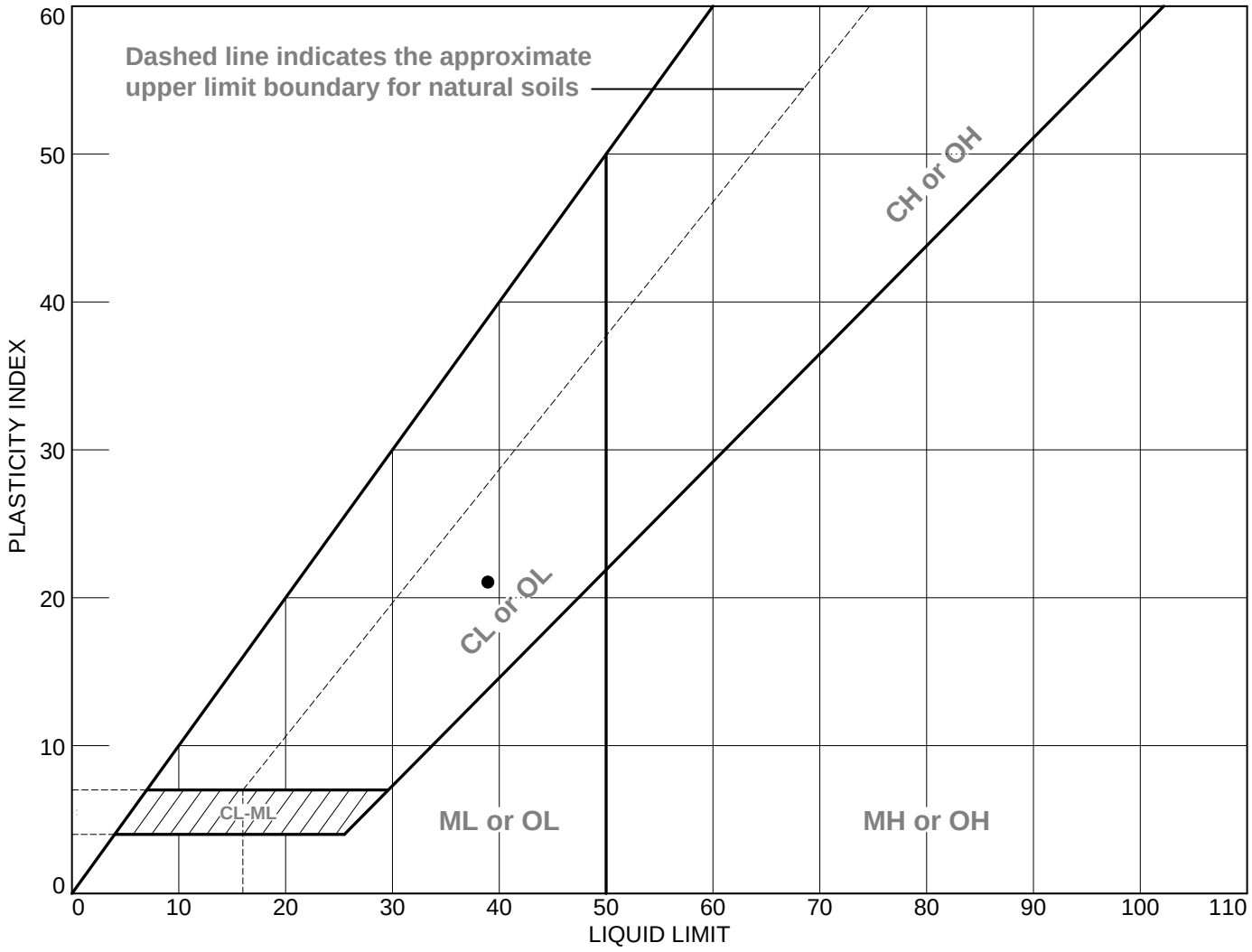

| SOIL DATA | | | | | | | | |
|---|---|---|---|---|---|---|---|---|
| SYMBOL | SOURCE | SAMPLE NO. | DEPTH | NATURAL WATER CONTENT (%) | PLASTIC LIMIT (%) | LIQUID LIMIT (%) | PLASTICITY INDEX (%) | USCS |
| ● | BULK SAMPLES | SB-1D-07 | 0.0'-2.0' | | NP | 22 | NP | SM |

AECOM

**Client:** KESTREL HORIZONS LLC
**Project:** PINEWOOD SITE IMPROVEMENT

**Project No.:** 60186203 **Figure**

# LIQUID AND PLASTIC LIMITS TEST REPORT



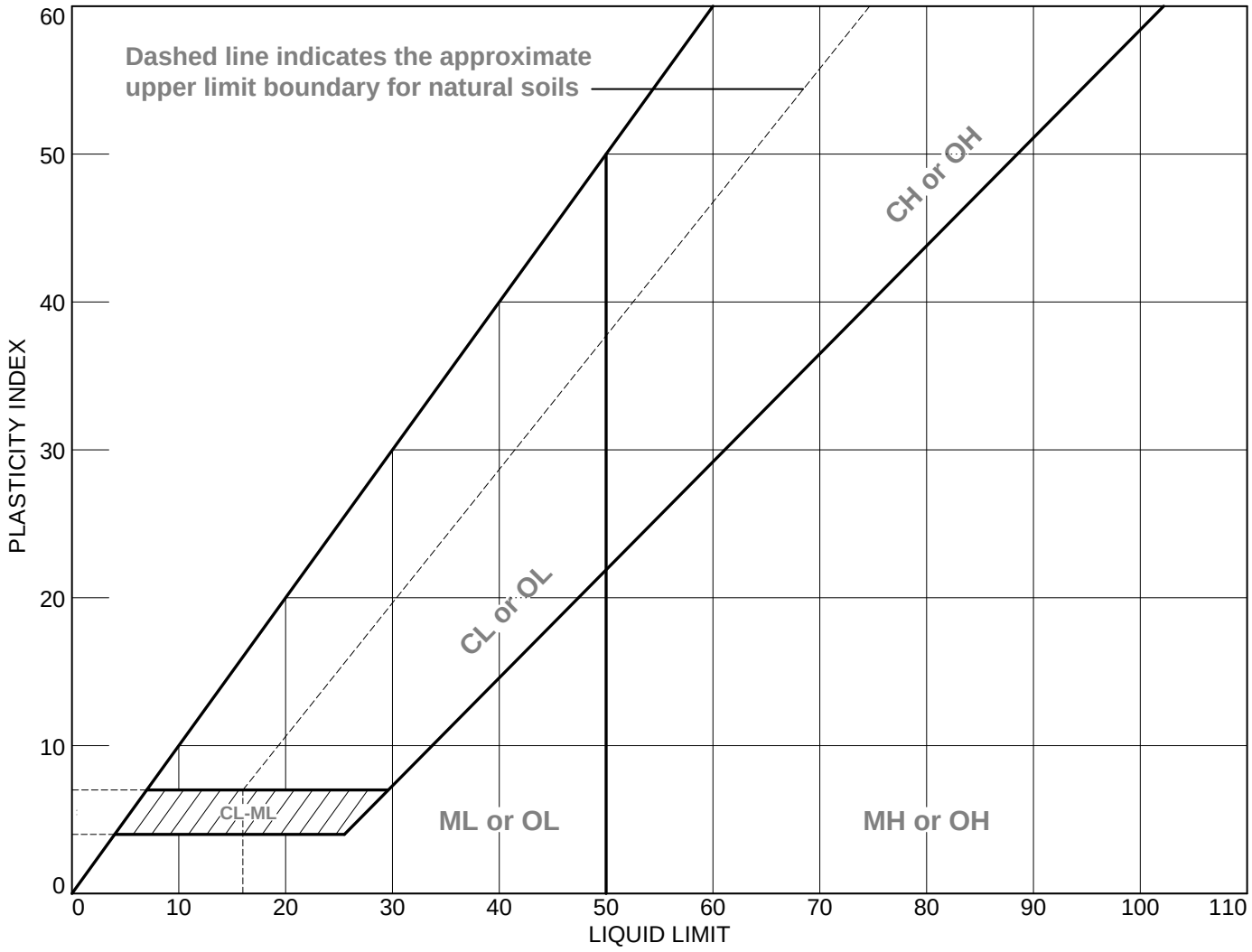

| SOIL DATA | | | | | | | | |
|---|---|---|---|---|---|---|---|---|
| SYMBOL | SOURCE | SAMPLE NO. | DEPTH | NATURAL WATER CONTENT (%) | PLASTIC LIMIT (%) | LIQUID LIMIT (%) | PLASTICITY INDEX (%) | USCS |
| ● | BULK SAMPLES | TP-1A-01 | | | 18 | 39 | 21 | SC |

AECOM

**Client:** KESTREL HORIZONS LLC
**Project:** PINEWOOD SITE IMPROVEMENT

**Project No.:** 60186203 **Figure**

# LIQUID AND PLASTIC LIMITS TEST REPORT



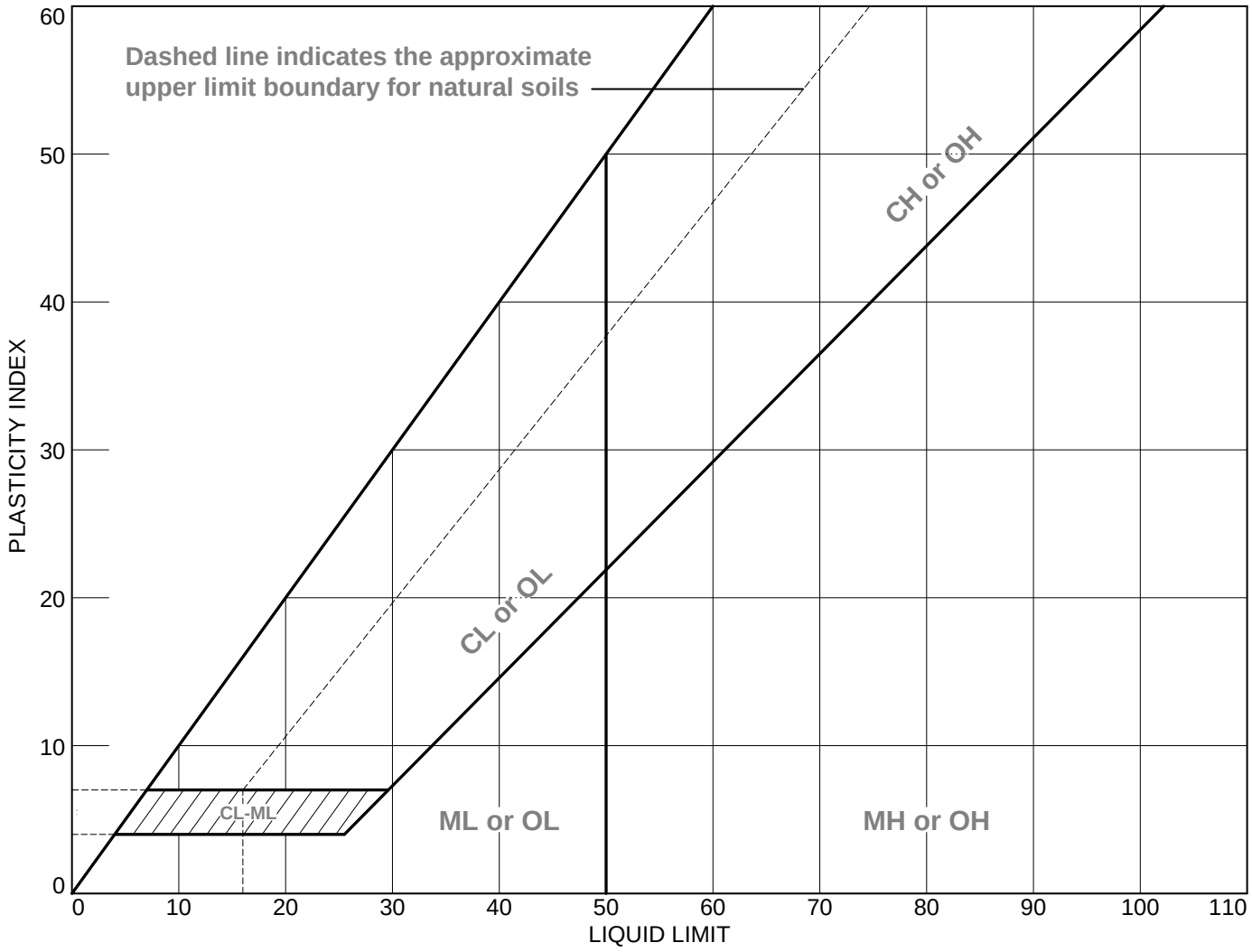

| SOIL DATA | | | | | | | | |
|---|---|---|---|---|---|---|---|---|
| SYMBOL | SOURCE | SAMPLE NO. | DEPTH | NATURAL WATER CONTENT (%) | PLASTIC LIMIT (%) | LIQUID LIMIT (%) | PLASTICITY INDEX (%) | USCS |
| ● | BULK SAMPLES | TP-1D-01 | | | NP | 28 | NP | SM |

AECOM

**Client:** KESTREL HORIZONS LLC
**Project:** PINEWOOD SITE IMPROVEMENT

**Project No.:** 60186203 **Figure**

# LIQUID AND PLASTIC LIMITS TEST REPORT



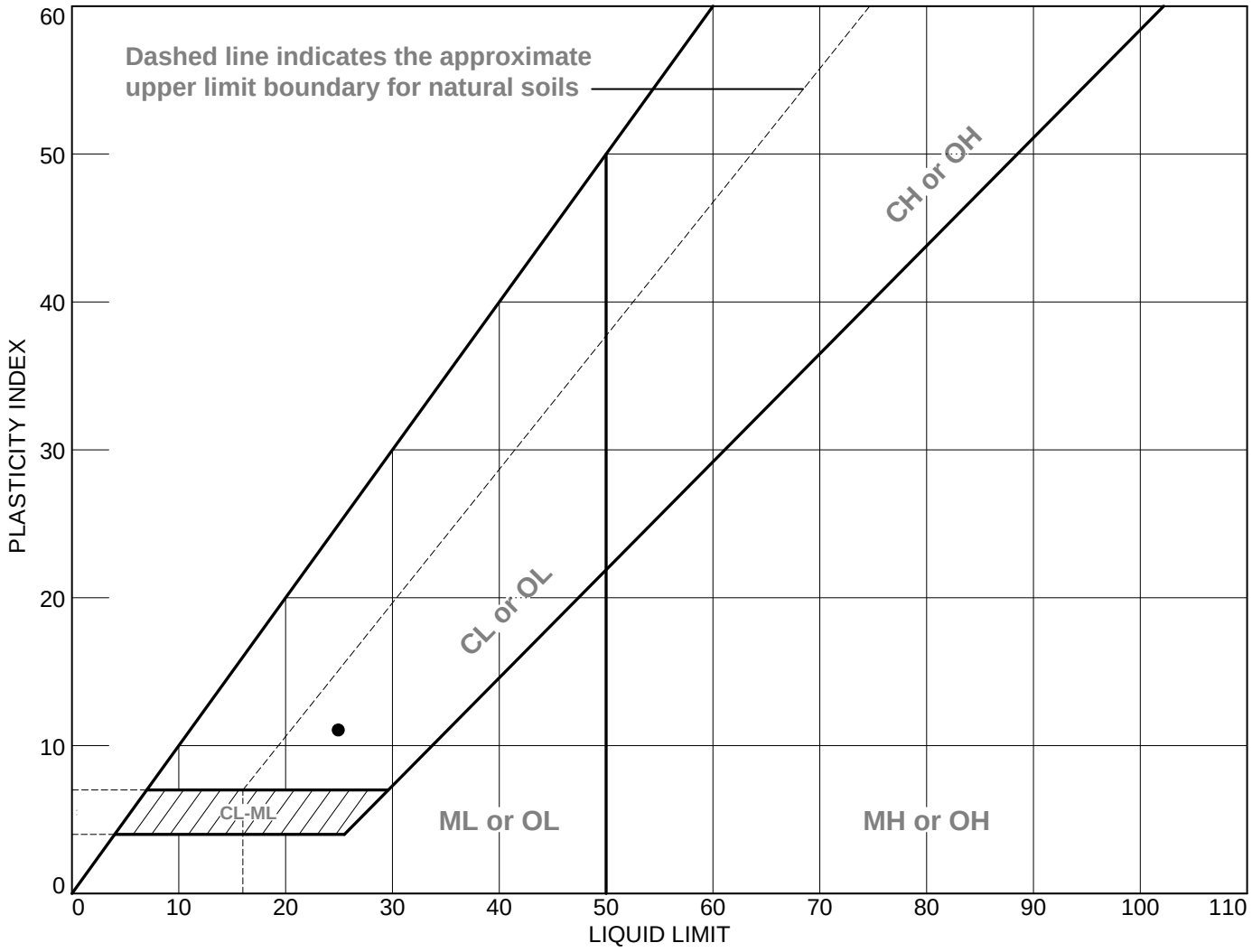

| SOIL DATA | | | | | | | | |
|---|---|---|---|---|---|---|---|---|
| SYMBOL | SOURCE | SAMPLE NO. | DEPTH | NATURAL WATER CONTENT (%) | PLASTIC LIMIT (%) | LIQUID LIMIT (%) | PLASTICITY INDEX (%) | USCS |
| ● | BULK SAMPLES | TP-1D-02 | 1.0'-2.0' | | NP | 15 | NP | SM |

AECOM

**Client:** KESTREL HORIZONS LLC
**Project:** PINEWOOD SITE IMPROVEMENT

**Project No.:** 60186203 **Figure**

# LIQUID AND PLASTIC LIMITS TEST REPORT



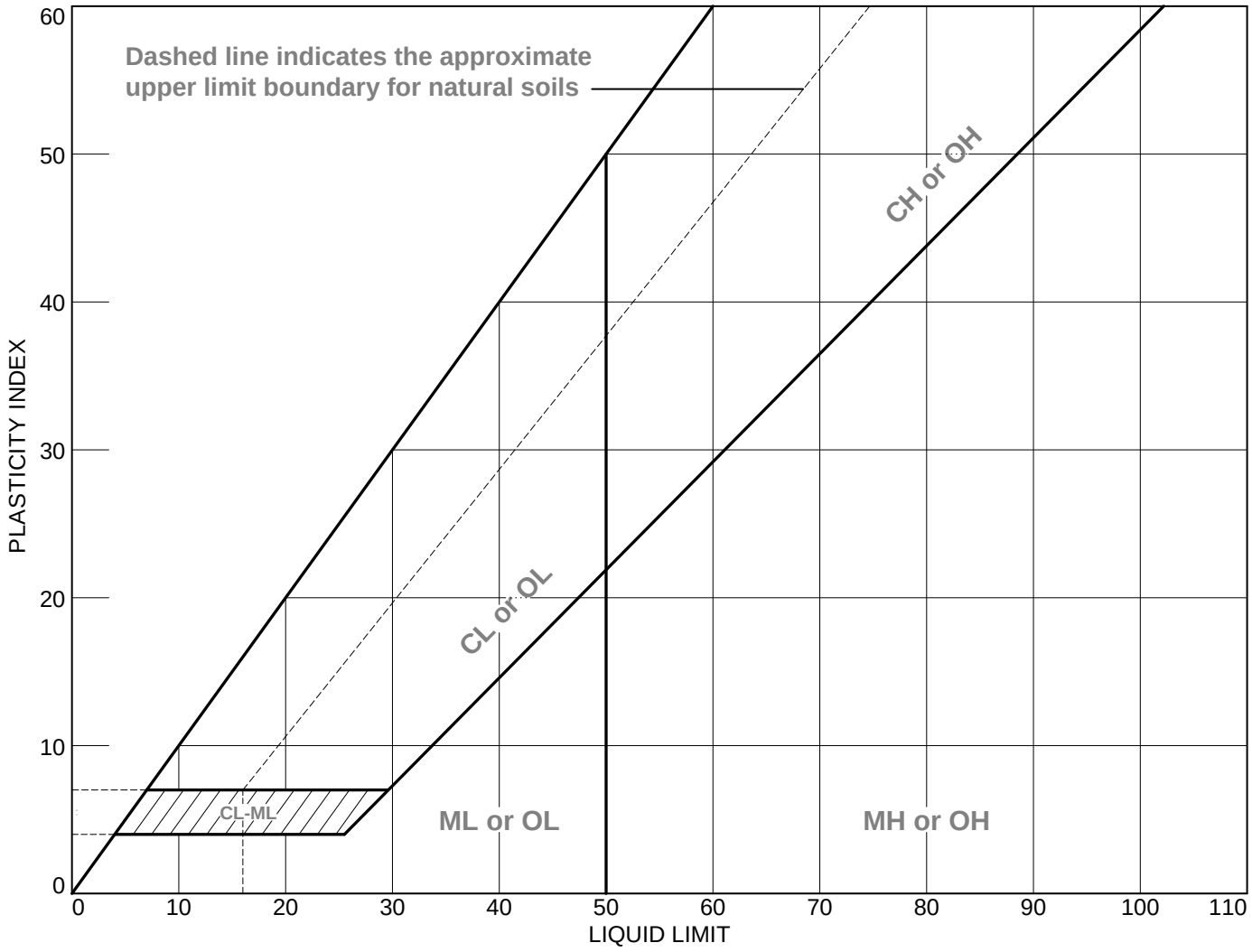

| SOIL DATA | | | | | | | | |
|---|---|---|---|---|---|---|---|---|
| SYMBOL | SOURCE | SAMPLE NO. | DEPTH | NATURAL WATER CONTENT (%) | PLASTIC LIMIT (%) | LIQUID LIMIT (%) | PLASTICITY INDEX (%) | USCS |
| ● | BULK SAMPLES | TP-1E-01 | 1.0'-2.0' | | 14 | 25 | 11 | SC |

AECOM

**Client:** KESTREL HORIZONS LLC
**Project:** PINEWOOD SITE IMPROVEMENT

**Project No.:** 60186203 **Figure**

# LIQUID AND PLASTIC LIMITS TEST REPORT



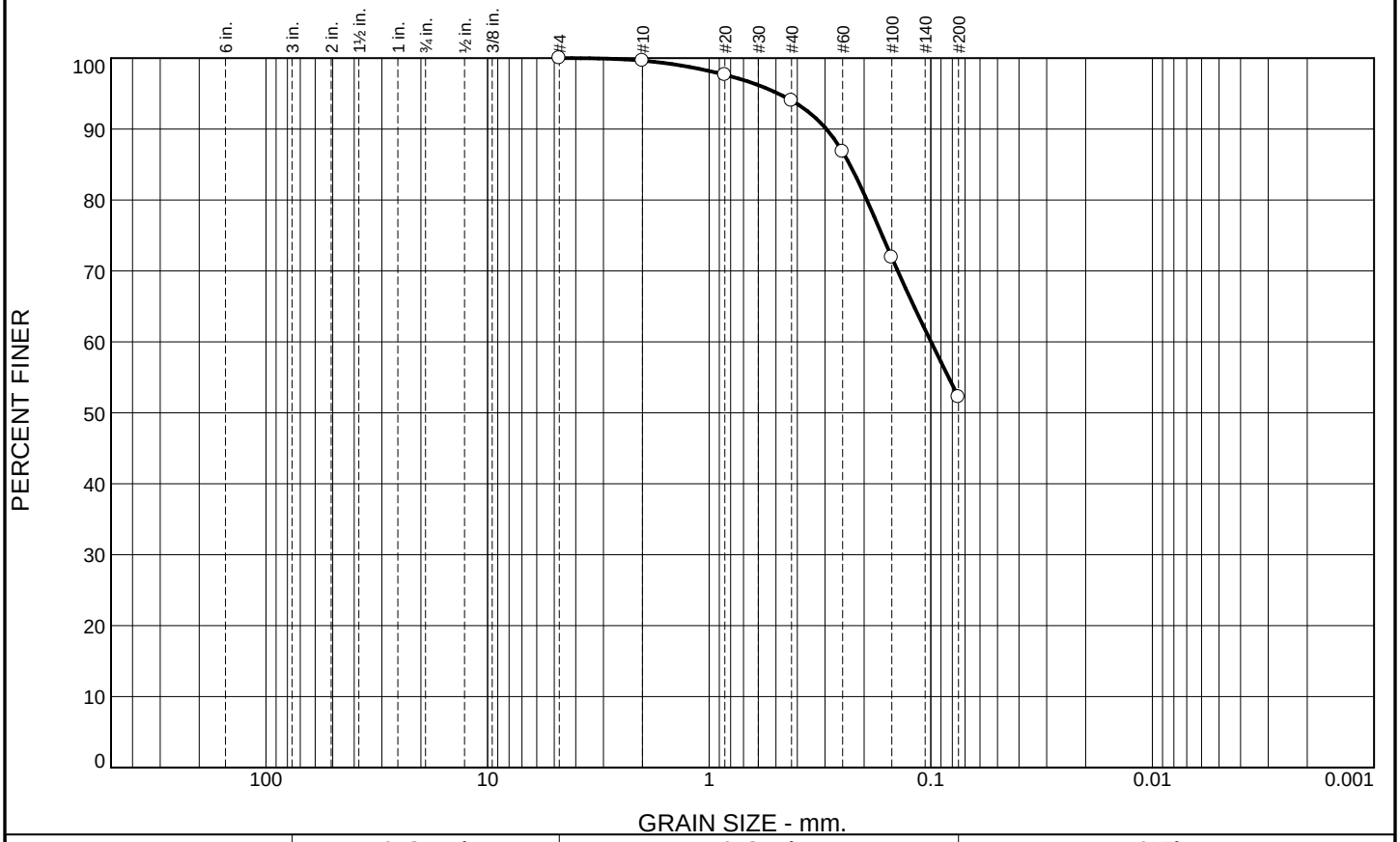

| SOIL DATA | | | | | | | | |
|---|---|---|---|---|---|---|---|---|
| SYMBOL | SOURCE | SAMPLE NO. | DEPTH | NATURAL WATER CONTENT (%) | PLASTIC LIMIT (%) | LIQUID LIMIT (%) | PLASTICITY INDEX (%) | USCS |
| ● | BULK SAMPLES | TP-1E-01 | 2.0'-2.9' | | NP | 24 | NP | SM |

AECOM

**Client:** KESTREL HORIZONS LLC
**Project:** PINEWOOD SITE IMPROVEMENT

**Project No.:** 60186203 **Figure**

# Particle Size Distribution Report




| % +3" | % Gravel | | % Sand | | | % Fines | |
|---|---|---|---|---|---|---|---|
| | Coarse | Fine | Coarse | Medium | Fine | Silt | Clay |
| 0.0 | 0.0 | 0.0 | 0.4 | 5.6 | 41.8 | 52.2 | |

| SIEVE SIZE | PERCENT FINER | SPEC.* PERCENT | PASS? (X=NO) |
|---|---|---|---|
| #4 | 100.0 | | |
| #10 | 99.6 | | |
| #20 | 97.7 | | |
| #40 | 94.0 | | |
| #60 | 86.8 | | |
| #100 | 71.9 | | |
| #200 | 52.2 | | |

* (no specification provided)

**Material Description**

SANDY SILT

**Atterberg Limits**

PL= 28 LL= 40 PI= 12

**Coefficients**

$D_{90}$= 0.2958 $D_{85}$= 0.2319 $D_{60}$= 0.0997
$D_{50}$= $D_{30}$= $D_{15}$=
$D_{10}$= $C_u$= $C_c$=

**Classification**

USCS= ML AASHTO= A-6(4)

**Remarks**

**Source of Sample:** BULK SAMPLES
**Sample Number:** AT-1B-01

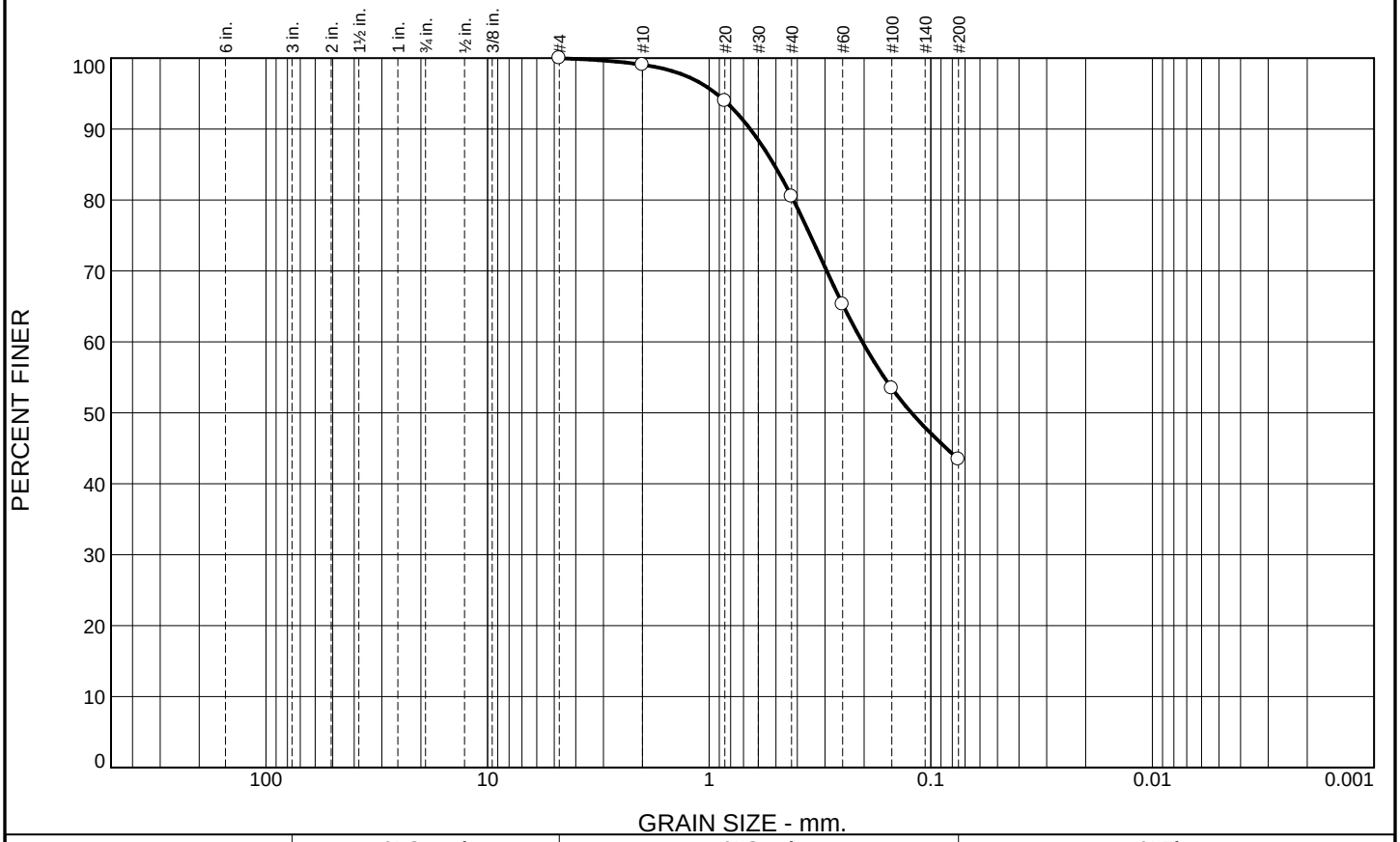
**Date:** 01/05/11

AECOM

**Client:** KESTREL HORIZONS LLC
**Project:** PINEWOOD SITE IMPROVEMENT

**Project No:** 60186203 **Figure**

# Particle Size Distribution Report




| % +3" | % Gravel | | % Sand | | | % Fines | |
|---|---|---|---|---|---|---|---|
| | Coarse | Fine | Coarse | Medium | Fine | Silt | Clay |
| 0.0 | 0.0 | 0.0 | 0.9 | 18.6 | 37.1 | 43.4 | |

| SIEVE SIZE | PERCENT FINER | SPEC.* PERCENT | PASS? (X=NO) |
|---|---|---|---|
| #4 | 100.0 | | |
| #10 | 99.1 | | |
| #20 | 94.0 | | |
| #40 | 80.5 | | |
| #60 | 65.3 | | |
| #100 | 53.5 | | |
| #200 | 43.4 | | |

* (no specification provided)

**Material Description**

SILTY SAND

**Atterberg Limits**

PL= 27 LL= 40 PI= 13

**Coefficients**

$D_{90}$= 0.6522 $D_{85}$= 0.5098 $D_{60}$= 0.2036
$D_{50}$= 0.1223 $D_{30}$= $D_{15}$=
$D_{10}$= $C_u$= $C_c$=

**Classification**

USCS= SM AASHTO= A-6(2)

**Remarks**

**Source of Sample:** BULK SAMPLES
**Sample Number:** AT-1C-01

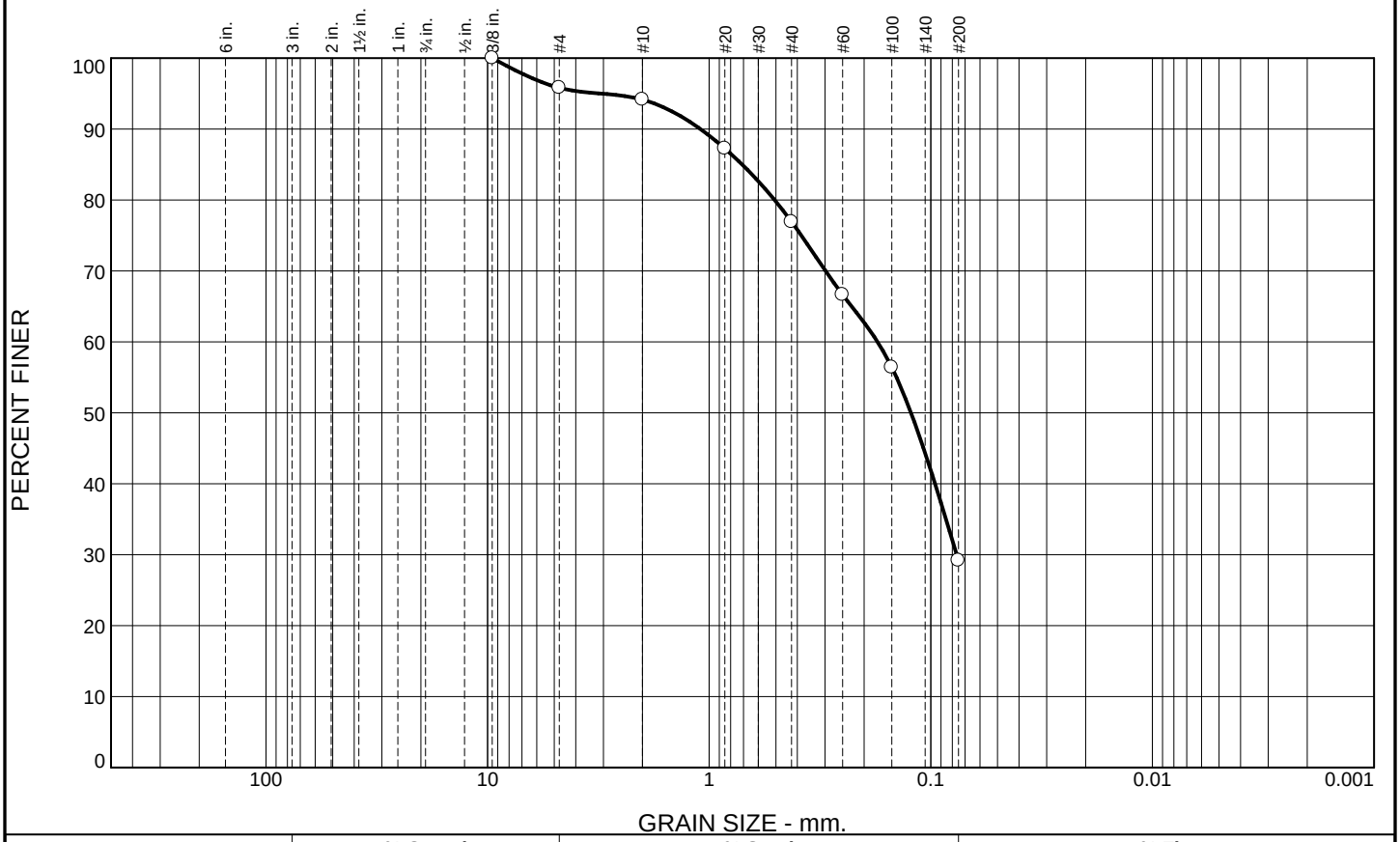
**Date:** 01/05/11

AECOM

**Client:** KESTREL HORIZONS LLC
**Project:** PINEWOOD SITE IMPROVEMENT

**Project No:** 60186203 **Figure**

# Particle Size Distribution Report




| % +3" | % Gravel | | % Sand | | | % Fines | |
|---|---|---|---|---|---|---|---|
| | Coarse | Fine | Coarse | Medium | Fine | Silt | Clay |
| 0.0 | 0.0 | 4.2 | 1.7 | 17.2 | 47.7 | 29.2 | |

| SIEVE SIZE | PERCENT FINER | SPEC.* PERCENT | PASS? (X=NO) |
|---|---|---|---|
| .375 | 100.0 | | |
| #4 | 95.8 | | |
| #10 | 94.1 | | |
| #20 | 87.3 | | |
| #40 | 76.9 | | |
| #60 | 66.7 | | |
| #100 | 56.4 | | |
| #200 | 29.2 | | |

* (no specification provided)

**Material Description**

SILTY CLAYEY FINE TO MEDIUM SAND, TRACE FINE GRAVEL

**Atterberg Limits**

PL= 23 LL= 36 PI= 13

**Coefficients**

$D_{90}$= 1.0947 $D_{85}$= 0.7097 $D_{60}$= 0.1739
$D_{50}$= 0.1228 $D_{30}$= 0.0764 $D_{15}$=
$D_{10}$= $C_u$= $C_c$=

**Classification**

USCS= SC AASHTO= A-2-6(0)

**Remarks**

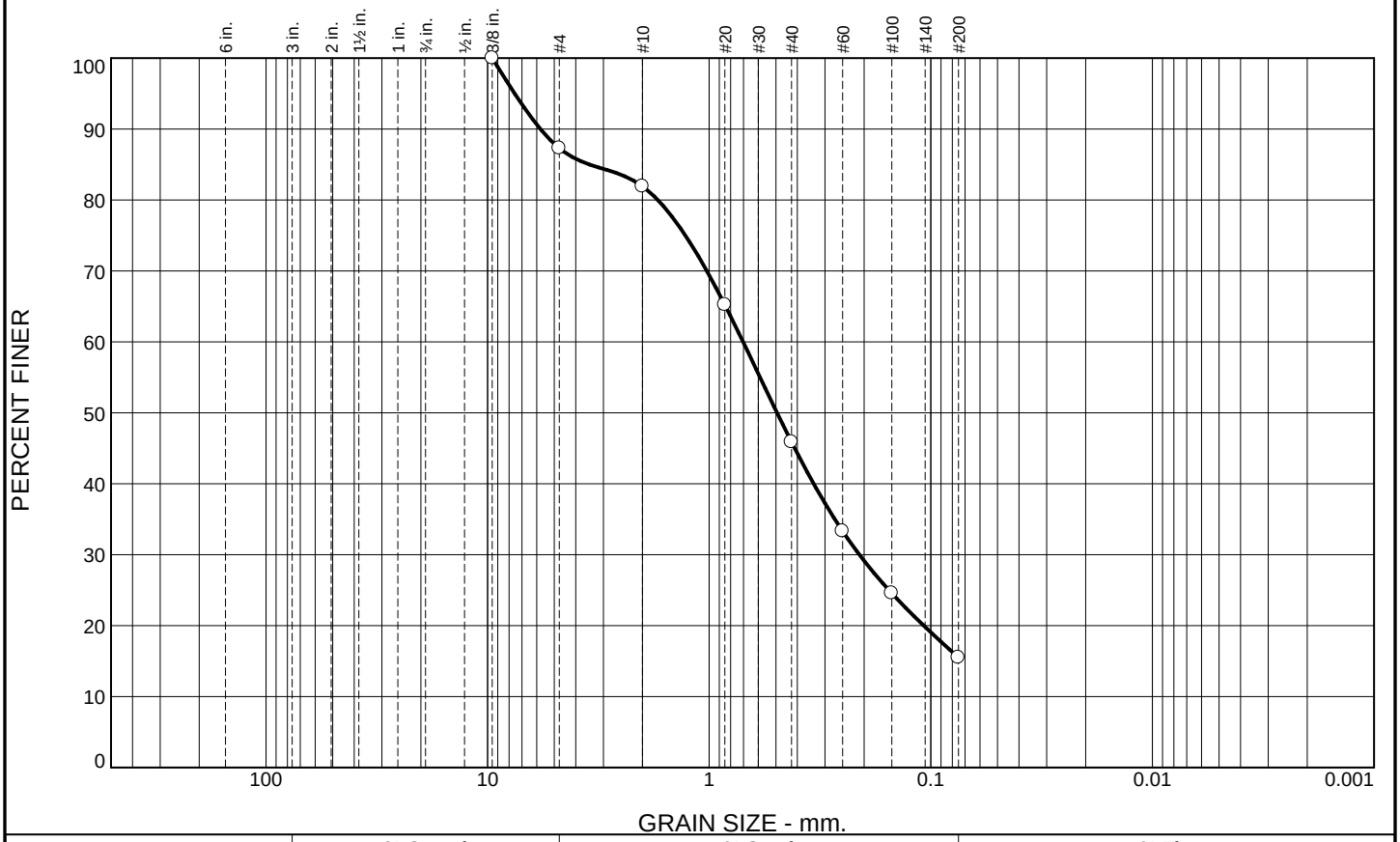
**Source of Sample:** BULK SAMPLES **Depth:** 2.0'-4.0'
**Sample Number:** SB-1B-02 **Date:**

AECOM

**Client:** KESTREL HORIZONS LLC
**Project:** PINEWOOD SITE IMPROVEMENT

**Project No:** 60186203 **Figure**

# Particle Size Distribution Report




| % +3" | % Gravel | | % Sand | | | % Fines | |
|---|---|---|---|---|---|---|---|
| | Coarse | Fine | Coarse | Medium | Fine | Silt | Clay |
| 0.0 | 0.0 | 12.7 | 5.4 | 36.0 | 30.4 | 15.5 | |

| SIEVE SIZE | PERCENT FINER | SPEC.* PERCENT | PASS? (X=NO) |
|---|---|---|---|
| .375 | 100.0 | | |
| #4 | 87.3 | | |
| #10 | 81.9 | | |
| #20 | 65.2 | | |
| #40 | 45.9 | | |
| #60 | 33.3 | | |
| #100 | 24.6 | | |
| #200 | 15.5 | | |

* (no specification provided)

**Material Description**

SILTY FINE TO COARSE SAND, LITTLE FINE GRAVEL

**Atterberg Limits**

PL= 36 LL= 47 PI= 11

**Coefficients**

$D_{90}$= 5.7743 $D_{85}$= 3.4664 $D_{60}$= 0.7028
$D_{50}$= 0.4941 $D_{30}$= 0.2099 $D_{15}$=
$D_{10}$= $C_u$= $C_c$=

**Classification**

USCS= ML AASHTO= A-2-7(0)

**Remarks**

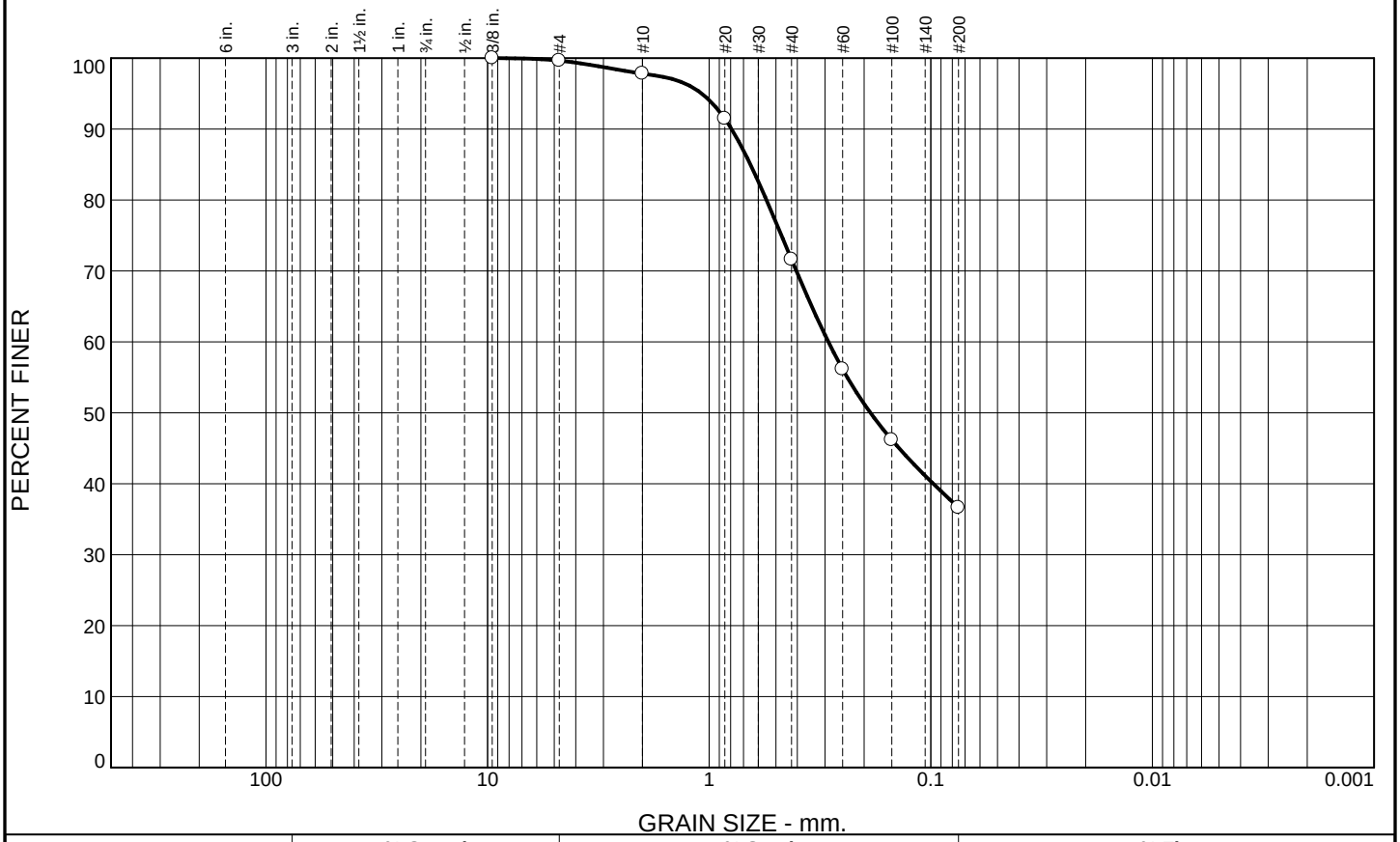
**Source of Sample:** BULK SAMPLES **Depth:** 2.0'-4.0'
**Sample Number:** SB-1D-06 **Date:** 01/04/11

AECOM

**Client:** KESTREL HORIZONS LLC
**Project:** PINEWOOD SITE IMPROVEMENT

**Project No:** 60186203 **Figure**

# Particle Size Distribution Report




| % +3" | % Gravel | | % Sand | | | % Fines | |
|---|---|---|---|---|---|---|---|
| | Coarse | Fine | Coarse | Medium | Fine | Silt | Clay |
| 0.0 | 0.0 | 0.3 | 1.9 | 26.2 | 35.0 | 36.6 | |

| SIEVE SIZE | PERCENT FINER | SPEC.* PERCENT | PASS? (X=NO) |
|---|---|---|---|
| .375 | 100.0 | | |
| #4 | 99.7 | | |
| #10 | 97.8 | | |
| #20 | 91.5 | | |
| #40 | 71.6 | | |
| #60 | 56.2 | | |
| #100 | 46.2 | | |
| #200 | 36.6 | | |

* (no specification provided)

**Material Description**

SILTY FINE TO MEDIUM SAND

**Atterberg Limits**

PL= NP LL= 22 PI= NP

**Coefficients**

$D_{90}$= 0.7919 $D_{85}$= 0.6512 $D_{60}$= 0.2898
$D_{50}$= 0.1873 $D_{30}$= $D_{15}$=
$D_{10}$= $C_u$= $C_c$=

**Classification**

USCS= SM AASHTO= A-4(0)

**Remarks**

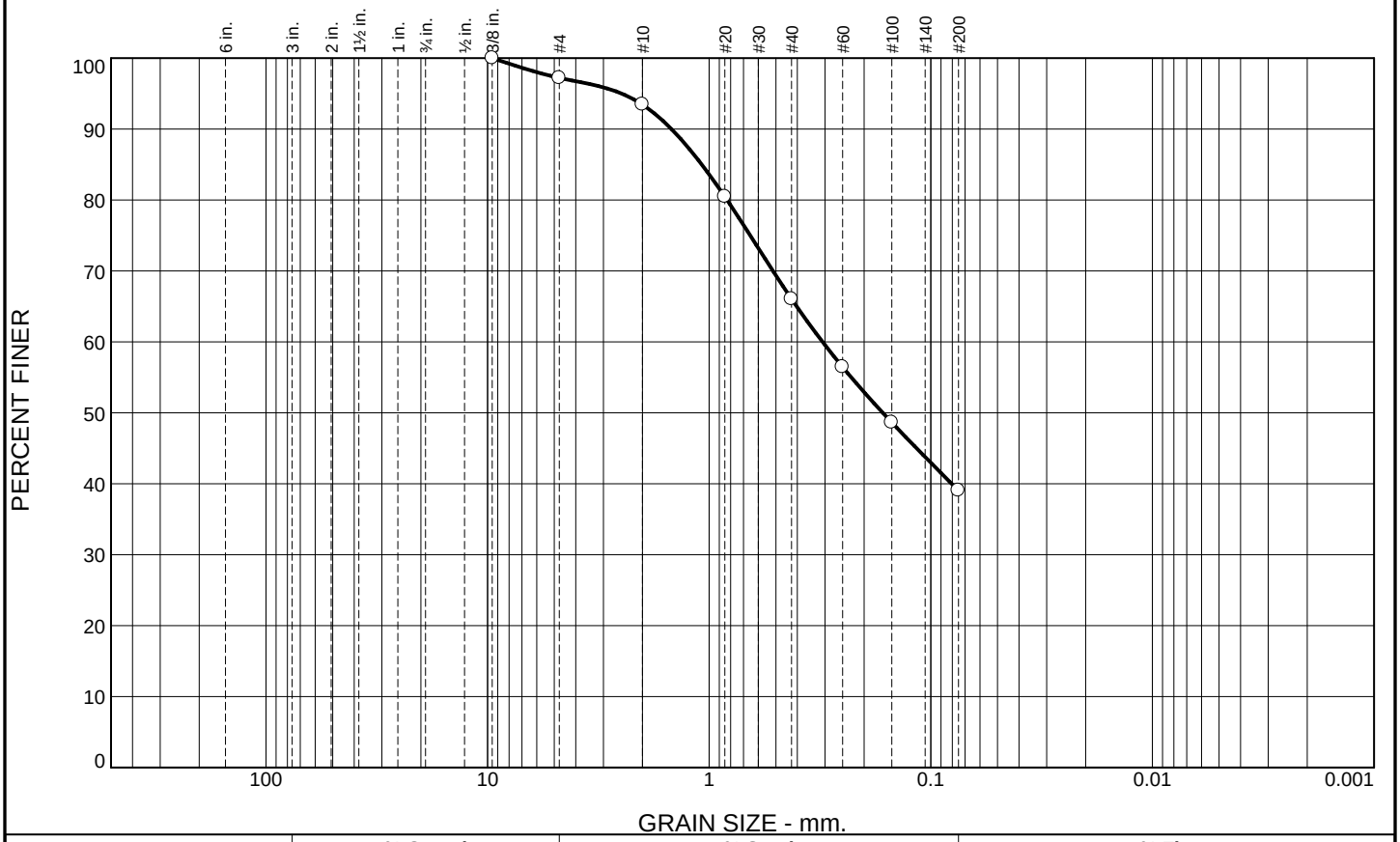
**Source of Sample:** BULK SAMPLES **Depth:** 0.0'-2.0'
**Sample Number:** SB-1D-07 **Date:** 1-26-11

AECOM

**Client:** KESTREL HORIZONS LLC
**Project:** PINEWOOD SITE IMPROVEMENT

**Project No:** 60186203 **Figure**

# Particle Size Distribution Report




| % +3" | % Gravel | | % Sand | | | % Fines | |
|---|---|---|---|---|---|---|---|
| | Coarse | Fine | Coarse | Medium | Fine | Silt | Clay |
| 0.0 | 0.0 | 2.8 | 3.7 | 27.5 | 26.9 | 39.1 | |

| SIEVE SIZE | PERCENT FINER | SPEC.* PERCENT | PASS? (X=NO) |
|---|---|---|---|
| .375 | 100.0 | | |
| #4 | 97.2 | | |
| #10 | 93.5 | | |
| #20 | 80.5 | | |
| #40 | 66.0 | | |
| #60 | 56.5 | | |
| #100 | 48.6 | | |
| #200 | 39.1 | | |

* (no specification provided)

**Material Description**

SILTY FINE TO MEDIUM SAND, TRACE FINE GRAVEL

**Atterberg Limits**

PL= 18 LL= 39 PI= 21

**Coefficients**

$D_{90}$= 1.4796 $D_{85}$= 1.0801 $D_{60}$= 0.3078
$D_{50}$= 0.1647 $D_{30}$= $D_{15}$=
$D_{10}$= $C_u$= $C_c$=

**Classification**

USCS= SC AASHTO= A-6(3)

**Remarks**

**Source of Sample:** BULK SAMPLES
**Sample Number:** TP-1A-01

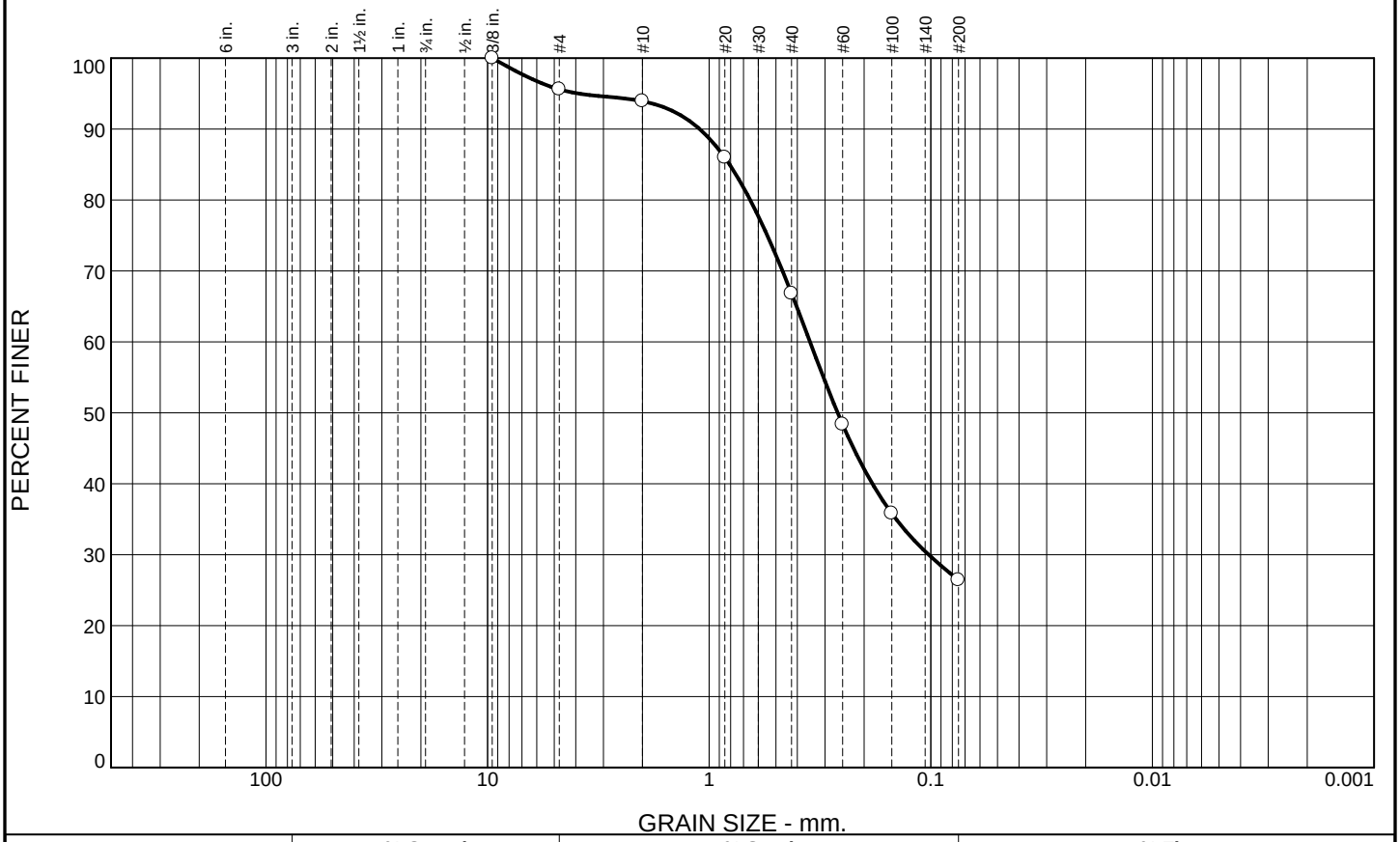
**Date:** 1-26-11

AECOM

**Client:** KESTREL HORIZONS LLC
**Project:** PINEWOOD SITE IMPROVEMENT

**Project No:** 60186203 **Figure**

# Particle Size Distribution Report




| % +3" | % Gravel | | % Sand | | | % Fines | |
|---|---|---|---|---|---|---|---|
| | Coarse | Fine | Coarse | Medium | Fine | Silt | Clay |
| 0.0 | 0.0 | 4.4 | 1.7 | 27.1 | 40.4 | 26.4 | |

| SIEVE SIZE | PERCENT FINER | SPEC.* PERCENT | PASS? (X=NO) |
|---|---|---|---|
| .375 | 100.0 | | |
| #4 | 95.6 | | |
| #10 | 93.9 | | |
| #20 | 86.0 | | |
| #40 | 66.8 | | |
| #60 | 48.4 | | |
| #100 | 35.8 | | |
| #200 | 26.4 | | |

* (no specification provided)

**Material Description**

SILTY FINE TO COARSE SAND, TRACE GRAVEL

**Atterberg Limits**

PL= NP LL= 28 PI= NP

**Coefficients**

$D_{90}$= 1.1038 $D_{85}$= 0.8084 $D_{60}$= 0.3508
$D_{50}$= 0.2632 $D_{30}$= 0.1022 $D_{15}$=
$D_{10}$= $C_u$= $C_c$=

**Classification**

USCS= SM AASHTO= A-2-4(0)

**Remarks**

**Source of Sample:** BULK SAMPLES
**Sample Number:** TP-1D-01

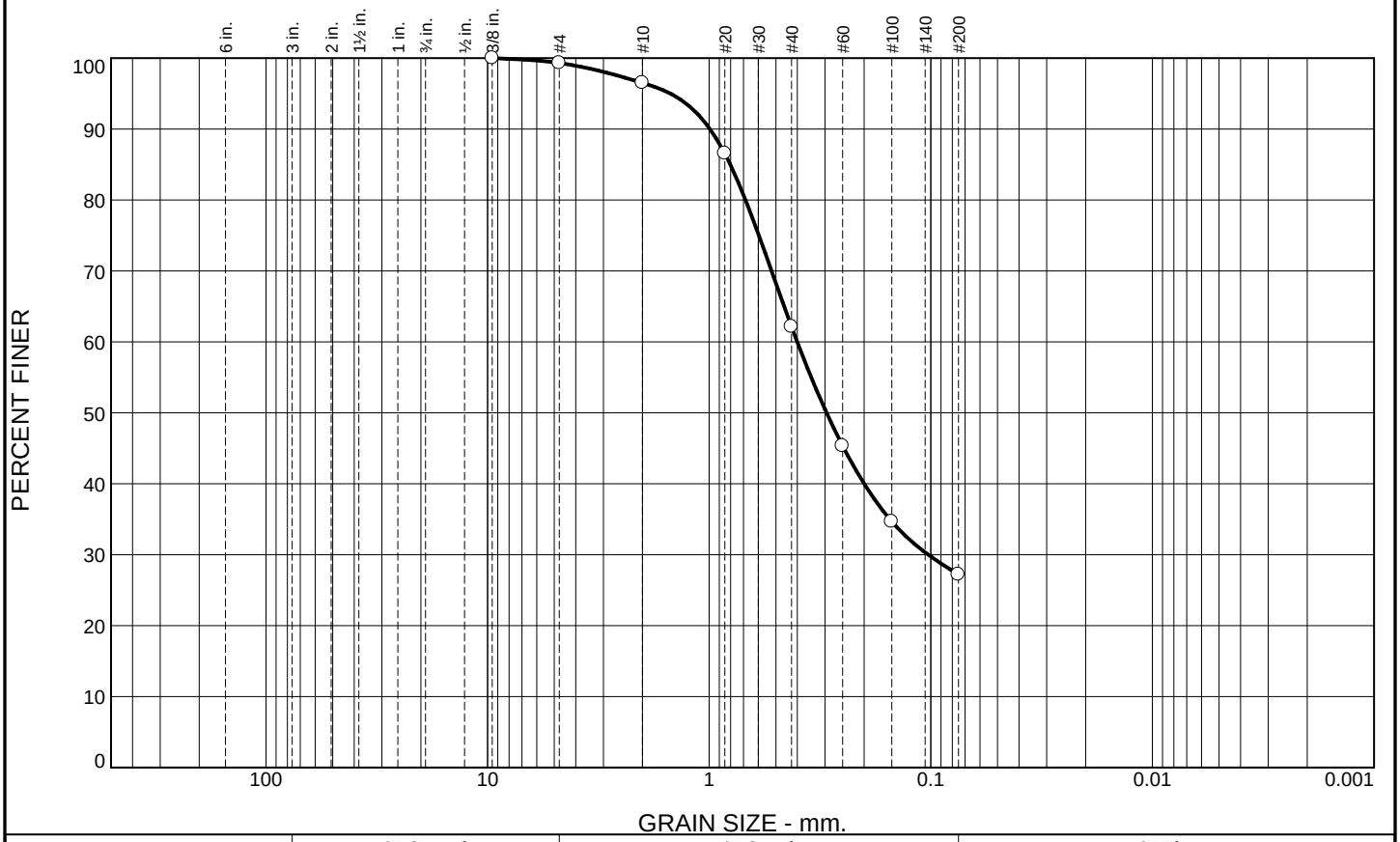
**Date:** 01/19/11

AECOM

**Client:** KESTREL HORIZONS LLC
**Project:** PINEWOOD SITE IMPROVEMENT

**Project No:** 60186203 **Figure**

# Particle Size Distribution Report




| % +3" | % Gravel | | % Sand | | | % Fines | |
|---|---|---|---|---|---|---|---|
| | Coarse | Fine | Coarse | Medium | Fine | Silt | Clay |
| 0.0 | 0.0 | 0.7 | 2.8 | 34.4 | 34.9 | 27.2 | |

| SIEVE SIZE | PERCENT FINER | SPEC.* PERCENT | PASS? (X=NO) |
|---|---|---|---|
| .375 | 100.0 | | |
| #4 | 99.3 | | |
| #10 | 96.5 | | |
| #20 | 86.6 | | |
| #40 | 62.1 | | |
| #60 | 45.3 | | |
| #100 | 34.7 | | |
| #200 | 27.2 | | |

* (no specification provided)

**Material Description**

SILTY FINE TO MEDIUM SAND

**Atterberg Limits**

PL= NP LL= 15 PI= NP

**Coefficients**

$D_{90}$= 0.9912 $D_{85}$= 0.8026 $D_{60}$= 0.4008
$D_{50}$= 0.2952 $D_{30}$= 0.1028 $D_{15}$=
$D_{10}$= $C_u$= $C_c$=

**Classification**

USCS= SM AASHTO= A-2-4(0)

**Remarks**

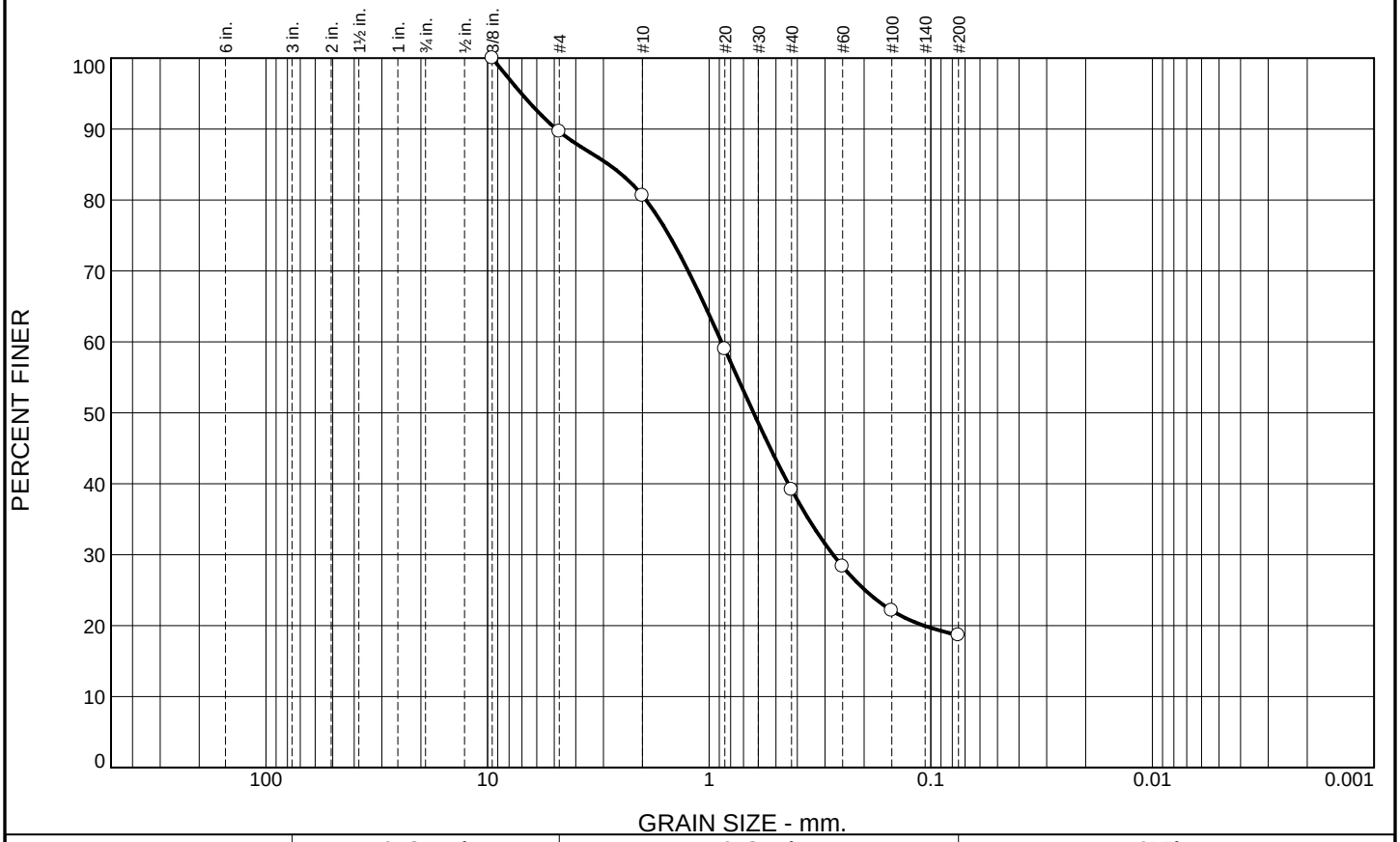
**Source of Sample:** BULK SAMPLES **Depth:** 1.0'-2.0'
**Sample Number:** TP-1D-02 **Date:** 1-26-11

AECOM

**Client:** KESTREL HORIZONS LLC
**Project:** PINEWOOD SITE IMPROVEMENT

**Project No:** 60186203 **Figure**

# Particle Size Distribution Report




| % +3" | % Gravel | | % Sand | | | % Fines | |
|---|---|---|---|---|---|---|---|
| | Coarse | Fine | Coarse | Medium | Fine | Silt | Clay |
| 0.0 | 0.0 | 10.3 | 9.1 | 41.4 | 20.6 | 18.6 | |

| SIEVE SIZE | PERCENT FINER | SPEC.* PERCENT | PASS? (X=NO) |
|---|---|---|---|
| .375 | 100.0 | | |
| #4 | 89.7 | | |
| #10 | 80.6 | | |
| #20 | 59.0 | | |
| #40 | 39.2 | | |
| #60 | 28.3 | | |
| #100 | 22.1 | | |
| #200 | 18.6 | | |

* (no specification provided)

**Material Description**

SILTY FINE TO COARSE SAND, LITTLE FINE GRAVEL

**Atterberg Limits**

PL= 14 LL= 25 PI= 11

**Coefficients**

$D_{90}$= 4.8986 $D_{85}$= 2.8394 $D_{60}$= 0.8796
$D_{50}$= 0.6302 $D_{30}$= 0.2760 $D_{15}$=
$D_{10}$= $C_u$= $C_c$=

**Classification**

USCS= SC AASHTO= A-2-6(0)

**Remarks**

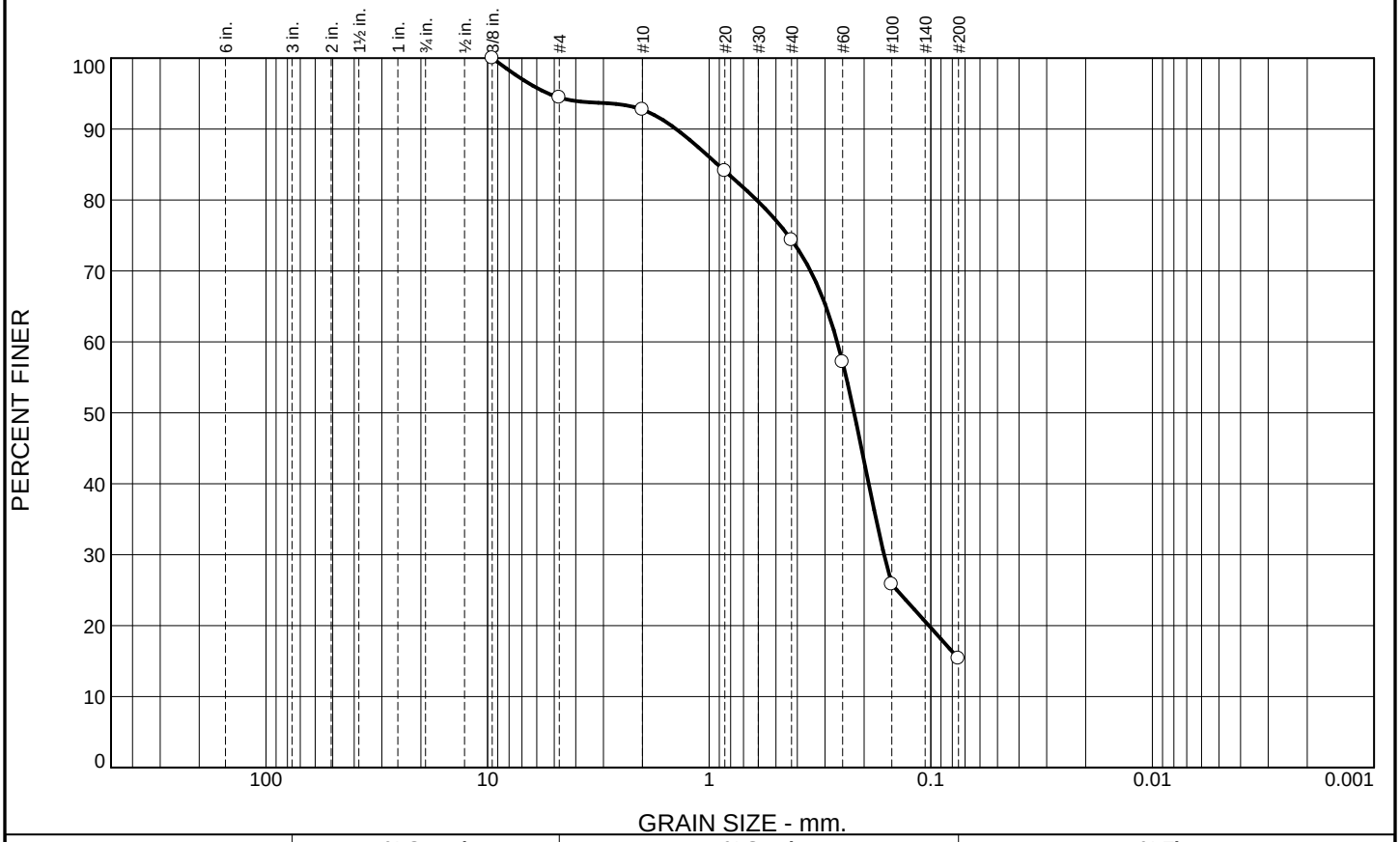
**Source of Sample:** BULK SAMPLES **Depth:** 1.0'-2.0'
**Sample Number:** TP-1E-01 **Date:** 1-26-11

AECOM

**Client:** KESTREL HORIZONS LLC
**Project:** PINEWOOD SITE IMPROVEMENT

**Project No:** 60186203 **Figure**

# Particle Size Distribution Report




| % +3" | % Gravel | | % Sand | | | % Fines | |
|---|---|---|---|---|---|---|---|
| | Coarse | Fine | Coarse | Medium | Fine | Silt | Clay |
| 0.0 | 0.0 | 5.6 | 1.7 | 18.3 | 59.0 | 15.4 | |

| SIEVE SIZE | PERCENT FINER | SPEC.* PERCENT | PASS? (X=NO) |
|---|---|---|---|
| .375 | 100.0 | | |
| #4 | 94.4 | | |
| #10 | 92.7 | | |
| #20 | 84.1 | | |
| #40 | 74.4 | | |
| #60 | 57.2 | | |
| #100 | 25.8 | | |
| #200 | 15.4 | | |

* (no specification provided)

**Material Description**

SILTY FINE TO MEDIUM SAND, TRACE FINE GRAVEL

**Atterberg Limits**

PL= NP LL= 24 PI= NP

**Coefficients**

$D_{90}$= 1.4097 $D_{85}$= 0.9154 $D_{60}$= 0.2643
$D_{50}$= 0.2217 $D_{30}$= 0.1625 $D_{15}$=
$D_{10}$= $C_u$= $C_c$=

**Classification**

USCS= SM AASHTO= A-2-4(0)

**Remarks**

**Source of Sample:** BULK SAMPLES **Depth:** 2.0'-2.9'
**Sample Number:** TP-1E-01 **Date:** 1-28-11

AECOM

**Client:** KESTREL HORIZONS LLC
**Project:** PINEWOOD SITE IMPROVEMENT

**Project No:** 60186203 **Figure**

TRI / Environmental, Inc.

January 18, 2011
February 8, 2011 Updated with Percent Plasticizer

**Mail To:**

**Attn: Sharon Korleski**
**AECOM**
10 Patewood Drive
Greenville, SC 29615

email: sharon.korleski@aecom.com

**Bill To:**

**<= Same**
**Project # : 60186203**

Dear Ms. Korleski:

Thank you for consulting TRI/Environmental, Inc. (TRI) for your geosynthetics testing needs. TRI is pleased to submit this final report for laboratory testing.

| | |
|---|---|
| Project: | **Pine Wood, Project # : 60186203** |
| TRI Job Reference Number: | E2352-06-10 |
| Material(s) Tested: | 10 Exposed PVC Liners |
| Test(s) Requested: | Thickness (ASTM D 5199<br>Tensile Properties (ASTM D 882)<br>Peel & Shear (ASTM D 6392/GRI GM19/D 4437/NSF 54, D6214) |
| Updated====> | Percent Plasticizer Content ( ASTM D 2124 ) |

If you have any questions or require any additional information, please call us at 1-800-880-8378.

Sincerely,

Mansukh Patel
Sr. Laboratory Coordinator
Geosynthetic Services Division
www.GeosyntheticTesting.com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# LABORATORY TEST RESULTS

**TRI Client: AECOM**
**Project: Pine Wood, Project # : 60186203**

**Material: Exposed PVC Liner**
**Sample Identification: AT-1B-01**
**TRI Log #: E2352-06-10**

| PARAMETER | TEST REPLICATE NUMBER | | | | | | | | | | MEAN | STD. DEV. |
|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | | |
| **Thickness (ASTM D 5199)** | | | | | | | | | | | | |
| Thickness (mils) | 18.3 | 18.2 | 18.1 | 16.5 | 18.1 | 18.3 | 18.6 | 18.9 | 18.4 | 18.8 | **18.2** | 0.7 |
| | | | | | | | | | | | **16.5** | << min |
| **Tensile Properties (ASTM D 882, 20 ipm strain rate)** | | | | | | | | | | | | |
| A Strength @ 100% Strain (ppi) | 47.1 | 47.3 | 49.1 | 54.1 | 44.4 | | | | | | **48.4** | 3.6 |
| B Strength @ 100% Strain (ppi) | 46.4 | 46.7 | 49.8 | 47.5 | 48.4 | | | | | | **47.7** | 1.4 |
| A Break Strength (ppi) | 52.6 | 54.6 | 55.7 | 54.9 | 57.1 | | | | | | **55.0** | 1.6 |
| B Break Strength (ppi) | 58.8 | 55.9 | 51.2 | 50.4 | 52.6 | | | | | | **53.8** | 3.5 |
| A Break Elongation (%) | 176 | 197 | 196 | 147 | 276 | | | | | | **198** | 48 |
| B Break Elongation (%) | 334 | 235 | 133 | 139 | 203 | | | | | | **209** | 82 |




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# LABORATORY TEST RESULTS

**TRI Client: AECOM**
**Project: Pine Wood, Project # : 60186203**

**Material: Exposed PVC Liner**
**Sample Identification: AT-1A-01**
**TRI Log #: E2352-06-10**

| PARAMETER | TEST REPLICATE NUMBER | | | | | | | | | | MEAN | STD. DEV. |
|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | | |
| **Thickness (ASTM D 5199)** | | | | | | | | | | | | |
| Thickness (mils) | 17.3 | 17.0 | 16.5 | 17.1 | 16.5 | 16.4 | 15.6 | 17.9 | 16.3 | 16.4 | **16.7** | 0.6 |
| | | | | | | | | | | | **15.6** | << min |
| **Tensile Properties (ASTM D 882, 20 ipm strain rate)** | | | | | | | | | | | | |
| A Strength @ 100% Strain (ppi) | 55.9 | 52.0 | 54.5 | 52.6 | 55.7 | | | | | | **54.1** | 1.8 |
| B Strength @ 100% Strain (ppi) | 48.7 | 53.4 | 53.2 | 50.0 | 46.1 | | | | | | **50.3** | 3.1 |
| A Break Strength (ppi) | 59.5 | 60.9 | 61.8 | 62.6 | 56.9 | | | | | | **60.3** | 2.2 |
| B Break Strength (ppi) | 51.2 | 53.4 | 53.2 | 54.2 | 50.8 | | | | | | **52.6** | 1.5 |
| A Break Elongation (%) | 181 | 241 | 228 | 255 | 144 | | | | | | **210** | 46 |
| B Break Elongation (%) | 175 | 115 | 117 | 268 | 213 | | | | | | **178** | 65 |
| **Plasticizer Content (ASTM D 2124)** | | | | | | | | | | | | |
| % Plasticizers Content: | | | | 16.3 | | | | | | | **16.3** | |




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# LABORATORY TEST RESULTS

**TRI Client: AECOM**
**Project: Pine Wood, Project # : 60186203**

**Material: Exposed PVC Liner**
**Sample Identification: AT-1C-01**
**TRI Log #: E2352-06-10**

| PARAMETER | TEST REPLICATE NUMBER | | | | | | | | | | MEAN | STD. DEV. |
|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | | |
| **Thickness (ASTM D 5199)** | | | | | | | | | | | | |
| Thickness (mils) | 20.9 | 20.0 | 20.5 | 20.0 | 19.8 | 20.4 | 20.9 | 20.4 | 19.9 | 19.8 | **20.2** | 0.4 |
| | | | | | | | | | | | **19.8** | << min |
| **Tensile Properties (ASTM D 882, 20 ipm strain rate)** | | | | | | | | | | | | |
| A Strength @ 100% Strain (ppi) | 41.9 | 40.4 | 41.4 | 42.5 | 42.5 | | | | | | **41.7** | 0.9 |
| B Strength @ 100% Strain (ppi) | 37.4 | 40.4 | 39.2 | 37.2 | 37.0 | | | | | | **38.2** | 1.5 |
| A Break Strength (ppi) | 59.3 | 60.8 | 61.1 | 57.7 | 52.6 | | | | | | **58.3** | 3.4 |
| B Break Strength (ppi) | 50.7 | 47.7 | 45.4 | 58.9 | 58.0 | | | | | | **52.2** | 6.1 |
| A Break Elongation (%) | 271 | 308 | 285 | 254 | 231 | | | | | | **270** | 29 |
| B Break Elongation (%) | 241 | 194 | 181 | 364 | 349 | | | | | | **266** | 86 |
| * Seam panel tested | | | | | | | | | | | | |
| **Peel and Shear (ASTM D 6392/GRI GM19/D 4437/NSF 54)** | | | | | | | | | | | | |
| Peel Strength (ppi) | | | | 20.7 | 18.1 | 17.0 | 20.5 | 14.3 | | | 18 | |
| Peel Incursion (%) | | | | 100 | 100 | 100 | 100 | 100 | | | | |
| Peel Locus of Failure Code | | | | AD | AD | AD | AD | AD | | | | |
| Peel NSF Failure Code | | | | NON-FTB | NON-FTB | NON-FTB | NON-FTB | NON-FTB | | | | |
| | | | | | | | | | | | Shear | |
| Shear Strength (ppi) | | | | 49.7 | 47.9 | 43.6 | 41.5 | 45.3 | | | 46 | |
| Shear Elongation @ Break (%) | | | | >50 | >50 | >50 | >50 | >50 | | | | |

**AD** Adhesion failure (100% Peel)
**NON-FTB** 100% peel




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# LABORATORY TEST RESULTS

**TRI Client: AECOM**
**Project: Pine Wood, Project # : 60186203**

**Material: Exposed PVC Liner**
**Sample Identification: TP-1D-01**
**TRI Log #: E2352-06-10**

| PARAMETER | TEST REPLICATE NUMBER | | | | | | | | | | MEAN | STD. DEV. |
|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | | |
| **Thickness (ASTM D 5199)** | | | | | | | | | | | | |
| Thickness (mils) | 20.5 | 20.3 | 19.4 | 19.7 | 20.3 | 20.4 | 20.6 | 20.7 | 21.0 | 20.8 | **20.3** | 0.5 |
| | | | | | | | | | | | **19.4** | << min |
| **Tensile Properties (ASTM D 882, 20 ipm strain rate)** | | | | | | | | | | | | |
| A Strength @ 100% Strain (ppi) | 31.1 | 31.3 | 29.5 | 31.5 | 32.6 | | | | | | **31.2** | 1.1 |
| B Strength @ 100% Strain (ppi) | 35.1 | 34.5 | 34.8 | 35.0 | 33.7 | | | | | | **34.6** | 0.6 |
| A Break Strength (ppi) | 55.1 | 54.3 | 56.7 | 53.3 | 57.1 | | | | | | **55.3** | 1.6 |
| B Break Strength (ppi) | 54.6 | 57.0 | 43.8 | 55.9 | 57.5 | | | | | | **53.8** | 5.7 |
| A Break Elongation (%) | 451 | 451 | 525 | 426 | 456 | | | | | | **462** | 37 |
| B Break Elongation (%) | 350 | 372 | 241 | 380 | 417 | | | | | | **352** | 67 |




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# LABORATORY TEST RESULTS

**TRI Client: AECOM**
**Project: Pine Wood, Project # : 60186203**

**Material: Exposed PVC Liner**
**Sample Identification: AT-1E-01**
**TRI Log #: E2352-06-10**

| PARAMETER | TEST REPLICATE NUMBER | | | | | | | | | | MEAN | STD. DEV. |
|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | | |
| **Thickness (ASTM D 5199)** | | | | | | | | | | | | |
| Thickness (mils) | 18.9 | 19.1 | 19.7 | 20.2 | 20.1 | 19.8 | 19.4 | 20.2 | 19.7 | 19.4 | **19.6** | 0.4 |
| | | | | | | | | | | | **18.9** | << min |
| **Tensile Properties (ASTM D 882, 20 ipm strain rate)** | | | | | | | | | | | | |
| A Strength @ 100% Strain (ppi) | 36.5 | 34.2 | 35.3 | 33.0 | 33.6 | | | | | | **34.5** | 1.4 |
| B Strength @ 100% Strain (ppi) | 34.4 | 31.8 | 31.5 | 32.4 | 31.5 | | | | | | **32.3** | 1.2 |
| A Break Strength (ppi) | 54.0 | 51.4 | 47.2 | 29.7 | 35.6 | | | | | | **43.6** | 10.5 |
| B Break Strength (ppi) | 35.8 | 48.5 | 39.9 | 48.7 | 49.6 | | | | | | **44.5** | 6.2 |
| A Break Elongation (%) | 331 | 305 | 237 | 124 | 164 | | | | | | **232** | 89 |
| B Break Elongation (%) | 137 | 299 | 251 | 300 | 328 | | | | | | **263** | 76 |
| * Seam panel tested | | | | | | | | | | | | |
| **Peel and Shear (ASTM D 6392/GRI GM19/D 4437/NSF 54)** | | | | | | | | | | | | |
| | | | | | | | | | | | Shear | |
| Shear Strength (ppi) | | | | 46.9 | 44.2 | 48.4 | 46.8 | 48.9 | | | 47 | |
| Shear Elongation @ Break (%) | | | | >50 | >50 | >50 | >50 | >50 | | | | |




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# LABORATORY TEST RESULTS

**TRI Client: AECOM**
**Project: Pine Wood, Project # : 60186203**

**Material: Exposed PVC Liner**
**Sample Identification: AT-1E-02**
**TRI Log #: E2352-06-10**

| PARAMETER | TEST REPLICATE NUMBER | | | | | | | | | | MEAN | STD. DEV. |
|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | | |
| **Thickness (ASTM D 5199)** | | | | | | | | | | | | |
| Thickness (mils) | 19.3 | 19.1 | 19.4 | 18.9 | 18.9 | 19.0 | 19.1 | 19.5 | 19.6 | 19.3 | **19.2** | 0.3 |
| | | | | | | | | | | | **18.9** | << min |
| **Tensile Properties (ASTM D 882, 20 ipm strain rate)** | | | | | | | | | | | | |
| A Strength @ 100% Strain (ppi) | 36.1 | 37.2 | 35.7 | 35.9 | 36.8 | | | | | | **36.4** | 0.6 |
| B Strength @ 100% Strain (ppi) | 35.5 | 35.9 | 34.2 | 35.4 | 37.9 | | | | | | **35.8** | 1.4 |
| A Break Strength (ppi) | 50.2 | 44.2 | 52.6 | 51.3 | 53.3 | | | | | | **50.3** | 3.6 |
| B Break Strength (ppi) | 52.3 | 50.7 | 53.9 | 52.5 | 54.9 | | | | | | **52.9** | 1.6 |
| A Break Elongation (%) | 270 | 216 | 308 | 287 | 310 | | | | | | **278** | 38 |
| B Break Elongation (%) | 325 | 288 | 352 | 310 | 342 | | | | | | **323** | 25 |




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# LABORATORY TEST RESULTS

**TRI Client: AECOM**
**Project: Pine Wood, Project # : 60186203**

**Material: Exposed PVC Liner**
**Sample Identification: TP-1A-01 - Upper**
**TRI Log #: E2352-06-10**

| PARAMETER | TEST REPLICATE NUMBER | | | | | | | | | | MEAN | STD. DEV. |
|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | | |
| **Thickness (ASTM D 5199)** | | | | | | | | | | | | |
| Thickness (mils) | 18.3 | 18.5 | 18.2 | 18.4 | 18.4 | 18.4 | 18.6 | 19.3 | 19.0 | 19.2 | **18.6** | 0.4 |
| | | | | | | | | | | | **18.2** | << min |
| **Tensile Properties (ASTM D 882, 20 ipm strain rate)** | | | | | | | | | | | | |
| A Strength @ 100% Strain (ppi) | 35.4 | 36.1 | 37.7 | 36.9 | 37.3 | | | | | | **36.6** | 0.9 |
| B Strength @ 100% Strain (ppi) | 32.1 | 31.5 | 32.8 | 30.0 | 29.6 | | | | | | **31.2** | 1.4 |
| A Break Strength (ppi) | 52.4 | 49.3 | 56.2 | 52.7 | 57.7 | | | | | | **53.7** | 3.3 |
| B Break Strength (ppi) | 50.4 | 47.9 | 46.1 | 43.6 | 42.0 | | | | | | **46.0** | 3.3 |
| A Break Elongation (%) | 307 | 243 | 324 | 278 | 356 | | | | | | **302** | 43 |
| B Break Elongation (%) | 338 | 325 | 285 | 289 | 271 | | | | | | **302** | 28 |




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# LABORATORY TEST RESULTS

**TRI Client: AECOM**
**Project: Pine Wood, Project # : 60186203**

**Material: Exposed PVC Liner**
**Sample Identification: TP-1A-01 - Lower**
**TRI Log #: E2352-06-10**

| PARAMETER | TEST REPLICATE NUMBER | | | | | | | | | | MEAN | STD. DEV. |
|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | | |
| **Thickness (ASTM D 5199)** | | | | | | | | | | | | |
| Thickness (mils) | 18.6 | 18.7 | 18.8 | 18.9 | 18.8 | 18.5 | 18.9 | 18.7 | 18.6 | 19.6 | **18.8** | 0.3 |
| | | | | | | | | | | | **18.5** | << min |
| **Tensile Properties (ASTM D 882, 20 ipm strain rate)** | | | | | | | | | | | | |
| A Strength @ 100% Strain (ppi) | 35.5 | 37.4 | 37.8 | 34.8 | 35.6 | | | | | | **36.2** | 1.3 |
| B Strength @ 100% Strain (ppi) | 30.4 | 30.1 | 30.8 | 30.3 | 32.7 | | | | | | **30.9** | 1.0 |
| A Break Strength (ppi) | 49.2 | 51.6 | 56.2 | 53.1 | 44.9 | | | | | | **51.0** | 4.3 |
| B Break Strength (ppi) | 51.5 | 49.2 | 48.1 | 50.5 | 49.2 | | | | | | **49.7** | 1.3 |
| A Break Elongation (%) | 261 | 287 | 343 | 316 | 216 | | | | | | **285** | 49 |
| B Break Elongation (%) | 427 | 368 | 336 | 380 | 322 | | | | | | **367** | 41 |




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# LABORATORY TEST RESULTS

**TRI Client: AECOM**
**Project: Pine Wood, Project # : 60186203**

**Material: Exposed PVC Liner**
**Sample Identification: TP-1E-01**
**TRI Log #: E2352-06-10**

| PARAMETER | TEST REPLICATE NUMBER | | | | | | | | | | MEAN | STD. DEV. |
|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | | |
| **Thickness (ASTM D 5199** | | | | | | | | | | | | |
| Thickness (mils) | 19.8 | 20.5 | 20.1 | 20.5 | 20.5 | 20.0 | 19.5 | 19.3 | 19.2 | 19.4 | **19.9** | 0.5 |
| | | | | | | | | | | | **19.2** | << min |
| **Tensile Properties (ASTM D 882, 20 ipm strain rate)** | | | | | | | | | | | | |
| A Strength @ 100% Strain (ppi) | 37.5 | 36.6 | 37.0 | 35.7 | 35.2 | | | | | | **36.4** | 0.9 |
| B Strength @ 100% Strain (ppi) | 30.3 | 30.6 | 31.0 | 30.1 | 31.3 | | | | | | **30.6** | 0.5 |
| A Break Strength (ppi) | 60.3 | 60.3 | 61.1 | 58.3 | 52.6 | | | | | | **58.5** | 3.5 |
| B Break Strength (ppi) | 44.5 | 46.0 | 53.1 | 47.1 | 47.9 | | | | | | **47.7** | 3.3 |
| A Break Elongation (%) | 347 | 349 | 353 | 346 | 292 | | | | | | **337** | 26 |
| B Break Elongation (%) | 298 | 310 | 407 | 323 | 331 | | | | | | **334** | 43 |




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# LABORATORY TEST RESULTS

**TRI Client: AECOM**
**Project: Pine Wood, Project # : 60186203**

**Material: Exposed PVC Liner**
**Sample Identification: TP-1D-02**
**TRI Log #: E2352-06-10**

| PARAMETER | TEST REPLICATE NUMBER | | | | | | | | | | MEAN | STD. DEV. |
|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | | |
| **Thickness (ASTM D 5199)** | | | | | | | | | | | | |
| Thickness (mils) | 19.3 | 18.3 | 18.5 | 18.3 | 18.6 | 18.5 | 18.5 | 18.8 | 18.6 | 19.0 | **18.6** | 0.3 |
| | | | | | | | | | | | **18.3** | << min |
| **Tensile Properties (ASTM D 882, 20 ipm strain rate)** | | | | | | | | | | | | |
| A Strength @ 100% Strain (ppi) | 36.8 | 36.2 | 34.2 | 34.7 | 33.2 | | | | | | **35.0** | 1.5 |
| B Strength @ 100% Strain (ppi) | 31.8 | 32.2 | 32.3 | 31.3 | 30.7 | | | | | | **31.7** | 0.7 |
| A Break Strength (ppi) | 60.8 | 55.3 | 56.9 | 54.5 | 55.7 | | | | | | **56.6** | 2.5 |
| B Break Strength (ppi) | 54.7 | 51.7 | 54.0 | 44.6 | 53.3 | | | | | | **51.7** | 4.1 |
| A Break Elongation (%) | 354 | 322 | 362 | 319 | 352 | | | | | | **342** | 20 |
| B Break Elongation (%) | 375 | 348 | 395 | 269 | 400 | | | | | | **357** | 53 |




**GeosyntheticTesting.com**
9063 Bee Caves Road / Austin, TX 78733 / 512 263 2101 / fax: 512 263 2558

# Appendix 2.3-1
# Leachate Evaluation Trend Plots

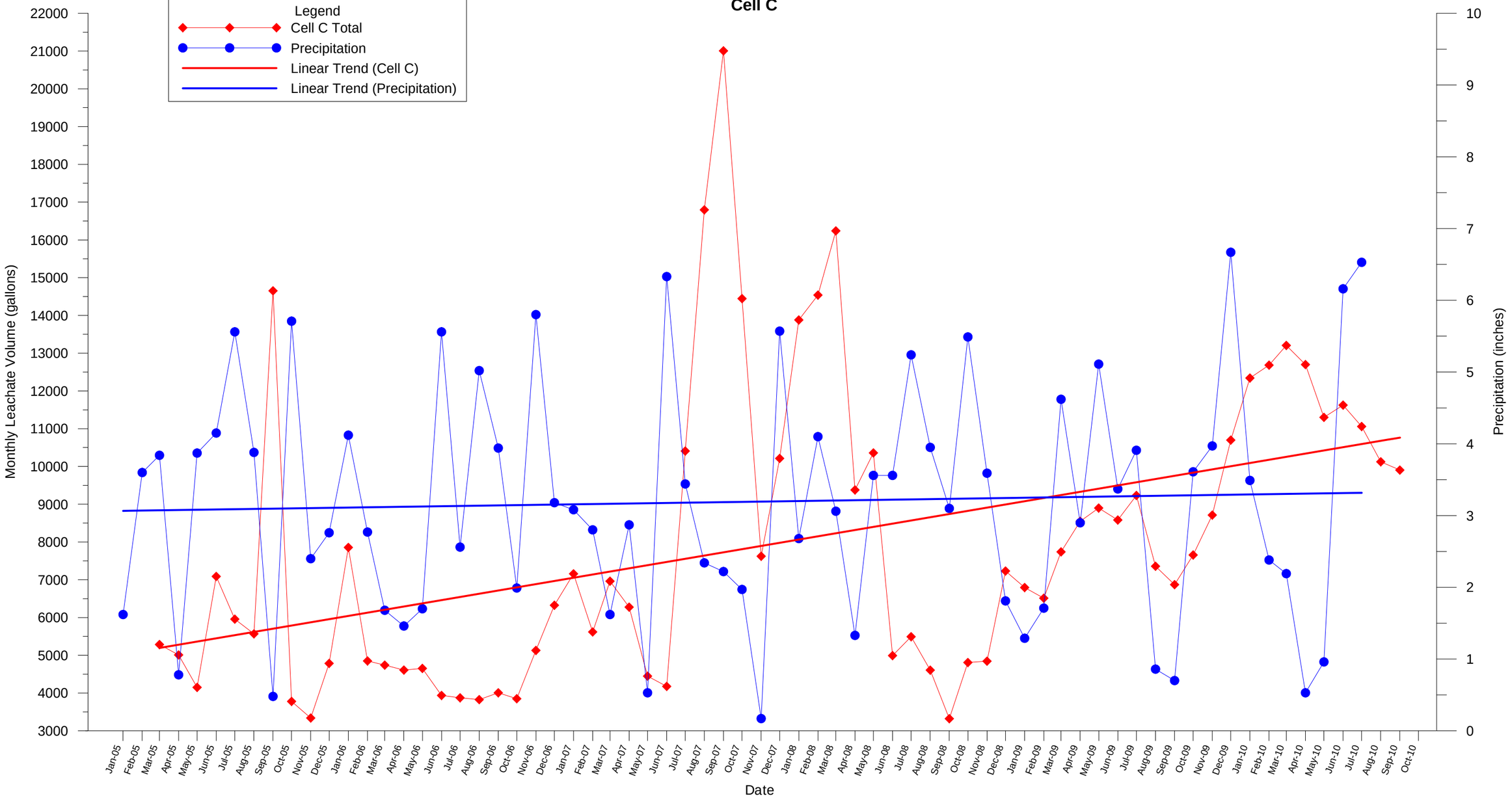
Monthly Rainfall vs. Leachate Production

5-Month Running Average Rainfall vs. Leachate Production

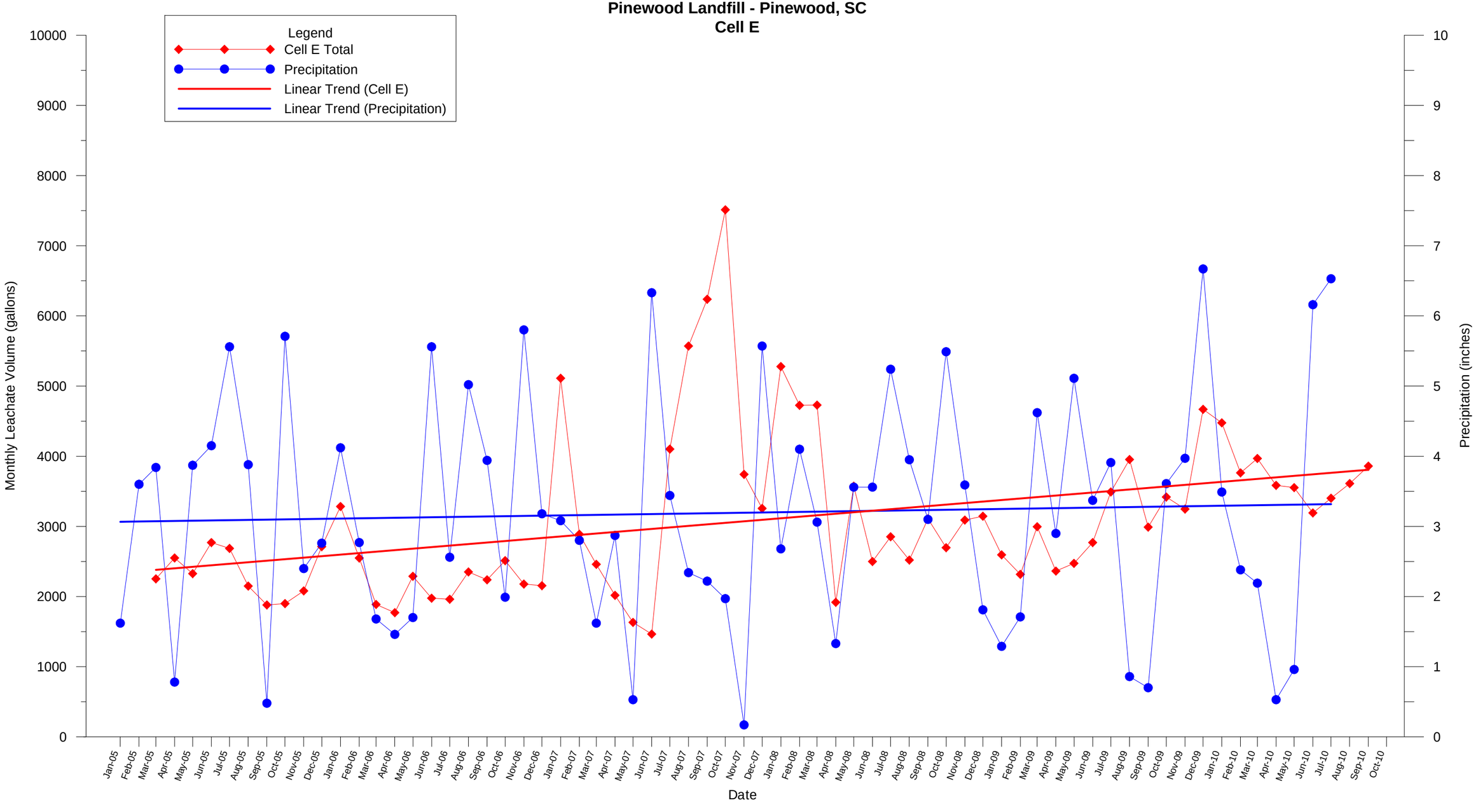
Rainfall Departure vs. Leachate Trend

# Monthly Rainfall vs. Leachate Production

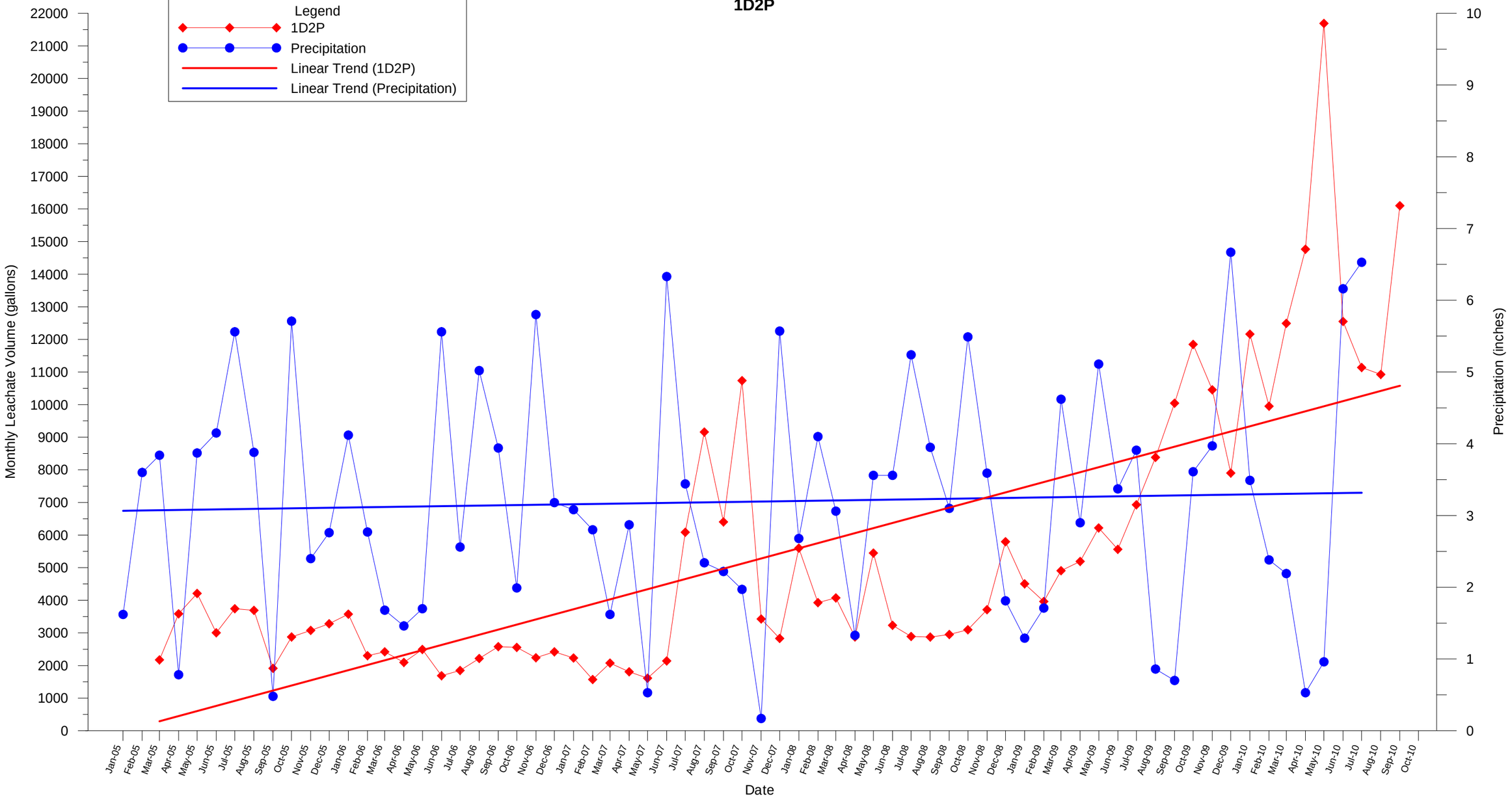
# Section I Primary Leachate Data and Precipitation
## March 2005 - September 2010
## Pinewood Landfill - Pinewood, SC
## Cell C



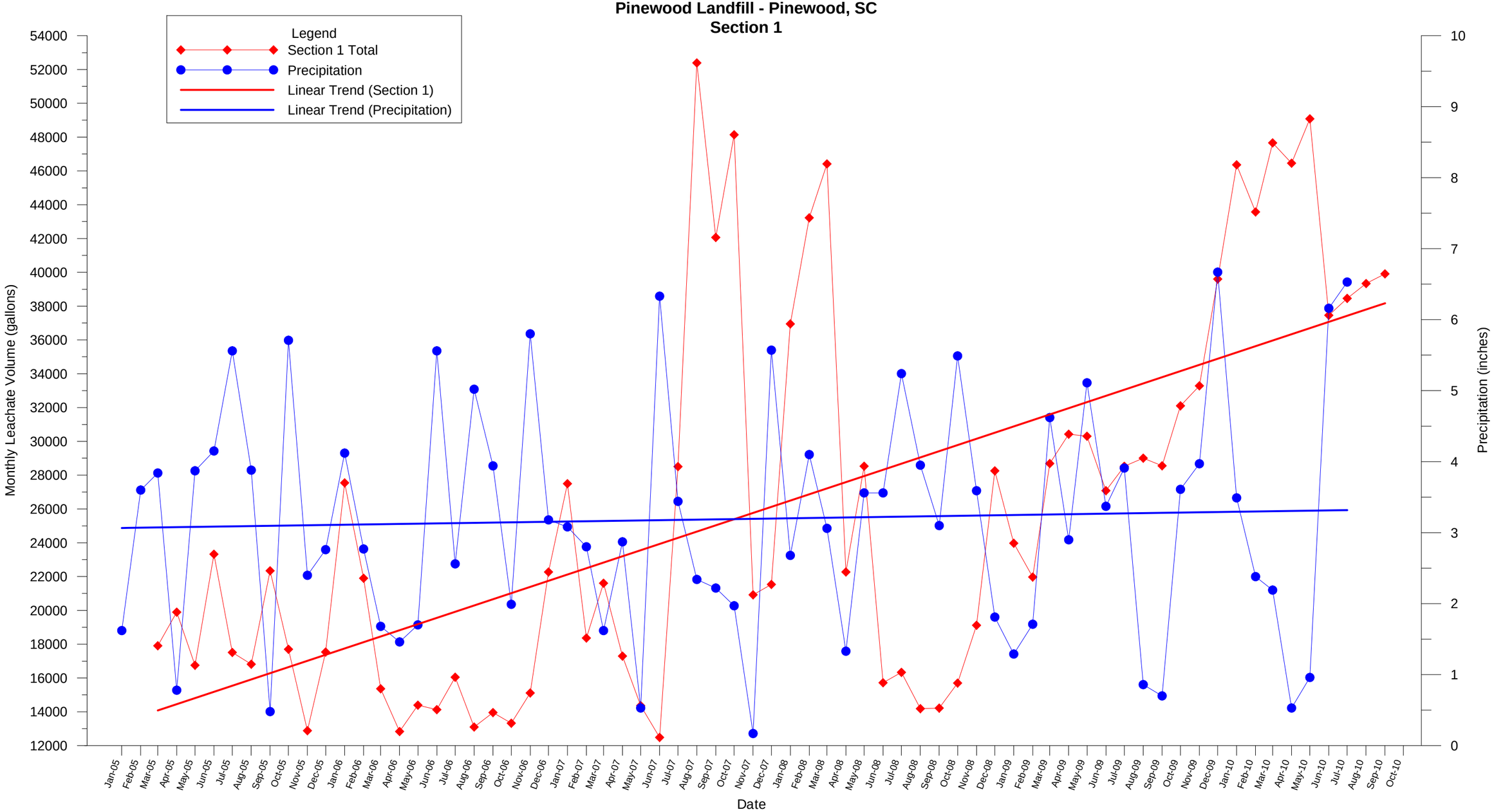
# Section I Primary Leachate Data and Precipitation
## March 2005 - September 2010
## Pinewood Landfill - Pinewood, SC
## Cell E



# Section I Primary Leachate Data and Precipitation
## March 2005 - September 2010
## Pinewood Landfill - Pinewood, SC
## 1D2P

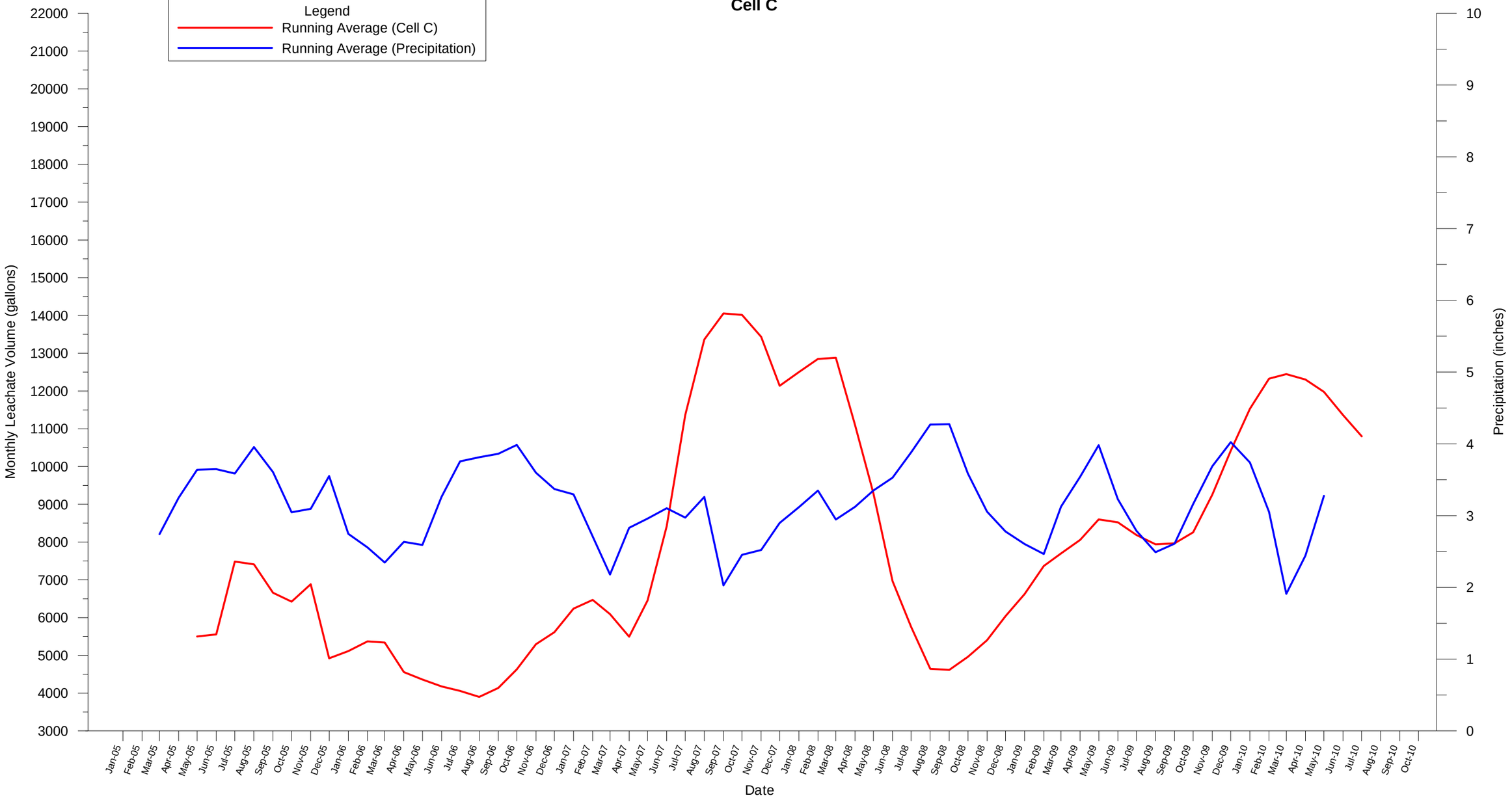


# Section I Primary Leachate Data and Precipitation
## March 2005 - September 2010
## Pinewood Landfill - Pinewood, SC
## Section 1

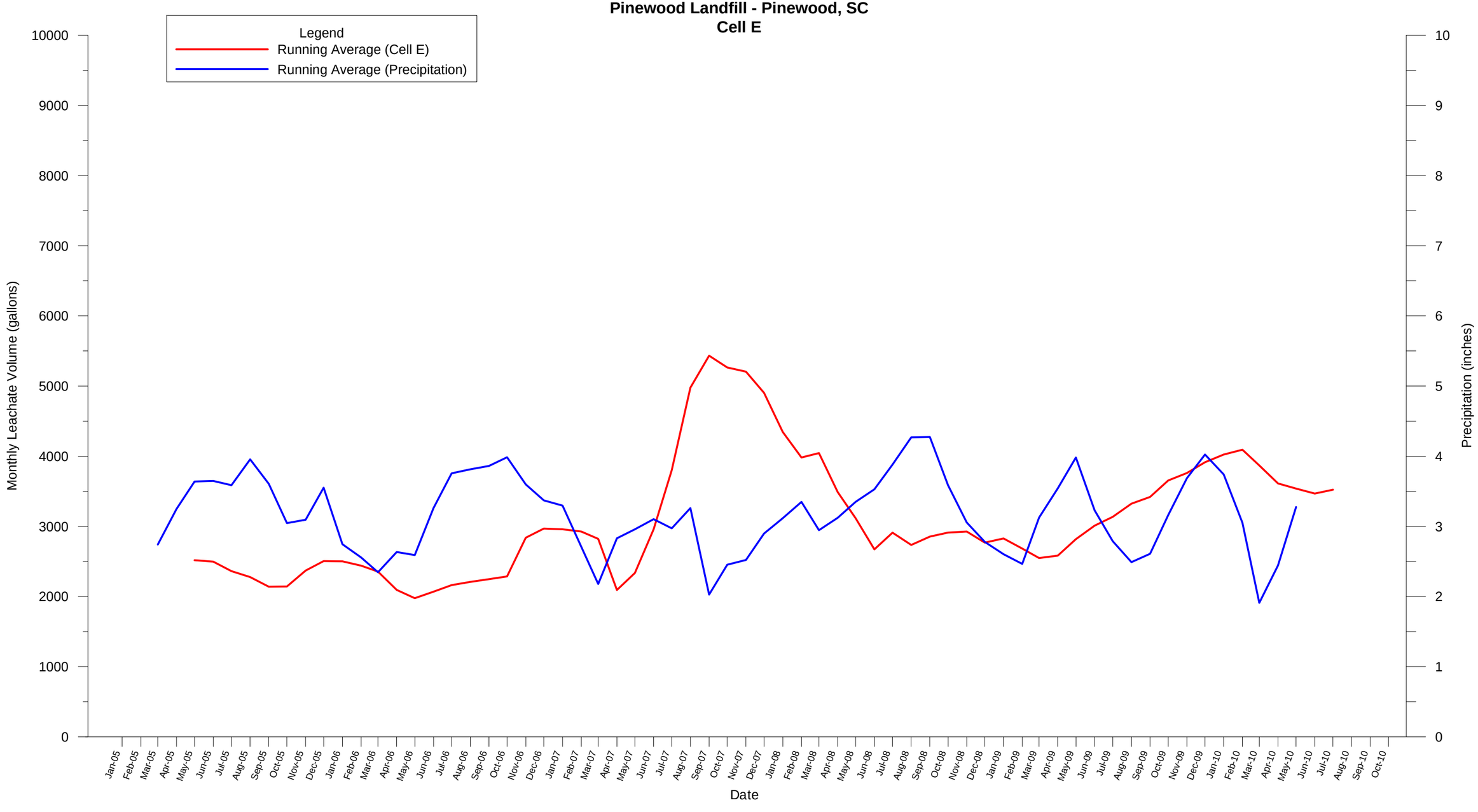


# 5-Month Running Average Rainfall vs. Leachate Production

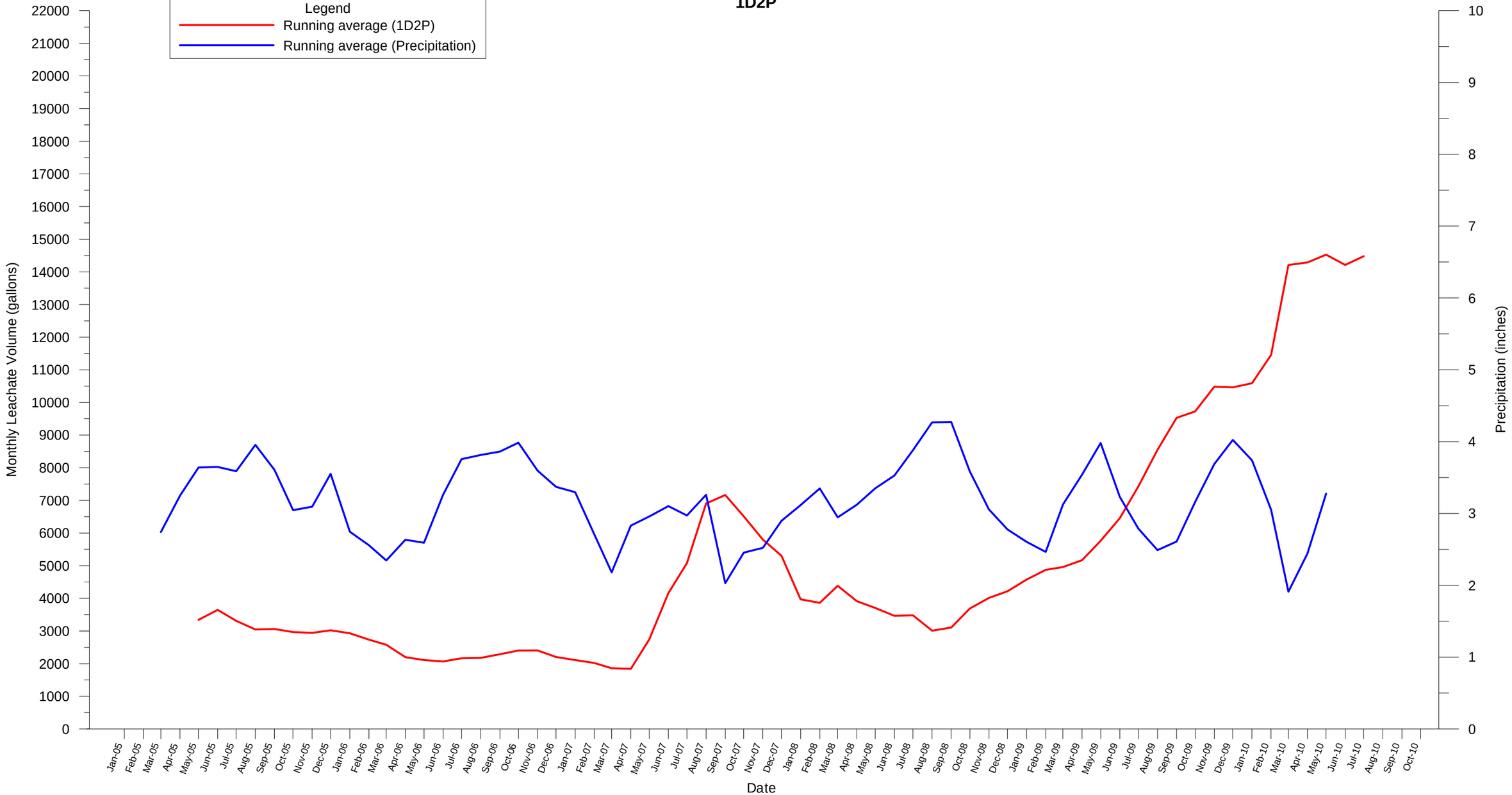
# Section I Primary Leachate Data and Precipitation
## March 2005 - September 2010
## Pinewood Landfill - Pinewood, SC
## Cell C



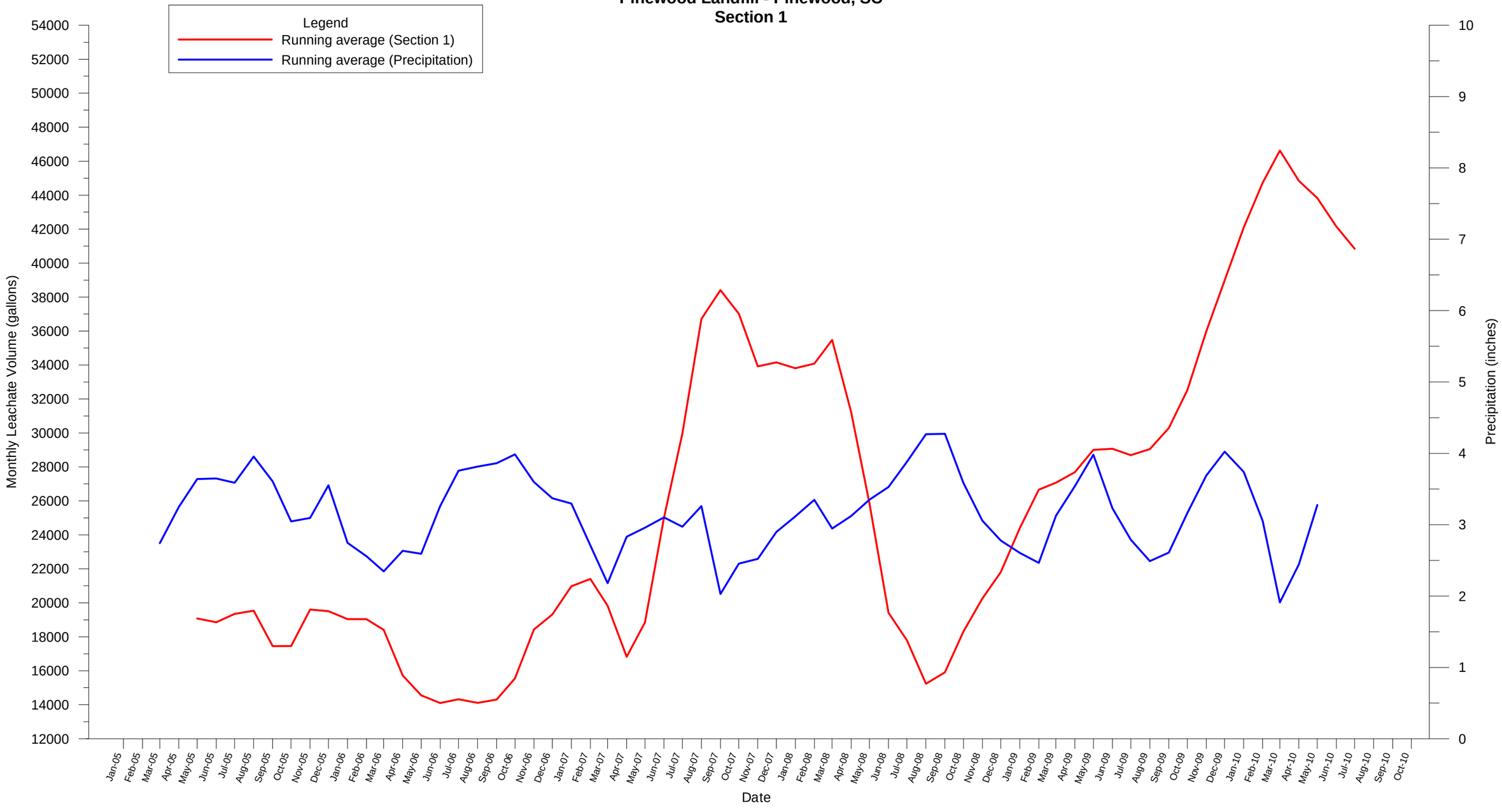
# Section I Primary Leachate Data and Precipitation
## March 2005 - September 2010
## Pinewood Landfill - Pinewood, SC
## Cell E



# Section I Primary Leachate Data and Precipitation
## March 2005 - September 2010
## Pinewood Landfill - Pinewood, SC
## 1D2P

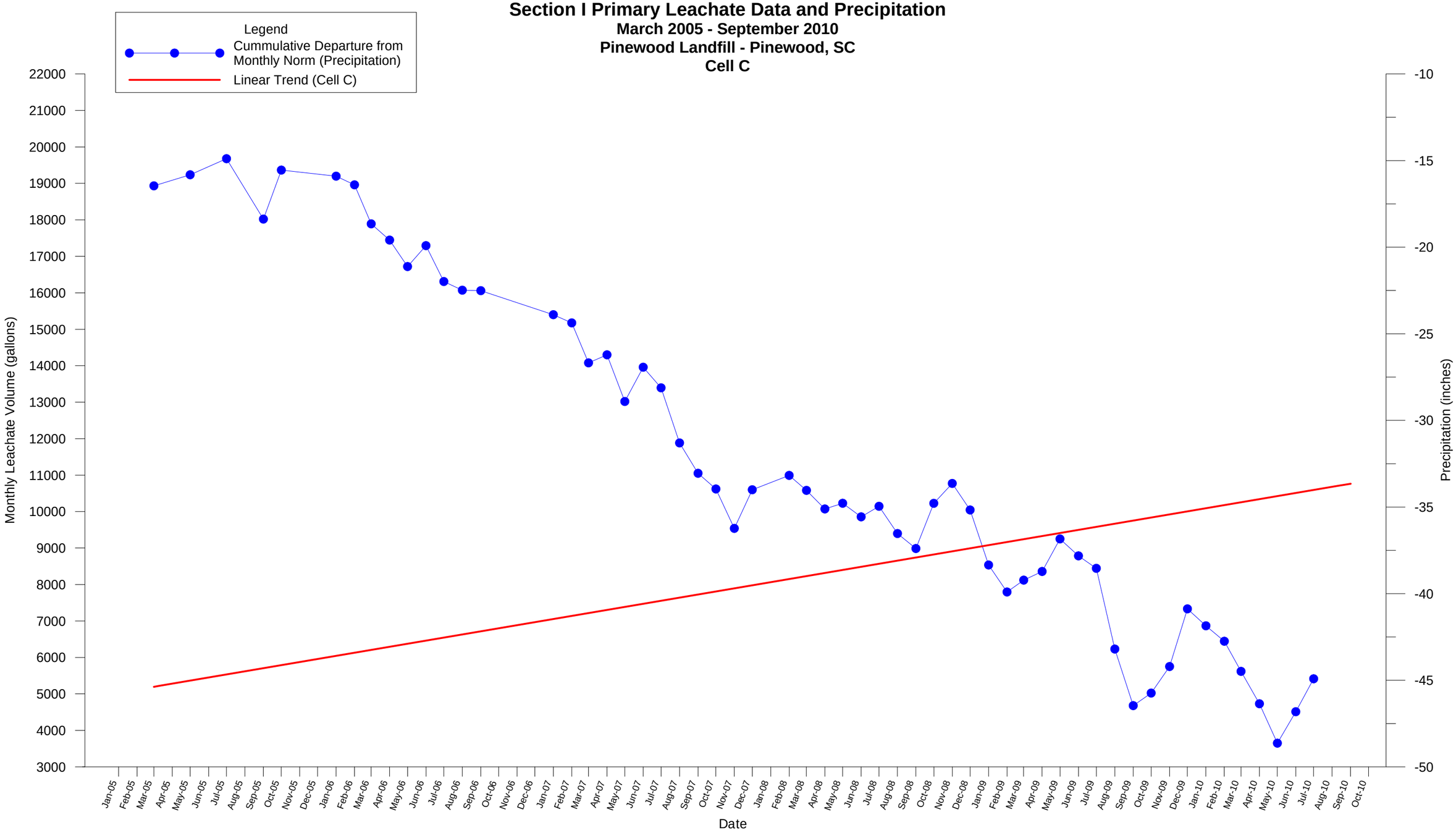


# Section I Primary Leachate Data and Precipitation
## March 2005 - September 2010
## Pinewood Landfill - Pinewood, SC
## Section 1

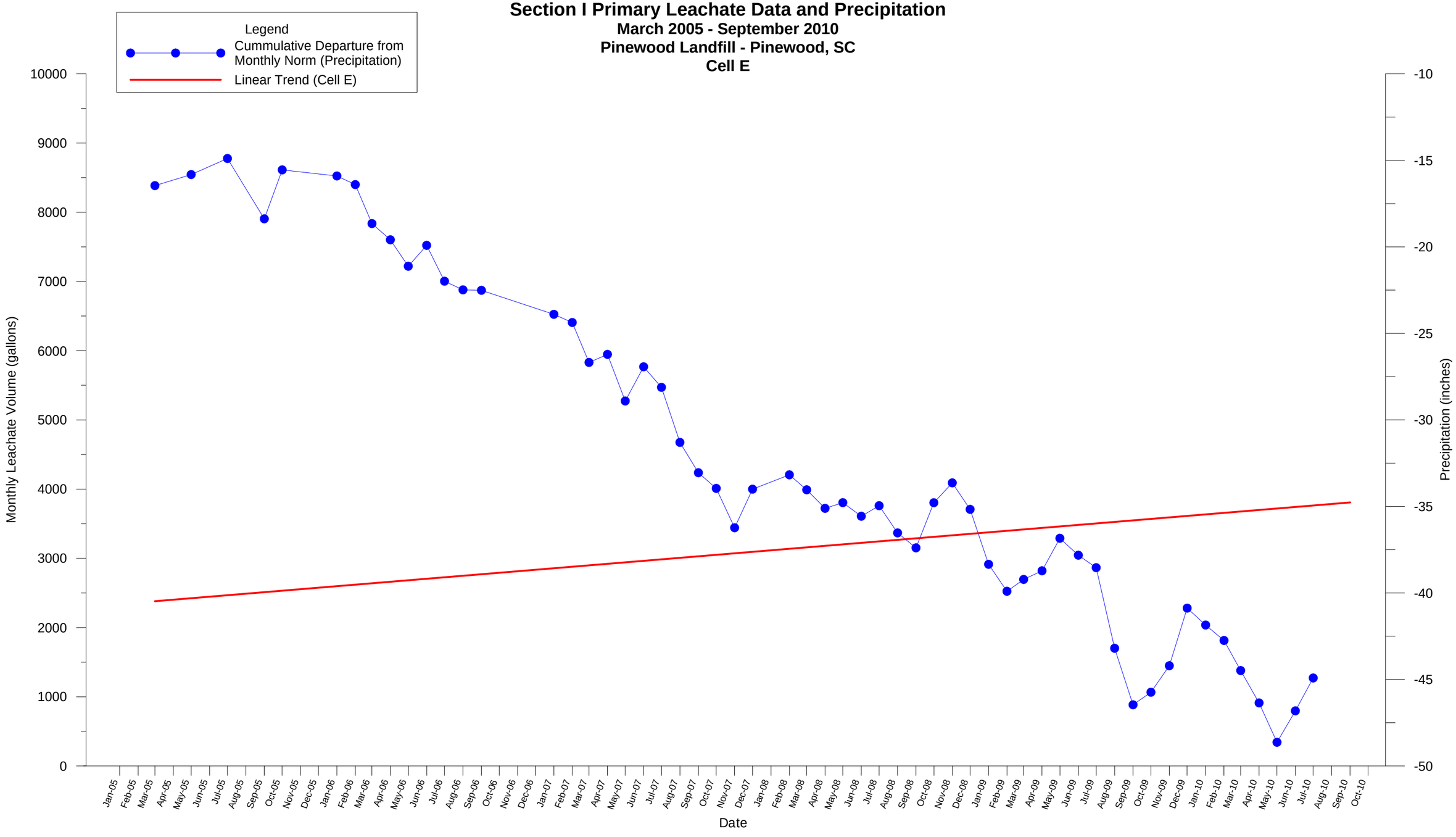


# Rainfall Departure vs. Leachate Trend

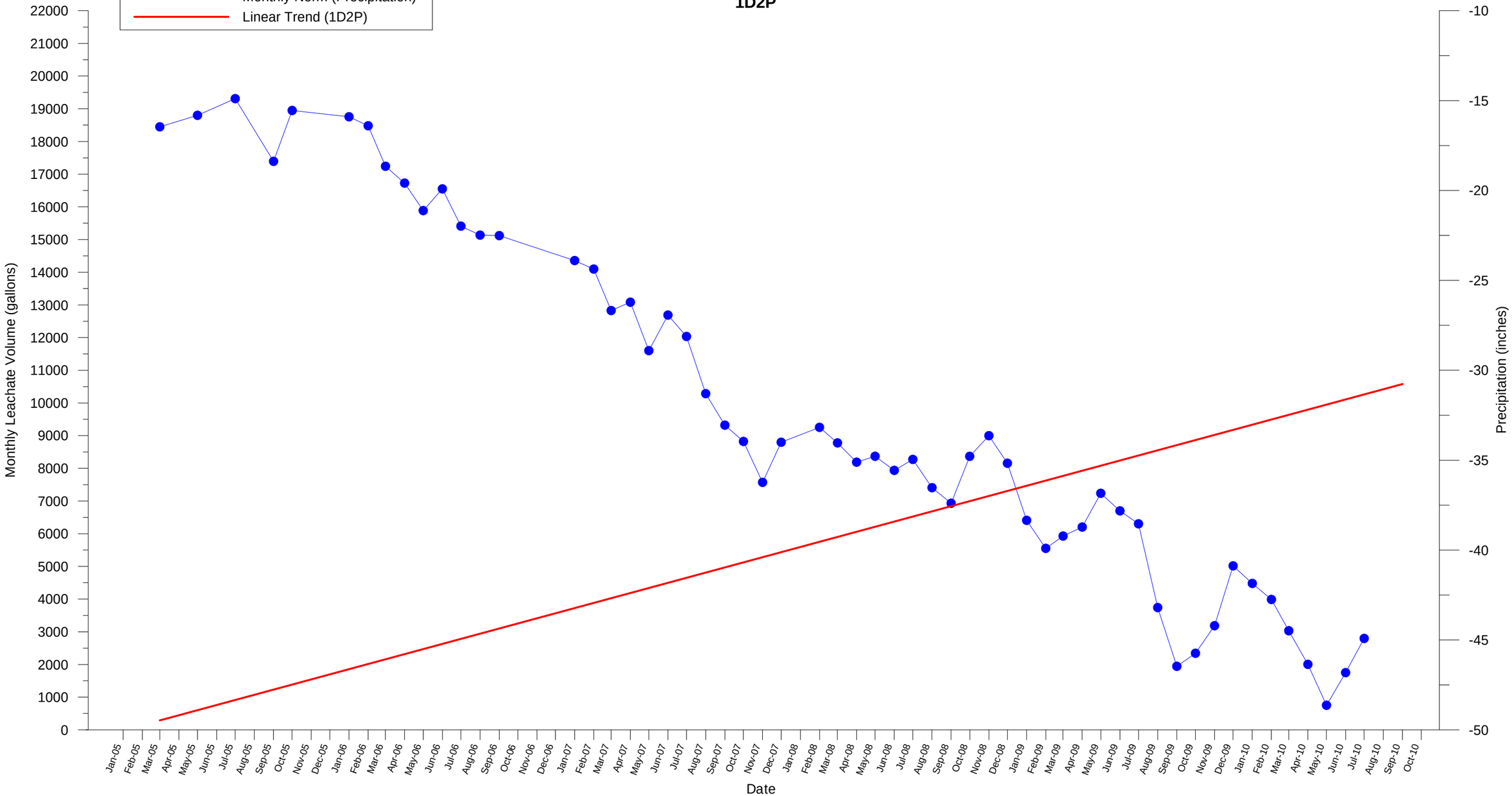
# Section I Primary Leachate Data and Precipitation
## March 2005 - September 2010
## Pinewood Landfill - Pinewood, SC
## Cell C



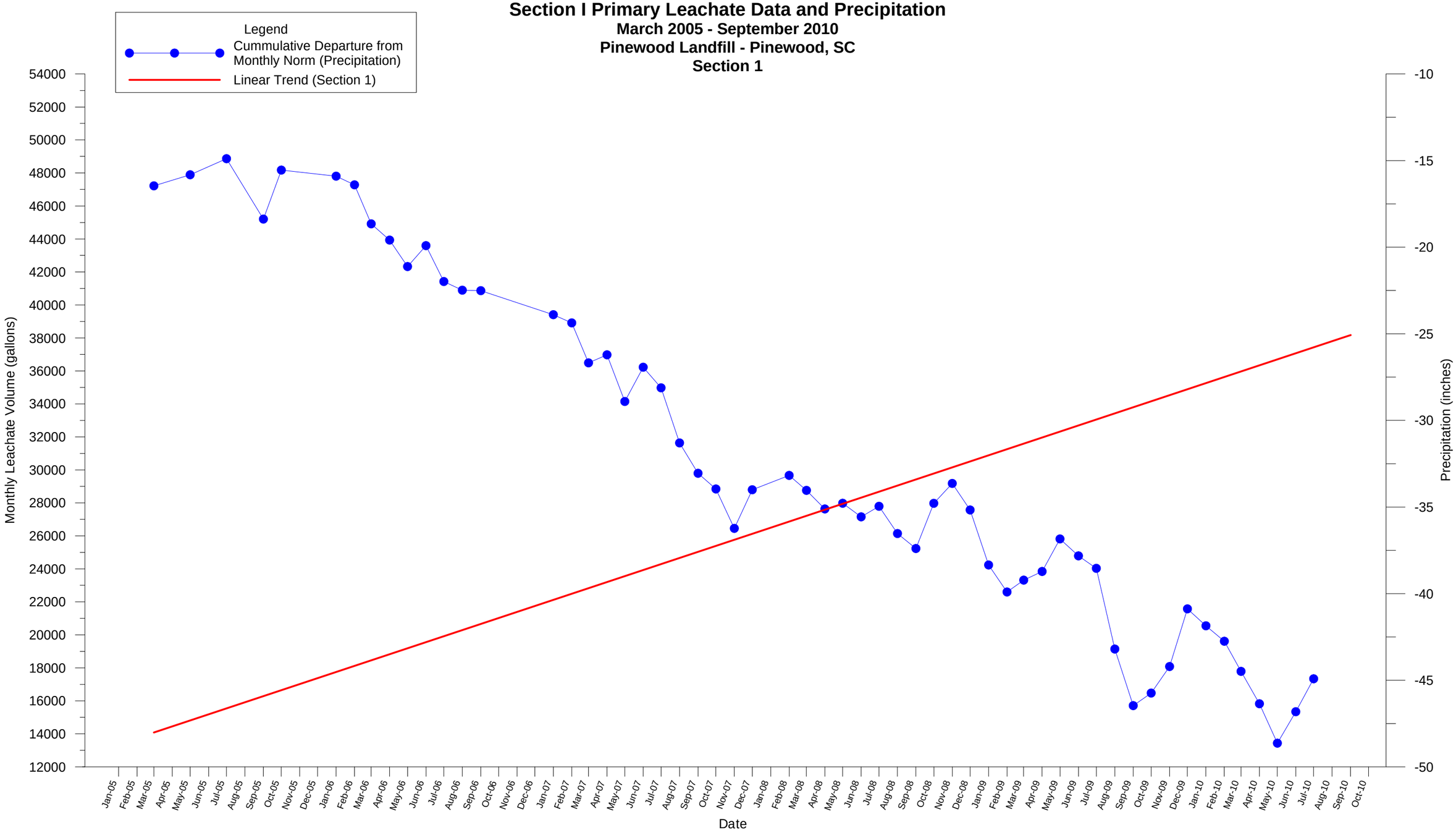
# Section I Primary Leachate Data and Precipitation
## March 2005 - September 2010
## Pinewood Landfill - Pinewood, SC
## Cell E



# Section I Primary Leachate Data and Precipitation
## March 2005 - September 2010
## Pinewood Landfill - Pinewood, SC
## 1D2P



# Section I Primary Leachate Data and Precipitation
## March 2005 - September 2010
## Pinewood Landfill - Pinewood, SC
## Section 1



# Appendix 2.5-1

WL Gore & Associates Report

# GORE® Surveys

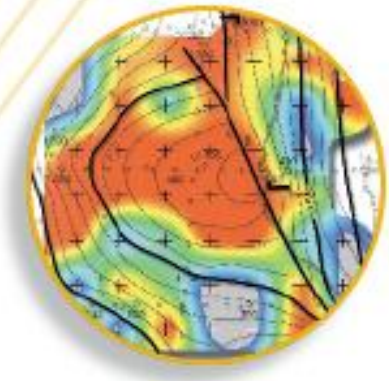
## Final Report

| | |
|---|---|
| Project: | PSCT Section I Cover, Pinewood, SC |
| Gore Order Number: | 20784505 |
| Date Prepared: | December 28, 2010 |
| Prepared for: | AECOM<br>10 Patewood Drive<br>Bldg. VI, Suite 500<br>Greenville, SC 29615 |

Written/Submitted by
James E. Whetzel
Project Manager

Reviewed/Approved by
Hilary G. Trethewey
Project Manager

Analytical Data Reviewed by
Ian McMullen
Chemist



W.L. Gore & Associates, Inc.
Survey Products Group

# GORE® Surveys - Final Report

**REPORT DATE:** 12/28/2010 **AUTHOR:** JW

## SITE INFORMATION

**Site Reference:** PSCT Section I Cover, Pinewood, SC
**Gore Production Order Number:** 20784505 **Gore Site Code:** FRM

## FIELD PROCEDURES

**# Modules shipped:** 59
**Installation Date(s):** 10/27/2010
**# Modules Installed:** 55
**Field work performed by:** AECOM

**Retrieval date(s):** 11/10/2010
**# Modules Retrieved:** 52
**# Modules Lost in Field:** 0
**# Modules Not Returned:** 0

**Exposure Time:** 14 **[days]**
**# Trip Blanks Returned:** 4
**# Unused Modules Returned:** 3

**Date/Time Received by Gore:** 11/12/2010 2:00 PM By: CW
**Chain of Custody Form attached:** Yes
**Chain of Custody discrepancies:** None
**Comments:**
Modules 648040, -052, -081, and -082 were identified as trip blanks.
Modules 648083 to -085 were returned unused.

# GORE® Surveys - Final Report

## QUALTIY ASSURANCE STATEMENT

**W.L. Gore & Associates´ Survey Products' Laboratory operates under the guidelines of ISO Standard 17025, its Quality Assurance Manual, Operating Procedures and Methods. For this project, the analytical method, reported results, and observations reported are considered screening level and do not fall within the scope of W.L. Gore's ISO 17025 accreditation.**

## ANALYTICAL PROCEDURES

Instrumentation consists of state of the art gas chromatographs equipped with mass selective detectors, coupled with automated thermal desorption units. Sample preparation simply involves cutting the tip off the bottom of the sample module and transferring one or more exposed sorbent containers (sorbers, each containing engineered adsorbents) to a thermal desorption tube for analysis. Sorbers remain clean and protected from dirt, soil, and ground water by the insertion/retrieval cord, and require no further sample preparation.

**Analytical Method Quality Assurance:**
The analytical method employed is a modified EPA method 8260/8270. Before each run sequence, two instrument blanks, a sorber containing 5µg BFB (Bromofluorobenzene), and a method blank are analyzed. The BFB mass spectra must meet the criteria set forth in the method before samples can be analyzed. A method blank and a sorber containing BFB are also analyzed after every 30 samples and/or trip blanks. Standards containing the selected target compounds at five calibration levels are analyzed at the beginning of each run. The criterion for each target compound is less than 25% RSD (relative standard deviation). If this criterion is not met for any target compound, the analyst has the option of generating second- or third-order standard curves, as appropriate. A second-source reference standard, at a level of 10µg per target compound, is analyzed after every ten samples and/or trip blanks, and at the end of the run sequence. Positive identification of target compounds is determined by 1) the presence of the target ion and at least two secondary ions; 2) retention time versus reference standard; and, 3) the analyst's judgment.

**NOTE: All data have been archived. Any replicate sorbers not used in the initial analysis will be discarded fifteen (15) days from the date of analysis.**

**Laboratory analysis:** thermal desorption, gas chromatography, mass selective detection
**Instrument ID:** # 5 **Chemist:** FN/ IM
**Compounds/mixtures requested:** A1
**Deviations from Standard Method:** None
**Comments:** Soil vapor analytes and abbreviations are tabulated in the Data Table Key (page 6). The top 5 tentatively identified compounds were identified using the NIST 2002 Mass Spectral Library. Estimated mass values were quantified using the response factor for undecane.

# GORE® Surveys - Final Report

## DATA TABULATION

**# CONTOUR MAPS ENCLOSED:** Six (6) B-sized color contour maps
**LIST OF MAPS ENCLOSED:**

- Benzene, Toluene, Ethyl benzene, and total Xylenes (BTEX)
- Tetrachloroethene (PCE)
- Trichloroethene (TCE)
- cis- & trans-1,2-Dichloroethene (c-, t-1,2-DCE)
- 1,1,1-Trichloroethane (1,1,1-TCA)
- 1,1-Dichloroethane (1,1-DCA)

**NOTE: All data values presented in Appendix A represent masses of compound(s) desorbed from the GORE® Modules received and analyzed by W.L. Gore & Associates, Inc., as identified in the Chain of Custody (Appendix A). The measurement traceability and instrument performance are reproducible and accurate for the measurement process documented. Semi-quantitation of the compound mass is based on a five-level standard calibration.**

### General Comments:

- This survey reports soil gas mass levels present in the vapor phase. Vapors are subject to a variety of attenuation factors during migration away from the source concentration to the module. Thus, mass levels reported from the module will often be less than concentrations reported in soil and groundwater matrix data. In most instances, the soil gas masses reported on the modules compare favorably with concentrations reported in the soil or groundwater (e.g., where soil gas levels are reported at greater levels relative to other sampled locations on the site, matrix data should reveal the same pattern, and vice versa). However, due to a variety of factors, a perfect comparison between matrix data and soil gas levels can rarely be achieved.
- Soil gas signals reported by this method cannot be identified specifically to soil adsorbed, groundwater, and/or free-product contamination. The soil gas signal reported from each module can evolve from all of these sources. Differentiation between soil and groundwater contamination can only be achieved with prior knowledge of the site history (i.e., the site is known to have groundwater contamination only).
- Total petroleum hydrocarbon (TPH) values were calculated using the area under the peaks observed in m/z 55 and 57 selected ion chromatograms. Quantitation of the mass value was performed using the response factor a specific alkane (present in the calibration standards).
- TPH values include the entire chromatogram and provide estimates for aliphatic hydrocarbon ranges of C4 to C20.

- QA/QC trip blank modules were provided to document potential exposures that were not part of the soil gas signal of interest (i.e., impact during module shipment, installation and retrieval, and storage). The trip blanks are identically manufactured and packaged soil gas modules to those modules placed in the subsurface. However, the trip blanks remain unopened during all phases of the soil gas survey. Levels reported on the trip blanks may indicate potential impact to modules other than the contaminant source of interest.
- Unresolved peak envelopes (UPEs) are represented as a series of compound peaks clustered together around a central gas chromatograph elution time in the total ion chromatogram. Typically, UPEs are indicative of complex fluid mixtures that are present in the subsurface. UPEs observed early in the chromatogram are considered to indicate the presence of more volatile fluids, while UPEs observed later in the chromatogram may indicate the presence of less volatile fluids. Multiple UPEs may indicate the presence of multiple complex fluids.
- Stacked total ion chromatograms (TICs) are included in Appendix A. The six-digit serial number of each module is incorporated into the TIC identification (e.g.: 123456S.D represents module #123456).

**Project Specific Comments:**

- The minimum (gray) contour level, for each mapped analyte or group of analytes, was set at the maximum blank level observed or the method detection limit, whichever was greater. When target compounds are combined (i.e., BTEX), the contour minimum is arbitrarily set at 0.02 µg or the maximum blank level, whichever is greater. The maximum contour level was set at the maximum value observed.
- No target compounds were detected on the trip blanks and/or the method blanks. Thus, target analyte levels reported for the field-installed modules that exceed trip and method blank levels, and the analyte method detection limit, are more likely to have originated from on-site sources.
- Up to five non-target peaks with the greatest area were identified for each sample using a mass spectral library. Estimated mass values were quantified using the response factor for undecane. Tentative identifications and estimated mass values are included in the appendix.
- The mapped spatial patterns indicated partially defined contaminant plumes in the survey area.

# GORE® Surveys - Final Report

## KEY TO DATA TABLE

**UNITS**

| | |
|---|---|
| µg | micrograms, relative mass value |
| MDL | method detection limit |
| bdl | below detection limit; compound was observed at level below the MDL |
| nd | non-detect, compound was not detected at any level |

**ANALYTES**

| | |
|---|---|
| TPH | total petroleum hydrocarbons |
| BTEX | combined masses of benzene, toluene, ethylbenzene and total xylenes (Gasoline Range Aromatics) |
| BENZ | benzene |
| TOL | toluene |
| EtBENZ | ethylbenzene |
| mpXYL | m-, p-xylene |
| oXYL | o-xylene |
| C11,C13&C15 | combined masses of undecane, tridecane, and pentadecane (C11+C13+C15) (Diesel Range Alkanes) |
| UNDEC | undecane |
| TRIDEC | tridecane |
| PENTADEC | pentadecane |
| TMBs | combined masses of 1,3,5-trimethylbenzene and 1,2,4-trimethylbenzene |
| 135TMB | 1,3,5-trimethylbenzene |
| 124TMB | 1,2,4-trimethylbenzene |
| ct12DCE | cis- & trans-1,2-dichloroethene |
| t12DCE | trans-1,2-dichloroethene |
| c12DCE | cis-1,2-dichloroethene |
| NAPH&2-MN | combined masses of naphthalene and 2-methyl naphthalene |
| NAPH | naphthalene |
| 2MeNAPH | 2-methyl naphthalene |
| MTBE | methyl t-butyl ether |
| 11DCA | 1,1-dichloroethane |
| $CHC1_3$ | chloroform |
| 111TCA | 1,1,1-trichloroethane |
| 12DCA | 1,2-dichloroethane |
| $CC1_4$ | carbon tetrachloride |
| TCE | trichloroethene |
| OCT | octane |
| PCE | tetrachloroethene |
| ClBENZ | chlorobenzene |
| 14DCB | 1,4-dichlorobenzene |
| 112TCA | 1,1,2-trichloroethane |
| 1112TetCA | 1,1,1,2-tetrachloroethane |
| 1122TetCA | 1,1,2,2-tetrachloroethane |
| 13DCB | 1,3-dichlorobenzene |
| 12DCB | 1,2-dichlorobenzene |
| 11DCE | 1,1-dichloroethene |

**BLANKS**

| | |
|---|---|
| method blank | QA/QC module, documents analytical conditions during analysis |

# APPENDIX A:

1. CHAIN OF CUSTODY AND INSTALLATION/ RETRIEVAL LOG
2. DATA TABLE
3. TENTATIVELY IDENTIFIED COMPOUNDS REPORT
4. STACKED TOTAL ION CHROMATOGRAMS
5. CONTOUR MAPS

# *GORE-SORBER® Screening Survey Chain of Custody*

For W.L. Gore & Associates use only
Production Order # 20784505


W. L. Gore & Associates, Inc., Survey Products Group
*100 Chesapeake Boulevard • Elkton, Maryland 21921 • Tel: (410) 392-7600 • Fax (410) 506-4780*


*Instructions: Customer must complete ALL shaded cells* PSCT SECTION I COVER

| | |
|---|---|
| Customer Name: AECOM | Site Name: ~~KESTREL HORIZONS~~ |
| Address: 10 PATEWOOD DRIVE | Site Address: PINEWOOD, SC |
| BLDG 6 SUITE 500 | |
| GREENVILLE SC 29615 | Project Manager: WALTER GERALD |
| Phone: (864) 234 8925 | Customer Project No.: 60186203 1 |
| FAX: | Customer P.O. #: 10820 ACM Quote #: |

| Serial # of Modules Shipped | | | | # of Modules for Installation: 55 | # of Trip Blanks: 4 |
|---|---|---|---|---|---|
| # 648027 | - # 648085 | # | - # | Total Modules Shipped: 59 | Pieces |
| # | - # | # | - # | Total Modules Received: 59 | Pieces |
| # | - # | # | - # | Total Modules Installed: 52 | Pieces |
| # | - # | # | - # | Serial # of Trip Blanks (*Client Decides*) | # |
| # | - # | # | - # | # 648040 | # |
| # | - # | # | - # | # 648052 | # |
| # | - # | # | - # | # 648081 | # |
| # | - # | # | - # | # 648082 | # |
| # | - # | # | - # | # | # |
| # | - # | # | - # | # | # |
| Prepared By: Mary Anne Menghe | | | | # | # |
| Verified By: | | | | # | # |

**Installation Performed By:**
Name (*please print*): ABHISHEK GUPTA / CHUCK SUDDETH
Company/Affiliation: AECOM

Installation Method(s) (*circle those that apply*):
Slide Hammer (Hammer Drill) Auger
Other:

Installation Start Date and Time: 10 / 26 / 2010 : 1339 AM PM
Installation Complete Date and Time: 10 / 27 / 2010 : 1715 AM PM

**Retrieval Performed By:**
Name (*please print*): ABHISHEK GUPTA / CHUCK SUDDETH
Company/Affiliation:1 AECOM

Total Modules Retrieved: 52 Pieces
Total Modules Lost in Field: 0 Pieces
Total Unused Modules Returned: 3 Pieces

Retrieval Start Date and Time: 11 / 10 / 10 10:26 (AM) PM
Retrieval Complete Date and Time: 11 / 11 / 10 / 12:15 AM (PM)

| Relinquished By | Date | Time | Received By: | Date | Time |
|---|---|---|---|---|---|
| Affiliation: W.L. Gore & Associates, Inc. | 10/21/10 | 2:00 | Affiliation: | | |
| Relinquished By: Charles K. Suddeth | Date | Time | Received By: | Date | Time |
| Affiliation: AECOM | 11/11/10 | 1900 | Affiliation: | | |
| Relinquished By | Date | Time | Received By: Clemente Coffy | Date | Time |
| Affiliation | | | Affiliation: W.L. Gore & Associates, Inc. | 11/12/10 | 14:00 |

# GORE-SORBER® Screening Survey Installation and Retrieval Log

Page 1 of 2

**SITE NAME & LOCATION**
PSCT Section I Cover
Pinewood, SC

| LINE # | MODULE # | INSTALLATION DATE/TIME | RETRIEVAL DATE/TIME | EVIDENCE OF LIQUID HYDROCARBONS (LPH) or HYDROCARBON ODOR (Check as appropriate) | | | MODULE IN WATER (check one) | | COMMENTS |
|---|---|---|---|---|---|---|---|---|---|
| | | | | LPH | ODOR | NONE | YES | NO | |
| 1. | 648027 | 10/26/10 1339 | 11/10/10 1026 | | | ✓ | | ✓ | BG-01 |
| 2. | 648028 | 10/26/10 1346 | 11/10/10 1034 | | | ✓ | | ✓ | BG-02 |
| 3. | 648029 | 10/26/10 14:13 | 11/10/10 1108 | | | ✓ | | ✓ | SG-1A-01 |
| 4. | 648030 | 10/26/10 14:26 | 11/10/10 1111 | | | ✓ | | ✓ | SG-1A-02 |
| 5. | 648031 | 10/26/10 14:31 | 11/10/10 1126 | | | ✓ | | ✓ | SG-1A-03 |
| 6. | 648032 | 10/26/10 14:44 | 11/10/10 1114 | | | ✓ | | ✓ | SG-1A-04 |
| 7. | 648033 | 10/26/10 14:52 | 11/10/10 1117 | | | ✓ | | ✓ | SG-1A-06 |
| 8. | 648034 | 10/26/10 15:02 | 11/10/10 1128 | | | ✓ | | ✓ | SG-1A-05 |
| 9. | 648035 | 10/26/10 15:10 | 11/10/10 1131 | | | ✓ | | ✓ | SG-1A-07 |
| 10. | 648036 | 10/26/10 15:15 | 11/10/10 1122 | | | ✓ | | ✓ | SG-1A-09 |
| 11. | 648037 | 10/26/10 15:27 | 11/10/10 1120 | | | ✓ | | ✓ | SG-1A-08 |
| 12. | 648038 | 10/26/10 15:45 | 11/10/10 1103 | | | ✓ | | ✓ | SG-1B-10 |
| 13. | 648039 | 10/26/10 15:52 | 11/10/10 1100 | | | ✓ | | ✓ | SG-1C-20 |
| 14. | 648040 | 10/26/10 1600 | 11/10/10 1104 | | | ✓ | | ✓ | TRIP BLANK-01 |
| 15. | 648041 | 10/26/10 1601 | 11/10/10 1105 | | | ✓ | | ✓ | SG-1B-11 |
| 16. | 648042 | 10/26/10 1627 | 11/10/10 1146 | | | ✓ | | ✓ | SG-1B-12 |
| 17. | 648043 | 10/26/10 1638 | 11/10/10 1149 | | | ✓ | | ✓ | SG-1B-13 |
| 18. | 648044 | 10/26/10 16:45 | 11/10/10 1152 | | | ✓ | | ✓ | SG-1B-14 |
| 19. | 648045 | 10/26/10 16:54 | 11/10/10 1156 | | | ✓ | | ✓ | SG-1B-15 |
| 20. | 648046 | 10/26/10 16:58 | 11/10/10 1158 | | | ✓ | | ✓ | SG-1B-16 |
| 21. | 648047 | 10/26/10 17:07 | 11/10/10 1144 | | | ✓ | | ✓ | SG-1C-22 |
| 22. | 648048 | 10/26/10 17:13 | 11/10/10 1200 | | | ✓ | | ✓ | SG-1C-24 |
| 23. | 648049 | 10/26/10 17:33 | 11/10/10 1141 | | | ✓ | ✓ | ✓ | SG-1C-26 |
| 24. | 648050 | 10/26/10 17:38 | 11/10/10 1135 | | | ✓ | | ✓ | SG-1B-17 |
| 25. | 648051 | 10/26/10 17:44 | 11/10/10 1137 | | | ✓ | | ✓ | SG-1B-18 |
| 26. | 648052 | 10/26/10 17:45 | 11/10/10 1205 | | | ✓ | | ✓ | TRIP BLANK-02 |
| 27. | 648053 | 10/27/10 09:29 | 11/10/10 1204 | | | ✓ | | ✓ | SG-1C-27 |
| 28. | 648054 | 10/27/10 11:47 | 11/10/10 1226 | | | ✓ | | ✓ | SG-1D-35 |
| 29. | 648055 | 10/27/10 10:04 | 11/10/10 1222 | | | ✓ | | ✓ | SG-1C-25 |
| 30. | 648056 | 10/27/10 10:10 | 11/10/10 1220 | | | ✓ | | ✓ | SG-1D-33 |
| 31. | 648057 | 10/27/10 10:28 | 11/10/10 1213 | | | ✓ | | ✓ | SG-1C-23 |
| 32. | 648058 | 10/27/10 10:32 | 11/10/10 1210 | | | ✓ | | ✓ | SG-1C-21 |
| 33. | 648059 | 10/27/10 10:49 | 11/10/10 1216 | | | ✓ | | ✓ | SG-1D-31 |
| 34. | 648060 | 10/27/10 11:13 | 11/10/10 1237 | | | ✓ | | ✓ | SG-1D-30 |
| 35. | 648061 | 10/27/10 11:25 | 11/10/10 1243 | | | ✓ | | ✓ | SG-1D-32 |
| 36. | 648062 | 10/27/10 11:33 | 11/10/10 1247 | | | ✓ | | ✓ | SG-1D-34 |
| 37. | 648063 | 10/27/10 11:37 | 11/10/10 1229 | | | ✓ | | ✓ | SG-1D-36 |
| 38. | 648064 | 10/27/10 13:58 | 11/10/10 1232 | | | ✓ | | ✓ | SG-1E-49 |
| 39. | 648065 | 10/27/10 14:05 | 11/10/10 1423 | | | ✓ | | ✓ | SG-1E-48 |
| 40. | 648066 | 10/27/10 14:19 | 11/10/10 1312 | | | ✓ | | ✓ | SG-1E-44 |
| 41. | 648067 | 10/27/10 14:28 | 11/10/10 1240 | | | ✓ | | ✓ | SG-1E-42 |
| 42. | 648068 | 10/27/10 14:38 | 11/10/10 1435 | | | ✓ | | ✓ | SG-1E-40 |

## GORE-SORBER® Screening Survey Installation and Retrieval Log

Page 2. of 2.

**SITE NAME & LOCATION**
PSCT SECTION I COVER
Pinewood, SC

| LINE # | MODULE # | INSTALLATION DATE/TIME | RETRIEVAL DATE/TIME | EVIDENCE OF LIQUID HYDROCARBONS (LPH) or HYDROCARBON ODOR (Check as appropriate) | | | MODULE IN WATER (check one) | | COMMENTS |
|---|---|---|---|---|---|---|---|---|---|
| | | | | LPH | ODOR | NONE | YES | NO | |
| 43. | 648069 | 10/27/10 1446 | 11/10/10 1433 | | | ✓ | | ✓ | SG-1E-39 |
| 44. | 648070 | 10/27/10 1448 | 11/10/10 1430 | | | ✓ | | ✓ | SG-1E-37 |
| 45. | 648071 | 10/27/10 1455 | 11/10/10 1438 | | | ✓ | | ✓ | SG-1E-41 |
| 46. | 648072 | 10/27/10 1459 | 11/10/10 1442 | | | ✓ | | ✓ | SG-1E-43 |
| 47. | 648073 | 10/27/10 1505 | 11/10/10 1451 | | | ✓ | | ✓ | SG-1E-46 |
| 48. | 648074 | 10/27/10 1527 | 11/10/10 1445 | | | ✓ | | ✓ | SG-1E-45 |
| 49. | 648075 | 10/27/10 1536 | 11/10/10 1453 | | | ✓ | | ✓ | SG-1E-47 |
| 50. | 648076 | 10/27/10 1540 | 11/10/10 1455 | | | ✓ | | ✓ | SG-1E-50 |
| 51. | 648077 | 10/27/10 1641 | 11/10/10 ~~1052~~ 1215 | | | ✓ | | ✓ | SG-1E-38 |
| 52. | 648078 | 10/27/10 1658 | 11/10/10 1049 | | | ✓ | | ✓ | SG-1D-28 |
| 53. | 648079 | 10/27/10 1710 | 11/10/10 1047 | | | ✓ | | ✓ | SG-1D-29 |
| 54. | 648080 | 10/27/10 1714 | 11/10/10 1043 | | | ✓ | | ✓ | SG-1C-19 |
| 55. | 648081 | 10/27/10 1715 | 11/10/10 1500 | | | ✓ | | ✓ | Trip Blank-03 |
| 56. | 648082 | 10/27/10 1715 | 11/10/10 1500 | | | ✓ | | ✓ | Trip Blank-04 |
| 57. | 648083 | | | | | | | | |
| 58. | 648084 | | | | | | | | |
| 59. | 648085 | | | | | | | | |
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*SPG-FCD-0298 March 12, 2010*
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GORE(TM) SURVEYS ANALYTICAL RESULTS
AECOM, GREENVILLE, SC
GORE STANDARD TARGET VOCs/SVOCs (A1)
PSCT, SECTION I COVER, PINEWOOD, SC
SITE FRM - PRODUCTION ORDER #20784505

| DATE ANALYZED | FIELD ID | SAMPLE NAME | TPH, ug | BTEX, ug | BENZ, ug | TOL, ug | EtBENZ, ug | mpXYL, ug | oXYL, ug | C11, C13, &C15, ug |
|---|---|---|---|---|---|---|---|---|---|---|
| | | MDL= | 0.02 | | 0.02 | 0.02 | 0.02 | 0.03 | 0.02 | |
| 11-19-10 | BG-01 | 648027 | 16.45 | 0.26 | 0.13 | 0.07 | 0.02 | 0.04 | bdl | 0.07 |
| 11-19-10 | BG-02 | 648028 | 0.11 | nd | nd | nd | nd | nd | nd | nd |
| 11-18-10 | SG-1A-01 | 648029 | 0.12 | 0.06 | 0.06 | nd | nd | nd | nd | nd |
| 11-19-10 | SG-1A-02 | 648030 | 0.09 | nd | nd | nd | nd | nd | nd | nd |
| 11-19-10 | SG-1A-03 | 648031 | 0.31 | nd | nd | nd | nd | nd | nd | nd |
| 11-19-10 | SG-1A-04 | 648032 | 0.18 | 0.02 | 0.02 | nd | nd | nd | nd | nd |
| 11-19-10 | SG-1A-06 | 648033 | 0.19 | nd | nd | nd | nd | nd | nd | nd |
| 11-19-10 | SG-1A-05 | 648034 | 0.16 | 0.04 | 0.04 | nd | nd | nd | nd | nd |
| 11-19-10 | SG-1A-07 | 648035 | 0.04 | nd | nd | nd | nd | nd | nd | nd |
| 11-20-10 | SG-1A-09 | 648036 | 0.06 | bdl | bdl | nd | nd | nd | nd | nd |
| 11-20-10 | SG-1A-08 | 648037 | 0.08 | nd | nd | nd | nd | nd | nd | nd |
| 11-19-10 | SG-1B-10 | 648038 | 0.08 | 0.06 | 0.06 | nd | nd | nd | nd | nd |
| 11-18-10 | SG-1C-20 | 648039 | 18.29 | 0.20 | 0.20 | bdl | nd | nd | nd | nd |
| 11-19-10 | SG-1B-11 | 648041 | 0.20 | nd | nd | nd | nd | nd | nd | nd |
| 11-19-10 | SG-1B-12 | 648042 | 0.02 | 0.05 | 0.05 | nd | nd | nd | nd | nd |
| 11-18-10 | SG-1B-13 | 648043 | 0.02 | bdl | bdl | nd | nd | nd | nd | nd |
| 11-19-10 | SG-1B-14 | 648044 | 0.12 | 0.05 | 0.05 | nd | nd | nd | nd | nd |
| 11-18-10 | SG-1B-15 | 648045 | 0.05 | nd | nd | nd | nd | nd | nd | nd |
| 11-18-10 | SG-1B-16 | 648046 | 0.05 | 0.09 | 0.09 | nd | nd | nd | nd | nd |
| 11-19-10 | SG-1B-22 | 648047 | 0.55 | 0.02 | 0.02 | nd | nd | nd | nd | nd |
| 11-19-10 | SG-1B-24 | 648048 | 0.05 | 0.04 | 0.04 | nd | nd | nd | nd | nd |
| 11-20-10 | SG-1B-26 | 648049 | 0.59 | 0.05 | 0.05 | nd | nd | nd | nd | nd |
| 11-19-10 | SG-1B-17 | 648050 | 0.31 | 0.03 | 0.03 | nd | nd | nd | nd | nd |
| 11-18-10 | SG-1B-18 | 648051 | 0.10 | 0.04 | 0.04 | nd | nd | nd | nd | nd |
| 11-19-10 | SG-1C-27 | 648053 | 0.08 | 0.13 | 0.13 | nd | nd | nd | nd | nd |
| 11-18-10 | SG-1D-35 | 648054 | 49.09 | 0.70 | 0.42 | 0.14 | 0.05 | 0.05 | 0.04 | 0.09 |
| 11-19-10 | SG-1C-25 | 648055 | 0.09 | 0.02 | 0.02 | nd | nd | nd | nd | nd |
| 11-19-10 | SG-1D-33 | 648056 | 0.91 | 0.08 | 0.05 | 0.02 | nd | nd | bdl | nd |
| 11-19-10 | SG-1C-23 | 648057 | 2.63 | 0.13 | 0.10 | 0.03 | nd | nd | bdl | bdl |
| 11-19-10 | SG-1C-21 | 648058 | 0.23 | 0.05 | 0.05 | nd | nd | nd | nd | nd |
| 11-19-10 | SG-1D-31 | 648059 | 1.58 | 0.04 | 0.04 | nd | nd | nd | nd | nd |

No mdl is available for summed combinations of analytes. In summed columns (eg., BTEX), the reported values should be considered ESTIMATED if any of the individual compounds were reported as bdl.

GORE(TM) SURVEYS ANALYTICAL RESULTS
AECOM, GREENVILLE, SC
GORE STANDARD TARGET VOCs/SVOCs (A1)
PSCT, SECTION I COVER, PINEWOOD, SC
SITE FRM - PRODUCTION ORDER #20784505

| DATE ANALYZED | FIELD ID | SAMPLE NAME | TPH, ug | BTEX, ug | BENZ, ug | TOL, ug | EtBENZ, ug | mpXYL, ug | oXYL, ug | C11, C13, &C15, ug |
|---|---|---|---|---|---|---|---|---|---|---|
| | | MDL= | 0.02 | | 0.02 | 0.02 | 0.02 | 0.03 | 0.02 | |
| 11-18-10 | SG-1D-30 | 648060 | 0.18 | 0.06 | 0.06 | nd | nd | nd | nd | nd |
| 11-19-10 | SG-1D-32 | 648061 | 0.47 | 0.09 | 0.09 | nd | nd | nd | nd | nd |
| 11-19-10 | SG-1D-34 | 648062 | 0.03 | 0.03 | 0.03 | nd | nd | nd | nd | nd |
| 11-18-10 | SG-1D-36 | 648063 | bdl | nd | nd | nd | nd | nd | nd | nd |
| 11-19-10 | SG-1E-49 | 648064 | 1.25 | 0.96 | 0.16 | 0.36 | 0.10 | 0.19 | 0.14 | nd |
| 11-19-10 | SG-1E-48 | 648065 | 0.47 | 0.07 | 0.05 | nd | 0.02 | bdl | nd | nd |
| 11-19-10 | SG-1E-44 | 648066 | 8.13 | 0.73 | 0.70 | nd | nd | nd | 0.03 | bdl |
| 11-19-10 | SG-1E-42 | 648067 | 0.12 | 0.05 | 0.05 | nd | nd | nd | nd | nd |
| 11-19-10 | SG-1E-40 | 648068 | 0.24 | nd | nd | nd | nd | nd | nd | nd |
| 11-19-10 | SG-1E-39 | 648069 | 0.38 | 0.20 | 0.20 | nd | nd | nd | nd | nd |
| 11-18-10 | SG-1E-37 | 648070 | 0.47 | 0.03 | 0.03 | nd | nd | nd | nd | nd |
| 11-19-10 | SG-1E-41 | 648071 | 0.10 | 0.02 | 0.02 | nd | nd | nd | nd | nd |
| 11-19-10 | SG-1E-43 | 648072 | 0.08 | 0.55 | 0.52 | 0.03 | nd | nd | nd | nd |
| 11-19-10 | SG-1E-46 | 648073 | 0.71 | 1.90 | 1.58 | 0.20 | nd | 0.05 | 0.06 | nd |
| 11-19-10 | SG-1E-45 | 648074 | 0.39 | 0.04 | 0.04 | nd | nd | nd | nd | nd |
| 11-19-10 | SG-1E-47 | 648075 | 0.09 | 0.09 | nd | nd | nd | nd | 0.09 | nd |
| 11-19-10 | SG-1E-50 | 648076 | bdl | 0.04 | 0.04 | nd | nd | nd | nd | nd |
| 11-18-10 | SG-1E-38 | 648077 | 25.83 | 0.07 | 0.07 | nd | nd | bdl | bdl | 0.02 |
| 11-19-10 | SG-1D-28 | 648078 | 0.07 | nd | nd | nd | nd | nd | nd | nd |
| 11-19-10 | SG-1D-29 | 648079 | 0.48 | 0.03 | 0.03 | nd | nd | nd | nd | nd |
| 11-18-10 | SG-1C-19 | 648080 | 0.53 | 0.05 | 0.05 | nd | nd | nd | nd | nd |
| | | | | | | | | | | |
| 11-19-10 | TRIP BLANK-01 | 648040 | nd | nd | nd | nd | nd | nd | nd | nd |
| 11-19-10 | TRIP BLANK-02 | 648052 | nd | nd | nd | nd | nd | nd | nd | nd |
| 11-19-10 | TRIP BLANK-03 | 648081 | nd | nd | nd | nd | nd | nd | nd | nd |
| 11-19-10 | TRIP BLANK-04 | 648082 | nd | nd | nd | nd | nd | nd | nd | nd |
| | | | | | | | | | | |
| 11-18-10 | method blank | method blank | nd | nd | nd | nd | nd | nd | nd | nd |
| 11-19-10 | method blank | method blank | nd | nd | nd | nd | nd | nd | nd | nd |
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No mdl is available for summed combinations of analytes. In summed columns (eg., BTEX), the reported values should be considered ESTIMATED if any of the individual compounds were reported as bdl.

GORE(TM) SURVEYS ANALYTICAL RESULTS
AECOM, GREENVILLE, SC
GORE STANDARD TARGET VOCs/SVOCs (A1)
PSCT, SECTION I COVER, PINEWOOD, SC
SITE FRM - PRODUCTION ORDER #20784505

| FIELD ID | SAMPLE NAME | UNDEC, ug | TRIDEC, ug | PENTADEC, ug | TMBs, ug | 124TMB, ug | 135TMB, ug | ct12DCE, ug | t12DCE, ug |
|---|---|---|---|---|---|---|---|---|---|
| | MDL= | 0.04 | 0.02 | 0.02 | | 0.02 | 0.03 | | 0.04 |
| BG-01 | 648027 | 0.07 | nd | nd | bdl | bdl | nd | nd | nd |
| BG-02 | 648028 | nd | nd | nd | nd | nd | nd | nd | nd |
| SG-1A-01 | 648029 | nd | nd | nd | nd | nd | nd | nd | nd |
| SG-1A-02 | 648030 | nd | nd | nd | nd | nd | nd | nd | nd |
| SG-1A-03 | 648031 | nd | nd | nd | nd | nd | nd | nd | nd |
| SG-1A-04 | 648032 | nd | nd | nd | nd | nd | nd | nd | nd |
| SG-1A-06 | 648033 | nd | nd | nd | nd | nd | nd | nd | nd |
| SG-1A-05 | 648034 | nd | nd | nd | nd | nd | nd | nd | nd |
| SG-1A-07 | 648035 | nd | nd | nd | nd | nd | nd | nd | nd |
| SG-1A-09 | 648036 | nd | nd | nd | nd | nd | nd | nd | nd |
| SG-1A-08 | 648037 | nd | nd | nd | nd | nd | nd | nd | nd |
| SG-1B-10 | 648038 | nd | nd | nd | nd | nd | nd | nd | nd |
| SG-1C-20 | 648039 | nd | nd | nd | nd | nd | nd | 26.33 | 4.00 |
| SG-1B-11 | 648041 | nd | nd | nd | nd | nd | nd | nd | nd |
| SG-1B-12 | 648042 | nd | nd | nd | nd | nd | nd | nd | nd |
| SG-1B-13 | 648043 | nd | nd | nd | nd | nd | nd | 0.22 | 0.06 |
| SG-1B-14 | 648044 | nd | nd | nd | nd | nd | nd | nd | nd |
| SG-1B-15 | 648045 | nd | nd | nd | nd | nd | nd | bdl | bdl |
| SG-1B-16 | 648046 | nd | nd | nd | nd | nd | nd | 1.43 | 0.68 |
| SG-1B-22 | 648047 | nd | nd | nd | nd | nd | nd | nd | nd |
| SG-1B-24 | 648048 | nd | nd | nd | nd | nd | nd | nd | nd |
| SG-1B-26 | 648049 | nd | nd | nd | bdl | nd | bdl | bdl | bdl |
| SG-1B-17 | 648050 | nd | nd | nd | nd | nd | nd | nd | nd |
| SG-1B-18 | 648051 | nd | nd | nd | nd | nd | nd | 0.35 | 0.14 |
| SG-1C-27 | 648053 | nd | nd | nd | nd | nd | nd | nd | nd |
| SG-1D-35 | 648054 | 0.09 | nd | nd | 0.02 | 0.02 | bdl | nd | nd |
| SG-1C-25 | 648055 | nd | nd | nd | nd | nd | nd | nd | nd |
| SG-1D-33 | 648056 | nd | nd | nd | nd | nd | nd | nd | nd |
| SG-1C-23 | 648057 | bdl | nd | nd | bdl | bdl | bdl | nd | nd |
| SG-1C-21 | 648058 | nd | nd | nd | nd | nd | nd | nd | nd |
| SG-1D-31 | 648059 | nd | nd | nd | nd | nd | nd | nd | nd |

No mdl is available for summed combinations of analytes. In summed columns (eg., BTEX), the reported values should be considered ESTIMATED if any of the individual compounds were reported as bdl.

GORE(TM) SURVEYS ANALYTICAL RESULTS
AECOM, GREENVILLE, SC
GORE STANDARD TARGET VOCs/SVOCs (A1)
PSCT, SECTION I COVER, PINEWOOD, SC
SITE FRM - PRODUCTION ORDER #20784505

| FIELD ID | SAMPLE NAME | UNDEC, ug | TRIDEC, ug | PENTADEC, ug | TMBs, ug | 124TMB, ug | 135TMB, ug | ct12DCE, ug | t12DCE, ug |
|---|---|---|---|---|---|---|---|---|---|
| | MDL= | 0.04 | 0.02 | 0.02 | | 0.02 | 0.03 | | 0.04 |
| SG-1D-30 | 648060 | nd | nd | nd | nd | nd | nd | 0.22 | 0.04 |
| SG-1D-32 | 648061 | nd | nd | nd | nd | nd | nd | 0.63 | nd |
| SG-1D-34 | 648062 | nd | nd | nd | nd | nd | nd | nd | nd |
| SG-1D-36 | 648063 | nd | nd | nd | nd | nd | nd | 0.07 | bdl |
| SG-1E-49 | 648064 | nd | nd | nd | bdl | nd | bdl | 0.47 | 0.04 |
| SG-1E-48 | 648065 | nd | nd | nd | nd | nd | nd | bdl | nd |
| SG-1E-44 | 648066 | bdl | nd | nd | nd | nd | nd | 31.43 | 1.02 |
| SG-1E-42 | 648067 | nd | nd | nd | nd | nd | nd | 0.45 | 0.10 |
| SG-1E-40 | 648068 | nd | nd | nd | nd | nd | nd | nd | nd |
| SG-1E-39 | 648069 | nd | nd | nd | nd | nd | nd | 0.22 | nd |
| SG-1E-37 | 648070 | nd | nd | nd | nd | nd | nd | nd | nd |
| SG-1E-41 | 648071 | nd | nd | nd | nd | nd | nd | 0.60 | 0.20 |
| SG-1E-43 | 648072 | nd | nd | nd | nd | nd | nd | 14.04 | 1.08 |
| SG-1E-46 | 648073 | nd | nd | nd | nd | nd | nd | 5.48 | 0.90 |
| SG-1E-45 | 648074 | nd | nd | nd | nd | nd | nd | nd | nd |
| SG-1E-47 | 648075 | nd | nd | nd | nd | nd | nd | 0.22 | bdl |
| SG-1E-50 | 648076 | nd | nd | nd | nd | nd | nd | nd | nd |
| SG-1E-38 | 648077 | bdl | 0.02 | bdl | 0.04 | 0.04 | bdl | nd | nd |
| SG-1D-28 | 648078 | nd | nd | nd | nd | nd | nd | bdl | nd |
| SG-1D-29 | 648079 | nd | nd | nd | nd | nd | nd | nd | nd |
| SG-1C-19 | 648080 | nd | nd | nd | nd | nd | nd | nd | nd |
| | | | | | | | | | |
| TRIP BLANK-01 | 648040 | nd | nd | nd | nd | nd | nd | nd | nd |
| TRIP BLANK-02 | 648052 | nd | nd | nd | nd | nd | nd | nd | nd |
| TRIP BLANK-03 | 648081 | nd | nd | nd | nd | nd | nd | nd | nd |
| TRIP BLANK-04 | 648082 | nd | nd | nd | nd | nd | nd | nd | nd |
| | | | | | | | | | |
| method blank | method blank | nd | nd | nd | nd | nd | nd | nd | nd |
| method blank | method blank | nd | nd | nd | nd | nd | nd | nd | nd |
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No mdl is available for summed combinations of analytes. In summed columns (eg., BTEX), the reported values should be considered ESTIMATED if any of the individual compounds were reported as bdl.

GORE(TM) SURVEYS ANALYTICAL RESULTS
AECOM, GREENVILLE, SC
GORE STANDARD TARGET VOCs/SVOCs (A1)
PSCT, SECTION I COVER, PINEWOOD, SC
SITE FRM - PRODUCTION ORDER #20784505

| FIELD ID | SAMPLE NAME | c12DCE, ug | NAPH&2-MN, ug | NAPH, ug | 2MeNAPH, ug | MTBE, ug | 11DCE, ug | 11DCA, ug | 111TCA, ug |
|---|---|---|---|---|---|---|---|---|---|
| | MDL= | 0.03 | | 0.02 | 0.02 | 0.03 | 0.02 | 0.02 | 0.03 |
| BG-01 | 648027 | nd | nd | nd | nd | nd | nd | nd | nd |
| BG-02 | 648028 | nd | nd | nd | nd | nd | nd | nd | nd |
| SG-1A-01 | 648029 | nd | nd | nd | nd | nd | 0.82 | 13.44 | nd |
| SG-1A-02 | 648030 | nd | nd | nd | nd | nd | nd | 0.09 | nd |
| SG-1A-03 | 648031 | nd | nd | nd | nd | nd | nd | nd | nd |
| SG-1A-04 | 648032 | nd | nd | nd | nd | nd | nd | 0.07 | nd |
| SG-1A-06 | 648033 | nd | nd | nd | nd | nd | nd | 0.12 | nd |
| SG-1A-05 | 648034 | nd | nd | nd | nd | nd | nd | nd | nd |
| SG-1A-07 | 648035 | nd | nd | nd | nd | nd | nd | nd | nd |
| SG-1A-09 | 648036 | nd | nd | nd | nd | nd | 0.24 | 1.13 | nd |
| SG-1A-08 | 648037 | nd | nd | nd | nd | nd | bdl | 0.05 | nd |
| SG-1B-10 | 648038 | nd | nd | nd | nd | nd | 0.31 | 3.72 | nd |
| SG-1C-20 | 648039 | 22.33 | nd | nd | nd | nd | 7.74 | 20.80 | 0.04 |
| SG-1B-11 | 648041 | nd | nd | nd | nd | nd | 0.06 | 1.51 | nd |
| SG-1B-12 | 648042 | nd | nd | nd | nd | nd | 0.10 | 1.33 | nd |
| SG-1B-13 | 648043 | 0.16 | nd | nd | nd | nd | 0.02 | 0.37 | nd |
| SG-1B-14 | 648044 | nd | nd | nd | nd | nd | nd | nd | nd |
| SG-1B-15 | 648045 | nd | nd | nd | nd | nd | 0.15 | 1.56 | nd |
| SG-1B-16 | 648046 | 0.75 | nd | nd | nd | nd | 0.50 | 5.70 | bdl |
| SG-1B-22 | 648047 | nd | nd | nd | nd | nd | nd | nd | nd |
| SG-1B-24 | 648048 | nd | nd | nd | nd | nd | nd | nd | nd |
| SG-1B-26 | 648049 | nd | nd | nd | nd | nd | 1.67 | 9.19 | bdl |
| SG-1B-17 | 648050 | nd | nd | nd | nd | nd | nd | nd | nd |
| SG-1B-18 | 648051 | 0.21 | nd | nd | nd | nd | 0.05 | 1.35 | nd |
| SG-1C-27 | 648053 | nd | nd | nd | nd | nd | nd | 0.05 | nd |
| SG-1D-35 | 648054 | nd | bdl | nd | bdl | nd | nd | nd | nd |
| SG-1C-25 | 648055 | nd | nd | nd | nd | nd | nd | nd | nd |
| SG-1D-33 | 648056 | nd | nd | nd | nd | nd | 0.03 | 0.31 | nd |
| SG-1C-23 | 648057 | nd | nd | nd | nd | nd | nd | nd | nd |
| SG-1C-21 | 648058 | nd | nd | nd | nd | nd | nd | nd | nd |
| SG-1D-31 | 648059 | nd | nd | nd | nd | nd | nd | nd | nd |

No mdl is available for summed combinations of analytes. In summed columns (eg., BTEX), the reported values should be considered ESTIMATED if any of the individual compounds were reported as bdl.

GORE(TM) SURVEYS ANALYTICAL RESULTS
AECOM, GREENVILLE, SC
GORE STANDARD TARGET VOCs/SVOCs (A1)
PSCT, SECTION I COVER, PINEWOOD, SC
SITE FRM - PRODUCTION ORDER #20784505

| FIELD ID | SAMPLE NAME | c12DCE, ug | NAPH&2-MN, ug | NAPH, ug | 2MeNAPH, ug | MTBE, ug | 11DCE, ug | 11DCA, ug | 111TCA, ug |
|---|---|---|---|---|---|---|---|---|---|
| | MDL= | 0.03 | | 0.02 | 0.02 | 0.03 | 0.02 | 0.02 | 0.03 |
| SG-1D-30 | 648060 | 0.18 | nd | nd | nd | nd | 0.17 | 6.00 | nd |
| SG-1D-32 | 648061 | 0.63 | nd | nd | nd | nd | nd | 35.81 | nd |
| SG-1D-34 | 648062 | nd | nd | nd | nd | nd | 0.75 | 2.67 | nd |
| SG-1D-36 | 648063 | 0.07 | nd | nd | nd | nd | 0.26 | 2.47 | nd |
| SG-1E-49 | 648064 | 0.43 | nd | nd | nd | nd | 3.45 | 3.07 | 11.35 |
| SG-1E-48 | 648065 | bdl | nd | nd | nd | bdl | 0.18 | 0.22 | nd |
| SG-1E-44 | 648066 | 30.41 | nd | nd | nd | nd | 8.30 | 35.44 | 1.35 |
| SG-1E-42 | 648067 | 0.35 | nd | nd | nd | bdl | 0.24 | 7.36 | nd |
| SG-1E-40 | 648068 | nd | nd | nd | nd | nd | 0.34 | 1.51 | nd |
| SG-1E-39 | 648069 | 0.22 | nd | nd | nd | nd | nd | nd | nd |
| SG-1E-37 | 648070 | nd | nd | nd | nd | 0.04 | 0.07 | 0.87 | nd |
| SG-1E-41 | 648071 | 0.39 | nd | nd | nd | nd | 0.68 | 15.25 | 0.06 |
| SG-1E-43 | 648072 | 12.95 | nd | nd | nd | nd | 1.23 | 20.93 | nd |
| SG-1E-46 | 648073 | 4.57 | nd | nd | nd | nd | 2.33 | 22.12 | 0.07 |
| SG-1E-45 | 648074 | nd | nd | nd | nd | nd | bdl | 0.75 | nd |
| SG-1E-47 | 648075 | 0.22 | nd | nd | nd | bdl | 0.04 | 2.43 | bdl |
| SG-1E-50 | 648076 | nd | nd | nd | nd | nd | nd | 0.19 | nd |
| SG-1E-38 | 648077 | nd | 0.16 | 0.07 | 0.10 | nd | nd | nd | nd |
| SG-1D-28 | 648078 | bdl | nd | nd | nd | nd | nd | 0.54 | nd |
| SG-1D-29 | 648079 | nd | nd | nd | nd | nd | 0.02 | 0.89 | nd |
| SG-1C-19 | 648080 | nd | nd | nd | nd | nd | nd | nd | nd |
| | | | | | | | | | |
| TRIP BLANK-01 | 648040 | nd | nd | nd | nd | nd | nd | nd | nd |
| TRIP BLANK-02 | 648052 | nd | nd | nd | nd | nd | nd | nd | nd |
| TRIP BLANK-03 | 648081 | nd | nd | nd | nd | nd | nd | nd | nd |
| TRIP BLANK-04 | 648082 | nd | nd | nd | nd | nd | nd | nd | nd |
| | | | | | | | | | |
| method blank | method blank | nd | nd | nd | nd | nd | nd | nd | nd |
| method blank | method blank | nd | nd | nd | nd | nd | nd | nd | nd |
| | | | | | | | | | |
| | | | | | | | | | |

No mdl is available for summed combinations of analytes. In summed columns (eg., BTEX), the reported values should be considered ESTIMATED if any of the individual compounds were reported as bdl.

GORE(TM) SURVEYS ANALYTICAL RESULTS
AECOM, GREENVILLE, SC
GORE STANDARD TARGET VOCs/SVOCs (A1)
PSCT, SECTION I COVER, PINEWOOD, SC
SITE FRM - PRODUCTION ORDER #20784505

| FIELD ID | SAMPLE NAME | 12DCA, ug | TCE, ug | OCT, ug | PCE, ug | 14DCB, ug | CHCl3, ug | CCl4, ug | 112TCA, ug | ClBENZ, ug | 1112TetCA, ug |
|---|---|---|---|---|---|---|---|---|---|---|---|
| | MDL= | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 | 0.03 | 0.02 | 0.02 | 0.03 |
| BG-01 | 648027 | nd | nd | bdl | nd | nd | nd | nd | nd | nd | nd |
| BG-02 | 648028 | nd | nd | nd | nd | nd | nd | nd | nd | nd | nd |
| SG-1A-01 | 648029 | nd | nd | nd | 0.23 | nd | 0.03 | nd | nd | nd | nd |
| SG-1A-02 | 648030 | nd | nd | nd | nd | nd | nd | nd | nd | nd | nd |
| SG-1A-03 | 648031 | nd | nd | nd | nd | nd | bdl | nd | nd | nd | nd |
| SG-1A-04 | 648032 | nd | nd | nd | nd | nd | nd | nd | nd | nd | nd |
| SG-1A-06 | 648033 | nd | nd | nd | nd | nd | nd | nd | nd | nd | nd |
| SG-1A-05 | 648034 | nd | nd | nd | nd | nd | nd | nd | nd | nd | nd |
| SG-1A-07 | 648035 | nd | nd | nd | nd | nd | 0.04 | nd | nd | nd | nd |
| SG-1A-09 | 648036 | nd | nd | nd | nd | nd | nd | nd | nd | nd | nd |
| SG-1A-08 | 648037 | nd | nd | nd | nd | nd | 0.03 | nd | nd | nd | nd |
| SG-1B-10 | 648038 | nd | nd | nd | 0.15 | nd | nd | nd | nd | nd | nd |
| SG-1C-20 | 648039 | nd | 10.57 | nd | 0.91 | nd | nd | nd | nd | nd | nd |
| SG-1B-11 | 648041 | 0.08 | bdl | nd | 0.03 | nd | nd | nd | nd | nd | nd |
| SG-1B-12 | 648042 | nd | nd | nd | nd | nd | 0.03 | nd | nd | nd | nd |
| SG-1B-13 | 648043 | nd | 1.17 | nd | nd | nd | nd | nd | nd | nd | nd |
| SG-1B-14 | 648044 | nd | nd | nd | nd | nd | nd | nd | nd | nd | nd |
| SG-1B-15 | 648045 | nd | 0.02 | nd | 0.56 | nd | 0.04 | nd | 0.15 | nd | nd |
| SG-1B-16 | 648046 | 0.32 | 8.76 | nd | 14.66 | nd | 0.35 | nd | 0.66 | nd | nd |
| SG-1B-22 | 648047 | nd | nd | nd | nd | nd | nd | nd | nd | nd | nd |
| SG-1B-24 | 648048 | nd | nd | nd | nd | nd | nd | nd | nd | nd | nd |
| SG-1B-26 | 648049 | 0.91 | 0.10 | nd | 1.55 | nd | nd | nd | nd | nd | nd |
| SG-1B-17 | 648050 | nd | nd | nd | nd | nd | nd | nd | nd | nd | nd |
| SG-1B-18 | 648051 | 0.37 | 0.59 | nd | 0.16 | nd | 0.03 | nd | nd | nd | nd |
| SG-1C-27 | 648053 | nd | nd | nd | nd | nd | 0.05 | nd | nd | nd | nd |
| SG-1D-35 | 648054 | nd | nd | 0.25 | 0.03 | nd | nd | nd | nd | nd | nd |
| SG-1C-25 | 648055 | nd | nd | nd | 0.04 | nd | 0.05 | nd | nd | nd | nd |
| SG-1D-33 | 648056 | nd | nd | nd | nd | nd | nd | nd | nd | nd | nd |
| SG-1C-23 | 648057 | nd | nd | bdl | nd | nd | nd | nd | nd | nd | nd |
| SG-1C-21 | 648058 | nd | nd | nd | nd | nd | nd | nd | nd | nd | nd |
| SG-1D-31 | 648059 | nd | nd | nd | nd | nd | nd | nd | nd | nd | nd |

No mdl is available for summed combinations of analytes. In summed columns (eg., BTEX), the reported values should be considered ESTIMATED if any of the individual compounds were reported as bdl.

GORE(TM) SURVEYS ANALYTICAL RESULTS
AECOM, GREENVILLE, SC
GORE STANDARD TARGET VOCs/SVOCs (A1)
PSCT, SECTION I COVER, PINEWOOD, SC
SITE FRM - PRODUCTION ORDER #20784505

| FIELD ID | SAMPLE NAME | 12DCA, ug | TCE, ug | OCT, ug | PCE, ug | 14DCB, ug | CHCl3, ug | CCl4, ug | 112TCA, ug | ClBENZ, ug | 1112TetCA, ug |
|---|---|---|---|---|---|---|---|---|---|---|---|
| | MDL= | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 | 0.03 | 0.02 | 0.02 | 0.03 |
| SG-1D-30 | 648060 | nd | nd | nd | nd | nd | nd | nd | nd | nd | nd |
| SG-1D-32 | 648061 | 0.23 | 7.06 | nd | 0.52 | nd | 0.10 | nd | 0.78 | nd | nd |
| SG-1D-34 | 648062 | nd | 0.02 | nd | nd | nd | nd | nd | nd | nd | nd |
| SG-1D-36 | 648063 | nd | 0.02 | nd | nd | nd | 0.04 | nd | nd | nd | nd |
| SG-1E-49 | 648064 | 0.45 | 3.61 | bdl | 2.24 | bdl | 0.81 | nd | 0.37 | nd | nd |
| SG-1E-48 | 648065 | nd | bdl | nd | 0.08 | nd | 0.02 | nd | nd | nd | nd |
| SG-1E-44 | 648066 | nd | 28.10 | 0.03 | 31.33 | 0.11 | 7.67 | nd | 19.62 | 0.12 | nd |
| SG-1E-42 | 648067 | nd | 1.60 | nd | 1.01 | nd | 0.04 | nd | nd | 0.05 | nd |
| SG-1E-40 | 648068 | nd | nd | nd | 0.41 | nd | 0.47 | nd | nd | 0.02 | nd |
| SG-1E-39 | 648069 | nd | bdl | nd | nd | nd | nd | nd | nd | nd | nd |
| SG-1E-37 | 648070 | nd | nd | nd | nd | nd | nd | nd | nd | nd | nd |
| SG-1E-41 | 648071 | nd | 1.92 | nd | 11.30 | nd | 0.10 | nd | nd | nd | nd |
| SG-1E-43 | 648072 | 4.78 | 27.87 | nd | 3.08 | nd | 0.08 | nd | nd | 0.47 | nd |
| SG-1E-46 | 648073 | 0.23 | 7.58 | nd | 3.77 | nd | 2.72 | nd | 3.26 | bdl | nd |
| SG-1E-45 | 648074 | nd | nd | nd | 0.04 | nd | nd | nd | nd | nd | nd |
| SG-1E-47 | 648075 | nd | 0.15 | nd | 0.16 | nd | 1.00 | nd | nd | 0.10 | nd |
| SG-1E-50 | 648076 | nd | nd | nd | 0.03 | nd | nd | nd | nd | nd | nd |
| SG-1E-38 | 648077 | nd | nd | nd | nd | nd | nd | nd | nd | nd | nd |
| SG-1D-28 | 648078 | nd | nd | nd | nd | nd | nd | nd | nd | nd | nd |
| SG-1D-29 | 648079 | nd | nd | nd | nd | nd | nd | nd | nd | nd | nd |
| SG-1C-19 | 648080 | nd | nd | nd | nd | nd | nd | nd | nd | nd | nd |
| | | | | | | | | | | | |
| TRIP BLANK-01 | 648040 | nd | nd | nd | nd | nd | nd | nd | nd | nd | nd |
| TRIP BLANK-02 | 648052 | nd | nd | nd | nd | nd | nd | nd | nd | nd | nd |
| TRIP BLANK-03 | 648081 | nd | nd | nd | nd | nd | nd | nd | nd | nd | nd |
| TRIP BLANK-04 | 648082 | nd | nd | nd | nd | nd | nd | nd | nd | nd | nd |
| | | | | | | | | | | | |
| method blank | method blank | nd | nd | nd | nd | nd | nd | nd | nd | nd | nd |
| method blank | method blank | nd | nd | nd | nd | nd | nd | nd | nd | nd | nd |
| | | | | | | | | | | | |
| | | | | | | | | | | | |

No mdl is available for summed combinations of analytes. In summed columns (eg., BTEX), the reported values should be considered ESTIMATED if any of the individual compounds were reported as bdl.

GORE(TM) SURVEYS ANALYTICAL RESULTS
AECOM, GREENVILLE, SC
GORE STANDARD TARGET VOCs/SVOCs (A1)
PSCT, SECTION I COVER, PINEWOOD, SC
SITE FRM - PRODUCTION ORDER #20784505

| FIELD ID | SAMPLE NAME | 1122TetCA, ug | 13DCB, ug | 12DCB, ug |
|---|---|---|---|---|
| | MDL= | 0.02 | 0.02 | 0.02 |
| BG-01 | 648027 | nd | nd | nd |
| BG-02 | 648028 | nd | nd | nd |
| SG-1A-01 | 648029 | nd | nd | nd |
| SG-1A-02 | 648030 | nd | nd | nd |
| SG-1A-03 | 648031 | nd | nd | nd |
| SG-1A-04 | 648032 | nd | nd | nd |
| SG-1A-06 | 648033 | nd | nd | nd |
| SG-1A-05 | 648034 | nd | nd | nd |
| SG-1A-07 | 648035 | nd | nd | nd |
| SG-1A-09 | 648036 | nd | nd | nd |
| SG-1A-08 | 648037 | nd | nd | nd |
| SG-1B-10 | 648038 | nd | nd | nd |
| SG-1C-20 | 648039 | nd | nd | nd |
| SG-1B-11 | 648041 | nd | nd | nd |
| SG-1B-12 | 648042 | nd | nd | nd |
| SG-1B-13 | 648043 | nd | nd | nd |
| SG-1B-14 | 648044 | nd | nd | nd |
| SG-1B-15 | 648045 | nd | nd | nd |
| SG-1B-16 | 648046 | nd | nd | nd |
| SG-1B-22 | 648047 | nd | nd | nd |
| SG-1B-24 | 648048 | nd | nd | nd |
| SG-1B-26 | 648049 | nd | nd | nd |
| SG-1B-17 | 648050 | nd | nd | nd |
| SG-1B-18 | 648051 | nd | nd | nd |
| SG-1C-27 | 648053 | nd | nd | nd |
| SG-1D-35 | 648054 | nd | nd | nd |
| SG-1C-25 | 648055 | nd | nd | nd |
| SG-1D-33 | 648056 | nd | nd | nd |
| SG-1C-23 | 648057 | nd | nd | nd |
| SG-1C-21 | 648058 | nd | nd | nd |
| SG-1D-31 | 648059 | nd | nd | nd |

No mdl is available for summed combinations of analytes. In summed columns (eg., BTEX), the reported values should be considered ESTIMATED if any of the individual compounds were reported as bdl.

GORE(TM) SURVEYS ANALYTICAL RESULTS
AECOM, GREENVILLE, SC
GORE STANDARD TARGET VOCs/SVOCs (A1)
PSCT, SECTION I COVER, PINEWOOD, SC
SITE FRM - PRODUCTION ORDER #20784505

| FIELD ID | SAMPLE NAME | 1122TetCA, ug | 13DCB, ug | 12DCB, ug |
|---|---|---|---|---|
| | MDL= | 0.02 | 0.02 | 0.02 |
| SG-1D-30 | 648060 | nd | nd | nd |
| SG-1D-32 | 648061 | nd | nd | nd |
| SG-1D-34 | 648062 | nd | nd | nd |
| SG-1D-36 | 648063 | nd | nd | nd |
| SG-1E-49 | 648064 | nd | nd | 0.05 |
| SG-1E-48 | 648065 | nd | nd | nd |
| SG-1E-44 | 648066 | 2.44 | 0.03 | 0.10 |
| SG-1E-42 | 648067 | nd | nd | nd |
| SG-1E-40 | 648068 | nd | nd | 0.06 |
| SG-1E-39 | 648069 | nd | nd | nd |
| SG-1E-37 | 648070 | nd | nd | nd |
| SG-1E-41 | 648071 | nd | nd | nd |
| SG-1E-43 | 648072 | nd | nd | 0.03 |
| SG-1E-46 | 648073 | 0.60 | nd | nd |
| SG-1E-45 | 648074 | nd | nd | nd |
| SG-1E-47 | 648075 | nd | nd | 0.09 |
| SG-1E-50 | 648076 | nd | nd | nd |
| SG-1E-38 | 648077 | nd | nd | nd |
| SG-1D-28 | 648078 | nd | nd | nd |
| SG-1D-29 | 648079 | nd | nd | nd |
| SG-1C-19 | 648080 | nd | nd | nd |
| | | | | |
| TRIP BLANK-01 | 648040 | nd | nd | nd |
| TRIP BLANK-02 | 648052 | nd | nd | nd |
| TRIP BLANK-03 | 648081 | nd | nd | nd |
| TRIP BLANK-04 | 648082 | nd | nd | nd |
| | | | | |
| method blank | method blank | nd | nd | nd |
| method blank | method blank | nd | nd | nd |
| | | | | |
| | | | | |

No mdl is available for summed combinations of analytes. In summed columns (eg., BTEX), the reported values should be considered ESTIMATED if any of the individual compounds were reported as bdl.

BLK_ENV-46297-LSCRPT.TXT
Library Search Compound Report

Data File : C:\MSDCHEM\5\20784505FRM\BLK_ENV-46297.D  Vial: 11
Acq On  : 18 Nov 2010  17:15  Operator: LIMS import
Sample  : METHOD BLANK Samples  Inst  : UC-SPG5-D
Misc  :  Multiplr: 1.00
MS Integration Params: jwint.p
Quant Method : C:\MSDCHEM\1\METHODS\LIMS_A1_5.M (RTE Integrator)
Title  : Gore Expanded Target VOCs/SVOCs
Library  : C:\DATABASE\NIST02.L

**********

Peak Number  1  Ethene, 1,2-difluoro-  Concentration Rank  1

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.52 | 0.22 ug | 22530 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Ethene, 1,1-difluoro- | 64 | C2H2F2 | 000075-38-7 | 3 |
| 2 | Ethene, 1,1-difluoro- | 64 | C2H2F2 | 000075-38-7 | 3 |
| 3 | Ethene, 1,2-difluoro- | 64 | C2H2F2 | 001691-13-0 | 3 |
| 4 | Ethene, 1,1-difluoro- | 64 | C2H2F2 | 000075-38-7 | 3 |

BLK_ENV-46297.D  LIMS_A1_5.M  Tue Dec 21 12:07:00 2010  D.00.00

BLK_ENV-46303-LSCRPT.TXT
Library Search Compound Report

Data File : C:\MSDCHEM\5\20784505FRM\BLK_ENV-46303.D  Vial: 47
Acq On  : 19 Nov 2010  10:01  Operator: LIMS import
Sample  : METHOD BLANK Samples  Inst  : UC-SPG5-D
Misc  :  Multiplr: 1.00
MS Integration Params: jwint.p
Quant Method : C:\MSDCHEM\1\METHODS\LIMS_A1_5.M (RTE Integrator)
Title  : Gore Expanded Target VOCs/SVOCs
Library  : C:\DATABASE\NIST02.L

**********

Peak Number  1  Ethene, 1,1-difluoro-  Concentration Rank  1

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.47 | 0.26 ug | 26054 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Ethene, 1,1-difluoro- | 64 | C2H2F2 | 000075-38-7 | 3 |
| 2 | Ethene, 1,1-difluoro- | 64 | C2H2F2 | 000075-38-7 | 3 |
| 3 | Ethene, 1,2-difluoro- | 64 | C2H2F2 | 001691-13-0 | 3 |
| 4 | Ethene, 1,1-difluoro- | 64 | C2H2F2 | 000075-38-7 | 3 |

BLK_ENV-46303.D  LIMS_A1_5.M  Tue Dec 21 12:04:55 2010  D.00.00

0648027-LSCRPT.TXT
Library Search Compound Report

Data File : C:\MSDCHEM\5\20784505FRM\0648027.D Vial: 55
Acq On : 19 Nov 2010 13:44 Operator: LIMS import
Sample : Inst : UC-SPG5-D
Misc : Multiplr: 1.00
MS Integration Params: jwint.p
Quant Method : C:\MSDCHEM\1\METHODS\LIMS_A1_5.M (RTE Integrator)
Title : Gore Expanded Target VOCs/SVOCs
Library : C:\DATABASE\NIST02.L

**********

Peak Number 1 Sulfur dioxide Concentration Rank 5

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.47 | 9.20 ug | 938750 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Sulfur dioxide | 64 | O2S | 007446-09-5 | 90 |
| 2 | Sulfur dioxide | 64 | O2S | 007446-09-5 | 83 |
| 3 | Aminomethanesulfonic acid | 111 | CH5NO3S | 013881-91-9 | 74 |
| 4 | Aminomethanesulfonic acid | 111 | CH5NO3S | 013881-91-9 | 64 |

**********

Peak Number 2 Cyclopentene, 3-isopropenyl... Concentration Rank 4

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 5.95 | 9.97 ug | 1016560 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Cyclopentene, 3-isopropenyl-5,5-... | 136 | C10H16 | 1000162-25-4 | 70 |
| 2 | Bicyclo[2.2.1]hept-2-ene, 1,7,7-... | 136 | C10H16 | 000464-17-5 | 55 |
| 3 | Cyclohexene, 1-methyl-4-(1-methy... | 136 | C10H16 | 000586-62-9 | 49 |
| 4 | Bicyclo[2.2.2]oct-5-en-2-one | 122 | C8H10O | 002220-40-8 | 46 |

**********

Peak Number 3 1R-.alpha.-Pinene Concentration Rank 1

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 6.25 | 454.47 ug | 46356100 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | 1R-.alpha.-Pinene | 136 | C10H16 | 007785-70-8 | 97 |
| 2 | 1R-.alpha.-Pinene | 136 | C10H16 | 007785-70-8 | 96 |
| 3 | .alpha.-Pinene | 136 | C10H16 | 000080-56-8 | 96 |
| 4 | Tricyclo[2.2.1.0(2,6)]heptane, 1... | 136 | C10H16 | 000488-97-1 | 95 |

**********

Peak Number 4 Camphene Concentration Rank 2

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 6.40 | 188.51 ug | 19228300 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Camphene | 136 | C10H16 | 000079-92-5 | 97 |
| 2 | Camphene | 136 | C10H16 | 000079-92-5 | 97 |
| 3 | Camphene | 136 | C10H16 | 000079-92-5 | 97 |
| 4 | Bicyclo[2.2.1]heptane, 2,2-dimet... | 136 | C10H16 | 005794-04-7 | 97 |

**********

Peak Number 5 .beta.-Pinene Concentration Rank 3

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 6.63 | 46.60 ug | 4753480 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Bicyclo[3.1.1]heptane, 6,6-dimet... | 136 | C10H16 | 018172-67-3 | 97 |
| 2 | .beta.-Pinene | 136 | C10H16 | 000127-91-3 | 97 |
| 3 | .beta.-Pinene | 136 | C10H16 | 000127-91-3 | 96 |
| 4 | .beta.-Pinene | 136 | C10H16 | 000127-91-3 | 95 |

0648027.D LIMS_A1_5.M Tue Dec 21 12:02:43 2010 D.00.00

0648028-LSCRPT.TXT
Library Search Compound Report

Data File : C:\MSDCHEM\5\20784505FRM\0648028.D Vial: 39
Acq On : 19 Nov 2010 6:18 Operator: LIMS import
Sample : Inst : UC-SPG5-D
Misc : Multiplr: 1.00
MS Integration Params: jwint.p
Quant Method : C:\MSDCHEM\1\METHODS\LIMS_A1_5.M (RTE Integrator)
Title : Gore Expanded Target VOCs/SVOCs
Library : C:\DATABASE\NIST02.L

**********

Peak Number 1 Carbon dioxide Concentration Rank 4

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.39 | 0.37 ug | 38003 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Carbon dioxide | 44 | CO2 | 000124-38-9 | 2 |
| 2 | Nitrous Oxide | 44 | N2O | 010024-97-2 | 2 |
| 3 | Ethyne, fluoro- | 44 | C2HF | 002713-09-9 | 2 |
| 4 | Nitrous Oxide | 44 | N2O | 010024-97-2 | 2 |

**********

Peak Number 2 Sulfur dioxide Concentration Rank 2

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.45 | 1.56 ug | 158852 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Sulfur dioxide | 64 | O2S | 007446-09-5 | 74 |
| 2 | Sulfur dioxide | 64 | O2S | 007446-09-5 | 74 |
| 3 | Aminomethanesulfonic acid | 111 | CH5NO3S | 013881-91-9 | 74 |
| 4 | Aminomethanesulfonic acid | 111 | CH5NO3S | 013881-91-9 | 64 |

**********

Peak Number 3 1R-.alpha.-Pinene Concentration Rank 1

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 6.21 | 3.40 ug | 346361 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | 1R-.alpha.-Pinene | 136 | C10H16 | 007785-70-8 | 96 |
| 2 | .alpha.-Pinene | 136 | C10H16 | 000080-56-8 | 96 |
| 3 | 1R-.alpha.-Pinene | 136 | C10H16 | 007785-70-8 | 95 |
| 4 | Bicyclo[3.1.1]hept-2-ene, 3,6,6-... | 136 | C10H16 | 004889-83-2 | 94 |

**********

Peak Number 4 Camphene Concentration Rank 3

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 6.38 | 1.40 ug | 142885 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Camphene | 136 | C10H16 | 000079-92-5 | 95 |
| 2 | Bicyclo[2.2.1]heptane, 2,2-dimet... | 136 | C10H16 | 005794-04-7 | 95 |
| 3 | Camphene | 136 | C10H16 | 000079-92-5 | 95 |
| 4 | Camphene | 136 | C10H16 | 000079-92-5 | 94 |

**********

Peak Number 5 Butane, 2,2-dimethyl- Concentration Rank 5

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 6.62 | 0.15 ug | 15539 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Butane, 2,2-dimethyl- | 86 | C6H14 | 000075-83-2 | 9 |
| 2 | Butane, 2,2-dimethyl- | 86 | C6H14 | 000075-83-2 | 9 |
| 3 | Butanal | 72 | C4H8O | 000123-72-8 | 7 |
| 4 | 1-Propene, 3-methoxy- | 72 | C4H8O | 000627-40-7 | 7 |

**********

Peak Number 6 Butane, 2,2-dimethyl- Concentration Rank 6

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 6.62 | 0.15 ug | 15539 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Butane, 2,2-dimethyl- | 86 | C6H14 | 000075-83-2 | 90 |
| 2 | Butane, 2,2-dimethyl- | 86 | C6H14 | 000075-83-2 | 90 |
| 3 | Butane, 2,2-dimethyl- | 86 | C6H14 | 000075-83-2 | 78 |
| 4 | Butane, 2,2-dimethyl- | 86 | C6H14 | 000075-83-2 | 72 |

0648028.D LIMS_A1_5.M Fri Dec 17 11:23:34 2010 D.00.00

0648070-LSCRPT.TXT
Library Search Compound Report

Data File : C:\MSDCHEM\5\20784505FRM\0648070.D Vial: 12
Acq On : 18 Nov 2010 17:43 Operator: LIMS import
Sample : Inst : UC-SPG5-D
Misc : Multiplr: 1.00
MS Integration Params: jwint.p
Quant Method : C:\MSDCHEM\1\METHODS\LIMS_A1_5.M (RTE Integrator)
Title : Gore Expanded Target VOCs/SVOCs
Library : C:\DATABASE\NIST02.L

**********

Peak Number 1 Carbon dioxide Concentration Rank 5

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.43 | 0.30 ug | 30826 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Carbon dioxide | 44 | CO2 | 000124-38-9 | 2 |
| 2 | Nitrous Oxide | 44 | N2O | 010024-97-2 | 2 |
| 3 | Carbon dioxide | 44 | CO2 | 000124-38-9 | 2 |
| 4 | Ethyne, fluoro- | 44 | C2HF | 002713-09-9 | 2 |

**********

Peak Number 2 Aminomethanesulfonic acid Concentration Rank 4

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.50 | 0.43 ug | 44019 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Sulfur dioxide | 64 | O2S | 007446-09-5 | 74 |
| 2 | Aminomethanesulfonic acid | 111 | CH5NO3S | 013881-91-9 | 74 |
| 3 | Aminomethanesulfonic acid | 111 | CH5NO3S | 013881-91-9 | 64 |
| 4 | Aminomethanesulfonic acid | 111 | CH5NO3S | 013881-91-9 | 9 |

**********

Peak Number 3 Trimethylsilyl fluoride Concentration Rank 1

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.58 | 2.22 ug | 226692 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Trimethylsilyl fluoride | 92 | C3H9FSi | 000420-56-4 | 91 |
| 2 | Trimethylsilyl fluoride | 92 | C3H9FSi | 000420-56-4 | 90 |
| 3 | Propane, 2-chloro-2-nitro- | 123 | C3H6ClNO2 | 000594-71-8 | 9 |
| 4 | Trimethylphosphine oxide | 92 | C3H9OP | 000676-96-0 | 4 |

**********

Peak Number 4 2-Methyl-1-butene Concentration Rank 3

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.75 | 0.97 ug | 99254 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | 2-Pentene, (Z)- | 70 | C5H10 | 000627-20-3 | 47 |
| 2 | 2-Methyl-1-butene | 70 | C5H10 | 000563-46-2 | 47 |
| 3 | Cyclopropane, ethyl- | 70 | C5H10 | 001191-96-4 | 43 |
| 4 | Cyclopropane, 1,2-dimethyl-, cis- | 70 | C5H10 | 000930-18-7 | 43 |

**********

Peak Number 5 Disiloxane, hexamethyl- Concentration Rank 2

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 3.74 | 1.03 ug | 105366 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Disiloxane, hexamethyl- | 162 | C6H18OSi2 | 000107-46-0 | 90 |
| 2 | Disiloxane, hexamethyl- | 162 | C6H18OSi2 | 000107-46-0 | 83 |
| 3 | Disiloxane, hexamethyl- | 162 | C6H18OSi2 | 000107-46-0 | 78 |
| 4 | Butylsemithiocarbazide | 147 | C5H13N3S | 006610-31-7 | 64 |

0648070.D LIMS_A1_5.M Tue Dec 21 11:32:57 2010 D.00.00

0648071-LSCRPT.TXT
Library Search Compound Report

Data File : C:\MSDCHEM\5\20784505FRM\0648071.D Vial: 64
Acq On : 19 Nov 2010 18:01 Operator: LIMS import
Sample : Inst : UC-SPG5-D
Misc : Multiplr: 1.00
MS Integration Params: jwint.p
Quant Method : C:\MSDCHEM\1\METHODS\LIMS_A1_5.M (RTE Integrator)
Title : Gore Expanded Target VOCs/SVOCs
Library : C:\DATABASE\NIST02.L

**********

Peak Number 1 Carbon dioxide Concentration Rank 5

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.41 | 0.38 ug | 39235 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Carbon dioxide | 44 | CO2 | 000124-38-9 | 2 |
| 2 | Nitrous Oxide | 44 | N2O | 010024-97-2 | 2 |
| 3 | Carbon dioxide | 44 | CO2 | 000124-38-9 | 2 |
| 4 | Ethyne, fluoro- | 44 | C2HF | 002713-09-9 | 2 |

**********

Peak Number 2 Ethene, chlorotrifluoro- Concentration Rank 2

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.46 | 0.71 ug | 72213 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Ethene, chlorotrifluoro- | 116 | C2ClF3 | 000079-38-9 | 97 |
| 2 | Ethene, chlorotrifluoro- | 116 | C2ClF3 | 000079-38-9 | 96 |
| 3 | 5-Chloro-1-methylimidazole | 116 | C4H5ClN2 | 000872-49-1 | 9 |
| 4 | 3-Ethylthiolane | 116 | C6H12S | 062184-67-2 | 9 |

**********

Peak Number 3 Phosphine, ethyl- Concentration Rank 3

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.52 | 0.53 ug | 54349 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | 1,2-Ethanediol | 62 | C2H6O2 | 000107-21-1 | 3 |
| 2 | Phosphine, ethyl- | 62 | C2H7P | 000593-68-0 | 3 |
| 3 | Ethanethiol | 62 | C2H6S | 000075-08-1 | 3 |
| 4 | Ethene, chloro- | 62 | C2H3Cl | 000075-01-4 | 3 |

**********

Peak Number 4 Ethene, 1,1-dichloro-2,2-di... Concentration Rank 1

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.63 | 1.20 ug | 122413 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Ethene, 1,1-dichloro-2,2-difluoro- | 132 | C2Cl2F2 | 000079-35-6 | 90 |
| 2 | Ethene, 1,1-dichloro-2,2-difluoro- | 132 | C2Cl2F2 | 000079-35-6 | 38 |
| 3 | Chloral Hydrate | 164 | C2H3Cl3O2 | 000302-17-0 | 22 |
| 4 | Trichloroacetic Acid | 162 | C2HCl3O2 | 000076-03-9 | 12 |

**********

Peak Number 5 trans-1,4-Hexadiene Concentration Rank 4

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.69 | 0.44 ug | 44426 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Cyclopropane, 1,2-dimethyl-3-met... | 82 | C6H10 | 062338-02-7 | 9 |
| 2 | 1,4-Pentadiene, 2-methyl- | 82 | C6H10 | 000763-30-4 | 9 |
| 3 | Ethenamine, N-methyl-N-nitroso- | 86 | C3H6N2O | 004549-40-0 | 9 |
| 4 | trans-1,4-Hexadiene | 82 | C6H10 | 007319-00-8 | 9 |

0648071.D LIMS_A1_5.M Tue Dec 21 11:34:32 2010 D.00.00

0648072-LSCRPT.TXT
Library Search Compound Report

Data File : C:\MSDCHEM\5\20784505FRM\0648072.D Vial: 31
Acq On : 19 Nov 2010 2:34 Operator: LIMS import
Sample : Inst : UC-SPG5-D
Misc : Multiplr: 1.00
MS Integration Params: jwint.p
Quant Method : C:\MSDCHEM\1\METHODS\LIMS_A1_5.M (RTE Integrator)
Title : Gore Expanded Target VOCs/SVOCs
Library : C:\DATABASE\NIST02.L

**********

Peak Number 1 Aminomethanesulfonic acid Concentration Rank 3

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.44 | 1.38 ug | 140667 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Aminomethanesulfonic acid | 111 | CH5NO3S | 013881-91-9 | 83 |
| 2 | Sulfur dioxide | 64 | O2S | 007446-09-5 | 74 |
| 3 | Sulfur dioxide | 64 | O2S | 007446-09-5 | 74 |
| 4 | Aminomethanesulfonic acid | 111 | CH5NO3S | 013881-91-9 | 74 |

**********

Peak Number 2 Phosphine, ethyl- Concentration Rank 4

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.49 | 0.89 ug | 90906 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Ethene, chloro- | 62 | C2H3Cl | 000075-01-4 | 78 |
| 2 | Ethene, chloro- | 62 | C2H3Cl | 000075-01-4 | 9 |
| 3 | Phosphine, ethyl- | 62 | C2H7P | 000593-68-0 | 9 |
| 4 | Ethanethiol | 62 | C2H6S | 000075-08-1 | 7 |

**********

Peak Number 3 Ethene, 1,1-dichloro-2,2-di... Concentration Rank 1

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.60 | 3.10 ug | 315766 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Ethene, 1,1-dichloro-2,2-difluoro- | 132 | C2Cl2F2 | 000079-35-6 | 92 |
| 2 | Ethene, 1,1-dichloro-2,2-difluoro- | 132 | C2Cl2F2 | 000079-35-6 | 46 |
| 3 | 1H-Purine, 2-methyl- | 134 | C6H6N4 | 000934-23-6 | 9 |
| 4 | 1,2,3-Trifluorobenzene | 132 | C6H3F3 | 001489-53-8 | 9 |

**********

Peak Number 4 Ethane, 1,2-dichloro-1,1,2-... Concentration Rank 2

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.67 | 2.19 ug | 222968 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Ethane, 1,2-dichloro-1,1,2-trifl... | 152 | C2HCl2F3 | 000354-23-4 | 68 |
| 2 | 1-Butyne, 3-methyl- | 68 | C5H8 | 000598-23-2 | 10 |
| 3 | 1,1'-Bicyclopropyl | 82 | C6H10 | 005685-46-1 | 10 |
| 4 | 2-Butyne | 54 | C4H6 | 000503-17-3 | 10 |

**********

Peak Number 5 Methylene Chloride Concentration Rank 5

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.83 | 0.66 ug | 66816 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Methylene Chloride | 84 | CH2Cl2 | 000075-09-2 | 91 |
| 2 | Methylene Chloride | 84 | CH2Cl2 | 000075-09-2 | 91 |
| 3 | Methylene Chloride | 84 | CH2Cl2 | 000075-09-2 | 91 |
| 4 | Methylene Chloride | 84 | CH2Cl2 | 000075-09-2 | 90 |

0648072.D LIMS_A1_5.M Tue Dec 21 11:35:48 2010 D.00.00

0648073-LSCRPT.TXT
Library Search Compound Report

Data File : C:\MSDCHEM\5\20784505FRM\0648073.D Vial: 45
Acq On : 19 Nov 2010 9:05 Operator: LIMS import
Sample : Inst : UC-SPG5-D
Misc : Multiplr: 1.00
MS Integration Params: jwint.p
Quant Method : C:\MSDCHEM\1\METHODS\LIMS_A1_5.M (RTE Integrator)
Title : Gore Expanded Target VOCs/SVOCs
Library : C:\DATABASE\NIST02.L

**********

Peak Number 1 Ethyl Chloride Concentration Rank 5

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.44 | 2.19 ug | 222949 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Ethyl Chloride | 64 | C2H5Cl | 000075-00-3 | 45 |
| 2 | Ethyl Chloride | 64 | C2H5Cl | 000075-00-3 | 38 |
| 3 | Ethyl Chloride | 64 | C2H5Cl | 000075-00-3 | 38 |
| 4 | (N-(-2-Acetamido))-2-aminoethane... | 182 | C4H10N2O4S | 007365-82-4 | 33 |

**********

Peak Number 2 Ethene, chloro- Concentration Rank 4

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.49 | 2.65 ug | 269967 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Ethene, chloro- | 62 | C2H3Cl | 000075-01-4 | 64 |
| 2 | Ethene, chloro- | 62 | C2H3Cl | 000075-01-4 | 64 |
| 3 | Ethane, 1,2-dichloro- | 98 | C2H4Cl2 | 000107-06-2 | 9 |
| 4 | Peroxide, dimethyl | 62 | C2H6O2 | 000690-02-8 | 7 |

**********

Peak Number 3 Ethene, 1,1-dichloro-2,2-di... Concentration Rank 3

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.60 | 3.49 ug | 355993 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Ethene, 1,1-dichloro-2,2-difluoro- | 132 | C2Cl2F2 | 000079-35-6 | 42 |
| 2 | Ethene, 1,1-dichloro-2,2-difluoro- | 132 | C2Cl2F2 | 000079-35-6 | 42 |
| 3 | Methyl methylphosphonofluoridate | 112 | C2H6FO2P | 000353-88-8 | 14 |
| 4 | n-Propylphosphonic dichloride | 160 | C3H7Cl2OP | 004708-04-7 | 10 |

**********

Peak Number 4 2-Butyne Concentration Rank 2

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.67 | 3.55 ug | 362059 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | 2-Butyne | 54 | C4H6 | 000503-17-3 | 80 |
| 2 | 2-Butyne | 54 | C4H6 | 000503-17-3 | 80 |
| 3 | 2-Butyne | 54 | C4H6 | 000503-17-3 | 80 |
| 4 | 1-Butyne | 54 | C4H6 | 000107-00-6 | 72 |

**********

Peak Number 5 Ethyl ether Concentration Rank 1

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.71 | 12.56 ug | 1281370 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Ethyl ether | 74 | C4H10O | 000060-29-7 | 90 |
| 2 | Ethyl ether | 74 | C4H10O | 000060-29-7 | 90 |
| 3 | Ethyl ether | 74 | C4H10O | 000060-29-7 | 90 |
| 4 | Ethane, 1,2-diethoxy- | 118 | C6H14O2 | 000629-14-1 | 78 |

0648073.D LIMS_A1_5.M Tue Dec 21 11:41:06 2010 D.00.00

0648074-LSCRPT.TXT
Library Search Compound Report

Data File : C:\MSDCHEM\5\20784505FRM\0648074.D Vial: 37
Acq On : 19 Nov 2010 5:21 Operator: LIMS import
Sample : Inst : UC-SPG5-D
Misc : Multiplr: 1.00
MS Integration Params: jwint.p
Quant Method : C:\MSDCHEM\1\METHODS\LIMS_A1_5.M (RTE Integrator)
Title : Gore Expanded Target VOCs/SVOCs
Library : C:\DATABASE\NIST02.L

**********

Peak Number 1 Carbon dioxide Concentration Rank 2

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.41 | 0.38 ug | 38436 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Carbon dioxide | 44 | CO2 | 000124-38-9 | 2 |
| 2 | Nitrous Oxide | 44 | N2O | 010024-97-2 | 2 |
| 3 | Carbon dioxide | 44 | CO2 | 000124-38-9 | 2 |
| 4 | Ethyne, fluoro- | 44 | C2HF | 002713-09-9 | 2 |

**********

Peak Number 2 Sulfur dioxide Concentration Rank 1

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.47 | 0.69 ug | 70805 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Sulfur dioxide | 64 | O2S | 007446-09-5 | 74 |
| 2 | Sulfur dioxide | 64 | O2S | 007446-09-5 | 74 |
| 3 | Aminomethanesulfonic acid | 111 | CH5NO3S | 013881-91-9 | 64 |
| 4 | Cysteic acid | 169 | C3H7NO5S | 1000131-23-1 | 64 |

**********

Peak Number 3 Indolizine Concentration Rank 3

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.68 | 0.24 ug | 24940 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Indolizine | 117 | C8H7N | 000274-40-8 | 4 |
| 2 | Chlorine dioxide | 67 | ClO2 | 010049-04-4 | 4 |
| 3 | Indole | 117 | C8H7N | 000120-72-9 | 2 |
| 4 | Benzonitrile, 2-methyl- | 117 | C8H7N | 000529-19-1 | 2 |

0648074.D LIMS_A1_5.M Tue Dec 21 11:42:21 2010 D.00.00

0648076-LSCRPT.TXT
Library Search Compound Report

Data File : C:\MSDCHEM\5\20784505FRM\0648076.D Vial: 44
Acq On : 19 Nov 2010 8:37 Operator: LIMS import
Sample : Inst : UC-SPG5-D
Misc : Multiplr: 1.00
MS Integration Params: jwint.p
Quant Method : C:\MSDCHEM\1\METHODS\LIMS_A1_5.M (RTE Integrator)
Title : Gore Expanded Target VOCs/SVOCs
Library : C:\DATABASE\NIST02.L

**********

Peak Number 1 Carbon dioxide Concentration Rank 2

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.39 | 0.30 ug | 30220 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Carbon dioxide | 44 | CO2 | 000124-38-9 | 2 |
| 2 | Nitrous Oxide | 44 | N2O | 010024-97-2 | 2 |
| 3 | Carbon dioxide | 44 | CO2 | 000124-38-9 | 2 |
| 4 | Ethyne, fluoro- | 44 | C2HF | 002713-09-9 | 2 |

**********

Peak Number 2 Sulfur dioxide Concentration Rank 1

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.44 | 0.71 ug | 72430 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Sulfur dioxide | 64 | O2S | 007446-09-5 | 74 |
| 2 | Sulfur dioxide | 64 | O2S | 007446-09-5 | 74 |
| 3 | L-Alanine, 3-sulfo- | 169 | C3H7NO5S | 000498-40-8 | 9 |
| 4 | Aminomethanesulfonic acid | 111 | CH5NO3S | 013881-91-9 | 9 |

**********

Peak Number 3 Oxetane, 2,4-dimethyl-, trans- Concentration Rank 3

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.69 | 0.14 ug | 14054 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Oxetane, 2,4-dimethyl-, trans- | 86 | C5H10O | 029424-94-0 | 4 |
| 2 | Fluoroacetic acid | 78 | C2H3FO2 | 000144-49-0 | 2 |
| 3 | 1-Propanol, 2-methyl- | 74 | C4H10O | 000078-83-1 | 2 |
| 4 | Butanenitrile, 2,3-dioxo-, dioxi... | 211 | C8H9N3O4 | 339246-62-7 | 1 |

0648076.D LIMS_A1_5.M Tue Dec 21 11:45:17 2010 D.00.00

0648075-LSCRPT.TXT
Library Search Compound Report

Data File : C:\MSDCHEM\5\20784505FRM\0648075.D Vial: 50
Acq On : 19 Nov 2010 11:25 Operator: LIMS import
Sample : Inst : UC-SPG5-D
Misc : Multiplr: 1.00
MS Integration Params: jwint.p
Quant Method : C:\MSDCHEM\1\METHODS\LIMS_A1_5.M (RTE Integrator)
Title : Gore Expanded Target VOCs/SVOCs
Library : C:\DATABASE\NIST02.L

**********

Peak Number 1 Carbon dioxide Concentration Rank 5

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.39 | 0.26 ug | 26144 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Carbon dioxide | 44 | CO2 | 000124-38-9 | 2 |
| 2 | Nitrous Oxide | 44 | N2O | 010024-97-2 | 2 |
| 3 | Carbon dioxide | 44 | CO2 | 000124-38-9 | 2 |
| 4 | Ethyne, fluoro- | 44 | C2HF | 002713-09-9 | 2 |

**********

Peak Number 2 Aminomethanesulfonic acid Concentration Rank 2

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.45 | 0.63 ug | 64169 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Sulfur dioxide | 64 | O2S | 007446-09-5 | 64 |
| 2 | Sulfur dioxide | 64 | O2S | 007446-09-5 | 64 |
| 3 | Aminomethanesulfonic acid | 111 | CH5NO3S | 013881-91-9 | 64 |
| 4 | Cysteic acid | 169 | C3H7NO5S | 1000131-23-1 | 64 |

**********

Peak Number 3 1-Propene, 2-methyl- Concentration Rank 3

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.50 | 0.51 ug | 52190 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | 1-Propene, 2-methyl- | 56 | C4H8 | 000115-11-7 | 45 |
| 2 | 1-Propene, 2-methyl- | 56 | C4H8 | 000115-11-7 | 42 |
| 3 | 1-Butene | 56 | C4H8 | 000106-98-9 | 33 |
| 4 | 1-Butene | 56 | C4H8 | 000106-98-9 | 33 |

**********

Peak Number 4 1-Propanol, 2-methyl- Concentration Rank 4

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.70 | 0.47 ug | 48175 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | 1,3-Dioxepin, 4,7-dihydro- | 100 | C5H8O2 | 005417-32-3 | 12 |
| 2 | Acetic acid, trifluoro-, pentyl ... | 184 | C7H11F3O2 | 000327-70-8 | 10 |
| 3 | 1-Propanol, 2-methyl- | 74 | C4H10O | 000078-83-1 | 9 |
| 4 | 1-Propanol, 2-methyl- | 74 | C4H10O | 000078-83-1 | 9 |

**********

Peak Number 5 Benzene, 1-chloro-2-methyl- Concentration Rank 1

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 6.38 | 24.77 ug | 2526340 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Benzene, 1-chloro-2-methyl- | 126 | C7H7Cl | 000095-49-8 | 97 |
| 2 | Benzene, 1-chloro-2-methyl- | 126 | C7H7Cl | 000095-49-8 | 96 |
| 3 | Benzene, 1-chloro-2-methyl- | 126 | C7H7Cl | 000095-49-8 | 95 |
| 4 | Benzene, 1-chloro-2-methyl- | 126 | C7H7Cl | 000095-49-8 | 95 |

0648075.D LIMS_A1_5.M Tue Dec 21 11:44:00 2010 D.00.00

0648078-LSCRPT.TXT
Library Search Compound Report

Data File : C:\MSDCHEM\5\20784505FRM\0648078.D Vial: 57
Acq On : 19 Nov 2010 14:40 Operator: LIMS import
Sample : Inst : UC-SPG5-D
Misc : Multiplr: 1.00
MS Integration Params: jwint.p
Quant Method : C:\MSDCHEM\1\METHODS\LIMS_A1_5.M (RTE Integrator)
Title : Gore Expanded Target VOCs/SVOCs
Library : C:\DATABASE\NIST02.L

**********

Peak Number 1 Carbon dioxide Concentration Rank 3

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.41 | 0.47 ug | 47535 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Carbon dioxide | 44 | CO2 | 000124-38-9 | 2 |
| 2 | Nitrous Oxide | 44 | N2O | 010024-97-2 | 2 |
| 3 | Ethyne, fluoro- | 44 | C2HF | 002713-09-9 | 2 |
| 4 | Nitrous Oxide | 44 | N2O | 010024-97-2 | 2 |

**********

Peak Number 2 Sulfur dioxide Concentration Rank 1

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.47 | 1.02 ug | 104477 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Sulfur dioxide | 64 | O2S | 007446-09-5 | 74 |
| 2 | Sulfur dioxide | 64 | O2S | 007446-09-5 | 74 |
| 3 | Aminomethanesulfonic acid | 111 | CH5NO3S | 013881-91-9 | 9 |
| 4 | Aminomethanesulfonic acid | 111 | CH5NO3S | 013881-91-9 | 9 |

**********

Peak Number 3 1-Propene, 2-methyl- Concentration Rank 2

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.52 | 0.53 ug | 53977 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | 1-Propene, 2-methyl- | 56 | C4H8 | 000115-11-7 | 7 |
| 2 | 2-Butene | 56 | C4H8 | 000107-01-7 | 7 |
| 3 | 1-Propene, 2-methyl- | 56 | C4H8 | 000115-11-7 | 7 |
| 4 | 1-Propene, 2-methyl- | 56 | C4H8 | 000115-11-7 | 7 |

**********

Peak Number 4 Ethylenimine Concentration Rank 5

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.64 | 0.14 ug | 13845 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Ethylenimine | 43 | C2H5N | 000151-56-4 | 5 |
| 2 | Ethylenimine | 43 | C2H5N | 000151-56-4 | 5 |
| 3 | Ethylenimine | 43 | C2H5N | 000151-56-4 | 5 |
| 4 | Cyclopropane | 42 | C3H6 | 000075-19-4 | 4 |

**********

Peak Number 5 1-Butanol Concentration Rank 4

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.71 | 0.34 ug | 34213 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Propene | 42 | C3H6 | 000115-07-1 | 37 |
| 2 | Propene | 42 | C3H6 | 000115-07-1 | 37 |
| 3 | 1-Butanol | 74 | C4H10O | 000071-36-3 | 2 |
| 4 | Propane, 1-chloro-2-methyl- | 92 | C4H9Cl | 000513-36-0 | 2 |

0648078.D LIMS_A1_5.M Tue Dec 21 11:48:42 2010 D.00.00

0648077-LSCRPT.TXT
Library Search Compound Report

Data File : C:\MSDCHEM\5\20784505FRM\0648077.D Vial: 15
Acq On : 18 Nov 2010 19:08 Operator: LIMS import
Sample : Inst : UC-SPG5-D
Misc : Multiplr: 1.00
MS Integration Params: jwint.p
Quant Method : C:\MSDCHEM\1\METHODS\LIMS_A1_5.M (RTE Integrator)
Title : Gore Expanded Target VOCs/SVOCs
Library : C:\DATABASE\NIST02.L

**********

Peak Number 1 Aminomethanesulfonic acid Concentration Rank 3

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.48 | 0.82 ug | 83837 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Aminomethanesulfonic acid | 111 | CH5NO3S | 013881-91-9 | 74 |
| 2 | Sulfur dioxide | 64 | O2S | 007446-09-5 | 74 |
| 3 | L-Alanine, 3-sulfo- | 169 | C3H7NO5S | 000498-40-8 | 9 |
| 4 | Aminomethanesulfonic acid | 111 | CH5NO3S | 013881-91-9 | 9 |

**********

Peak Number 2 1-Propene, 2-methyl- Concentration Rank 1

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.53 | 3.15 ug | 321604 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | 1-Propene, 2-methyl- | 56 | C4H8 | 000115-11-7 | 83 |
| 2 | 1-Propene, 2-methyl- | 56 | C4H8 | 000115-11-7 | 83 |
| 3 | 1-Butene | 56 | C4H8 | 000106-98-9 | 80 |
| 4 | 2-Butene, (Z)- | 56 | C4H8 | 000590-18-1 | 72 |

**********

Peak Number 3 Cyclopropane, ethyl- Concentration Rank 2

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.72 | 3.12 ug | 318054 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Cyclopropane, ethyl- | 70 | C5H10 | 001191-96-4 | 74 |
| 2 | 2-Pentene | 70 | C5H10 | 000109-68-2 | 62 |
| 3 | 2-Pentene, (Z)- | 70 | C5H10 | 000627-20-3 | 58 |
| 4 | 3-Buten-1-ol | 72 | C4H8O | 000627-27-0 | 52 |

**********

Peak Number 4 Cyclopropane, 1,1-dimethyl- Concentration Rank 5

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.79 | 0.57 ug | 58164 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | 2-Pentene, (E)- | 70 | C5H10 | 000646-04-8 | 9 |
| 2 | 2-Pentene | 70 | C5H10 | 000109-68-2 | 9 |
| 3 | 2-Pentene, (Z)- | 70 | C5H10 | 000627-20-3 | 9 |
| 4 | Cyclopropane, 1,1-dimethyl- | 70 | C5H10 | 001630-94-0 | 7 |

**********

Peak Number 5 1-Pentene, 4-methyl- Concentration Rank 4

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 3.17 | 0.60 ug | 61247 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | 1-Pentene, 4-methyl- | 84 | C6H12 | 000691-37-2 | 52 |
| 2 | 1-Pentene, 4-methyl- | 84 | C6H12 | 000691-37-2 | 50 |
| 3 | Hexane | 86 | C6H14 | 000110-54-3 | 43 |
| 4 | 1-Pentene, 4-methyl- | 84 | C6H12 | 000691-37-2 | 38 |

0648077.D LIMS_A1_5.M Tue Dec 21 11:46:51 2010 D.00.00

0648079-LSCRPT.TXT
Library Search Compound Report

Data File : C:\MSDCHEM\5\20784505FRM\0648079.D Vial: 30
Acq On : 19 Nov 2010 2:06 Operator: LIMS import
Sample : Inst : UC-SPG5-D
Misc : Multiplr: 1.00
MS Integration Params: jwint.p
Quant Method : C:\MSDCHEM\1\METHODS\LIMS_A1_5.M (RTE Integrator)
Title : Gore Expanded Target VOCs/SVOCs
Library : C:\DATABASE\NIST02.L

**********

Peak Number 1 Carbon dioxide Concentration Rank 4

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.39 | 0.28 ug | 28242 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Carbon dioxide | 44 | CO2 | 000124-38-9 | 2 |
| 2 | Nitrous Oxide | 44 | N2O | 010024-97-2 | 2 |
| 3 | Carbon dioxide | 44 | CO2 | 000124-38-9 | 2 |
| 4 | Ethyne, fluoro- | 44 | C2HF | 002713-09-9 | 2 |

**********

Peak Number 2 Aminomethanesulfonic acid Concentration Rank 3

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.45 | 0.29 ug | 29300 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Sulfur dioxide | 64 | O2S | 007446-09-5 | 74 |
| 2 | Aminomethanesulfonic acid | 111 | CH5NO3S | 013881-91-9 | 64 |
| 3 | 2-Aminoethyl hydrogen sulfate | 141 | C2H7NO4S | 000926-39-6 | 9 |
| 4 | L-Alanine, 3-sulfo- | 169 | C3H7NO5S | 000498-40-8 | 9 |

**********

Peak Number 3 1-Propene, 2-methyl- Concentration Rank 2

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.50 | 1.19 ug | 120937 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | 1-Butene | 56 | C4H8 | 000106-98-9 | 64 |
| 2 | 1-Propene, 2-methyl- | 56 | C4H8 | 000115-11-7 | 64 |
| 3 | 1-Propene, 2-methyl- | 56 | C4H8 | 000115-11-7 | 59 |
| 4 | 2-Butene, (Z)- | 56 | C4H8 | 000590-18-1 | 58 |

**********

Peak Number 4 Cyclopropane, ethyl- Concentration Rank 1

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.69 | 1.19 ug | 121690 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Pentane | 72 | C5H12 | 000109-66-0 | 59 |
| 2 | Cyclopropane, ethyl- | 70 | C5H10 | 001191-96-4 | 58 |
| 3 | Cyclopropane, ethyl- | 70 | C5H10 | 001191-96-4 | 58 |
| 4 | Cyclopropane, ethyl- | 70 | C5H10 | 001191-96-4 | 53 |

**********

Peak Number 5 Hexane Concentration Rank 5

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 3.14 | 0.27 ug | 27815 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Tetrahydropyran | 86 | C5H10O | 000142-68-7 | 9 |
| 2 | Hexane | 86 | C6H14 | 000110-54-3 | 9 |
| 3 | Propanal, 2,2-dimethyl- | 86 | C5H10O | 000630-19-3 | 7 |
| 4 | Hexane | 86 | C6H14 | 000110-54-3 | 7 |

0648079.D LIMS_A1_5.M Tue Dec 21 11:50:53 2010 D.00.00

0648081-LSCRPT.TXT
Library Search Compound Report

Data File : C:\MSDCHEM\5\20784505FRM\0648081.D Vial: 74
Acq On : 19 Nov 2010 22:41 Operator: LIMS import
Sample : Inst : UC-SPG5-D
Misc : Multiplr: 1.00
MS Integration Params: jwint.p
Quant Method : C:\MSDCHEM\1\METHODS\LIMS_A1_5.M (RTE Integrator)
Title : Gore Expanded Target VOCs/SVOCs
Library : C:\DATABASE\NIST02.L

**********

Peak Number 1 Ethene, 1,2-difluoro- Concentration Rank 1

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.47 | 0.94 ug | 95946 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Ethene, 1,1-difluoro- | 64 | C2H2F2 | 000075-38-7 | 7 |
| 2 | Ethene, 1,2-difluoro- | 64 | C2H2F2 | 001691-13-0 | 5 |
| 3 | Ethene, 1,1-difluoro- | 64 | C2H2F2 | 000075-38-7 | 3 |
| 4 | Ethene, 1,1-difluoro- | 64 | C2H2F2 | 000075-38-7 | 3 |

**********

Peak Number 2 Acetone Concentration Rank 2

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.72 | 0.12 ug | 12508 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Acetone | 58 | C3H6O | 000067-64-1 | 3 |
| 2 | Ethylamine | 45 | C2H7N | 000075-04-7 | 3 |
| 3 | Acetone | 58 | C3H6O | 000067-64-1 | 3 |
| 4 | Acetone | 58 | C3H6O | 000067-64-1 | 3 |

0648081.D LIMS_A1_5.M Tue Dec 21 11:53:28 2010 D.00.00

0648080-LSCRPT.TXT
Library Search Compound Report

Data File : C:\MSDCHEM\5\20784505FRM\0648080.D Vial: 18
Acq On : 18 Nov 2010 20:31 Operator: LIMS import
Sample : Inst : UC-SPG5-D
Misc : Multiplr: 1.00
MS Integration Params: jwint.p
Quant Method : C:\MSDCHEM\1\METHODS\LIMS_A1_5.M (RTE Integrator)
Title : Gore Expanded Target VOCs/SVOCs
Library : C:\DATABASE\NIST02.L

**********

Peak Number 1 Carbon dioxide Concentration Rank 4

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.39 | 0.34 ug | 34665 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Carbon dioxide | 44 | CO2 | 000124-38-9 | 2 |
| 2 | Nitrous Oxide | 44 | N2O | 010024-97-2 | 2 |
| 3 | Carbon dioxide | 44 | CO2 | 000124-38-9 | 2 |
| 4 | Ethyne, fluoro- | 44 | C2HF | 002713-09-9 | 2 |

**********

Peak Number 2 Sulfur dioxide Concentration Rank 1

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.44 | 1.79 ug | 182220 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Sulfur dioxide | 64 | O2S | 007446-09-5 | 90 |
| 2 | Sulfur dioxide | 64 | O2S | 007446-09-5 | 83 |
| 3 | Aminomethanesulfonic acid | 111 | CH5NO3S | 013881-91-9 | 74 |
| 4 | Aminomethanesulfonic acid | 111 | CH5NO3S | 013881-91-9 | 64 |

**********

Peak Number 3 1-Propene, 2-methyl- Concentration Rank 2

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.50 | 1.24 ug | 126949 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | 1-Propene, 2-methyl- | 56 | C4H8 | 000115-11-7 | 59 |
| 2 | 1-Propene, 2-methyl- | 56 | C4H8 | 000115-11-7 | 50 |
| 3 | 2-Butene, (E)- | 56 | C4H8 | 000624-64-6 | 16 |
| 4 | 1-Propene, 2-methyl- | 56 | C4H8 | 000115-11-7 | 9 |

**********

Peak Number 4 Butane, 2-methyl- Concentration Rank 3

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.69 | 1.16 ug | 118521 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Butane, 2-methyl- | 72 | C5H12 | 000078-78-4 | 59 |
| 2 | Butane, 2-methyl- | 72 | C5H12 | 000078-78-4 | 59 |
| 3 | Pentane | 72 | C5H12 | 000109-66-0 | 59 |
| 4 | 3-Buten-1-ol | 72 | C4H8O | 000627-27-0 | 53 |

**********

Peak Number 5 1-Pentene, 3-methyl- Concentration Rank 5

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.92 | 0.26 ug | 26783 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | 1-Pentene, 3-methyl- | 84 | C6H12 | 000760-20-3 | 47 |
| 2 | 1-Pentene, 3-methyl- | 84 | C6H12 | 000760-20-3 | 43 |
| 3 | 1-Pentene, 3-methyl- | 84 | C6H12 | 000760-20-3 | 43 |
| 4 | Cyclopropane, 1-ethyl-2-methyl-,... | 84 | C6H12 | 019781-68-1 | 38 |

0648080.D LIMS_A1_5.M Tue Dec 21 11:52:28 2010 D.00.00

0648082-LSCRPT.TXT
Library Search Compound Report

Data File : C:\MSDCHEM\5\20784505FRM\0648082.D Vial: 43
Acq On : 19 Nov 2010 8:09 Operator: LIMS import
Sample : Inst : UC-SPG5-D
Misc : Multiplr: 1.00
MS Integration Params: jwint.p
Quant Method : C:\MSDCHEM\1\METHODS\LIMS_A1_5.M (RTE Integrator)
Title : Gore Expanded Target VOCs/SVOCs
Library : C:\DATABASE\NIST02.L

**********

Peak Number 1 Propene, hexafluoro- Concentration Rank 1

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.42 | 0.31 ug | 31250 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Propene, hexafluoro- | 150 | C3F6 | 000116-15-4 | 47 |
| 2 | 2-Butenoic acid, methyl ester, (Z)- | 100 | C5H8O2 | 004358-59-2 | 5 |
| 3 | Propene, hexafluoro- | 150 | C3F6 | 000116-15-4 | 4 |
| 4 | Butane, 1-(ethenyloxy)- | 100 | C6H12O | 000111-34-2 | 4 |

**********

Peak Number 2 Ethene, 1,2-difluoro- Concentration Rank 2

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.49 | 0.23 ug | 23734 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Ethene, 1,2-difluoro- | 64 | C2H2F2 | 001691-13-0 | 5 |
| 2 | Ethene, 1,1-difluoro- | 64 | C2H2F2 | 000075-38-7 | 5 |
| 3 | Ethene, 1,1-difluoro- | 64 | C2H2F2 | 000075-38-7 | 3 |
| 4 | Ethene, 1,1-difluoro- | 64 | C2H2F2 | 000075-38-7 | 3 |

0648082.D LIMS_A1_5.M Tue Dec 21 11:55:18 2010 D.00.00

0648029-LSCRPT.TXT
Library Search Compound Report

Data File : C:\MSDCHEM\5\20784505FRM\0648029.D Vial: 14
Acq On : 18 Nov 2010 18:40 Operator: LIMS import
Sample : Inst : UC-SPG5-D
Misc : Multiplr: 1.00
MS Integration Params: jwint.p
Quant Method : C:\MSDCHEM\1\METHODS\LIMS_A1_5.M (RTE Integrator)
Title : Gore Expanded Target VOCs/SVOCs
Library : C:\DATABASE\NIST02.L

**********

Peak Number 1 Carbon dioxide Concentration Rank 4

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.42 | 0.32 ug | 32749 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Carbon dioxide | 44 | CO2 | 000124-38-9 | 3 |
| 2 | Ethyne, fluoro- | 44 | C2HF | 002713-09-9 | 3 |
| 3 | Carbon dioxide | 44 | CO2 | 000124-38-9 | 3 |
| 4 | Ethylene oxide | 44 | C2H4O | 000075-21-8 | 3 |

**********

Peak Number 2 Hexane, tetradecafluoro- Concentration Rank 1

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.50 | 2.50 ug | 254597 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Hexane, tetradecafluoro- | 338 | C6F14 | 000355-42-0 | 72 |
| 2 | Heptane, hexadecafluoro- | 388 | C7F16 | 000335-57-9 | 72 |
| 3 | Heptane, hexadecafluoro- | 388 | C7F16 | 000335-57-9 | 64 |
| 4 | Hexane, tetradecafluoro- | 338 | C6F14 | 000355-42-0 | 59 |

**********

Peak Number 3 Perfluoro[1,2-bis(tetrahydr... Concentration Rank 2

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.52 | 2.16 ug | 220215 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Perfluoro[1,2-bis(tetrahydrofury... | 458 | C10H2F16O2 | 1000222-75-5 | 38 |
| 2 | [2,2,3,3,4,4-Hexafluoro-4-(fluor... | 367 | C5HF12NO2S | 091940-19-1 | 23 |
| 3 | 2H-Imidazole-2-thione, 1,3-dihydro- | 100 | C3H4N2S | 000872-35-5 | 9 |
| 4 | 3,3-Di(trifluoromethyl)diazirine | 178 | C3F6N2 | 003024-50-8 | 9 |

**********

Peak Number 4 Pentane Concentration Rank 3

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.72 | 0.36 ug | 37117 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Pentane | 72 | C5H12 | 000109-66-0 | 64 |
| 2 | Pentane | 72 | C5H12 | 000109-66-0 | 64 |
| 3 | Pentane | 72 | C5H12 | 000109-66-0 | 50 |
| 4 | 1-Butanol | 74 | C4H10O | 000071-36-3 | 43 |

0648029.D  LIMS_A1_5.M  Fri Dec 17 11:26:37 2010  D.00.00

0648030-LSCRPT.TXT
Library Search Compound Report

Data File : C:\MSDCHEM\5\20784505FRM\0648030.D Vial: 33
Acq On : 19 Nov 2010 3:30 Operator: LIMS import
Sample : Inst : UC-SPG5-D
Misc : Multiplr: 1.00
MS Integration Params: jwint.p
Quant Method : C:\MSDCHEM\1\METHODS\LIMS_A1_5.M (RTE Integrator)
Title : Gore Expanded Target VOCs/SVOCs
Library : C:\DATABASE\NIST02.L

**********

Peak Number 1 Carbon dioxide Concentration Rank 3

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.41 | 0.24 ug | 24514 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Ethylene oxide | 44 | C2H4O | 000075-21-8 | 2 |
| 2 | Acetaldehyde | 44 | C2H4O | 000075-07-0 | 2 |
| 3 | Carbon dioxide | 44 | CO2 | 000124-38-9 | 2 |
| 4 | Ethyne, fluoro- | 44 | C2HF | 002713-09-9 | 2 |

**********

Peak Number 2 1-Propene, 2-methyl- Concentration Rank 1

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.51 | 0.61 ug | 62413 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | 1-Propene, 2-methyl- | 56 | C4H8 | 000115-11-7 | 25 |
| 2 | 1-Propene, 2-methyl- | 56 | C4H8 | 000115-11-7 | 22 |
| 3 | 1-Propene, 2-methyl- | 56 | C4H8 | 000115-11-7 | 22 |
| 4 | 1-Butene | 56 | C4H8 | 000106-98-9 | 9 |

**********

Peak Number 3 Cyclopropane Concentration Rank 4

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.64 | 0.12 ug | 12155 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Cyclopropane | 42 | C3H6 | 000075-19-4 | 7 |
| 2 | Cyclopropane | 42 | C3H6 | 000075-19-4 | 7 |
| 3 | Cyanamide | 42 | CH2N2 | 000420-04-2 | 2 |
| 4 | Ketene | 42 | C2H2O | 000463-51-4 | 2 |

**********

Peak Number 4 1-Pentanol Concentration Rank 2

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.71 | 0.31 ug | 31223 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Acetic acid, trifluoro-, pentyl ... | 184 | C7H11F3O2 | 000327-70-8 | 23 |
| 2 | 1-Pentanol | 88 | C5H12O | 000071-41-0 | 17 |
| 3 | Pentane | 72 | C5H12 | 000109-66-0 | 9 |
| 4 | Pentane | 72 | C5H12 | 000109-66-0 | 9 |

**********

Peak Number 5 Butane, 2,3-dimethyl- Concentration Rank 5

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.97 | 0.11 ug | 11291 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Butane, 2,3-dimethyl- | 86 | C6H14 | 000079-29-8 | 4 |
| 2 | cis-1,3-Cyclohexanediamine | 114 | C6H14N2 | 026772-34-9 | 4 |
| 3 | n-Propyl chloride | 78 | C3H7Cl | 000540-54-5 | 3 |
| 4 | n-Propyl chloride | 78 | C3H7Cl | 000540-54-5 | 3 |

0648030.D LIMS_A1_5.M Fri Dec 17 11:32:41 2010 D.00.00

0648031-LSCRPT.TXT
Library Search Compound Report

Data File : C:\MSDCHEM\5\20784505FRM\0648031.D Vial: 70
Acq On : 19 Nov 2010 20:49 Operator: LIMS import
Sample : Inst : UC-SPG5-D
Misc : Multiplr: 1.00
MS Integration Params: jwint.p
Quant Method : C:\MSDCHEM\1\METHODS\LIMS_A1_5.M (RTE Integrator)
Title : Gore Expanded Target VOCs/SVOCs
Library : C:\DATABASE\NIST02.L

**********

Peak Number 1 Carbon dioxide Concentration Rank 4

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.40 | 0.29 ug | 29396 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Ethylene oxide | 44 | C2H4O | 000075-21-8 | 2 |
| 2 | Acetaldehyde | 44 | C2H4O | 000075-07-0 | 2 |
| 3 | Carbon dioxide | 44 | CO2 | 000124-38-9 | 2 |
| 4 | Ethyne, fluoro- | 44 | C2HF | 002713-09-9 | 2 |

**********

Peak Number 2 Sulfur dioxide Concentration Rank 3

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.46 | 0.45 ug | 45580 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Sulfur dioxide | 64 | O2S | 007446-09-5 | 74 |
| 2 | Aminomethanesulfonic acid | 111 | CH5NO3S | 013881-91-9 | 74 |
| 3 | Sulfur dioxide | 64 | O2S | 007446-09-5 | 74 |
| 4 | Aminomethanesulfonic acid | 111 | CH5NO3S | 013881-91-9 | 64 |

**********

Peak Number 3 1-Butene Concentration Rank 1

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.51 | 0.56 ug | 57471 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | 1-Butene | 56 | C4H8 | 000106-98-9 | 9 |
| 2 | 1-Butene | 56 | C4H8 | 000106-98-9 | 9 |
| 3 | 1-Propene, 2-methyl- | 56 | C4H8 | 000115-11-7 | 9 |
| 4 | 1-Propene, 2-methyl- | 56 | C4H8 | 000115-11-7 | 9 |

**********

Peak Number 4 Pentane Concentration Rank 2

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.70 | 0.54 ug | 54659 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Pentane | 72 | C5H12 | 000109-66-0 | 49 |
| 2 | Diaziridine,3,3-dimethyl- | 72 | C3H8N2 | 004901-76-2 | 38 |
| 3 | Diaziridine,3,3-dimethyl- | 72 | C3H8N2 | 004901-76-2 | 35 |
| 4 | Cyclopropane, ethyl- | 70 | C5H10 | 001191-96-4 | 16 |

**********

Peak Number 5 Acetamide, 2-fluoro- Concentration Rank 5

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.97 | 0.22 ug | 22434 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | 2-Propenamide | 71 | C3H5NO | 000079-06-1 | 5 |
| 2 | 2-Propenamide | 71 | C3H5NO | 000079-06-1 | 5 |
| 3 | Acetamide, 2-fluoro- | 77 | C2H4FNO | 000640-19-7 | 4 |
| 4 | 2-Propenamide | 71 | C3H5NO | 000079-06-1 | 4 |

0648031.D envdef.m Mon Dec 20 12:01:43 2010 D.00.00

0648032-LSCRPT.TXT
Library Search Compound Report

Data File : C:\MSDCHEM\5\20784505FRM\0648032.D Vial: 41
Acq On : 19 Nov 2010 7:13 Operator: LIMS import
Sample : Inst : UC-SPG5-D
Misc : Multiplr: 1.00
MS Integration Params: jwint.p
Quant Method : C:\MSDCHEM\1\METHODS\LIMS_A1_5.M (RTE Integrator)
Title : Gore Expanded Target VOCs/SVOCs
Library : C:\DATABASE\NIST02.L

**********

Peak Number 1 Ethyne, fluoro- Concentration Rank 3

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.38 | 0.24 ug | 24932 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Acetaldehyde | 44 | C2H4O | 000075-07-0 | 3 |
| 2 | Ethylene oxide | 44 | C2H4O | 000075-21-8 | 3 |
| 3 | Acetaldehyde | 44 | C2H4O | 000075-07-0 | 3 |
| 4 | Ethyne, fluoro- | 44 | C2HF | 002713-09-9 | 3 |

**********

Peak Number 2 Aminomethanesulfonic acid Concentration Rank 4

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.44 | 0.19 ug | 18947 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Sulfur dioxide | 64 | O2S | 007446-09-5 | 74 |
| 2 | Sulfur dioxide | 64 | O2S | 007446-09-5 | 74 |
| 3 | Aminomethanesulfonic acid | 111 | CH5NO3S | 013881-91-9 | 64 |
| 4 | Cysteic acid | 169 | C3H7NO5S | 1000131-23-1 | 64 |

**********

Peak Number 3 1-Propene, 2-methyl- Concentration Rank 1

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.49 | 0.50 ug | 51314 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | 1-Propene, 2-methyl- | 56 | C4H8 | 000115-11-7 | 58 |
| 2 | 1-Butene | 56 | C4H8 | 000106-98-9 | 53 |
| 3 | 1-Propene, 2-methyl- | 56 | C4H8 | 000115-11-7 | 53 |
| 4 | 1-Butene | 56 | C4H8 | 000106-98-9 | 53 |

**********

Peak Number 4 Pentane Concentration Rank 2

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.68 | 0.30 ug | 30663 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Aziridine, 2,2-dimethyl- | 71 | C4H9N | 002658-24-4 | 25 |
| 2 | Pentane | 72 | C5H12 | 000109-66-0 | 9 |
| 3 | Oxirane, ethyl- | 72 | C4H8O | 000106-88-7 | 9 |
| 4 | Pentane | 72 | C5H12 | 000109-66-0 | 9 |

**********

Peak Number 5 Cyclopropane Concentration Rank 5

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 3.12 | 0.11 ug | 11660 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | 2-Propen-1-amine | 57 | C3H7N | 000107-11-9 | 4 |
| 2 | Cyclopropane | 42 | C3H6 | 000075-19-4 | 4 |
| 3 | Cyclopropane | 42 | C3H6 | 000075-19-4 | 4 |
| 4 | Ethylenimine | 43 | C2H5N | 000151-56-4 | 4 |

0648032.D envdef.m Mon Dec 20 12:05:32 2010 D.00.00

0648033-LSCRPT.TXT
Library Search Compound Report

Data File : C:\MSDCHEM\5\20784505FRM\0648033.D Vial: 59
Acq On : 19 Nov 2010 15:36 Operator: LIMS import
Sample : Inst : UC-SPG5-D
Misc : Multiplr: 1.00
MS Integration Params: jwint.p
Quant Method : C:\MSDCHEM\1\METHODS\LIMS_A1_5.M (RTE Integrator)
Title : Gore Expanded Target VOCs/SVOCs
Library : C:\DATABASE\NIST02.L

**********

Peak Number 1 Carbon dioxide Concentration Rank 4

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.41 | 0.39 ug | 39610 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Carbon dioxide | 44 | CO2 | 000124-38-9 | 2 |
| 2 | Nitrous Oxide | 44 | N2O | 010024-97-2 | 2 |
| 3 | Ethylene oxide | 44 | C2H4O | 000075-21-8 | 2 |
| 4 | Carbon dioxide | 44 | CO2 | 000124-38-9 | 2 |

**********

Peak Number 2 Aminomethanesulfonic acid Concentration Rank 3

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.47 | 0.51 ug | 51947 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Aminomethanesulfonic acid | 111 | CH5NO3S | 013881-91-9 | 74 |
| 2 | Sulfur dioxide | 64 | O2S | 007446-09-5 | 74 |
| 3 | Aminomethanesulfonic acid | 111 | CH5NO3S | 013881-91-9 | 64 |
| 4 | Aminomethanesulfonic acid | 111 | CH5NO3S | 013881-91-9 | 64 |

**********

Peak Number 3 1-Propene, 2-methyl- Concentration Rank 2

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.52 | 0.58 ug | 59241 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | 1-Propene, 2-methyl- | 56 | C4H8 | 000115-11-7 | 50 |
| 2 | 1-Propene, 2-methyl- | 56 | C4H8 | 000115-11-7 | 50 |
| 3 | 1-Butene | 56 | C4H8 | 000106-98-9 | 9 |
| 4 | 1-Propene, 2-methyl- | 56 | C4H8 | 000115-11-7 | 9 |

**********

Peak Number 4 Pentane Concentration Rank 1

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.72 | 0.67 ug | 67898 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Pentane | 72 | C5H12 | 000109-66-0 | 43 |
| 2 | Pentane | 72 | C5H12 | 000109-66-0 | 43 |
| 3 | Cyclopropane, ethyl- | 70 | C5H10 | 001191-96-4 | 9 |
| 4 | Butane, 2-methyl- | 72 | C5H12 | 000078-78-4 | 9 |

**********

Peak Number 5 1-Propene, 2-methyl- Concentration Rank 5

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.94 | 0.16 ug | 16486 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | 1-Octanamine | 129 | C8H19N | 000111-86-4 | 9 |
| 2 | 1-Propene, 2-methyl- | 56 | C4H8 | 000115-11-7 | 7 |
| 3 | Propene | 42 | C3H6 | 000115-07-1 | 7 |
| 4 | 1-Propene, 2-methyl- | 56 | C4H8 | 000115-11-7 | 4 |

0648033.D envdef.m Mon Dec 20 12:07:17 2010 D.00.00

0648034-LSCRPT.TXT
Library Search Compound Report

Data File : C:\MSDCHEM\5\20784505FRM\0648034.D Vial: 42
Acq On : 19 Nov 2010 7:41 Operator: LIMS import
Sample : Inst : UC-SPG5-D
Misc : Multiplr: 1.00
MS Integration Params: jwint.p
Quant Method : C:\MSDCHEM\1\METHODS\LIMS_A1_5.M (RTE Integrator)
Title : Gore Expanded Target VOCs/SVOCs
Library : C:\DATABASE\NIST02.L

**********

Peak Number 1 Carbon dioxide Concentration Rank 4

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.39 | 0.35 ug | 35950 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Carbon dioxide | 44 | CO2 | 000124-38-9 | 2 |
| 2 | Nitrous Oxide | 44 | N2O | 010024-97-2 | 2 |
| 3 | Ethylene oxide | 44 | C2H4O | 000075-21-8 | 2 |
| 4 | Carbon dioxide | 44 | CO2 | 000124-38-9 | 2 |

**********

Peak Number 2 Aminomethanesulfonic acid Concentration Rank 1

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.44 | 0.72 ug | 73677 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Aminomethanesulfonic acid | 111 | CH5NO3S | 013881-91-9 | 74 |
| 2 | Sulfur dioxide | 64 | O2S | 007446-09-5 | 74 |
| 3 | Sulfur dioxide | 64 | O2S | 007446-09-5 | 74 |
| 4 | Aminomethanesulfonic acid | 111 | CH5NO3S | 013881-91-9 | 64 |

**********

Peak Number 3 1-Propene, 2-methyl- Concentration Rank 2

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.50 | 0.62 ug | 63271 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | 1-Propene, 2-methyl- | 56 | C4H8 | 000115-11-7 | 43 |
| 2 | 1-Propene, 2-methyl- | 56 | C4H8 | 000115-11-7 | 37 |
| 3 | 1-Propene, 2-methyl- | 56 | C4H8 | 000115-11-7 | 37 |
| 4 | Propane, 1-nitro- | 89 | C3H7NO2 | 000108-03-2 | 12 |

**********

Peak Number 4 Cyclopropane Concentration Rank 5

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.63 | 0.21 ug | 20991 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Propene | 42 | C3H6 | 000115-07-1 | 7 |
| 2 | Cyclopropane | 42 | C3H6 | 000075-19-4 | 7 |
| 3 | Cyclopropane | 42 | C3H6 | 000075-19-4 | 4 |
| 4 | Cyclobutane | 56 | C4H8 | 000287-23-0 | 4 |

**********

Peak Number 5 Pentane Concentration Rank 3

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.69 | 0.44 ug | 45193 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Pentane | 72 | C5H12 | 000109-66-0 | 47 |
| 2 | Pentane | 72 | C5H12 | 000109-66-0 | 46 |
| 3 | Pentane | 72 | C5H12 | 000109-66-0 | 43 |
| 4 | Pentane | 72 | C5H12 | 000109-66-0 | 43 |

0648034.D envdef.m Mon Dec 20 12:08:58 2010 D.00.00

0648036-LSCRPT.TXT
Library Search Compound Report

Data File : C:\MSDCHEM\5\20784505FRM\0648036.D Vial: 79
Acq On : 20 Nov 2010 1:00 Operator: LIMS import
Sample : Inst : UC-SPG5-D
Misc : Multiplr: 1.00
MS Integration Params: jwint.p
Quant Method : C:\MSDCHEM\1\METHODS\LIMS_A1_5.M (RTE Integrator)
Title : Gore Expanded Target VOCs/SVOCs
Library : C:\DATABASE\NIST02.L

**********

Peak Number 1 Carbon dioxide Concentration Rank 2

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.42 | 0.33 ug | 33623 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Carbon dioxide | 44 | CO2 | 000124-38-9 | 2 |
| 2 | Nitrous Oxide | 44 | N2O | 010024-97-2 | 2 |
| 3 | Carbon dioxide | 44 | CO2 | 000124-38-9 | 2 |
| 4 | Ethyne, fluoro- | 44 | C2HF | 002713-09-9 | 2 |

**********

Peak Number 2 Aminomethanesulfonic acid Concentration Rank 4

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.47 | 0.25 ug | 25607 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Sulfur dioxide | 64 | O2S | 007446-09-5 | 74 |
| 2 | Aminomethanesulfonic acid | 111 | CH5NO3S | 013881-91-9 | 74 |
| 3 | Aminomethanesulfonic acid | 111 | CH5NO3S | 013881-91-9 | 64 |
| 4 | Aminomethanesulfonic acid | 111 | CH5NO3S | 013881-91-9 | 9 |

**********

Peak Number 3 2-Butene, (Z)- Concentration Rank 1

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.52 | 0.38 ug | 39154 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | 2-Butene, (Z)- | 56 | C4H8 | 000590-18-1 | 5 |
| 2 | 2-Butene, (E)- | 56 | C4H8 | 000624-64-6 | 5 |
| 3 | 2-Butene, (E)- | 56 | C4H8 | 000624-64-6 | 5 |
| 4 | 2-Butene, (Z)- | 56 | C4H8 | 000590-18-1 | 5 |

**********

Peak Number 4 Butane, 2-methyl- Concentration Rank 3

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.72 | 0.25 ug | 25759 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Ethylenimine | 43 | C2H5N | 000151-56-4 | 5 |
| 2 | Butane, 2-methyl- | 72 | C5H12 | 000078-78-4 | 4 |
| 3 | Ethylenimine | 43 | C2H5N | 000151-56-4 | 4 |
| 4 | Cyanamide | 42 | CH2N2 | 000420-04-2 | 3 |

**********

Peak Number 5 Ketene Concentration Rank 5

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.99 | 0.14 ug | 14385 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Ketene | 42 | C2H2O | 000463-51-4 | 3 |
| 2 | Cyanamide | 42 | CH2N2 | 000420-04-2 | 3 |
| 3 | Methane, diazo- | 42 | CH2N2 | 000334-88-3 | 3 |
| 4 | 1-Butanol | 74 | C4H10O | 000071-36-3 | 2 |

0648036.D envdef.m Mon Dec 20 12:12:29 2010 D.00.00

0648035-LSCRPT.TXT
Library Search Compound Report

Data File : C:\MSDCHEM\5\20784505FRM\0648035.D Vial: 52
Acq On : 19 Nov 2010 12:20 Operator: LIMS import
Sample : Inst : UC-SPG5-D
Misc : Multiplr: 1.00
MS Integration Params: jwint.p
Quant Method : C:\MSDCHEM\1\METHODS\LIMS_A1_5.M (RTE Integrator)
Title : Gore Expanded Target VOCs/SVOCs
Library : C:\DATABASE\NIST02.L

**********

Peak Number 1 Carbon dioxide Concentration Rank 2

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.40 | 0.44 ug | 44960 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Carbon dioxide | 44 | CO2 | 000124-38-9 | 2 |
| 2 | Nitrous Oxide | 44 | N2O | 010024-97-2 | 2 |
| 3 | Ethylene oxide | 44 | C2H4O | 000075-21-8 | 2 |
| 4 | Carbon dioxide | 44 | CO2 | 000124-38-9 | 2 |

**********

Peak Number 2 Aminomethanesulfonic acid Concentration Rank 1

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.47 | 0.64 ug | 65473 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Aminomethanesulfonic acid | 111 | CH5NO3S | 013881-91-9 | 74 |
| 2 | Sulfur dioxide | 64 | O2S | 007446-09-5 | 74 |
| 3 | Sulfur dioxide | 64 | O2S | 007446-09-5 | 74 |
| 4 | L-Alanine, 3-sulfo- | 169 | C3H7NO5S | 000498-40-8 | 9 |

**********

Peak Number 3 2-Butene, (Z)- Concentration Rank 3

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.52 | 0.38 ug | 39264 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | 2-Butene, (Z)- | 56 | C4H8 | 000590-18-1 | 9 |
| 2 | 2-Butene, (E)- | 56 | C4H8 | 000624-64-6 | 9 |
| 3 | 2-Butene, (Z)- | 56 | C4H8 | 000590-18-1 | 9 |
| 4 | 2-Butene | 56 | C4H8 | 000107-01-7 | 9 |

**********

Peak Number 4 Pentanal, 2-methyl- Concentration Rank 4

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.71 | 0.32 ug | 32682 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Acetone | 58 | C3H6O | 000067-64-1 | 7 |
| 2 | Acetone | 58 | C3H6O | 000067-64-1 | 7 |
| 3 | Butane | 58 | C4H10 | 000106-97-8 | 4 |
| 4 | Pentanal, 2-methyl- | 100 | C6H12O | 000123-15-9 | 4 |

**********

Peak Number 5 1,3-Cyclopentadiene, 1,2-di... Concentration Rank 5

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.90 | 0.15 ug | 15247 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | 1,4-Cyclohexadiene, 1-methyl- | 94 | C7H10 | 004313-57-9 | 9 |
| 2 | 1,3,5-Hexatriene, 3-methyl-, (E)- | 94 | C7H10 | 024587-26-6 | 9 |
| 3 | 1,3-Cyclopentadiene, 1,2-dimethyl- | 94 | C7H10 | 004784-86-5 | 9 |
| 4 | Ethene, 1,2-difluoro- | 64 | C2H2F2 | 001691-13-0 | 5 |

0648035.D envdef.m Mon Dec 20 12:10:26 2010 D.00.00

0648037-LSCRPT.TXT
Library Search Compound Report

Data File : C:\MSDCHEM\5\20784505FRM\0648037.D Vial: 78
Acq On : 20 Nov 2010 00:33 Operator: LIMS import
Sample : Inst : UC-SPG5-D
Misc : Multiplr: 1.00
MS Integration Params: jwint.p
Quant Method : C:\MSDCHEM\1\METHODS\LIMS_A1_5.M (RTE Integrator)
Title : Gore Expanded Target VOCs/SVOCs
Library : C:\DATABASE\NIST02.L

**********

Peak Number 1 Carbon dioxide Concentration Rank 2

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.41 | 0.27 ug | 27317 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Carbon dioxide | 44 | CO2 | 000124-38-9 | 2 |
| 2 | Nitrous Oxide | 44 | N2O | 010024-97-2 | 2 |
| 3 | Carbon dioxide | 44 | CO2 | 000124-38-9 | 2 |
| 4 | Ethyne, fluoro- | 44 | C2HF | 002713-09-9 | 2 |

**********

Peak Number 2 Aminomethanesulfonic acid Concentration Rank 1

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.46 | 0.38 ug | 39260 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Sulfur dioxide | 64 | O2S | 007446-09-5 | 74 |
| 2 | Aminomethanesulfonic acid | 111 | CH5NO3S | 013881-91-9 | 74 |
| 3 | Aminomethanesulfonic acid | 111 | CH5NO3S | 013881-91-9 | 64 |
| 4 | Aminomethanesulfonic acid | 111 | CH5NO3S | 013881-91-9 | 9 |

**********

Peak Number 3 2-Butene, (E)- Concentration Rank 3

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.51 | 0.23 ug | 23653 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | 2-Butene, (E)- | 56 | C4H8 | 000624-64-6 | 5 |
| 2 | Cyclobutane | 56 | C4H8 | 000287-23-0 | 5 |
| 3 | 2-Butene, (Z)- | 56 | C4H8 | 000590-18-1 | 5 |
| 4 | Cyclobutane | 56 | C4H8 | 000287-23-0 | 4 |

**********

Peak Number 4 Cyclopropane Concentration Rank 4

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.71 | 0.18 ug | 18654 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Cyclopropane | 42 | C3H6 | 000075-19-4 | 4 |
| 2 | Cyclopropane | 42 | C3H6 | 000075-19-4 | 4 |
| 3 | Cyclopropane | 42 | C3H6 | 000075-19-4 | 4 |
| 4 | Ethanamine, N-methylene- | 57 | C3H7N | 043729-97-1 | 4 |

**********

Peak Number 5 Ethylenimine Concentration Rank 5

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 3.15 | 0.12 ug | 12525 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Ethylenimine | 43 | C2H5N | 000151-56-4 | 4 |
| 2 | Azetidine | 57 | C3H7N | 000503-29-7 | 4 |
| 3 | Ethylenimine | 43 | C2H5N | 000151-56-4 | 4 |
| 4 | Ethylenimine | 43 | C2H5N | 000151-56-4 | 4 |

0648037.D envdef.m Mon Dec 20 12:13:53 2010 D.00.00

0648038-LSCRPT.TXT
Library Search Compound Report

Data File : C:\MSDCHEM\5\20784505FRM\0648038.D Vial: 56
Acq On : 19 Nov 2010 14:12 Operator: LIMS import
Sample : Inst : UC-SPG5-D
Misc : Multiplr: 1.00
MS Integration Params: jwint.p
Quant Method : C:\MSDCHEM\1\METHODS\LIMS_A1_5.M (RTE Integrator)
Title : Gore Expanded Target VOCs/SVOCs
Library : C:\DATABASE\NIST02.L

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Peak Number 1 Carbon dioxide Concentration Rank 3

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.40 | 0.46 ug | 46615 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Carbon dioxide | 44 | CO2 | 000124-38-9 | 3 |
| 2 | Ethyne, fluoro- | 44 | C2HF | 002713-09-9 | 3 |
| 3 | Carbon dioxide | 44 | CO2 | 000124-38-9 | 3 |
| 4 | Ethylene oxide | 44 | C2H4O | 000075-21-8 | 3 |

**********

Peak Number 2 Sulfur dioxide Concentration Rank 1

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.46 | 0.85 ug | 86533 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | 2-Aminoethyl hydrogen sulfate | 141 | C2H7NO4S | 000926-39-6 | 74 |
| 2 | Aminomethanesulfonic acid | 111 | CH5NO3S | 013881-91-9 | 74 |
| 3 | Sulfur dioxide | 64 | O2S | 007446-09-5 | 74 |
| 4 | Sulfur dioxide | 64 | O2S | 007446-09-5 | 74 |

**********

Peak Number 3 Pyridine, pentafluoro- Concentration Rank 2

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.50 | 0.70 ug | 71156 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Carbamic chloride, diethyl- | 135 | C5H10ClNO | 000088-10-8 | 9 |
| 2 | 2-Propanone, dimethylhydrazone | 100 | C5H12N2 | 013483-31-3 | 5 |
| 3 | Pyridine, pentafluoro- | 169 | C5F5N | 000700-16-3 | 5 |
| 4 | 8-Fluoro-6-methyltetrazolo[1,5-c... | 169 | C5H4FN5O | 144877-46-3 | 4 |

**********

Peak Number 4 Butane Concentration Rank 5

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.70 | 0.30 ug | 31068 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Butane | 58 | C4H10 | 000106-97-8 | 7 |
| 2 | Butane | 58 | C4H10 | 000106-97-8 | 7 |
| 3 | Butane | 58 | C4H10 | 000106-97-8 | 4 |
| 4 | 1-Butanol | 74 | C4H10O | 000071-36-3 | 4 |

**********

Peak Number 5 Pyridine, 2-chloro- Concentration Rank 4

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 6.25 | 0.35 ug | 36189 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Pyridine, 2-chloro- | 113 | C5H4ClN | 000109-09-1 | 91 |
| 2 | Pyridine, 2-chloro- | 113 | C5H4ClN | 000109-09-1 | 91 |
| 3 | Pyridine, 3-chloro- | 113 | C5H4ClN | 000626-60-8 | 91 |
| 4 | Pyridine, 4-chloro- | 113 | C5H4ClN | 000626-61-9 | 91 |

0648038.D envdef.m Mon Dec 20 12:16:15 2010 D.00.00

0648039-LSCRPT.TXT
Library Search Compound Report

Data File : C:\MSDCHEM\5\20784505FRM\0648039.D Vial: 21
Acq On : 18 Nov 2010 21:55 Operator: LIMS import
Sample : Inst : UC-SPG5-D
Misc : Multiplr: 1.00
MS Integration Params: jwint.p
Quant Method : C:\MSDCHEM\1\METHODS\LIMS_A1_5.M (RTE Integrator)
Title : Gore Expanded Target VOCs/SVOCs
Library : C:\DATABASE\NIST02.L

**********

Peak Number 1 Hexane, tetradecafluoro- Concentration Rank 1

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.52 | 241.02 ug | 24583900 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Hexane, tetradecafluoro- | 338 | C6F14 | 000355-42-0 | 40 |
| 2 | Perfluorooctane | 438 | C8F18 | 000307-34-6 | 37 |
| 3 | Butanoic acid, heptafluoro-, eth... | 242 | C6H5F7O2 | 000356-27-4 | 36 |
| 4 | Hexane, tetradecafluoro- | 338 | C6F14 | 000355-42-0 | 35 |

**********

Peak Number 2 Pentane Concentration Rank 5

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.71 | 3.28 ug | 334067 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Pentane | 72 | C5H12 | 000109-66-0 | 80 |
| 2 | Pentane | 72 | C5H12 | 000109-66-0 | 78 |
| 3 | Pentane | 72 | C5H12 | 000109-66-0 | 78 |
| 4 | Pentane | 72 | C5H12 | 000109-66-0 | 64 |

**********

Peak Number 3 Hexane Concentration Rank 2

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 3.15 | 11.18 ug | 1140310 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Hexane | 86 | C6H14 | 000110-54-3 | 91 |
| 2 | Hexane | 86 | C6H14 | 000110-54-3 | 91 |
| 3 | Hexane | 86 | C6H14 | 000110-54-3 | 91 |
| 4 | Pentane, 2,2,3,4-tetramethyl- | 128 | C9H20 | 001186-53-4 | 42 |

**********

Peak Number 4 Heptane, 3-ethyl- Concentration Rank 4

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 3.82 | 4.57 ug | 466275 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Heptane, 2,5-dimethyl- | 128 | C9H20 | 002216-30-0 | 53 |
| 2 | Heptane, 2,2,3,5-tetramethyl- | 156 | C11H24 | 061868-42-6 | 50 |
| 3 | Pentane, 2,2,4-trimethyl- | 114 | C8H18 | 000540-84-1 | 47 |
| 4 | Heptane, 3-ethyl- | 128 | C9H20 | 015869-80-4 | 47 |

**********

Peak Number 5 Cyclohexane, methyl- Concentration Rank 3

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 4.19 | 6.49 ug | 662489 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Cyclohexane, methyl- | 98 | C7H14 | 000108-87-2 | 96 |
| 2 | Cyclohexane, methyl- | 98 | C7H14 | 000108-87-2 | 93 |
| 3 | Cyclohexane, methyl- | 98 | C7H14 | 000108-87-2 | 91 |
| 4 | Cyclohexane, methyl- | 98 | C7H14 | 000108-87-2 | 91 |

0648039.D envdef.m Mon Dec 20 12:17:22 2010 D.00.00

0648040-LSCRPT.TXT
Library Search Compound Report

Data File : C:\MSDCHEM\5\20784505FRM\0648040.D Vial: 32
Acq On : 19 Nov 2010 3:02 Operator: LIMS import
Sample : Inst : UC-SPG5-D
Misc : Multiplr: 1.00
MS Integration Params: jwint.p
Quant Method : C:\MSDCHEM\1\METHODS\LIMS_A1_5.M (RTE Integrator)
Title : Gore Expanded Target VOCs/SVOCs
Library : C:\DATABASE\NIST02.L

**********

Peak Number 1 (N-(-2-Acetamido))-2-aminoe... Concentration Rank 1

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.46 | 0.35 ug | 35213 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | (N-(-2-Acetamido))-2-aminoethane... | 182 | C4H10N2O4S | 007365-82-4 | 9 |
| 2 | Sulfur dioxide | 64 | O2S | 007446-09-5 | 7 |
| 3 | Ethylene oxide | 44 | C2H4O | 000075-21-8 | 4 |
| 4 | 2,3-Dimethylamphetamine | 163 | C11H17N | 075659-60-8 | 4 |

**********

Peak Number 2 Sulfur dioxide Concentration Rank 2

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.51 | 0.28 ug | 28145 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Ethene, 1,1-difluoro- | 64 | C2H2F2 | 000075-38-7 | 5 |
| 2 | Ethene, 1,2-difluoro- | 64 | C2H2F2 | 001691-13-0 | 5 |
| 3 | Sulfur dioxide | 64 | O2S | 007446-09-5 | 3 |
| 4 | Ethene, 1,1-difluoro- | 64 | C2H2F2 | 000075-38-7 | 3 |

0648040.D envdef.m Mon Dec 20 12:19:29 2010 D.00.00

0648041-LSCRPT.TXT
Library Search Compound Report

Data File : C:\MSDCHEM\5\20784505FRM\0648041.D Vial: 62
Acq On : 19 Nov 2010 17:05 Operator: LIMS import
Sample : Inst : UC-SPG5-D
Misc : Multiplr: 1.00
MS Integration Params: jwint.p
Quant Method : C:\MSDCHEM\1\METHODS\LIMS_A1_5.M (RTE Integrator)
Title : Gore Expanded Target VOCs/SVOCs
Library : C:\DATABASE\NIST02.L

**********

Peak Number 1 Carbon dioxide Concentration Rank 5

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.40 | 0.29 ug | 29243 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Carbon dioxide | 44 | CO2 | 000124-38-9 | 2 |
| 2 | Nitrous Oxide | 44 | N2O | 010024-97-2 | 2 |
| 3 | Carbon dioxide | 44 | CO2 | 000124-38-9 | 2 |
| 4 | Ethyne, fluoro- | 44 | C2HF | 002713-09-9 | 2 |

**********

Peak Number 2 Sulfur dioxide Concentration Rank 2

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.46 | 0.60 ug | 61415 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Sulfur dioxide | 64 | O2S | 007446-09-5 | 74 |
| 2 | Sulfur dioxide | 64 | O2S | 007446-09-5 | 74 |
| 3 | Aminomethanesulfonic acid | 111 | CH5NO3S | 013881-91-9 | 64 |
| 4 | Aminomethanesulfonic acid | 111 | CH5NO3S | 013881-91-9 | 64 |

**********

Peak Number 3 1-Propene, 2-methyl- Concentration Rank 3

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.51 | 0.40 ug | 41235 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | 1-Propene, 2-methyl- | 56 | C4H8 | 000115-11-7 | 38 |
| 2 | 1-Propene, 2-methyl- | 56 | C4H8 | 000115-11-7 | 32 |
| 3 | 2-Butenal, 2-ethenyl- | 96 | C6H8O | 020521-42-0 | 12 |
| 4 | Heptafluorobutyric acid, 2-methy... | 270 | C8H9F7O2 | 049669-71-8 | 12 |

**********

Peak Number 4 Pentane, 1-chloro- Concentration Rank 4

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.70 | 0.37 ug | 37839 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Pentane, 1-chloro- | 106 | C5H11Cl | 000543-59-9 | 9 |
| 2 | Cyclopropane | 42 | C3H6 | 000075-19-4 | 4 |
| 3 | Cyclopropane | 42 | C3H6 | 000075-19-4 | 4 |
| 4 | Cyclopropanecarboxaldehyde | 70 | C4H6O | 001489-69-6 | 4 |

**********

Peak Number 5 1,4-Dioxane Concentration Rank 1

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 4.03 | 1.09 ug | 111352 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | 1,4-Dioxane | 88 | C4H8O2 | 000123-91-1 | 91 |
| 2 | 1,4-Dioxane | 88 | C4H8O2 | 000123-91-1 | 91 |
| 3 | 1,4-Dioxane | 88 | C4H8O2 | 000123-91-1 | 90 |
| 4 | 1,4-Dioxane | 88 | C4H8O2 | 000123-91-1 | 83 |

0648041.D envdef.m Mon Dec 20 12:22:23 2010 D.00.00

0648042-LSCRPT.TXT
Library Search Compound Report

Data File : C:\MSDCHEM\5\20784505FRM\0648042.D Vial: 67
Acq On : 19 Nov 2010 19:25 Operator: LIMS import
Sample : Inst : UC-SPG5-D
Misc : Multiplr: 1.00
MS Integration Params: jwint.p
Quant Method : C:\MSDCHEM\1\METHODS\LIMS_A1_5.M (RTE Integrator)
Title : Gore Expanded Target VOCs/SVOCs
Library : C:\DATABASE\NIST02.L

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Peak Number 1 Carbon dioxide Concentration Rank 3

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.41 | 0.36 ug | 36451 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Carbon dioxide | 44 | CO2 | 000124-38-9 | 2 |
| 2 | Nitrous Oxide | 44 | N2O | 010024-97-2 | 2 |
| 3 | Ethylene oxide | 44 | C2H4O | 000075-21-8 | 2 |
| 4 | Carbon dioxide | 44 | CO2 | 000124-38-9 | 2 |

**********

Peak Number 2 Perfluoro[1,2-bis(tetrahydr... Concentration Rank 1

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.51 | 5.51 ug | 562221 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Perfluoro(2-methylpentane) | 338 | C6F14 | 000355-04-4 | 53 |
| 2 | Perfluoro[1,2-bis(tetrahydrofury... | 458 | C10H2F16O2 | 1000222-75-5 | 52 |
| 3 | Perfluorooctane | 438 | C8F18 | 000307-34-6 | 47 |
| 4 | Perfluorooctane | 438 | C8F18 | 000307-34-6 | 40 |

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Peak Number 3 Propene Concentration Rank 5

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.64 | 0.11 ug | 10803 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Propene | 42 | C3H6 | 000115-07-1 | 7 |
| 2 | Cyclopropanecarboxaldehyde | 70 | C4H6O | 001489-69-6 | 4 |
| 3 | Furan, 2,5-dihydro- | 70 | C4H6O | 001708-29-8 | 4 |
| 4 | Isobutyl nitrite | 103 | C4H9NO2 | 000542-56-3 | 2 |

**********

Peak Number 4 Benzyl nitrile Concentration Rank 2

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.68 | 0.36 ug | 37025 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Benzyl nitrile | 117 | C8H7N | 000140-29-4 | 7 |
| 2 | Benzyl nitrile | 117 | C8H7N | 000140-29-4 | 5 |
| 3 | Benzene, (isocyanomethyl)- | 117 | C8H7N | 010340-91-7 | 5 |
| 4 | 2-Thio-2,4-oxazolidinedione | 117 | C3H3NO2S | 002346-24-9 | 4 |

**********

Peak Number 5 Formamide, N-methylthio Concentration Rank 4

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.98 | 0.20 ug | 20456 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Formamide, N-methylthio | 75 | C2H5NS | 018952-41-5 | 7 |
| 2 | Glycine | 75 | C2H5NO2 | 000056-40-6 | 4 |
| 3 | Silanol, trimethyl- | 90 | C3H10OSi | 001066-40-6 | 4 |
| 4 | Propane, 1,1-dimethoxy- | 104 | C5H12O2 | 004744-10-9 | 4 |

0648042.D envdef.m Mon Dec 20 12:23:38 2010 D.00.00

0648043-LSCRPT.TXT
Library Search Compound Report

Data File : C:\MSDCHEM\5\20784505FRM\0648043.D Vial: 24
Acq On : 18 Nov 2010 23:19 Operator: LIMS import
Sample : Inst : UC-SPG5-D
Misc : Multiplr: 1.00
MS Integration Params: jwint.p
Quant Method : C:\MSDCHEM\1\METHODS\LIMS_A1_5.M (RTE Integrator)
Title : Gore Expanded Target VOCs/SVOCs
Library : C:\DATABASE\NIST02.L

**********

Peak Number 1 Carbon dioxide Concentration Rank 1

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.41 | 0.37 ug | 38213 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Carbon dioxide | 44 | CO2 | 000124-38-9 | 2 |
| 2 | Nitrous Oxide | 44 | N2O | 010024-97-2 | 2 |
| 3 | Carbon dioxide | 44 | CO2 | 000124-38-9 | 2 |
| 4 | Ethyne, fluoro- | 44 | C2HF | 002713-09-9 | 2 |

**********

Peak Number 2 Ethene, 1,1-difluoro- Concentration Rank 3

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.47 | 0.21 ug | 21799 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Ethene, 1,1-difluoro- | 64 | C2H2F2 | 000075-38-7 | 3 |
| 2 | Ethene, 1,1-difluoro- | 64 | C2H2F2 | 000075-38-7 | 3 |
| 3 | Ethene, 1,2-difluoro- | 64 | C2H2F2 | 001691-13-0 | 3 |
| 4 | Ethene, 1,1-difluoro- | 64 | C2H2F2 | 000075-38-7 | 3 |

**********

Peak Number 3 2-Butene Concentration Rank 2

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.52 | 0.27 ug | 27735 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | 2-Butene, (E)- | 56 | C4H8 | 000624-64-6 | 9 |
| 2 | 2-Butene, (E)- | 56 | C4H8 | 000624-64-6 | 9 |
| 3 | 2-Butene | 56 | C4H8 | 000107-01-7 | 9 |
| 4 | 2-Butene, (Z)- | 56 | C4H8 | 000590-18-1 | 9 |

**********

Peak Number 4 Pentane Concentration Rank 4

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.72 | 0.18 ug | 18147 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Diaziridine,3,3-dimethyl- | 72 | C3H8N2 | 004901-76-2 | 9 |
| 2 | Cyclopropane | 42 | C3H6 | 000075-19-4 | 5 |
| 3 | Cyclopropane | 42 | C3H6 | 000075-19-4 | 5 |
| 4 | Pentane | 72 | C5H12 | 000109-66-0 | 4 |

0648043.D  envdef.m  Mon Dec 20 12:25:58 2010  D.00.00

0648044-LSCRPT.TXT
Library Search Compound Report

Data File : C:\MSDCHEM\5\20784505FRM\0648044.D Vial: 68
Acq On : 19 Nov 2010 19:53 Operator: LIMS import
Sample : Inst : UC-SPG5-D
Misc : Multiplr: 1.00
MS Integration Params: jwint.p
Quant Method : C:\MSDCHEM\1\METHODS\LIMS_A1_5.M (RTE Integrator)
Title : Gore Expanded Target VOCs/SVOCs
Library : C:\DATABASE\NIST02.L

**********

Peak Number 1 Carbon dioxide Concentration Rank 4

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.41 | 0.48 ug | 48678 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Carbon dioxide | 44 | CO2 | 000124-38-9 | 2 |
| 2 | Nitrous Oxide | 44 | N2O | 010024-97-2 | 2 |
| 3 | Ethylene oxide | 44 | C2H4O | 000075-21-8 | 2 |
| 4 | Carbon dioxide | 44 | CO2 | 000124-38-9 | 2 |

**********

Peak Number 2 Aminomethanesulfonic acid Concentration Rank 1

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.47 | 1.16 ug | 118764 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Aminomethanesulfonic acid | 111 | CH5NO3S | 013881-91-9 | 74 |
| 2 | Sulfur dioxide | 64 | O2S | 007446-09-5 | 74 |
| 3 | Sulfur dioxide | 64 | O2S | 007446-09-5 | 74 |
| 4 | Aminomethanesulfonic acid | 111 | CH5NO3S | 013881-91-9 | 64 |

**********

Peak Number 3 3-Methyl-3-butenoic acid Concentration Rank 2

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.52 | 0.71 ug | 72870 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | 3-Methyl-3-butenoic acid | 100 | C5H8O2 | 001617-31-8 | 38 |
| 2 | Furan, 2,5-dihydro-3-methyl- | 84 | C5H8O | 001708-31-2 | 23 |
| 3 | Spiro { 6,6-dimethyl-2,3-diazobi... | 136 | C8H12N2 | 135485-30-2 | 12 |
| 4 | Bis(3-methylbutyl) fluorene-2,7-... | 466 | C23H30O6S2 | 253664-95-8 | 12 |

**********

Peak Number 4 Propene Concentration Rank 5

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.62 | 0.16 ug | 15851 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Propene | 42 | C3H6 | 000115-07-1 | 7 |
| 2 | Propane | 44 | C3H8 | 000074-98-6 | 3 |
| 3 | Propane | 44 | C3H8 | 000074-98-6 | 3 |
| 4 | Ethylene oxide | 44 | C2H4O | 000075-21-8 | 2 |

**********

Peak Number 5 Propene Concentration Rank 3

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.72 | 0.50 ug | 51279 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Cyclopropanecarboxaldehyde | 70 | C4H6O | 001489-69-6 | 25 |
| 2 | Propene | 42 | C3H6 | 000115-07-1 | 7 |
| 3 | 1-Butene, 3-methyl- | 70 | C5H10 | 000563-45-1 | 5 |
| 4 | 1-Butene, 3-methyl- | 70 | C5H10 | 000563-45-1 | 5 |

0648044.D envdef.m Mon Dec 20 12:27:15 2010 D.00.00

0648045-LSCRPT.TXT
Library Search Compound Report

Data File : C:\MSDCHEM\5\20784505FRM\0648045.D Vial: 25
Acq On : 18 Nov 2010 23:47 Operator: LIMS import
Sample : Inst : UC-SPG5-D
Misc : Multiplr: 1.00
MS Integration Params: jwint.p
Quant Method : C:\MSDCHEM\1\METHODS\LIMS_A1_5.M (RTE Integrator)
Title : Gore Expanded Target VOCs/SVOCs
Library : C:\DATABASE\NIST02.L

**********

Peak Number 1 Carbon dioxide Concentration Rank 3

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.40 | 0.28 ug | 28087 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Carbon dioxide | 44 | CO2 | 000124-38-9 | 2 |
| 2 | Nitrous Oxide | 44 | N2O | 010024-97-2 | 2 |
| 3 | Carbon dioxide | 44 | CO2 | 000124-38-9 | 2 |
| 4 | Ethyne, fluoro- | 44 | C2HF | 002713-09-9 | 2 |

**********

Peak Number 2 Sulfur dioxide Concentration Rank 1

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.47 | 0.32 ug | 32810 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Sulfur dioxide | 64 | O2S | 007446-09-5 | 74 |
| 2 | Sulfur dioxide | 64 | O2S | 007446-09-5 | 74 |
| 3 | Aminomethanesulfonic acid | 111 | CH5NO3S | 013881-91-9 | 64 |
| 4 | L-Alanine, 3-sulfo- | 169 | C3H7NO5S | 000498-40-8 | 9 |

**********

Peak Number 3 2-Butene Concentration Rank 2

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.51 | 0.29 ug | 29682 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | 2-Butene | 56 | C4H8 | 000107-01-7 | 9 |
| 2 | 2-Butene | 56 | C4H8 | 000107-01-7 | 7 |
| 3 | 1-Propene, 2-methyl- | 56 | C4H8 | 000115-11-7 | 7 |
| 4 | 1-Propene, 2-methyl- | 56 | C4H8 | 000115-11-7 | 7 |

**********

Peak Number 4 Vinyl Ether Concentration Rank 5

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.71 | 0.17 ug | 17558 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Vinyl Ether | 70 | C4H6O | 000109-93-3 | 4 |
| 2 | 1,4-Butanediamine | 88 | C4H12N2 | 000110-60-1 | 4 |
| 3 | Ethylamine | 45 | C2H7N | 000075-04-7 | 4 |
| 4 | Ethylamine | 45 | C2H7N | 000075-04-7 | 3 |

**********

Peak Number 5 Durohydroquinone Concentration Rank 4

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 9.29 | 0.21 ug | 21444 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Benzaldehyde, 2,3-dimethoxy- | 166 | C9H10O3 | 000086-51-1 | 58 |
| 2 | Benzaldehyde, 2,3-dimethoxy- | 166 | C9H10O3 | 000086-51-1 | 52 |
| 3 | Benzaldehyde, 2,5-dimethoxy- | 166 | C9H10O3 | 000093-02-7 | 50 |
| 4 | Durohydroquinone | 166 | C10H14O2 | 000527-18-4 | 47 |

0648045.D envdef.m Mon Dec 20 12:29:54 2010 D.00.00

0648047-LSCRPT.TXT
Library Search Compound Report

Data File : C:\MSDCHEM\5\20784505FRM\0648047.D Vial: 65
Acq On : 19 Nov 2010 18:29 Operator: LIMS import
Sample : Inst : UC-SPG5-D
Misc : Multiplr: 1.00
MS Integration Params: jwint.p
Quant Method : C:\MSDCHEM\1\METHODS\LIMS_A1_5.M (RTE Integrator)
Title : Gore Expanded Target VOCs/SVOCs
Library : C:\DATABASE\NIST02.L

**********

Peak Number 1 Carbon dioxide Concentration Rank 5

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.41 | 0.36 ug | 36487 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Carbon dioxide | 44 | CO2 | 000124-38-9 | 2 |
| 2 | Nitrous Oxide | 44 | N2O | 010024-97-2 | 2 |
| 3 | Carbon dioxide | 44 | CO2 | 000124-38-9 | 2 |
| 4 | Ethyne, fluoro- | 44 | C2HF | 002713-09-9 | 2 |

**********

Peak Number 2 Aminomethanesulfonic acid Concentration Rank 3

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.47 | 0.48 ug | 49258 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Sulfur dioxide | 64 | O2S | 007446-09-5 | 74 |
| 2 | Aminomethanesulfonic acid | 111 | CH5NO3S | 013881-91-9 | 64 |
| 3 | Aminomethanesulfonic acid | 111 | CH5NO3S | 013881-91-9 | 64 |
| 4 | L-Alanine, 3-sulfo- | 169 | C3H7NO5S | 000498-40-8 | 9 |

**********

Peak Number 3 1-Butene Concentration Rank 2

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.52 | 1.08 ug | 109734 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | 1-Butene | 56 | C4H8 | 000106-98-9 | 80 |
| 2 | 1-Propene, 2-methyl- | 56 | C4H8 | 000115-11-7 | 80 |
| 3 | 2-Butene, (Z)- | 56 | C4H8 | 000590-18-1 | 72 |
| 4 | 1-Propene, 2-methyl- | 56 | C4H8 | 000115-11-7 | 72 |

**********

Peak Number 4 Butane, 2-methyl- Concentration Rank 4

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.65 | 0.38 ug | 39067 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Butane, 2-methyl- | 72 | C5H12 | 000078-78-4 | 40 |
| 2 | Butane, 2-methyl- | 72 | C5H12 | 000078-78-4 | 40 |
| 3 | Butane, 2-methyl- | 72 | C5H12 | 000078-78-4 | 39 |
| 4 | Propane, 2-methyl-1-nitro- | 103 | C4H9NO2 | 000625-74-1 | 9 |

**********

Peak Number 5 Pentane Concentration Rank 1

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.72 | 1.17 ug | 119307 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Pentane | 72 | C5H12 | 000109-66-0 | 72 |
| 2 | Cyclopropane, ethyl- | 70 | C5H10 | 001191-96-4 | 46 |
| 3 | Pentane | 72 | C5H12 | 000109-66-0 | 45 |
| 4 | Cyclopropane, ethyl- | 70 | C5H10 | 001191-96-4 | 43 |

0648047.D envdef.m Mon Dec 20 12:38:38 2010 D.00.00

0648046-LSCRPT.TXT
Library Search Compound Report

Data File : C:\MSDCHEM\5\20784505FRM\0648046.D Vial: 17
Acq On : 18 Nov 2010 20:03 Operator: LIMS import
Sample : Inst : UC-SPG5-D
Misc : Multiplr: 1.00
MS Integration Params: jwint.p
Quant Method : C:\MSDCHEM\1\METHODS\LIMS_A1_5.M (RTE Integrator)
Title : Gore Expanded Target VOCs/SVOCs
Library : C:\DATABASE\NIST02.L

**********

Peak Number 1 Acetaldehyde Concentration Rank 4

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.39 | 0.33 ug | 33649 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Acetaldehyde | 44 | C2H4O | 000075-07-0 | 3 |
| 2 | Ethyne, fluoro- | 44 | C2HF | 002713-09-9 | 3 |
| 3 | Acetaldehyde | 44 | C2H4O | 000075-07-0 | 3 |
| 4 | Carbon dioxide | 44 | CO2 | 000124-38-9 | 3 |

**********

Peak Number 2 Sulfur dioxide Concentration Rank 1

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.44 | 1.87 ug | 190316 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Sulfur dioxide | 64 | O2S | 007446-09-5 | 90 |
| 2 | Sulfur dioxide | 64 | O2S | 007446-09-5 | 74 |
| 3 | Aminomethanesulfonic acid | 111 | CH5NO3S | 013881-91-9 | 74 |
| 4 | Cysteic acid | 169 | C3H7NO5S | 1000131-23-1 | 74 |

**********

Peak Number 3 Fluorodichloromethane Concentration Rank 2

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.59 | 0.62 ug | 63320 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Fluorodichloromethane | 102 | CHCl2F | 000075-43-4 | 47 |
| 2 | Cyclopentene, 3-methyl- | 82 | C6H10 | 001120-62-3 | 38 |
| 3 | Fluorodichloromethane | 102 | CHCl2F | 000075-43-4 | 37 |
| 4 | 1,4-Hexadiene, (Z)- | 82 | C6H10 | 007318-67-4 | 9 |

**********

Peak Number 4 Cyclopropane, 1,2-dimethyl-... Concentration Rank 3

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.66 | 0.51 ug | 51592 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Cyclopropane, 1,2-dimethyl-3-met... | 82 | C6H10 | 062338-02-7 | 43 |
| 2 | 1,4-Pentadiene, 3-methyl- | 82 | C6H10 | 001115-08-8 | 9 |
| 3 | Isopropenylcyclopropane | 82 | C6H10 | 004663-22-3 | 9 |
| 4 | 1,3-Pentadiene, 3-methyl-, (Z)- | 82 | C6H10 | 002787-45-3 | 9 |

**********

Peak Number 5 Ethene, chloro- Concentration Rank 5

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 5.31 | 0.22 ug | 22321 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Ethene, chloro- | 62 | C2H3Cl | 000075-01-4 | 9 |
| 2 | Ethene, chloro- | 62 | C2H3Cl | 000075-01-4 | 9 |
| 3 | Peroxide, dimethyl | 62 | C2H6O2 | 000690-02-8 | 4 |
| 4 | Peroxide, dimethyl | 62 | C2H6O2 | 000690-02-8 | 4 |

0648046.D envdef.m Mon Dec 20 12:31:50 2010 D.00.00

0648048-LSCRPT.TXT
Library Search Compound Report

Data File : C:\MSDCHEM\5\20784505FRM\0648048.D Vial: 71
Acq On : 19 Nov 2010 21:17 Operator: LIMS import
Sample : Inst : UC-SPG5-D
Misc : Multiplr: 1.00
MS Integration Params: jwint.p
Quant Method : C:\MSDCHEM\1\METHODS\LIMS_A1_5.M (RTE Integrator)
Title : Gore Expanded Target VOCs/SVOCs
Library : C:\DATABASE\NIST02.L

**********

Peak Number 1 Carbon dioxide Concentration Rank 3

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.41 | 0.29 ug | 29556 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Carbon dioxide | 44 | CO2 | 000124-38-9 | 2 |
| 2 | Nitrous Oxide | 44 | N2O | 010024-97-2 | 2 |
| 3 | Carbon dioxide | 44 | CO2 | 000124-38-9 | 2 |
| 4 | Ethyne, fluoro- | 44 | C2HF | 002713-09-9 | 2 |

**********

Peak Number 2 Sulfur dioxide Concentration Rank 2

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.47 | 0.31 ug | 31784 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Sulfur dioxide | 64 | O2S | 007446-09-5 | 74 |
| 2 | Sulfur dioxide | 64 | O2S | 007446-09-5 | 74 |
| 3 | Cysteic acid | 169 | C3H7NO5S | 1000131-23-1 | 9 |
| 4 | Aminomethanesulfonic acid | 111 | CH5NO3S | 013881-91-9 | 9 |

**********

Peak Number 3 1-Propene, 2-methyl- Concentration Rank 1

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.52 | 0.43 ug | 43644 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | 1-Propene, 2-methyl- | 56 | C4H8 | 000115-11-7 | 9 |
| 2 | 1-Propene, 2-methyl- | 56 | C4H8 | 000115-11-7 | 7 |
| 3 | 2-Butene, (Z)- | 56 | C4H8 | 000590-18-1 | 5 |
| 4 | Cyclobutane | 56 | C4H8 | 000287-23-0 | 5 |

**********

Peak Number 4 Cyclopropane Concentration Rank 4

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.71 | 0.27 ug | 27813 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Cyclopropane | 42 | C3H6 | 000075-19-4 | 9 |
| 2 | Cyclopropane | 42 | C3H6 | 000075-19-4 | 9 |
| 3 | Cyclopropane | 42 | C3H6 | 000075-19-4 | 9 |
| 4 | Cyclopropanecarboxylic acid | 86 | C4H6O2 | 001759-53-1 | 9 |

**********

Peak Number 5 Cyclopropene, 3-methyl-3-vi... Concentration Rank 5

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.89 | 0.16 ug | 16703 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Mercaptamine | 77 | C2H7NS | 000060-23-1 | 3 |
| 2 | 1,2,5-Hexatriene | 80 | C6H8 | 003642-18-0 | 2 |
| 3 | Mercaptamine | 77 | C2H7NS | 000060-23-1 | 2 |
| 4 | Cyclopropene, 3-methyl-3-vinyl- | 80 | C6H8 | 071153-30-5 | 1 |

0648048.D envdef.m Mon Dec 20 12:40:09 2010 D.00.00

0648049-LSCRPT.TXT
Library Search Compound Report

Data File : C:\MSDCHEM\5\20784505FRM\0648049.D Vial: 77
Acq On : 20 Nov 2010 00:05 Operator: LIMS import
Sample : Inst : UC-SPG5-D
Misc : Multiplr: 1.00
MS Integration Params: jwint.p
Quant Method : C:\MSDCHEM\1\METHODS\LIMS_A1_5.M (RTE Integrator)
Title : Gore Expanded Target VOCs/SVOCs
Library : C:\DATABASE\NIST02.L

**********

Peak Number 1 Carbon dioxide Concentration Rank 4

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.42 | 0.39 ug | 39315 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Carbon dioxide | 44 | CO2 | 000124-38-9 | 2 |
| 2 | Carbon dioxide | 44 | CO2 | 000124-38-9 | 2 |
| 3 | Nitrous Oxide | 44 | N2O | 010024-97-2 | 2 |
| 4 | Ethylene oxide | 44 | C2H4O | 000075-21-8 | 2 |

**********

Peak Number 2 Aminomethanesulfonic acid Concentration Rank 3

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.47 | 0.81 ug | 82254 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Aminomethanesulfonic acid | 111 | CH5NO3S | 013881-91-9 | 74 |
| 2 | Sulfur dioxide | 64 | O2S | 007446-09-5 | 74 |
| 3 | Sulfur dioxide | 64 | O2S | 007446-09-5 | 74 |
| 4 | 2-Aminoethyl hydrogen sulfate | 141 | C2H7NO4S | 000926-39-6 | 9 |

**********

Peak Number 3 1,2-Dimethyl cyclopropene Concentration Rank 2

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.53 | 0.91 ug | 92783 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Methylenecyclopropane | 54 | C4H6 | 006142-73-0 | 52 |
| 2 | Cyclobutene | 54 | C4H6 | 000822-35-5 | 40 |
| 3 | 1,2-Dimethyl cyclopropene | 68 | C5H8 | 014309-32-1 | 27 |
| 4 | 1,3-Butadiene | 54 | C4H6 | 000106-99-0 | 9 |

**********

Peak Number 4 Cyclopropane, ethyl- Concentration Rank 1

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.72 | 1.08 ug | 110396 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Cyclopropane, ethyl- | 70 | C5H10 | 001191-96-4 | 52 |
| 2 | 3-Buten-1-ol | 72 | C4H8O | 000627-27-0 | 47 |
| 3 | Pentane | 72 | C5H12 | 000109-66-0 | 46 |
| 4 | 3-Buten-1-ol | 72 | C4H8O | 000627-27-0 | 43 |

**********

Peak Number 5 3-Penten-1-yne, (E)- Concentration Rank 5

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.88 | 0.30 ug | 30235 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | 3-Penten-1-yne, (E)- | 66 | C5H6 | 002004-69-5 | 14 |
| 2 | 1-Buten-3-yne, 2-methyl- | 66 | C5H6 | 000078-80-8 | 14 |
| 3 | 3-Penten-1-yne, (E)- | 66 | C5H6 | 002004-69-5 | 14 |
| 4 | 3-Penten-1-yne | 66 | C5H6 | 002206-23-7 | 10 |

0648049.D envdef.m Mon Dec 20 12:40:56 2010 D.00.00

0648050-LSCRPT.TXT
Library Search Compound Report

Data File : C:\MSDCHEM\5\20784505FRM\0648050.D Vial: 53
Acq On : 19 Nov 2010 12:48 Operator: LIMS import
Sample : Inst : UC-SPG5-D
Misc : Multiplr: 1.00
MS Integration Params: jwint.p
Quant Method : C:\MSDCHEM\1\METHODS\LIMS_A1_5.M (RTE Integrator)
Title : Gore Expanded Target VOCs/SVOCs
Library : C:\DATABASE\NIST02.L

**********

Peak Number 1 Carbon dioxide Concentration Rank 4

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.40 | 0.43 ug | 43373 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Carbon dioxide | 44 | CO2 | 000124-38-9 | 2 |
| 2 | Nitrous Oxide | 44 | N2O | 010024-97-2 | 2 |
| 3 | Ethylene oxide | 44 | C2H4O | 000075-21-8 | 2 |
| 4 | Carbon dioxide | 44 | CO2 | 000124-38-9 | 2 |

**********

Peak Number 2 Sulfur dioxide Concentration Rank 2

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.46 | 0.79 ug | 80594 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Sulfur dioxide | 64 | O2S | 007446-09-5 | 74 |
| 2 | Sulfur dioxide | 64 | O2S | 007446-09-5 | 74 |
| 3 | Aminomethanesulfonic acid | 111 | CH5NO3S | 013881-91-9 | 64 |
| 4 | L-Alanine, 3-sulfo- | 169 | C3H7NO5S | 000498-40-8 | 9 |

**********

Peak Number 3 1-Propene, 2-methyl- Concentration Rank 1

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.51 | 0.88 ug | 90245 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | 1-Propene, 2-methyl- | 56 | C4H8 | 000115-11-7 | 72 |
| 2 | 1-Propene, 2-methyl- | 56 | C4H8 | 000115-11-7 | 64 |
| 3 | 1-Propene, 2-methyl- | 56 | C4H8 | 000115-11-7 | 64 |
| 4 | 1-Butene | 56 | C4H8 | 000106-98-9 | 64 |

**********

Peak Number 4 2-Butene, (Z)- Concentration Rank 5

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.64 | 0.15 ug | 15806 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | 2-Butene, (Z)- | 56 | C4H8 | 000590-18-1 | 5 |
| 2 | 2-Butene, (E)- | 56 | C4H8 | 000624-64-6 | 5 |
| 3 | Methane, isocyanato- | 57 | C2H3NO | 000624-83-9 | 4 |
| 4 | Cyclopropane | 42 | C3H6 | 000075-19-4 | 4 |

**********

Peak Number 5 Diaziridine,3,3-dimethyl- Concentration Rank 3

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.71 | 0.62 ug | 63334 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Diaziridine,3,3-dimethyl- | 72 | C3H8N2 | 004901-76-2 | 23 |
| 2 | Diaziridine,3,3-dimethyl- | 72 | C3H8N2 | 004901-76-2 | 23 |
| 3 | Oxirane, ethyl- | 72 | C4H8O | 000106-88-7 | 12 |
| 4 | Cyclobutanol | 72 | C4H8O | 002919-23-5 | 9 |

0648050.D envdef.m Mon Dec 20 14:24:08 2010 D.00.00

0648051-LSCRPT.TXT
Library Search Compound Report

Data File : C:\MSDCHEM\5\20784505FRM\0648051.D Vial: 13
Acq On : 18 Nov 2010 18:11 Operator: LIMS import
Sample : Inst : UC-SPG5-D
Misc : Multiplr: 1.00
MS Integration Params: jwint.p
Quant Method : C:\MSDCHEM\1\METHODS\LIMS_A1_5.M (RTE Integrator)
Title : Gore Expanded Target VOCs/SVOCs
Library : C:\DATABASE\NIST02.L

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Peak Number 1 Carbon dioxide Concentration Rank 4

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.41 | 0.37 ug | 37513 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Carbon dioxide | 44 | CO2 | 000124-38-9 | 2 |
| 2 | Nitrous Oxide | 44 | N2O | 010024-97-2 | 2 |
| 3 | Carbon dioxide | 44 | CO2 | 000124-38-9 | 2 |
| 4 | Ethyne, fluoro- | 44 | C2HF | 002713-09-9 | 2 |

**********

Peak Number 2 Sulfur dioxide Concentration Rank 2

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.47 | 1.08 ug | 109672 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Sulfur dioxide | 64 | O2S | 007446-09-5 | 74 |
| 2 | Sulfur dioxide | 64 | O2S | 007446-09-5 | 74 |
| 3 | Aminomethanesulfonic acid | 111 | CH5NO3S | 013881-91-9 | 74 |
| 4 | Aminomethanesulfonic acid | 111 | CH5NO3S | 013881-91-9 | 64 |

**********

Peak Number 3 Phosphine, ethyl- Concentration Rank 3

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.51 | 0.48 ug | 49160 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Phosphine, ethyl- | 62 | C2H7P | 000593-68-0 | 5 |
| 2 | Isobutylamine | 73 | C4H11N | 000078-81-9 | 4 |
| 3 | Ethene, chloro- | 62 | C2H3Cl | 000075-01-4 | 3 |
| 4 | Ethene, chloro- | 62 | C2H3Cl | 000075-01-4 | 3 |

**********

Peak Number 4 Ethene, 1,1-dichloro-2,2-di... Concentration Rank 5

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.62 | 0.35 ug | 35214 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Ethene, 1,1-dichloro-2,2-difluoro- | 132 | C2Cl2F2 | 000079-35-6 | 43 |
| 2 | Ethene, 1,1-dichloro-2,2-difluoro- | 132 | C2Cl2F2 | 000079-35-6 | 38 |
| 3 | n-Propylphosphonic dichloride | 160 | C3H7Cl2OP | 004708-04-7 | 22 |
| 4 | Spiropentanoic acid, methyl ester | 126 | C7H10O2 | 033447-49-3 | 12 |

**********

Peak Number 5 Ethane, 1,2-dichloro-1,1,2-... Concentration Rank 1

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.69 | 1.33 ug | 135427 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Ethane, 1,2-dichloro-1,1,2-trifl... | 152 | C2HCl2F3 | 000354-23-4 | 91 |
| 2 | Cyclopropane, 1,2-dimethyl-3-met... | 82 | C6H10 | 062338-02-7 | 12 |
| 3 | 1,4-Pentadiene, 2-methyl- | 82 | C6H10 | 000763-30-4 | 9 |
| 4 | 1-Butyne, 3,3-dimethyl- | 82 | C6H10 | 000917-92-0 | 9 |

0648051.D envdef.m Mon Dec 20 14:48:09 2010 D.00.00

0648052-LSCRPT.TXT
Library Search Compound Report

Data File : C:\MSDCHEM\5\20784505FRM\0648052.D Vial: 63
Acq On : 19 Nov 2010 17:33 Operator: LIMS import
Sample : Inst : UC-SPG5-D
Misc : Multiplr: 1.00
MS Integration Params: jwint.p
Quant Method : C:\MSDCHEM\1\METHODS\LIMS_A1_5.M (RTE Integrator)
Title : Gore Expanded Target VOCs/SVOCs
Library : C:\DATABASE\NIST02.L

**********

Peak Number 1 Aminomethanesulfonic acid Concentration Rank 1

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.47 | 1.11 ug | 112981 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Aminomethanesulfonic acid | 111 | CH5NO3S | 013881-91-9 | 78 |
| 2 | Sulfur dioxide | 64 | O2S | 007446-09-5 | 64 |
| 3 | Aminomethanesulfonic acid | 111 | CH5NO3S | 013881-91-9 | 43 |
| 4 | Aminomethanesulfonic acid | 111 | CH5NO3S | 013881-91-9 | 43 |

**********

Peak Number 2 Acetone Concentration Rank 2

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.72 | 0.12 ug | 11907 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Acetone | 58 | C3H6O | 000067-64-1 | 4 |
| 2 | Acetone | 58 | C3H6O | 000067-64-1 | 4 |
| 3 | Acetone | 58 | C3H6O | 000067-64-1 | 4 |
| 4 | Acetone | 58 | C3H6O | 000067-64-1 | 4 |

0648052.D envdef.m Mon Dec 20 14:48:52 2010 D.00.00

0648053-LSCRPT.TXT
Library Search Compound Report

Data File : C:\MSDCHEM\5\20784505FRM\0648053.D Vial: 38
Acq On : 19 Nov 2010 5:50 Operator: LIMS import
Sample : Inst : UC-SPG5-D
Misc : Multiplr: 1.00
MS Integration Params: jwint.p
Quant Method : C:\MSDCHEM\1\METHODS\LIMS_A1_5.M (RTE Integrator)
Title : Gore Expanded Target VOCs/SVOCs
Library : C:\DATABASE\NIST02.L

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Peak Number 1 Carbon dioxide Concentration Rank 2

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.40 | 0.38 ug | 38794 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Carbon dioxide | 44 | CO2 | 000124-38-9 | 2 |
| 2 | Nitrous Oxide | 44 | N2O | 010024-97-2 | 2 |
| 3 | Carbon dioxide | 44 | CO2 | 000124-38-9 | 2 |
| 4 | Ethyne, fluoro- | 44 | C2HF | 002713-09-9 | 2 |

**********

Peak Number 2 Sulfur dioxide Concentration Rank 3

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.46 | 0.35 ug | 36151 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Sulfur dioxide | 64 | O2S | 007446-09-5 | 74 |
| 2 | Aminomethanesulfonic acid | 111 | CH5NO3S | 013881-91-9 | 74 |
| 3 | L-Alanine, 3-sulfo- | 169 | C3H7NO5S | 000498-40-8 | 9 |
| 4 | Aminomethanesulfonic acid | 111 | CH5NO3S | 013881-91-9 | 9 |

**********

Peak Number 3 1-Propene, 2-methyl- Concentration Rank 1

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.51 | 0.50 ug | 51152 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | 1-Propene, 2-methyl- | 56 | C4H8 | 000115-11-7 | 72 |
| 2 | 1-Propene, 2-methyl- | 56 | C4H8 | 000115-11-7 | 59 |
| 3 | 2-Butene, (Z)- | 56 | C4H8 | 000590-18-1 | 59 |
| 4 | 1-Propene, 2-methyl- | 56 | C4H8 | 000115-11-7 | 53 |

**********

Peak Number 4 Cyclopropane Concentration Rank 5

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.64 | 0.15 ug | 15191 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Aziridine, 1-methyl- | 57 | C3H7N | 001072-44-2 | 4 |
| 2 | Aziridine, 1-methyl- | 57 | C3H7N | 001072-44-2 | 4 |
| 3 | Cyclopropane | 42 | C3H6 | 000075-19-4 | 4 |
| 4 | Cyclopropane | 42 | C3H6 | 000075-19-4 | 4 |

**********

Peak Number 5 1-Pentanol Concentration Rank 4

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.70 | 0.32 ug | 32430 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | 1-Pentanol | 88 | C5H12O | 000071-41-0 | 9 |
| 2 | 1-Pentanol | 88 | C5H12O | 000071-41-0 | 9 |
| 3 | Cyclopropane | 42 | C3H6 | 000075-19-4 | 7 |
| 4 | Cyclobutane, methyl- | 70 | C5H10 | 000598-61-8 | 7 |

0648053.D envdef.m Mon Dec 20 14:50:22 2010 D.00.00

0648054-LSCRPT.TXT
Library Search Compound Report

Data File : C:\MSDCHEM\5\20784505FRM\0648054.D Vial: 20
Acq On : 18 Nov 2010 21:27 Operator: LIMS import
Sample : Inst : UC-SPG5-D
Misc : Multiplr: 1.00
MS Integration Params: jwint.p
Quant Method : C:\MSDCHEM\1\METHODS\LIMS_A1_5.M (RTE Integrator)
Title : Gore Expanded Target VOCs/SVOCs
Library : C:\DATABASE\NIST02.L

**********

Peak Number 1 Sulfur dioxide Concentration Rank 5

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.45 | 7.56 ug | 770779 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Sulfur dioxide | 64 | O2S | 007446-09-5 | 90 |
| 2 | Sulfur dioxide | 64 | O2S | 007446-09-5 | 83 |
| 3 | L-Alanine, 3-sulfo- | 169 | C3H7NO5S | 000498-40-8 | 64 |
| 4 | Aminomethanesulfonic acid | 111 | CH5NO3S | 013881-91-9 | 64 |

**********

Peak Number 2 1-Propene, 2-methyl- Concentration Rank 2

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.51 | 14.04 ug | 1432020 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | 1-Propene, 2-methyl- | 56 | C4H8 | 000115-11-7 | 72 |
| 2 | 1-Propene, 2-methyl- | 56 | C4H8 | 000115-11-7 | 59 |
| 3 | 2-Butene, (Z)- | 56 | C4H8 | 000590-18-1 | 49 |
| 4 | 2-Butene, (E)- | 56 | C4H8 | 000624-64-6 | 46 |

**********

Peak Number 3 1-Pentene Concentration Rank 1

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.68 | 29.30 ug | 2988800 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | 1-Pentene | 70 | C5H10 | 000109-67-1 | 81 |
| 2 | Cyclopropane, ethyl- | 70 | C5H10 | 001191-96-4 | 76 |
| 3 | Cyclobutane, methyl- | 70 | C5H10 | 000598-61-8 | 72 |
| 4 | Cyclopropane, ethyl- | 70 | C5H10 | 001191-96-4 | 72 |

**********

Peak Number 4 2-Pentene, (Z)- Concentration Rank 3

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.76 | 8.06 ug | 822284 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | 2-Pentene, (Z)- | 70 | C5H10 | 000627-20-3 | 78 |
| 2 | 2-Pentene, (E)- | 70 | C5H10 | 000646-04-8 | 78 |
| 3 | 2-Pentene | 70 | C5H10 | 000109-68-2 | 78 |
| 4 | Cyclopropane, 1,2-dimethyl-, trans- | 70 | C5H10 | 002402-06-4 | 72 |

**********

Peak Number 5 Pentane, 2-methyl- Concentration Rank 4

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.97 | 7.79 ug | 794983 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Pentane, 2-methyl- | 86 | C6H14 | 000107-83-5 | 80 |
| 2 | Pentane, 2-methyl- | 86 | C6H14 | 000107-83-5 | 80 |
| 3 | Butane, 2,3-dimethyl- | 86 | C6H14 | 000079-29-8 | 43 |
| 4 | Pentane, 2-bromo- | 150 | C5H11Br | 000107-81-3 | 38 |

0648054.D LIMS_A1_5.M Mon Dec 20 15:10:49 2010 D.00.00

0648055-LSCRPT.TXT
Library Search Compound Report

Data File : C:\MSDCHEM\5\20784505FRM\0648055.D Vial: 66
Acq On : 19 Nov 2010 18:57 Operator: LIMS import
Sample : Inst : UC-SPG5-D
Misc : Multiplr: 1.00
MS Integration Params: jwint.p
Quant Method : C:\MSDCHEM\1\METHODS\LIMS_A1_5.M (RTE Integrator)
Title : Gore Expanded Target VOCs/SVOCs
Library : C:\DATABASE\NIST02.L

**********

Peak Number 1 Carbon dioxide Concentration Rank 4

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.40 | 0.33 ug | 33667 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Carbon dioxide | 44 | CO2 | 000124-38-9 | 2 |
| 2 | Nitrous Oxide | 44 | N2O | 010024-97-2 | 2 |
| 3 | Carbon dioxide | 44 | CO2 | 000124-38-9 | 2 |
| 4 | Ethyne, fluoro- | 44 | C2HF | 002713-09-9 | 2 |

**********

Peak Number 2 Sulfur dioxide Concentration Rank 1

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.46 | 0.64 ug | 65337 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Sulfur dioxide | 64 | O2S | 007446-09-5 | 74 |
| 2 | Sulfur dioxide | 64 | O2S | 007446-09-5 | 74 |
| 3 | Aminomethanesulfonic acid | 111 | CH5NO3S | 013881-91-9 | 64 |
| 4 | L-Alanine, 3-sulfo- | 169 | C3H7NO5S | 000498-40-8 | 9 |

**********

Peak Number 3 2-Butene Concentration Rank 2

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.51 | 0.57 ug | 57936 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Methacrolein | 70 | C4H6O | 000078-85-3 | 17 |
| 2 | 1-Propene, 2-methyl- | 56 | C4H8 | 000115-11-7 | 9 |
| 3 | 2-Butene | 56 | C4H8 | 000107-01-7 | 9 |
| 4 | 1-Propene, 2-methyl- | 56 | C4H8 | 000115-11-7 | 9 |

**********

Peak Number 4 1-Hepten-4-ol Concentration Rank 5

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.60 | 0.12 ug | 12665 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Propane, 1-nitro- | 89 | C3H7NO2 | 000108-03-2 | 2 |
| 2 | Hydrogen azide | 43 | HN3 | 007782-79-8 | 1 |
| 3 | 1-Hepten-4-ol | 114 | C7H14O | 003521-91-3 | 1 |
| 4 | Propane, 2-nitro- | 89 | C3H7NO2 | 000079-46-9 | 1 |

**********

Peak Number 5 Cyclobutane, methyl- Concentration Rank 3

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.70 | 0.36 ug | 36474 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Acetic acid, trifluoro-, pentyl ... | 184 | C7H11F3O2 | 000327-70-8 | 9 |
| 2 | Cyclopropane | 42 | C3H6 | 000075-19-4 | 7 |
| 3 | Cyclobutane, methyl- | 70 | C5H10 | 000598-61-8 | 7 |
| 4 | Cyclopropane | 42 | C3H6 | 000075-19-4 | 7 |

0648055.D LIMS_A1_5.M Mon Dec 20 15:13:26 2010 D.00.00

0648057-LSCRPT.TXT
Library Search Compound Report

Data File : C:\MSDCHEM\5\20784505FRM\0648057.D Vial: 75
Acq On : 19 Nov 2010 23:09 Operator: LIMS import
Sample : Inst : UC-SPG5-D
Misc : Multiplr: 1.00
MS Integration Params: jwint.p
Quant Method : C:\MSDCHEM\1\METHODS\LIMS_A1_5.M (RTE Integrator)
Title : Gore Expanded Target VOCs/SVOCs
Library : C:\DATABASE\NIST02.L

**********

Peak Number 1 Sulfur dioxide Concentration Rank 3

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.46 | 1.59 ug | 162258 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Sulfur dioxide | 64 | O2S | 007446-09-5 | 90 |
| 2 | Sulfur dioxide | 64 | O2S | 007446-09-5 | 83 |
| 3 | Aminomethanesulfonic acid | 111 | CH5NO3S | 013881-91-9 | 74 |
| 4 | Aminomethanesulfonic acid | 111 | CH5NO3S | 013881-91-9 | 74 |

**********

Peak Number 2 1-Propene, 2-methyl- Concentration Rank 2

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.52 | 2.44 ug | 249270 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | 1-Propene, 2-methyl- | 56 | C4H8 | 000115-11-7 | 59 |
| 2 | 1-Propene, 2-methyl- | 56 | C4H8 | 000115-11-7 | 50 |
| 3 | 2-Butene, (Z)- | 56 | C4H8 | 000590-18-1 | 43 |
| 4 | 2-Butene, (E)- | 56 | C4H8 | 000624-64-6 | 38 |

**********

Peak Number 3 Cyclopropane, ethyl- Concentration Rank 1

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.71 | 2.85 ug | 290335 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Cyclopropane, ethyl- | 70 | C5H10 | 001191-96-4 | 64 |
| 2 | Cyclopropane, ethyl- | 70 | C5H10 | 001191-96-4 | 59 |
| 3 | 3-Buten-1-ol | 72 | C4H8O | 000627-27-0 | 53 |
| 4 | Pentane | 72 | C5H12 | 000109-66-0 | 52 |

**********

Peak Number 4 2-Pentene Concentration Rank 5

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.77 | 0.68 ug | 69392 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | 2-Pentene | 70 | C5H10 | 000109-68-2 | 50 |
| 2 | 2-Pentene, (Z)- | 70 | C5H10 | 000627-20-3 | 50 |
| 3 | 2-Pentene, (E)- | 70 | C5H10 | 000646-04-8 | 42 |
| 4 | 2-Pentene, (E)- | 70 | C5H10 | 000646-04-8 | 40 |

**********

Peak Number 5 Pentane, 2-methyl- Concentration Rank 4

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.97 | 0.77 ug | 79049 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Pentane, 2-methyl- | 86 | C6H14 | 000107-83-5 | 64 |
| 2 | Pentane, 2-methyl- | 86 | C6H14 | 000107-83-5 | 64 |
| 3 | Pentane, 2-bromo- | 150 | C5H11Br | 000107-81-3 | 42 |
| 4 | Butane, 2,3-dimethyl- | 86 | C6H14 | 000079-29-8 | 9 |

0648057.D LIMS_A1_5.M Mon Dec 20 15:15:06 2010 D.00.00

# Library Search Compound Report

Data File : C:\MSDCHEM\5\20784505FRM\0648056.D Vial: 58
Acq On : 19 Nov 2010 15:08 Operator: LIMS import
Sample : Inst : UC-SPG5-D
Misc : Multiplr: 1.00
MS Integration Params: jwint.p
Quant Method : C:\MSDCHEM\1\METHODS\LIMS_A1_5.M (RTE Integrator)
Title : Gore Expanded Target VOCs/SVOCs
Library : C:\DATABASE\NIST02.L

**********

Peak Number 1 Aminomethanesulfonic acid Concentration Rank 3

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.47 | 0.84 ug | 85535 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Aminomethanesulfonic acid | 111 | CH5NO3S | 013881-91-9 | 74 |
| 2 | Sulfur dioxide | 64 | O2S | 007446-09-5 | 74 |
| 3 | Sulfur dioxide | 64 | O2S | 007446-09-5 | 74 |
| 4 | L-Alanine, 3-sulfo- | 169 | C3H7NO5S | 000498-40-8 | 9 |

**********

Peak Number 2 1-Propene, 2-methyl- Concentration Rank 2

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.52 | 1.66 ug | 169162 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | 1-Propene, 2-methyl- | 56 | C4H8 | 000115-11-7 | 50 |
| 2 | 1-Propene, 2-methyl- | 56 | C4H8 | 000115-11-7 | 50 |
| 3 | 1-Propene, 2-methyl- | 56 | C4H8 | 000115-11-7 | 50 |
| 4 | 1-Butene | 56 | C4H8 | 000106-98-9 | 35 |

**********

Peak Number 3 Cyclopropane, ethyl- Concentration Rank 1

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.71 | 1.77 ug | 180481 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Cyclopropane, ethyl- | 70 | C5H10 | 001191-96-4 | 64 |
| 2 | 2-Pentene, (Z)- | 70 | C5H10 | 000627-20-3 | 53 |
| 3 | 2-Pentene, (E)- | 70 | C5H10 | 000646-04-8 | 53 |
| 4 | 2-Pentene | 70 | C5H10 | 000109-68-2 | 53 |

**********

Peak Number 4 3-Hexene, (Z)- Concentration Rank 4

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.94 | 0.45 ug | 46316 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | 3-Hexene, (Z)- | 84 | C6H12 | 007642-09-3 | 64 |
| 2 | 2-Hexene, (Z)- | 84 | C6H12 | 007688-21-3 | 59 |
| 3 | 1-Pentene, 3-methyl- | 84 | C6H12 | 000760-20-3 | 52 |
| 4 | 3-Hexene, (E)- | 84 | C6H12 | 013269-52-8 | 50 |

**********

Peak Number 5 Cyclopropane, ethyl- Concentration Rank 5

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.97 | 0.39 ug | 39396 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Acetic acid, trifluoro-, pentyl ... | 184 | C7H11F3O2 | 000327-70-8 | 28 |
| 2 | 2-Carbomethoxyaziridine | 101 | C4H7NO2 | 005950-34-5 | 25 |
| 3 | 1-Butanol | 74 | C4H10O | 000071-36-3 | 23 |
| 4 | Cyclopropane, ethyl- | 70 | C5H10 | 001191-96-4 | 9 |

0648056.D LIMS_A1_5.M Mon Dec 20 15:14:13 2010 D.00.00

0648058-LSCRPT.TXT
Library Search Compound Report

Data File : C:\MSDCHEM\5\20784505FRM\0648058.D Vial: 26
Acq On : 19 Nov 2010 00:14 Operator: LIMS import
Sample : Inst : UC-SPG5-D
Misc : Multiplr: 1.00
MS Integration Params: jwint.p
Quant Method : C:\MSDCHEM\1\METHODS\LIMS_A1_5.M (RTE Integrator)
Title : Gore Expanded Target VOCs/SVOCs
Library : C:\DATABASE\NIST02.L

**********

Peak Number 1 Carbon dioxide Concentration Rank 3

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.40 | 0.33 ug | 33589 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Carbon dioxide | 44 | CO2 | 000124-38-9 | 2 |
| 2 | Nitrous Oxide | 44 | N2O | 010024-97-2 | 2 |
| 3 | Carbon dioxide | 44 | CO2 | 000124-38-9 | 2 |
| 4 | Ethyne, fluoro- | 44 | C2HF | 002713-09-9 | 2 |

**********

Peak Number 2 Sulfur dioxide Concentration Rank 4

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.47 | 0.26 ug | 26916 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Sulfur dioxide | 64 | O2S | 007446-09-5 | 74 |
| 2 | Aminomethanesulfonic acid | 111 | CH5NO3S | 013881-91-9 | 74 |
| 3 | Sulfur dioxide | 64 | O2S | 007446-09-5 | 74 |
| 4 | Aminomethanesulfonic acid | 111 | CH5NO3S | 013881-91-9 | 64 |

**********

Peak Number 3 1-Propene, 2-methyl- Concentration Rank 1

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.52 | 0.68 ug | 69092 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | 1-Propene, 2-methyl- | 56 | C4H8 | 000115-11-7 | 53 |
| 2 | 1-Propene, 2-methyl- | 56 | C4H8 | 000115-11-7 | 42 |
| 3 | 2-Butene, (E)- | 56 | C4H8 | 000624-64-6 | 9 |
| 4 | 2-Butene, (Z)- | 56 | C4H8 | 000590-18-1 | 9 |

**********

Peak Number 4 Cyclopropane, ethyl- Concentration Rank 2

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.71 | 0.62 ug | 63695 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Cyclopropane, ethyl- | 70 | C5H10 | 001191-96-4 | 59 |
| 2 | 1-Butanol, 3-methyl- | 88 | C5H12O | 000123-51-3 | 53 |
| 3 | 1-Butanol, 3-methyl- | 88 | C5H12O | 000123-51-3 | 50 |
| 4 | 3-Buten-1-ol | 72 | C4H8O | 000627-27-0 | 50 |

**********

Peak Number 5 Pentane, 3-methylene- Concentration Rank 5

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.97 | 0.15 ug | 15302 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Pentane, 3-methylene- | 84 | C6H12 | 000760-21-4 | 10 |
| 2 | 2-Pentene, 2-methyl- | 84 | C6H12 | 000625-27-4 | 9 |
| 3 | 3-Penten-2-one | 84 | C5H8O | 000625-33-2 | 9 |
| 4 | 2-Pentene, 3-methyl- | 84 | C6H12 | 000922-61-2 | 9 |

0648058.D LIMS_A1_5.M Mon Dec 20 15:16:01 2010 D.00.00

# Library Search Compound Report

Data File : C:\MSDCHEM\5\20784505FRM\0648059.D Vial: 27
Acq On : 19 Nov 2010 00:42 Operator: LIMS import
Sample : Inst : UC-SPG5-D
Misc : Multiplr: 1.00
MS Integration Params: jwint.p
Quant Method : C:\MSDCHEM\1\METHODS\LIMS_A1_5.M (RTE Integrator)
Title : Gore Expanded Target VOCs/SVOCs
Library : C:\DATABASE\NIST02.L

**********

Peak Number 1 Aminomethanesulfonic acid Concentration Rank 3

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.45 | 0.76 ug | 77383 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Aminomethanesulfonic acid | 111 | CH5NO3S | 013881-91-9 | 74 |
| 2 | Aminomethanesulfonic acid | 111 | CH5NO3S | 013881-91-9 | 64 |
| 3 | Sulfur dioxide | 64 | O2S | 007446-09-5 | 64 |
| 4 | Sulfur dioxide | 64 | O2S | 007446-09-5 | 64 |

**********

Peak Number 2 1-Propene, 2-methyl- Concentration Rank 1

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.51 | 3.36 ug | 343125 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | 1-Butene | 56 | C4H8 | 000106-98-9 | 86 |
| 2 | 1-Propene, 2-methyl- | 56 | C4H8 | 000115-11-7 | 86 |
| 3 | 1-Propene, 2-methyl- | 56 | C4H8 | 000115-11-7 | 86 |
| 4 | 2-Butene, (Z)- | 56 | C4H8 | 000590-18-1 | 80 |

**********

Peak Number 3 Cyclopropane, ethyl- Concentration Rank 2

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.70 | 2.55 ug | 260205 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Cyclopropane, ethyl- | 70 | C5H10 | 001191-96-4 | 64 |
| 2 | Cyclopropane, ethyl- | 70 | C5H10 | 001191-96-4 | 46 |
| 3 | 1-Butene, 3-methyl- | 70 | C5H10 | 000563-45-1 | 46 |
| 4 | Cyclopropane, ethyl- | 70 | C5H10 | 001191-96-4 | 43 |

**********

Peak Number 4 Cyclopropane, 1,1-dimethyl- Concentration Rank 4

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.77 | 0.72 ug | 73931 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Cyclopropane, 1,1-dimethyl- | 70 | C5H10 | 001630-94-0 | 64 |
| 2 | 2-Pentene, (E)- | 70 | C5H10 | 000646-04-8 | 9 |
| 3 | 2-Pentene, (Z)- | 70 | C5H10 | 000627-20-3 | 7 |
| 4 | 2-Pentene | 70 | C5H10 | 000109-68-2 | 7 |

**********

Peak Number 5 1-Butene, 2,3-dimethyl- Concentration Rank 5

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.97 | 0.64 ug | 65602 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Cyclopropane, ethyl- | 70 | C5H10 | 001191-96-4 | 9 |
| 2 | Cyclopropane, ethyl- | 70 | C5H10 | 001191-96-4 | 9 |
| 3 | 2-Pentene, 2-methyl- | 84 | C6H12 | 000625-27-4 | 9 |
| 4 | 1-Butene, 2,3-dimethyl- | 84 | C6H12 | 000563-78-0 | 9 |

0648059.D LIMS_A1_5.M Mon Dec 20 15:17:45 2010 D.00.00

Library Search Compound Report

Data File : C:\MSDCHEM\5\20784505FRM\0648060.D Vial: 19
Acq On : 18 Nov 2010 20:59 Operator: LIMS import
Sample : Inst : UC-SPG5-D
Misc : Multiplr: 1.00
MS Integration Params: jwint.p
Quant Method : C:\MSDCHEM\1\METHODS\LIMS_A1_5.M (RTE Integrator)
Title : Gore Expanded Target VOCs/SVOCs
Library : C:\DATABASE\NIST02.L

**********

Peak Number 1 Sulfur dioxide Concentration Rank 4

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.45 | 0.61 ug | 61979 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | 2-Aminoethyl hydrogen sulfate | 141 | C2H7NO4S | 000926-39-6 | 74 |
| 2 | Sulfur dioxide | 64 | O2S | 007446-09-5 | 74 |
| 3 | Aminomethanesulfonic acid | 111 | CH5NO3S | 013881-91-9 | 9 |
| 4 | Aminomethanesulfonic acid | 111 | CH5NO3S | 013881-91-9 | 9 |

**********

Peak Number 2 Ethene, chloro- Concentration Rank 1

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.49 | 0.85 ug | 86201 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Ethene, chloro- | 62 | C2H3Cl | 000075-01-4 | 56 |
| 2 | Ethanethiol | 62 | C2H6S | 000075-08-1 | 5 |
| 3 | Ethanethiol | 62 | C2H6S | 000075-08-1 | 5 |
| 4 | Ethanethiol | 62 | C2H6S | 000075-08-1 | 5 |

**********

Peak Number 3 1,3-Butadiene, 2-ethyl- Concentration Rank 2

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.67 | 0.80 ug | 82105 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | 1,3-Butadiene, 2-ethyl- | 82 | C6H10 | 003404-63-5 | 9 |
| 2 | Chlorine dioxide | 67 | ClO2 | 010049-04-4 | 7 |
| 3 | 1H-Pyrrole-2,5-dicarbonitrile | 117 | C6H3N3 | 059215-66-6 | 4 |
| 4 | Oxazole, 4,5-dihydro-2-methyl- | 85 | C4H7NO | 001120-64-5 | 4 |

**********

Peak Number 4 Carbon disulfide Concentration Rank 3

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.86 | 0.62 ug | 62756 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Carbon disulfide | 76 | CS2 | 000075-15-0 | 74 |
| 2 | Carbon disulfide | 76 | CS2 | 000075-15-0 | 9 |
| 3 | Thiourea | 76 | CH4N2S | 000062-56-6 | 7 |
| 4 | Thiourea | 76 | CH4N2S | 000062-56-6 | 5 |

**********

Peak Number 5 1-Propanol, 2-(1-methyletho... Concentration Rank 5

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 3.15 | 0.50 ug | 51094 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | 1-Propanol, 2-(1-methylethoxy)- | 118 | C6H14O2 | 003944-37-4 | 83 |
| 2 | Diisopropyl ether | 102 | C6H14O | 000108-20-3 | 83 |
| 3 | Diisopropyl ether | 102 | C6H14O | 000108-20-3 | 83 |
| 4 | Diisopropyl ether | 102 | C6H14O | 000108-20-3 | 83 |

0648060.D LIMS_A1_5.M Mon Dec 20 15:18:59 2010 D.00.00

Library Search Compound Report

Data File : C:\MSDCHEM\5\20784505FRM\0648061.D Vial: 51
Acq On : 19 Nov 2010 11:53 Operator: LIMS import
Sample : Inst : UC-SPG5-D
Misc : Multiplr: 1.00
MS Integration Params: jwint.p
Quant Method : C:\MSDCHEM\1\METHODS\LIMS_A1_5.M (RTE Integrator)
Title : Gore Expanded Target VOCs/SVOCs
Library : C:\DATABASE\NIST02.L

**********

Peak Number 1 Sulfur dioxide Concentration Rank 3

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.44 | 2.77 ug | 282617 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Sulfur dioxide | 64 | O2S | 007446-09-5 | 90 |
| 2 | Sulfur dioxide | 64 | O2S | 007446-09-5 | 83 |
| 3 | 2-Aminoethyl hydrogen sulfate | 141 | C2H7NO4S | 000926-39-6 | 74 |
| 4 | Aminomethanesulfonic acid | 111 | CH5NO3S | 013881-91-9 | 64 |

**********

Peak Number 2 1-Propene, 2-methyl- Concentration Rank 4

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.49 | 1.45 ug | 148105 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | 1-Propene, 2-methyl- | 56 | C4H8 | 000115-11-7 | 10 |
| 2 | 1-Propene, 2-methyl- | 56 | C4H8 | 000115-11-7 | 10 |
| 3 | 1-Butene | 56 | C4H8 | 000106-98-9 | 10 |
| 4 | 2-Butene | 56 | C4H8 | 000107-01-7 | 10 |

**********

Peak Number 3 Fluorodichloromethane Concentration Rank 5

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.59 | 1.22 ug | 124787 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Fluorodichloromethane | 102 | CHCl2F | 000075-43-4 | 91 |
| 2 | Fluorodichloromethane | 102 | CHCl2F | 000075-43-4 | 91 |
| 3 | Fluorodichloromethane | 102 | CHCl2F | 000075-43-4 | 90 |
| 4 | Methanamine, N,N-difluoro- | 67 | CH3F2N | 000753-58-2 | 5 |

**********

Peak Number 4 3-Pentyn-1-ol Concentration Rank 2

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.67 | 2.91 ug | 296570 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | 3-Pentyn-1-ol | 84 | C5H8O | 010229-10-4 | 83 |
| 2 | 1,2-Butadiene | 54 | C4H6 | 000590-19-2 | 80 |
| 3 | 2-Butyne | 54 | C4H6 | 000503-17-3 | 78 |
| 4 | 3-Pentyn-1-ol | 84 | C5H8O | 010229-10-4 | 78 |

**********

Peak Number 5 Ethene, 1,1-dichloro- Concentration Rank 1

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.75 | 36.13 ug | 3685610 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Ethene, 1,1-dichloro- | 96 | C2H2Cl2 | 000075-35-4 | 97 |
| 2 | Ethene, 1,1-dichloro- | 96 | C2H2Cl2 | 000075-35-4 | 97 |
| 3 | Ethene, 1,2-dichloro-, (E)- | 96 | C2H2Cl2 | 000156-60-5 | 94 |
| 4 | Ethene, 1,2-dichloro-, (Z)- | 96 | C2H2Cl2 | 000156-59-2 | 94 |

0648061.D LIMS_A1_5.M Mon Dec 20 15:20:03 2010 D.00.00

0648063-LSCRPT.TXT
Library Search Compound Report

Data File : C:\MSDCHEM\5\20784505FRM\0648063.D Vial: 16
Acq On : 18 Nov 2010 19:35 Operator: LIMS import
Sample : Inst : UC-SPG5-D
Misc : Multiplr: 1.00
MS Integration Params: jwint.p
Quant Method : C:\MSDCHEM\1\METHODS\LIMS_A1_5.M (RTE Integrator)
Title : Gore Expanded Target VOCs/SVOCs
Library : C:\DATABASE\NIST02.L

**********

Peak Number 1 Carbon dioxide Concentration Rank 4

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.39 | 0.30 ug | 30503 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Carbon dioxide | 44 | CO2 | 000124-38-9 | 2 |
| 2 | Nitrous Oxide | 44 | N2O | 010024-97-2 | 2 |
| 3 | Carbon dioxide | 44 | CO2 | 000124-38-9 | 2 |
| 4 | Ethyne, fluoro- | 44 | C2HF | 002713-09-9 | 2 |

**********

Peak Number 2 Sulfur dioxide Concentration Rank 3

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.46 | 0.31 ug | 31475 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Cysteic acid | 169 | C3H7NO5S | 1000131-23-1 | 74 |
| 2 | Aminomethanesulfonic acid | 111 | CH5NO3S | 013881-91-9 | 74 |
| 3 | Sulfur dioxide | 64 | O2S | 007446-09-5 | 74 |
| 4 | Sulfur dioxide | 64 | O2S | 007446-09-5 | 74 |

**********

Peak Number 3 Ethanethiol Concentration Rank 2

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.50 | 0.37 ug | 37655 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Ethanethiol | 62 | C2H6S | 000075-08-1 | 3 |
| 2 | Ethanethiol | 62 | C2H6S | 000075-08-1 | 3 |
| 3 | Ethene, chloro- | 62 | C2H3Cl | 000075-01-4 | 3 |
| 4 | Phosphine, ethyl- | 62 | C2H7P | 000593-68-0 | 3 |

**********

Peak Number 4 Ethane, 1,2-dichloro-1,1,2-... Concentration Rank 1

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.67 | 0.39 ug | 39287 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Ethane, 1,2-dichloro-1,1,2-trifl... | 152 | C2HCl2F3 | 000354-23-4 | 86 |
| 2 | Benzyl nitrile | 117 | C8H7N | 000140-29-4 | 7 |
| 3 | Benzene, (3-chloro-1-propenyl)- | 152 | C9H9Cl | 002687-12-9 | 7 |
| 4 | Benzyl nitrile | 117 | C8H7N | 000140-29-4 | 7 |

**********

Peak Number 5 1,2,5-Hexatriene Concentration Rank 5

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.87 | 0.20 ug | 20750 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | 1,2,5-Hexatriene | 80 | C6H8 | 003642-18-0 | 7 |
| 2 | Cyclopropane, ethenylmethylene- | 80 | C6H8 | 019995-92-7 | 4 |
| 3 | Cyclopropene, 3-methyl-3-vinyl- | 80 | C6H8 | 071153-30-5 | 4 |
| 4 | 2-Hexen-4-yne | 80 | C6H8 | 014092-20-7 | 3 |

0648063.D LIMS_A1_5.M Mon Dec 20 15:23:08 2010 D.00.00

0648062-LSCRPT.TXT
Library Search Compound Report

Data File : C:\MSDCHEM\5\20784505FRM\0648062.D Vial: 69
Acq On : 19 Nov 2010 20:21 Operator: LIMS import
Sample : Inst : UC-SPG5-D
Misc : Multiplr: 1.00
MS Integration Params: jwint.p
Quant Method : C:\MSDCHEM\1\METHODS\LIMS_A1_5.M (RTE Integrator)
Title : Gore Expanded Target VOCs/SVOCs
Library : C:\DATABASE\NIST02.L

**********

Peak Number 1 Carbon dioxide Concentration Rank 3

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.41 | 0.38 ug | 39010 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Carbon dioxide | 44 | CO2 | 000124-38-9 | 2 |
| 2 | Nitrous Oxide | 44 | N2O | 010024-97-2 | 2 |
| 3 | Ethylene oxide | 44 | C2H4O | 000075-21-8 | 2 |
| 4 | Carbon dioxide | 44 | CO2 | 000124-38-9 | 2 |

**********

Peak Number 2 Sulfur dioxide Concentration Rank 1

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.47 | 0.68 ug | 69288 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Sulfur dioxide | 64 | O2S | 007446-09-5 | 74 |
| 2 | Aminomethanesulfonic acid | 111 | CH5NO3S | 013881-91-9 | 74 |
| 3 | Sulfur dioxide | 64 | O2S | 007446-09-5 | 74 |
| 4 | Aminomethanesulfonic acid | 111 | CH5NO3S | 013881-91-9 | 64 |

**********

Peak Number 3 2,3-Diazabicyclo[2.2.1]-hep... Concentration Rank 4

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.61 | 0.15 ug | 15413 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Pyrrole | 67 | C4H5N | 000109-97-7 | 9 |
| 2 | 2,3-Diazabicyclo[2.2.1]-hept-2-ene | 96 | C5H8N2 | 002721-32-6 | 9 |
| 3 | Cyclopropene | 40 | C3H4 | 002781-85-3 | 5 |
| 4 | Cyclopropane, ethylidene- | 68 | C5H8 | 018631-83-9 | 4 |

**********

Peak Number 4 2,4-Hexadiene, (E,Z)- Concentration Rank 2

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.69 | 0.47 ug | 47963 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | 1,4-Pentadiene, 2-methyl- | 82 | C6H10 | 000763-30-4 | 9 |
| 2 | Cyclopropane, 1,2-dimethyl-3-met... | 82 | C6H10 | 005070-00-8 | 9 |
| 3 | Cyclopropane, 1,2-dimethyl-3-met... | 82 | C6H10 | 004866-55-1 | 9 |
| 4 | 2,4-Hexadiene, (E,Z)- | 82 | C6H10 | 005194-50-3 | 9 |

**********

Peak Number 5 Mercaptamine Concentration Rank 5

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.89 | 0.13 ug | 13710 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Mercaptamine | 77 | C2H7NS | 000060-23-1 | 4 |
| 2 | Mercaptamine | 77 | C2H7NS | 000060-23-1 | 2 |
| 3 | Methane, nitroso- | 45 | CH3NO | 000865-40-7 | 2 |
| 4 | 2-Chloroethylamine | 79 | C2H6ClN | 000689-98-5 | 2 |

0648062.D LIMS_A1_5.M Mon Dec 20 15:21:32 2010 D.00.00

0648064-LSCRPT.TXT
Library Search Compound Report

Data File : C:\MSDCHEM\5\20784505FRM\0648064.D Vial: 29
Acq On : 19 Nov 2010 1:38 Operator: LIMS import
Sample : Inst : UC-SPG5-D
Misc : Multiplr: 1.00
MS Integration Params: jwint.p
Quant Method : C:\MSDCHEM\1\METHODS\LIMS_A1_5.M (RTE Integrator)
Title : Gore Expanded Target VOCs/SVOCs
Library : C:\DATABASE\NIST02.L

**********

Peak Number 1 Ethene, chlorotrifluoro- Concentration Rank 4

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.44 | 0.92 ug | 93726 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Ethene, chlorotrifluoro- | 116 | C2ClF3 | 000079-38-9 | 96 |
| 2 | Ethene, chlorotrifluoro- | 116 | C2ClF3 | 000079-38-9 | 87 |
| 3 | 5-Chloro-1-methylimidazole | 116 | C4H5ClN2 | 000872-49-1 | 9 |
| 4 | 1-Propene, 1-(ethylthio)-2-methyl- | 116 | C6H12S | 027482-14-0 | 9 |

**********

Peak Number 2 1-Propene, 2-methyl- Concentration Rank 3

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.50 | 1.80 ug | 183510 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | 1-Propene, 2-methyl- | 56 | C4H8 | 000115-11-7 | 53 |
| 2 | 1-Butene | 56 | C4H8 | 000106-98-9 | 49 |
| 3 | 1-Propene, 2-methyl- | 56 | C4H8 | 000115-11-7 | 46 |
| 4 | 2-Butene, (E)- | 56 | C4H8 | 000624-64-6 | 46 |

**********

Peak Number 3 Pentane Concentration Rank 1

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.70 | 2.51 ug | 256518 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Pentane | 72 | C5H12 | 000109-66-0 | 43 |
| 2 | Cyclopropane | 42 | C3H6 | 000075-19-4 | 38 |
| 3 | Pentane | 72 | C5H12 | 000109-66-0 | 38 |
| 4 | Pentane | 72 | C5H12 | 000109-66-0 | 38 |

**********

Peak Number 4 Methylene Chloride Concentration Rank 2

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.84 | 2.11 ug | 215177 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Methylene Chloride | 84 | CH2Cl2 | 000075-09-2 | 94 |
| 2 | Methylene Chloride | 84 | CH2Cl2 | 000075-09-2 | 91 |
| 3 | Methylene Chloride | 84 | CH2Cl2 | 000075-09-2 | 91 |
| 4 | Methylene Chloride | 84 | CH2Cl2 | 000075-09-2 | 52 |

**********

Peak Number 5 Hexane Concentration Rank 5

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 3.14 | 0.51 ug | 51790 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Hexane | 86 | C6H14 | 000110-54-3 | 78 |
| 2 | Hexane | 86 | C6H14 | 000110-54-3 | 45 |
| 3 | Hexane | 86 | C6H14 | 000110-54-3 | 28 |
| 4 | 1-Pentene, 4-methyl- | 84 | C6H12 | 000691-37-2 | 9 |

0648064.D LIMS_A1_5.M Mon Dec 20 15:23:52 2010 D.00.00

# Library Search Compound Report

Data File : C:\MSDCHEM\5\20784505FRM\0648066.D Vial: 76
Acq On : 19 Nov 2010 23:37 Operator: LIMS import
Sample : Inst : UC-SPG5-D
Misc : Multiplr: 1.00
MS Integration Params: jwint.p
Quant Method : C:\MSDCHEM\1\METHODS\LIMS_A1_5.M (RTE Integrator)
Title : Gore Expanded Target VOCs/SVOCs
Library : C:\DATABASE\NIST02.L

**********

Peak Number 1 Ethene, chlorotrifluoro- Concentration Rank 2

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.45 | 5.39 ug | 549600 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Ethene, chlorotrifluoro- | 116 | C2ClF3 | 000079-38-9 | 96 |
| 2 | Ethene, chlorotrifluoro- | 116 | C2ClF3 | 000079-38-9 | 86 |
| 3 | 3-Ethylthiolane | 116 | C6H12S | 062184-67-2 | 22 |
| 4 | 5-Chloro-1-methylimidazole | 116 | C4H5ClN2 | 000872-49-1 | 9 |

**********

Peak Number 2 1-Propene, 2-methyl- Concentration Rank 3

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.52 | 4.82 ug | 491564 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | 1-Propene, 2-methyl- | 56 | C4H8 | 000115-11-7 | 52 |
| 2 | 1-Propene, 2-methyl- | 56 | C4H8 | 000115-11-7 | 43 |
| 3 | 2-Butene | 56 | C4H8 | 000107-01-7 | 43 |
| 4 | 1-Butene | 56 | C4H8 | 000106-98-9 | 38 |

**********

Peak Number 3 Ethene, 1,1-dichloro-2,2-di... Concentration Rank 5

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.62 | 2.78 ug | 283323 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Ethene, 1,1-dichloro-2,2-difluoro- | 132 | C2Cl2F2 | 000079-35-6 | 89 |
| 2 | Ethene, 1,1-dichloro-2,2-difluoro- | 132 | C2Cl2F2 | 000079-35-6 | 60 |
| 3 | 1,3-Pentadiene, 3-methyl-, (E)- | 82 | C6H10 | 002787-43-1 | 38 |
| 4 | 1,3-Pentadiene, 2-methyl-, (E)- | 82 | C6H10 | 000926-54-5 | 38 |

**********

Peak Number 4 1,2-Butadiene Concentration Rank 1

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.70 | 10.07 ug | 1026700 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | 1,2-Butadiene | 54 | C4H6 | 000590-19-2 | 80 |
| 2 | 2-Butyne | 54 | C4H6 | 000503-17-3 | 72 |
| 3 | 1-Butyne | 54 | C4H6 | 000107-00-6 | 72 |
| 4 | 2-Butyne | 54 | C4H6 | 000503-17-3 | 64 |

**********

Peak Number 5 1,4-Dioxane Concentration Rank 4

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 4.03 | 3.36 ug | 343131 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | 1,4-Dioxane | 88 | C4H8O2 | 000123-91-1 | 91 |
| 2 | 1,4-Dioxane | 88 | C4H8O2 | 000123-91-1 | 90 |
| 3 | 1,4-Dioxane | 88 | C4H8O2 | 000123-91-1 | 83 |
| 4 | 1,4-Dioxane | 88 | C4H8O2 | 000123-91-1 | 83 |

0648066.D LIMS_A1_5.M Mon Dec 20 15:26:26 2010 D.00.00

0648065-LSCRPT.TXT
Library Search Compound Report

Data File : C:\MSDCHEM\5\20784505FRM\0648065.D Vial: 28
Acq On : 19 Nov 2010 1:10 Operator: LIMS import
Sample : Inst : UC-SPG5-D
Misc : Multiplr: 1.00
MS Integration Params: jwint.p
Quant Method : C:\MSDCHEM\1\METHODS\LIMS_A1_5.M (RTE Integrator)
Title : Gore Expanded Target VOCs/SVOCs
Library : C:\DATABASE\NIST02.L

**********

Peak Number 1 Carbon dioxide Concentration Rank 5

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.39 | 0.21 ug | 21795 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Carbon dioxide | 44 | CO2 | 000124-38-9 | 2 |
| 2 | Nitrous Oxide | 44 | N2O | 010024-97-2 | 2 |
| 3 | Carbon dioxide | 44 | CO2 | 000124-38-9 | 2 |
| 4 | Ethyne, fluoro- | 44 | C2HF | 002713-09-9 | 2 |

**********

Peak Number 2 Sulfur dioxide Concentration Rank 3

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.44 | 0.76 ug | 77769 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Sulfur dioxide | 64 | O2S | 007446-09-5 | 9 |
| 2 | Aminomethanesulfonic acid | 111 | CH5NO3S | 013881-91-9 | 9 |
| 3 | Aminomethanesulfonic acid | 111 | CH5NO3S | 013881-91-9 | 9 |
| 4 | Sulfur dioxide | 64 | O2S | 007446-09-5 | 7 |

**********

Peak Number 3 1-Propene, 2-methyl- Concentration Rank 2

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.51 | 0.88 ug | 90182 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | 1-Propene, 2-methyl- | 56 | C4H8 | 000115-11-7 | 42 |
| 2 | 1-Propene, 2-methyl- | 56 | C4H8 | 000115-11-7 | 9 |
| 3 | 1-Butene | 56 | C4H8 | 000106-98-9 | 9 |
| 4 | 1-Butene | 56 | C4H8 | 000106-98-9 | 9 |

**********

Peak Number 4 Cyclopropane, ethyl- Concentration Rank 1

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.70 | 0.99 ug | 101026 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Cyclopropane, ethyl- | 70 | C5H10 | 001191-96-4 | 64 |
| 2 | 3-Buten-1-ol | 72 | C4H8O | 000627-27-0 | 53 |
| 3 | Cyclopropane, 1,2-dimethyl-, cis- | 70 | C5H10 | 000930-18-7 | 50 |
| 4 | Pentane | 72 | C5H12 | 000109-66-0 | 47 |

**********

Peak Number 5 2-Butene, (E)- Concentration Rank 4

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 3.15 | 0.25 ug | 25330 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | 2-Butene, (E)- | 56 | C4H8 | 000624-64-6 | 9 |
| 2 | 2-Butene | 56 | C4H8 | 000107-01-7 | 5 |
| 3 | 2-Butene, (Z)- | 56 | C4H8 | 000590-18-1 | 5 |
| 4 | Cyclobutane | 56 | C4H8 | 000287-23-0 | 5 |

0648065.D LIMS_A1_5.M Mon Dec 20 15:25:03 2010 D.00.00

0648068-LSCRPT.TXT
Library Search Compound Report

Data File : C:\MSDCHEM\5\20784505FRM\0648068.D Vial: 36
Acq On : 19 Nov 2010 4:53 Operator: LIMS import
Sample : Inst : UC-SPG5-D
Misc : Multiplr: 1.00
MS Integration Params: jwint.p
Quant Method : C:\MSDCHEM\1\METHODS\LIMS_A1_5.M (RTE Integrator)
Title : Gore Expanded Target VOCs/SVOCs
Library : C:\DATABASE\NIST02.L

**********

Peak Number 1 Cysteic acid Concentration Rank 4

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.46 | 0.37 ug | 37319 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Sulfur dioxide | 64 | O2S | 007446-09-5 | 74 |
| 2 | Sulfur dioxide | 64 | O2S | 007446-09-5 | 74 |
| 3 | Cysteic acid | 169 | C3H7NO5S | 1000131-23-1 | 64 |
| 4 | Aminomethanesulfonic acid | 111 | CH5NO3S | 013881-91-9 | 64 |

**********

Peak Number 2 1-Propene, 2-methyl- Concentration Rank 1

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.51 | 0.61 ug | 62019 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | 1-Propene, 2-methyl- | 56 | C4H8 | 000115-11-7 | 9 |
| 2 | 1-Propene, 2-methyl- | 56 | C4H8 | 000115-11-7 | 7 |
| 3 | 1-Propene, 2-methyl- | 56 | C4H8 | 000115-11-7 | 5 |
| 4 | 1-Butene | 56 | C4H8 | 000106-98-9 | 4 |

**********

Peak Number 3 Silane, tetramethyl- Concentration Rank 3

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.60 | 0.47 ug | 48037 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Silane, tetramethyl- | 88 | C4H12Si | 000075-76-3 | 72 |
| 2 | 1-Propene-1-thiol | 74 | C3H6S | 000925-89-3 | 72 |
| 3 | Silane, tetramethyl- | 88 | C4H12Si | 000075-76-3 | 59 |
| 4 | Silane, tetramethyl- | 88 | C4H12Si | 000075-76-3 | 56 |

**********

Peak Number 4 Pentane Concentration Rank 2

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.71 | 0.58 ug | 59158 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Pentane | 72 | C5H12 | 000109-66-0 | 53 |
| 2 | Pentane | 72 | C5H12 | 000109-66-0 | 53 |
| 3 | Pentane | 72 | C5H12 | 000109-66-0 | 40 |
| 4 | 1-Butanol | 74 | C4H10O | 000071-36-3 | 36 |

**********

Peak Number 5 Diisopropyl ether Concentration Rank 5

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 3.16 | 0.33 ug | 33932 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Diisopropyl ether | 102 | C6H14O | 000108-20-3 | 40 |
| 2 | Diisopropyl ether | 102 | C6H14O | 000108-20-3 | 40 |
| 3 | 2-Hexanol, 3-methyl- | 116 | C7H16O | 002313-65-7 | 38 |
| 4 | 2-Pentanol, 3-chloro-4-methyl-, ... | 136 | C6H13ClO | 074685-47-5 | 9 |

0648068.D LIMS_A1_5.M Tue Dec 21 11:29:54 2010 D.00.00

0648067-LSCRPT.TXT
Library Search Compound Report

Data File : C:\MSDCHEM\5\20784505FRM\0648067.D Vial: 54
Acq On : 19 Nov 2010 13:16 Operator: LIMS import
Sample : Inst : UC-SPG5-D
Misc : Multiplr: 1.00
MS Integration Params: jwint.p
Quant Method : C:\MSDCHEM\1\METHODS\LIMS_A1_5.M (RTE Integrator)
Title : Gore Expanded Target VOCs/SVOCs
Library : C:\DATABASE\NIST02.L

**********

Peak Number 1 Sulfur dioxide Concentration Rank 2

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.45 | 1.04 ug | 106376 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Sulfur dioxide | 64 | O2S | 007446-09-5 | 74 |
| 2 | Aminomethanesulfonic acid | 111 | CH5NO3S | 013881-91-9 | 74 |
| 3 | Aminomethanesulfonic acid | 111 | CH5NO3S | 013881-91-9 | 74 |
| 4 | Sulfur dioxide | 64 | O2S | 007446-09-5 | 74 |

**********

Peak Number 2 Ethanethiol Concentration Rank 5

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.50 | 0.56 ug | 56614 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Ethanethiol | 62 | C2H6S | 000075-08-1 | 56 |
| 2 | Ethanethiol | 62 | C2H6S | 000075-08-1 | 9 |
| 3 | Ethanethiol | 62 | C2H6S | 000075-08-1 | 9 |
| 4 | Phosphine, ethyl- | 62 | C2H7P | 000593-68-0 | 9 |

**********

Peak Number 3 Fluorodichloromethane Concentration Rank 1

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.61 | 1.49 ug | 151959 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Fluorodichloromethane | 102 | CHCl2F | 000075-43-4 | 68 |
| 2 | Fluorodichloromethane | 102 | CHCl2F | 000075-43-4 | 59 |
| 3 | Fluorodichloromethane | 102 | CHCl2F | 000075-43-4 | 43 |
| 4 | 3-Heptyn-1-ol | 112 | C7H12O | 014916-79-1 | 9 |

**********

Peak Number 4 1,2-Butadiene Concentration Rank 4

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.68 | 0.71 ug | 72150 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | 1,2-Butadiene | 54 | C4H6 | 000590-19-2 | 53 |
| 2 | 1,2-Butadiene | 54 | C4H6 | 000590-19-2 | 42 |
| 3 | 2-Butyne | 54 | C4H6 | 000503-17-3 | 42 |
| 4 | 3-Pentyn-1-ol | 84 | C5H8O | 010229-10-4 | 38 |

**********

Peak Number 5 1,4-Dioxane Concentration Rank 3

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 4.02 | 0.77 ug | 78155 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | 1,4-Dioxane | 88 | C4H8O2 | 000123-91-1 | 91 |
| 2 | 1,4-Dioxane | 88 | C4H8O2 | 000123-91-1 | 91 |
| 3 | 1,4-Dioxane | 88 | C4H8O2 | 000123-91-1 | 90 |
| 4 | 1,4-Dioxane | 88 | C4H8O2 | 000123-91-1 | 90 |

0648067.D LIMS_A1_5.M Tue Dec 21 11:28:24 2010 D.00.00

0648069-LSCRPT.TXT
Library Search Compound Report

Data File : C:\MSDCHEM\5\20784505FRM\0648069.D Vial: 40
Acq On : 19 Nov 2010 6:45 Operator: LIMS import
Sample : Inst : UC-SPG5-D
Misc : Multiplr: 1.00
MS Integration Params: jwint.p
Quant Method : C:\MSDCHEM\1\METHODS\LIMS_A1_5.M (RTE Integrator)
Title : Gore Expanded Target VOCs/SVOCs
Library : C:\DATABASE\NIST02.L

**********

Peak Number 1 Sulfur dioxide Concentration Rank 3

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.43 | 1.52 ug | 155015 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Sulfur dioxide | 64 | O2S | 007446-09-5 | 74 |
| 2 | Sulfur dioxide | 64 | O2S | 007446-09-5 | 74 |
| 3 | Ethene, 1,1-difluoro- | 64 | C2H2F2 | 000075-38-7 | 9 |
| 4 | Aminomethanesulfonic acid | 111 | CH5NO3S | 013881-91-9 | 9 |

**********

Peak Number 2 Trimethylsilyl fluoride Concentration Rank 2

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.51 | 1.79 ug | 182910 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Trimethylsilyl fluoride | 92 | C3H9FSi | 000420-56-4 | 91 |
| 2 | Trimethylsilyl fluoride | 92 | C3H9FSi | 000420-56-4 | 49 |
| 3 | Propane, 2-chloro-2-nitro- | 123 | C3H6ClNO2 | 000594-71-8 | 9 |
| 4 | Trimethylphosphine oxide | 92 | C3H9OP | 000676-96-0 | 4 |

**********

Peak Number 3 2-Butyne Concentration Rank 4

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.66 | 0.81 ug | 82242 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | 1,2-Butadiene | 54 | C4H6 | 000590-19-2 | 86 |
| 2 | 2-Butyne | 54 | C4H6 | 000503-17-3 | 86 |
| 3 | 2-Butyne | 54 | C4H6 | 000503-17-3 | 86 |
| 4 | 1,2-Butadiene | 54 | C4H6 | 000590-19-2 | 72 |

**********

Peak Number 4 Ethyl ether Concentration Rank 5

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.70 | 0.74 ug | 75124 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | Ethyl ether | 74 | C4H10O | 000060-29-7 | 90 |
| 2 | Ethyl ether | 74 | C4H10O | 000060-29-7 | 83 |
| 3 | Ethane, 1,2-diethoxy- | 118 | C6H14O2 | 000629-14-1 | 56 |
| 4 | Hydrazine, trimethyl- | 74 | C3H10N2 | 001741-01-1 | 9 |

**********

Peak Number 5 Silanol, trimethyl- Concentration Rank 1

| R.T. | EstConc | Area | Relative to ISTD | R.T. |
|---|---|---|---|---|
| 2.95 | 11.02 ug | 1124020 | External Standard | 0.00 |

| Hit# of 4 | Tentative ID | MW | MolForm | CAS# | Qual |
|---|---|---|---|---|---|
| 1 | tert-Butyldimethylsilanol | 132 | C6H16OSi | 018173-64-3 | 83 |
| 2 | Silanol, dimethyl(1,1,2-trimethy... | 160 | C8H20OSi | 055644-10-5 | 78 |
| 3 | Silanol, trimethyl- | 90 | C3H10OSi | 001066-40-6 | 64 |
| 4 | Silanol, trimethyl- | 90 | C3H10OSi | 001066-40-6 | 60 |

0648069.D LIMS_A1_5.M Tue Dec 21 11:31:58 2010 D.00.00

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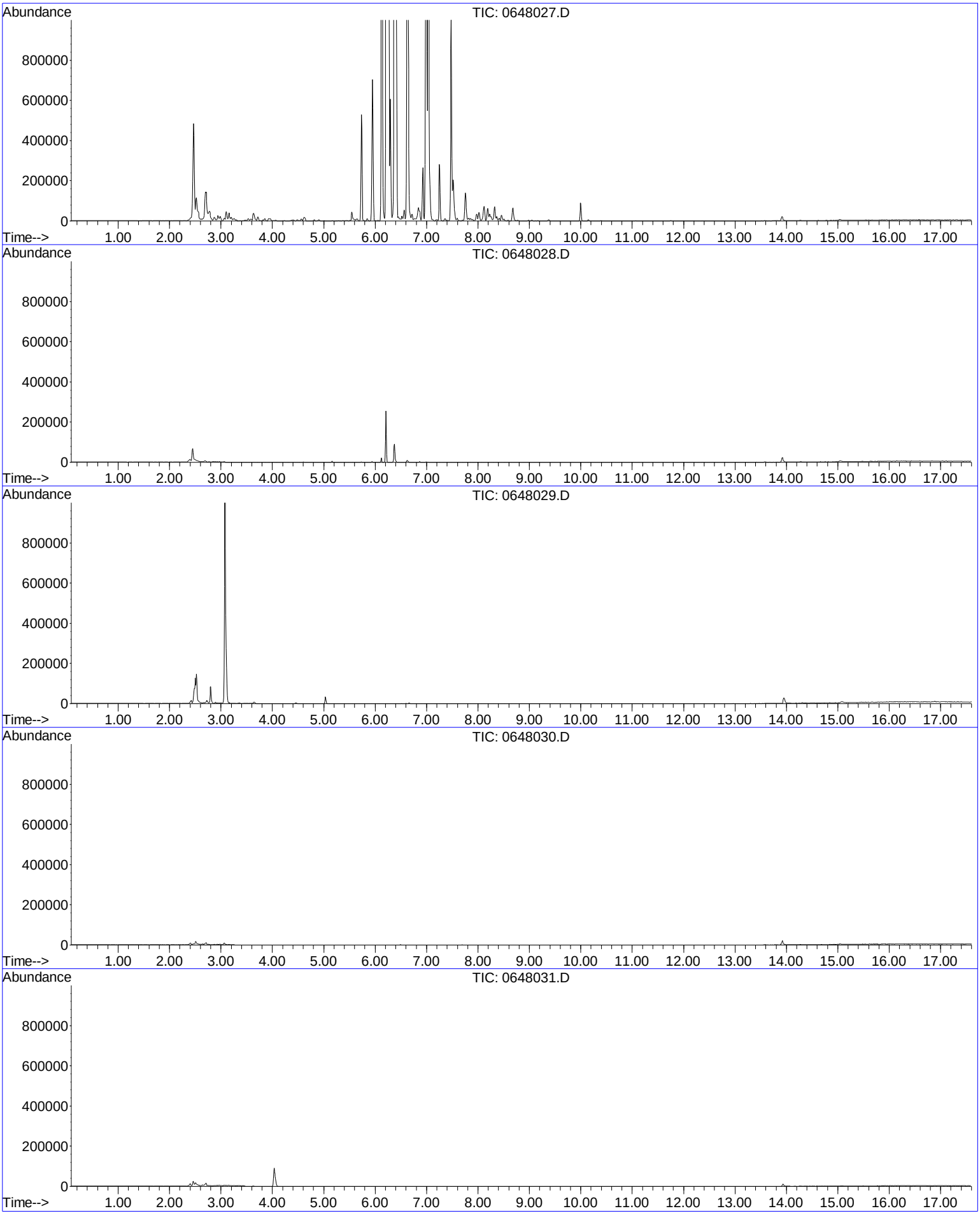
IN NUMERICAL ORDER



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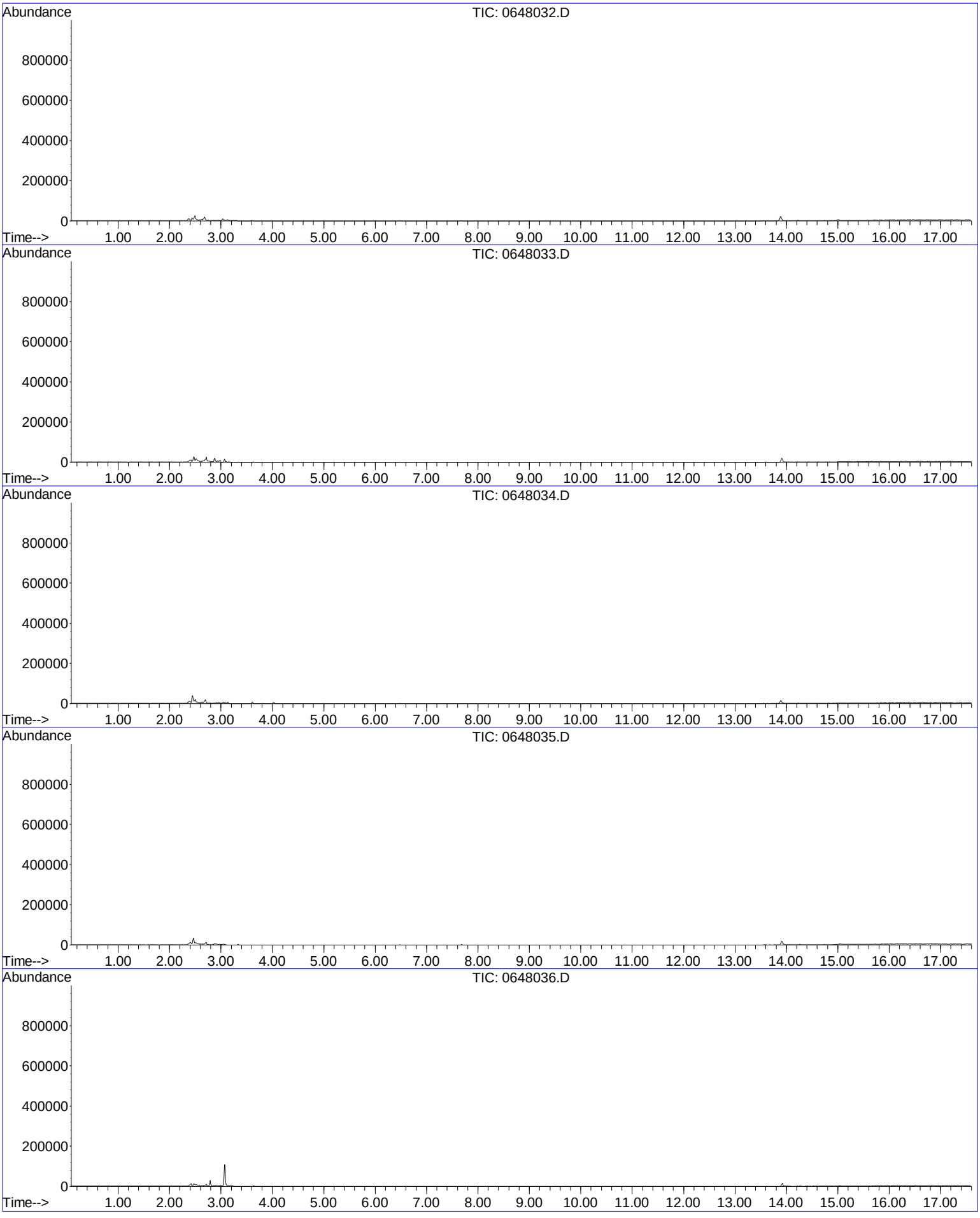
IN NUMERICAL ORDER



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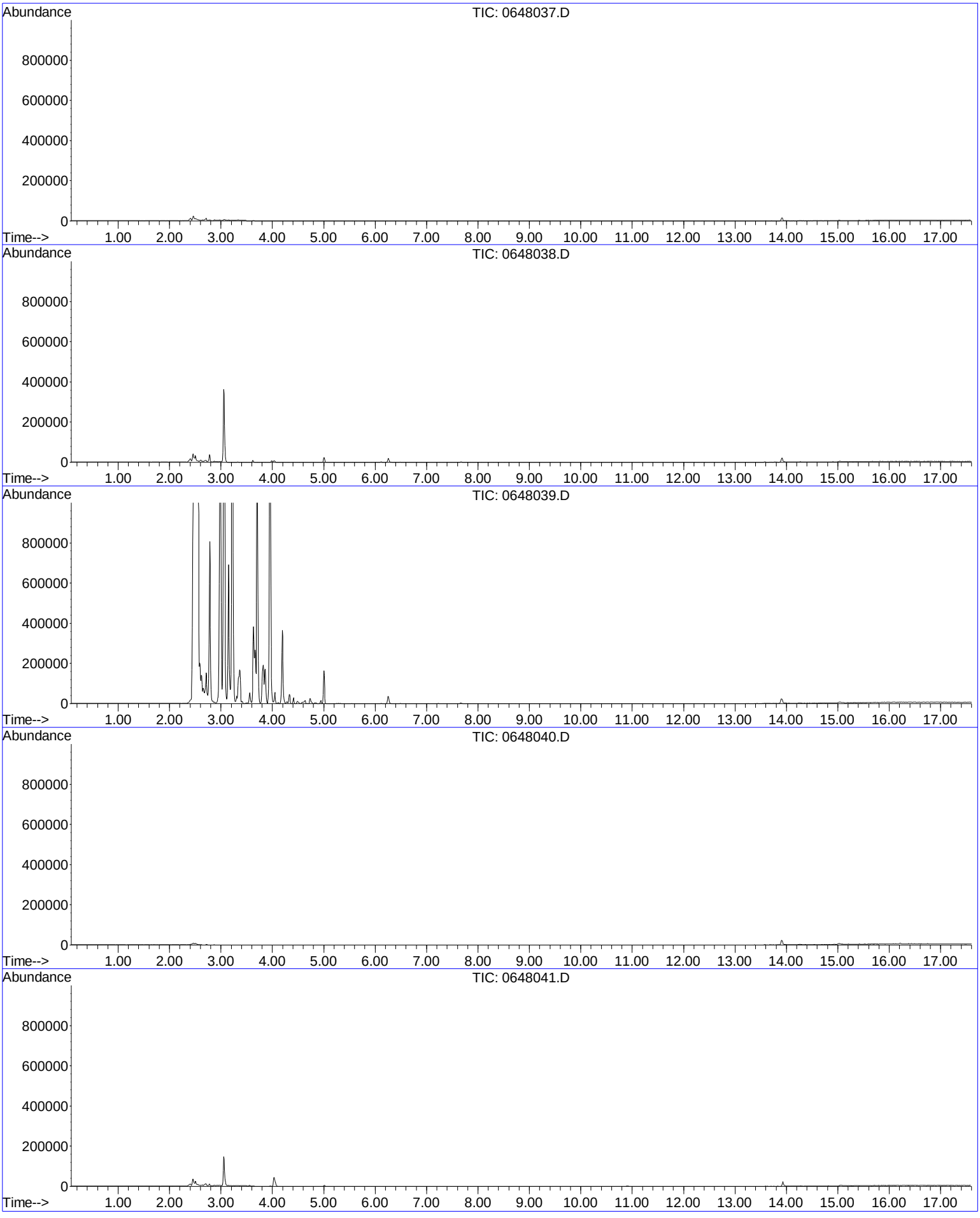
IN NUMERICAL ORDER



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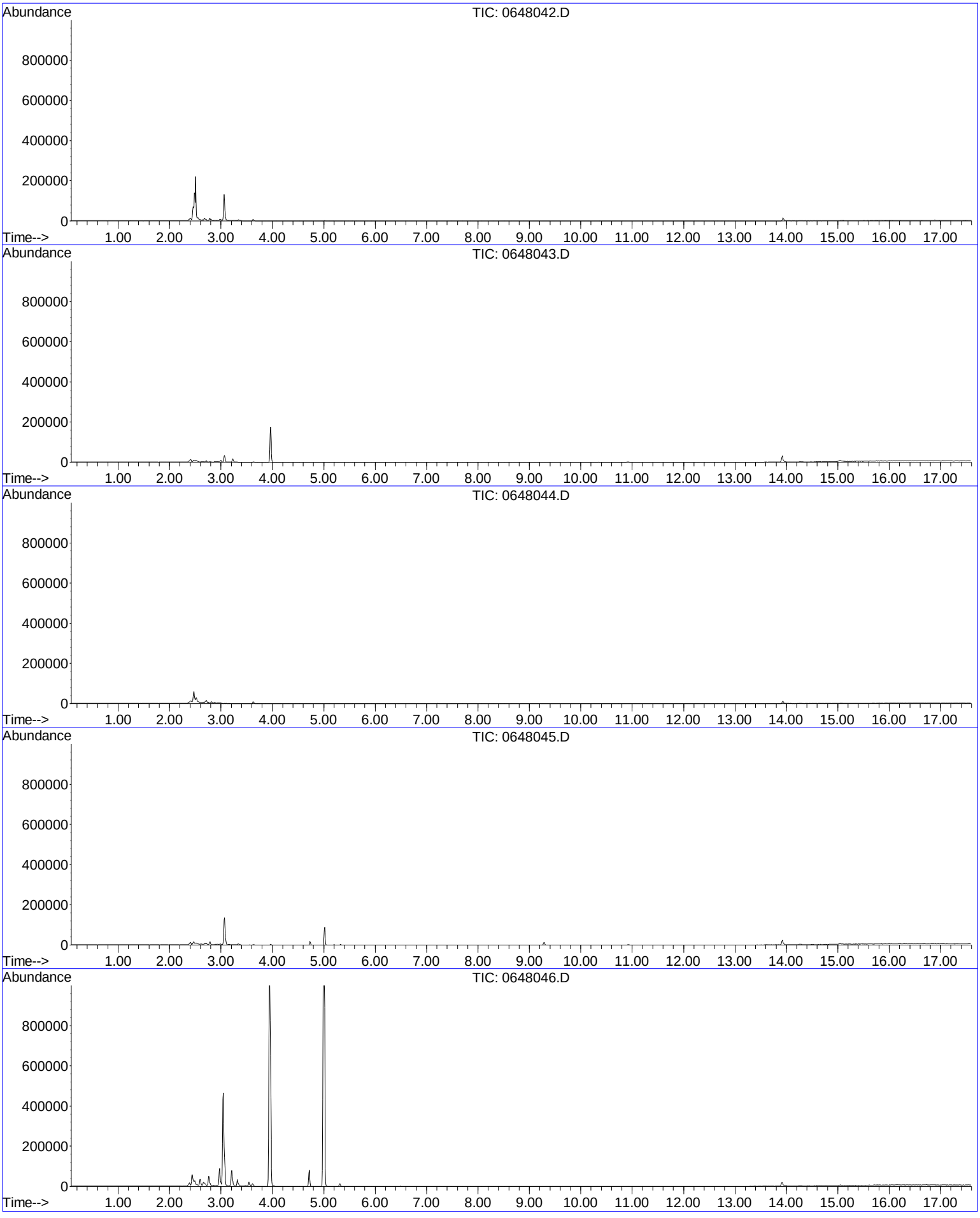
IN NUMERICAL ORDER



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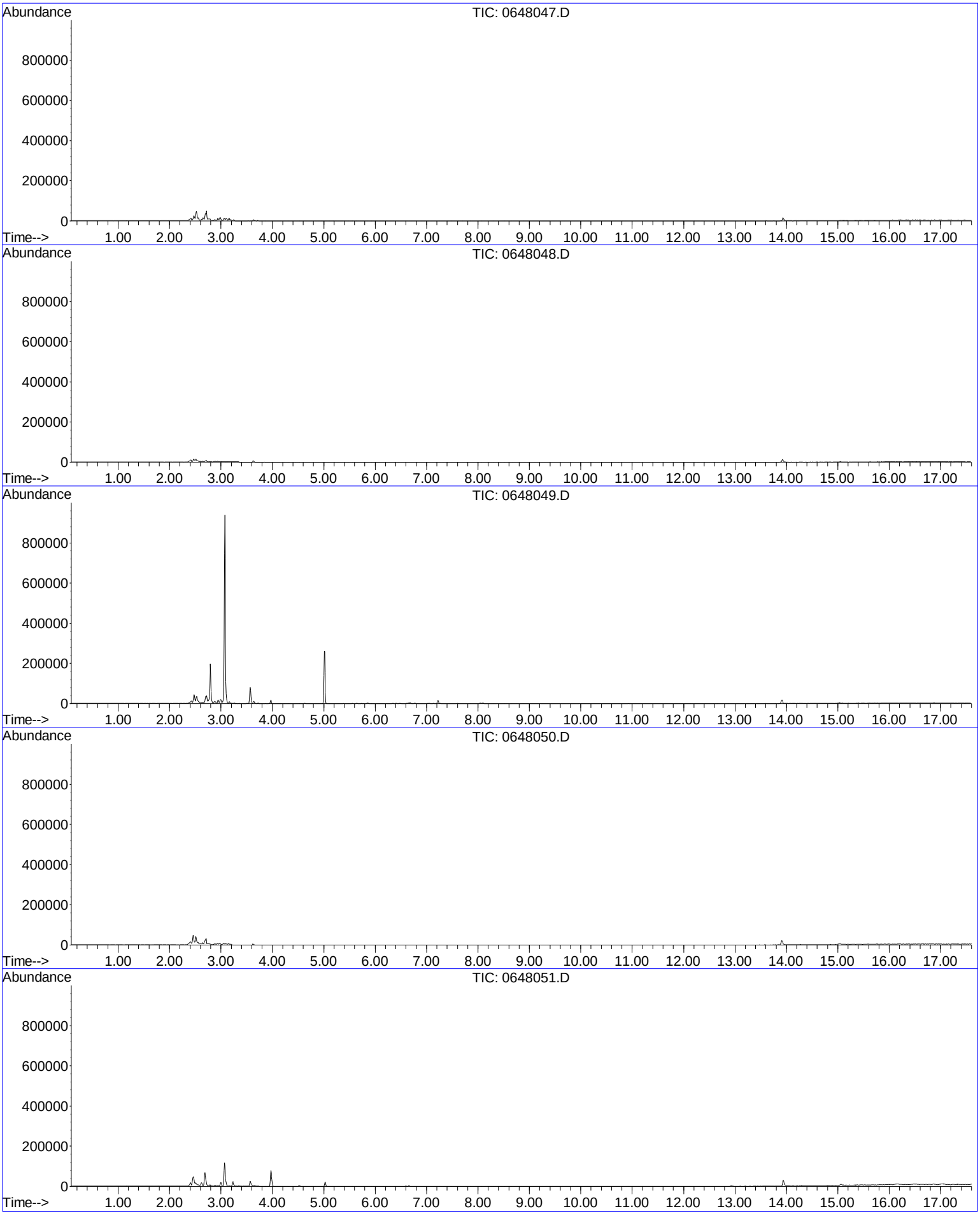
IN NUMERICAL ORDER



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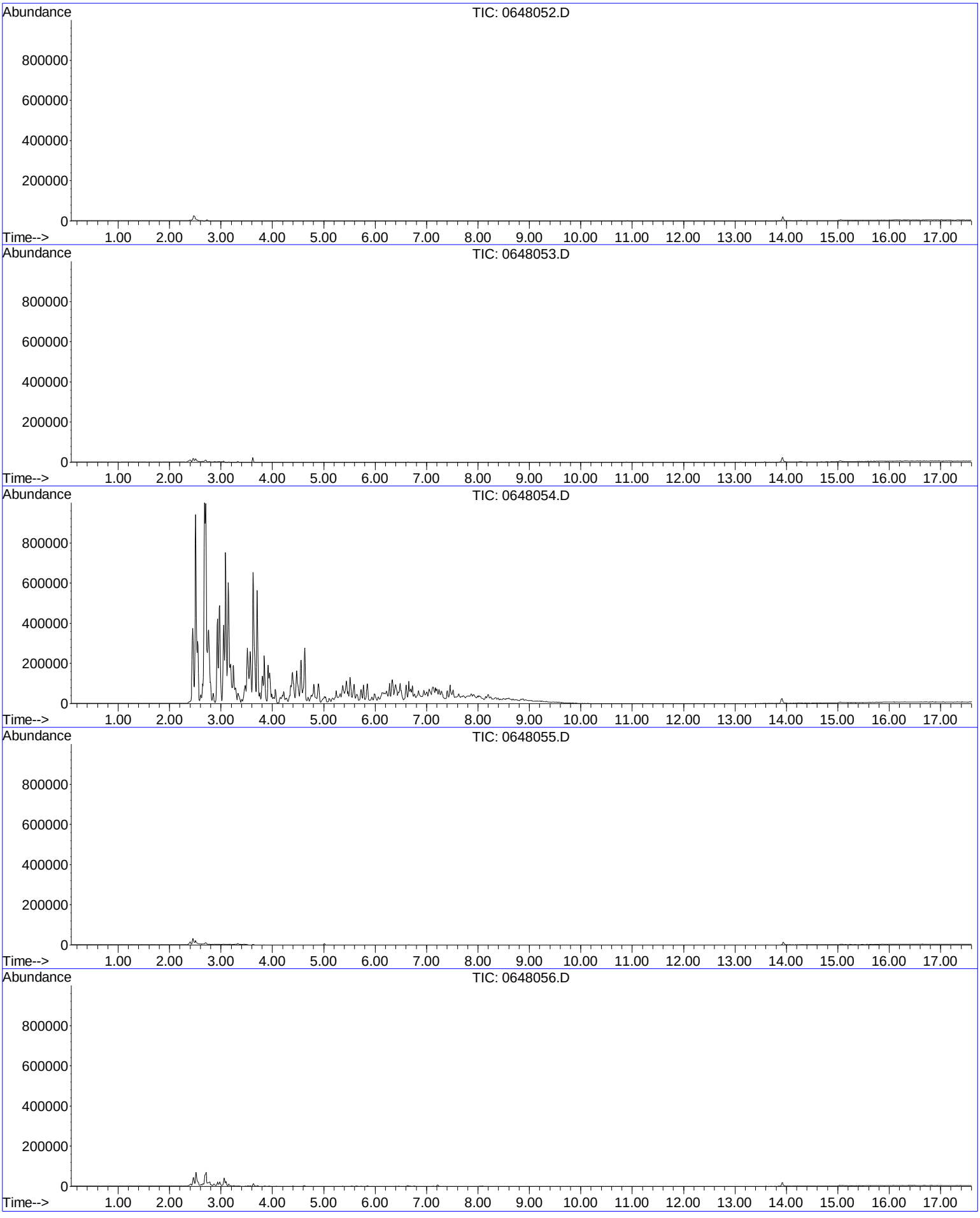
IN NUMERICAL ORDER



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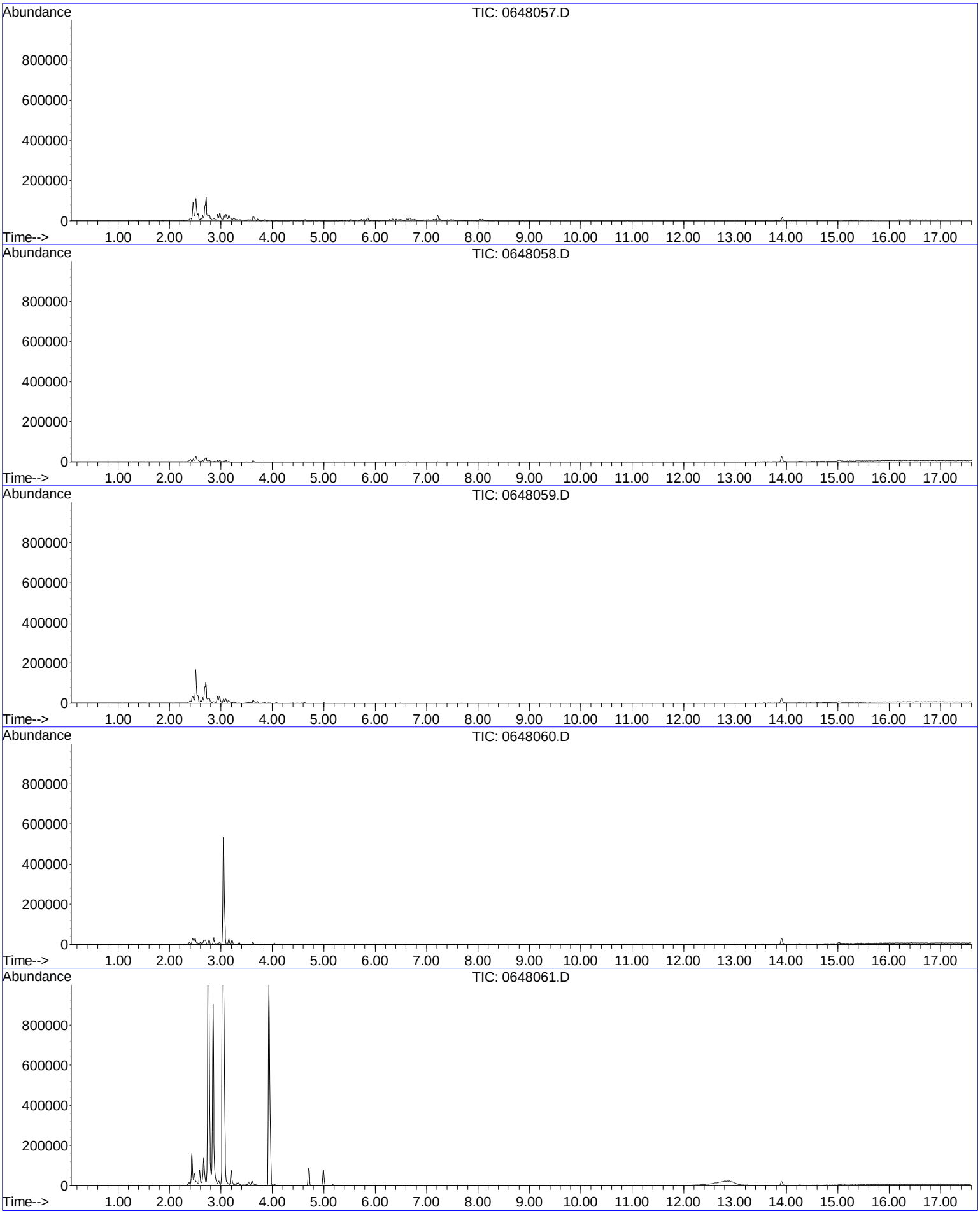
IN NUMERICAL ORDER



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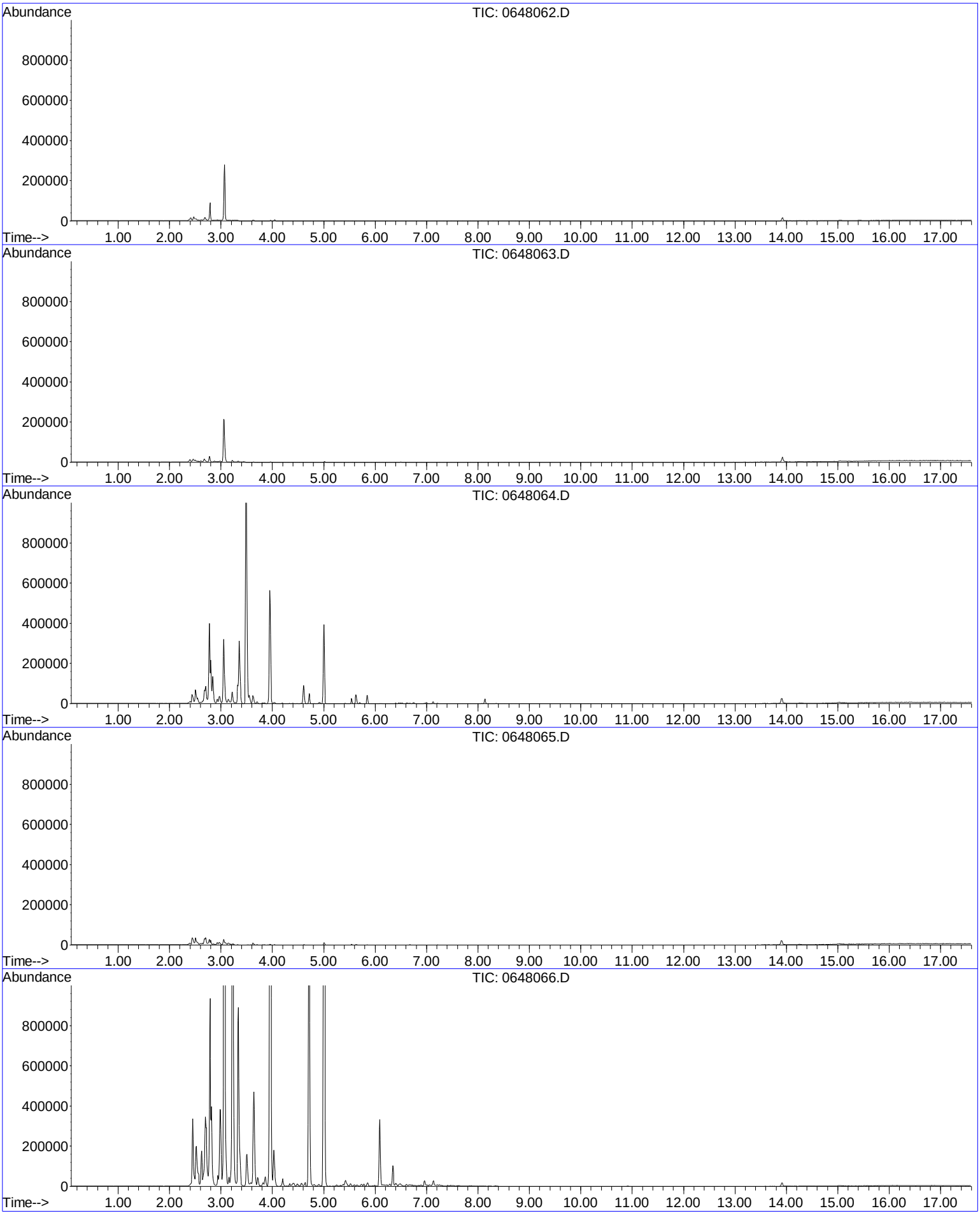

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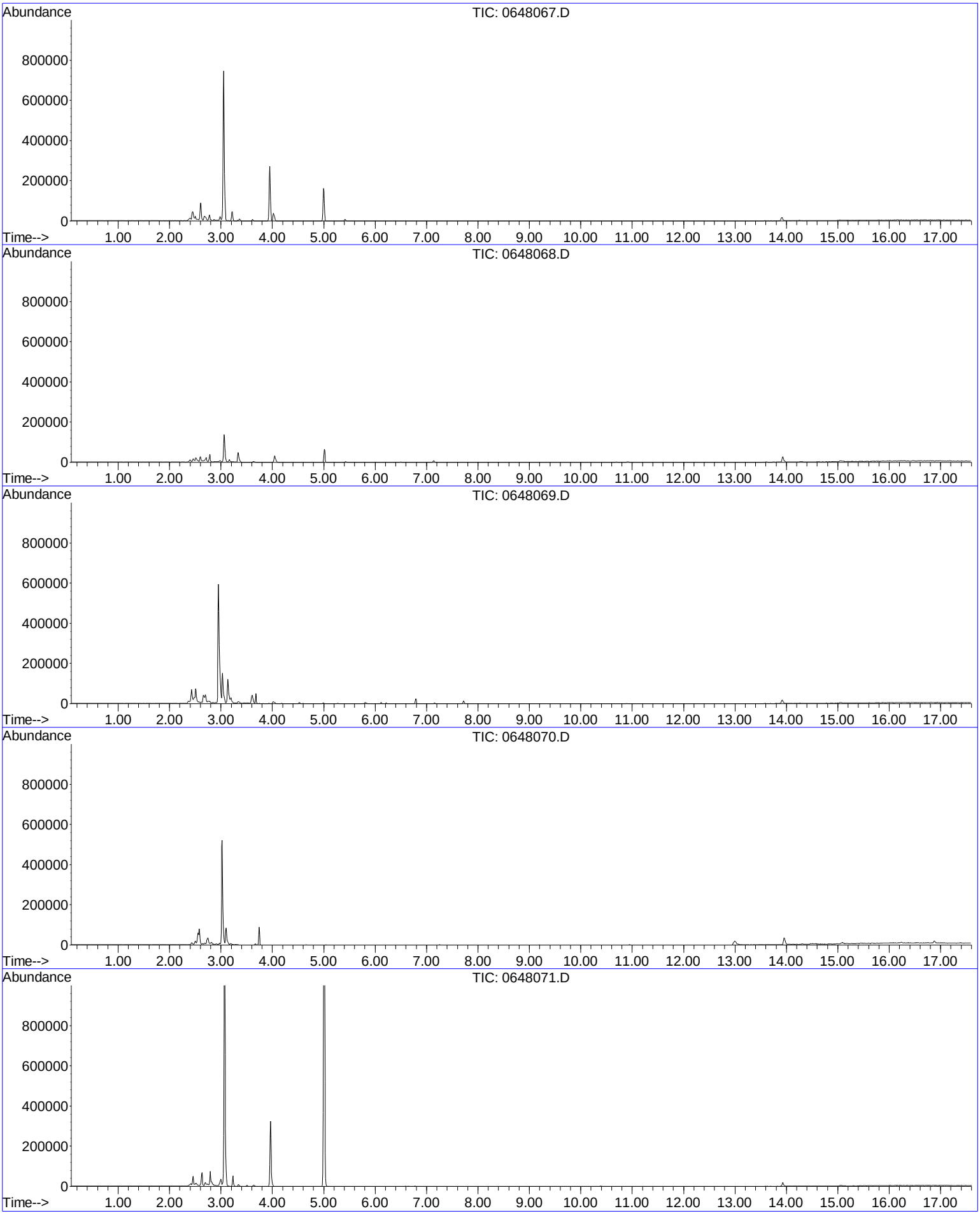
IN NUMERICAL ORDER



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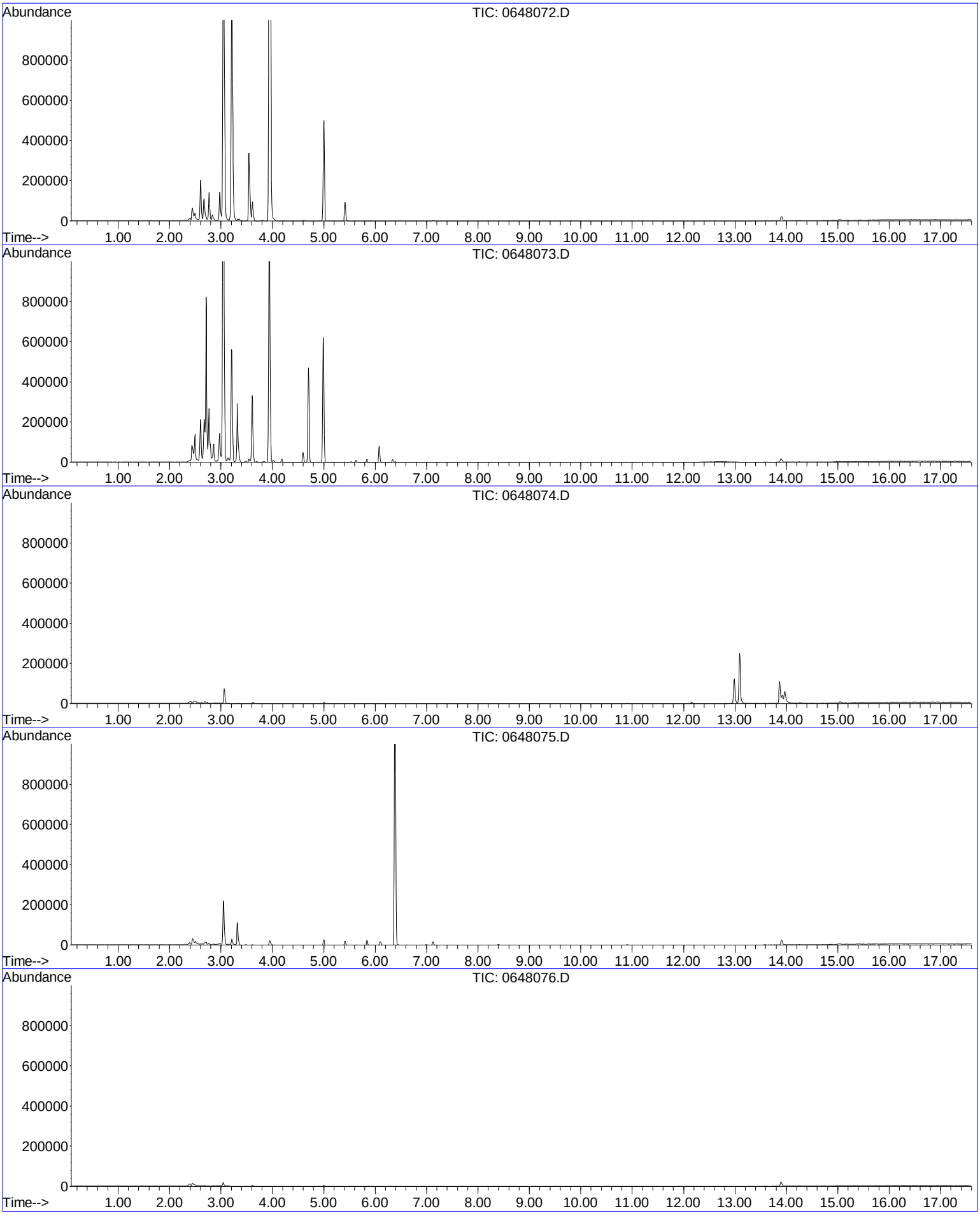
IN NUMERICAL ORDER



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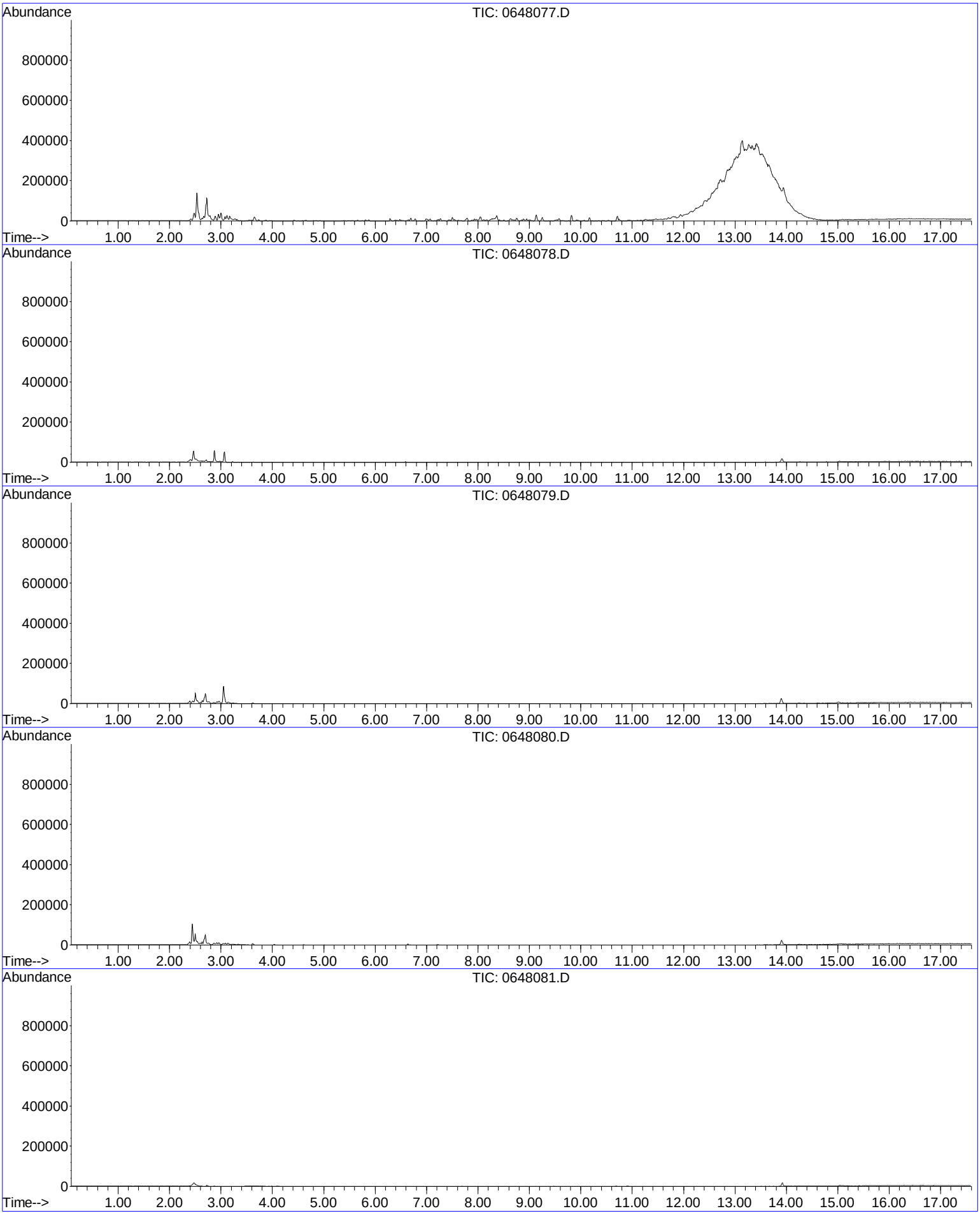
IN NUMERICAL ORDER



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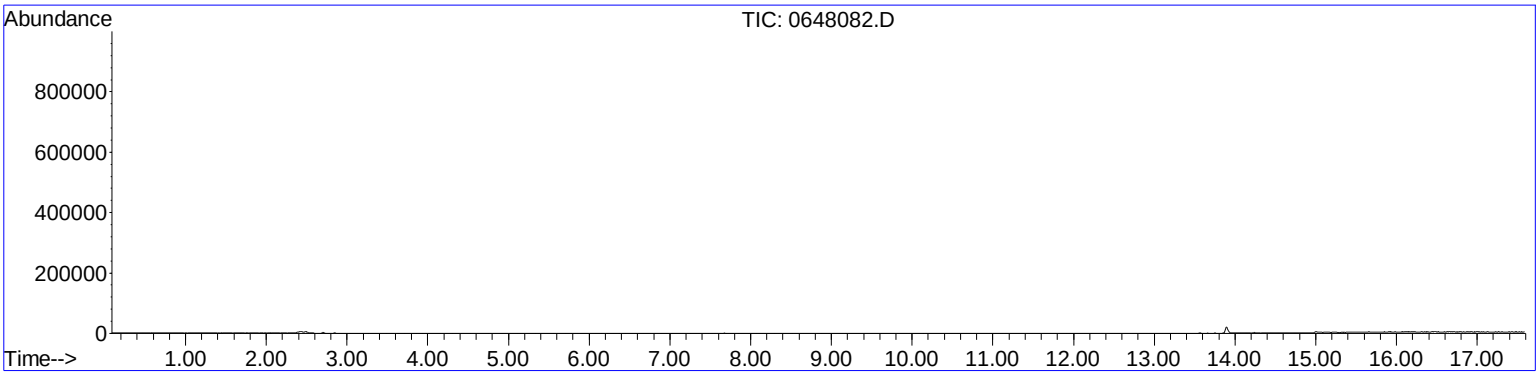
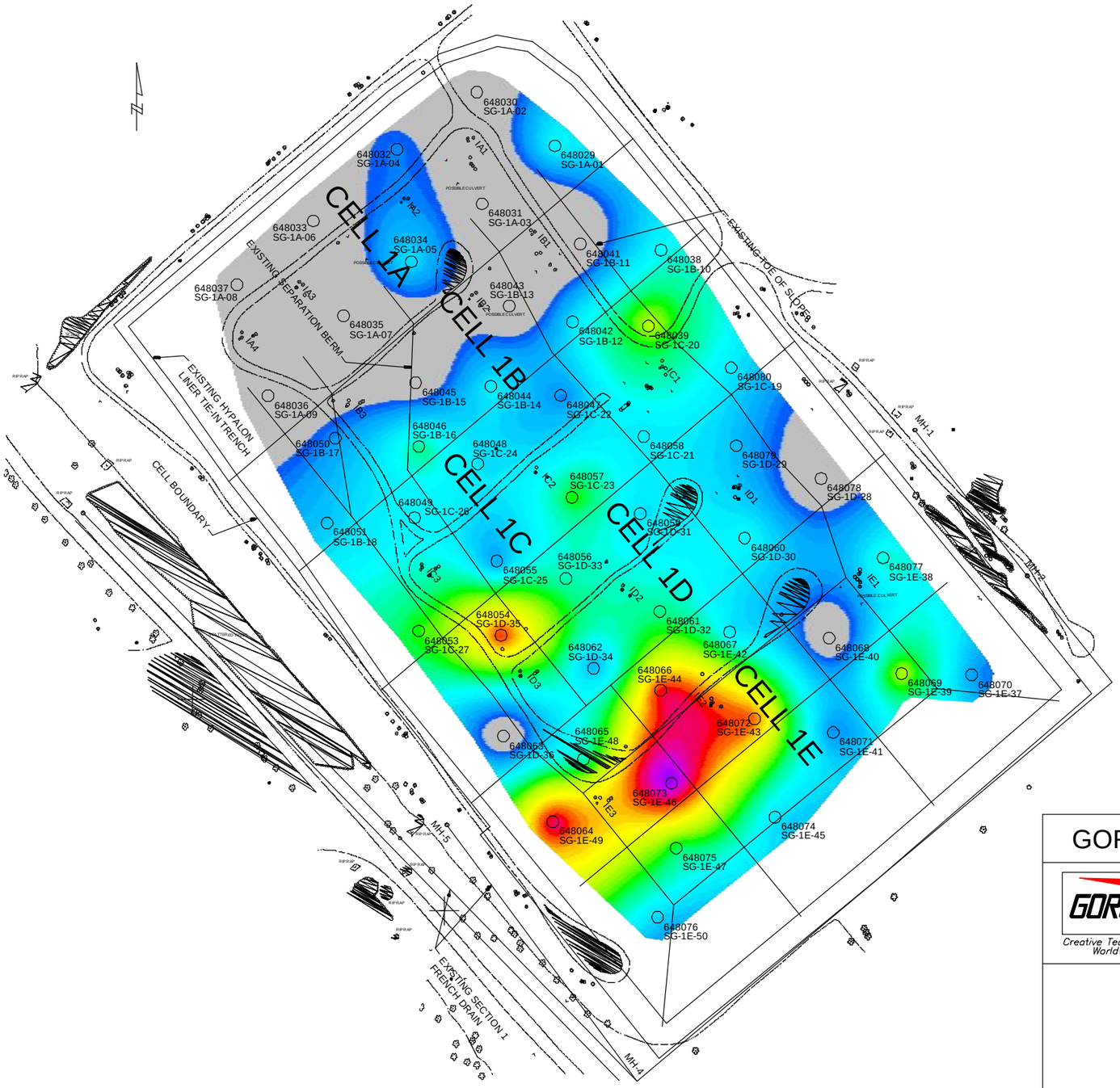
IN NUMERICAL ORDER






Scale 1:2040

100 0 100 200 300 400

(feet)



# GORE ™ Surveys for Environmental Site Assessment

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*Creative Technologies Worldwide*

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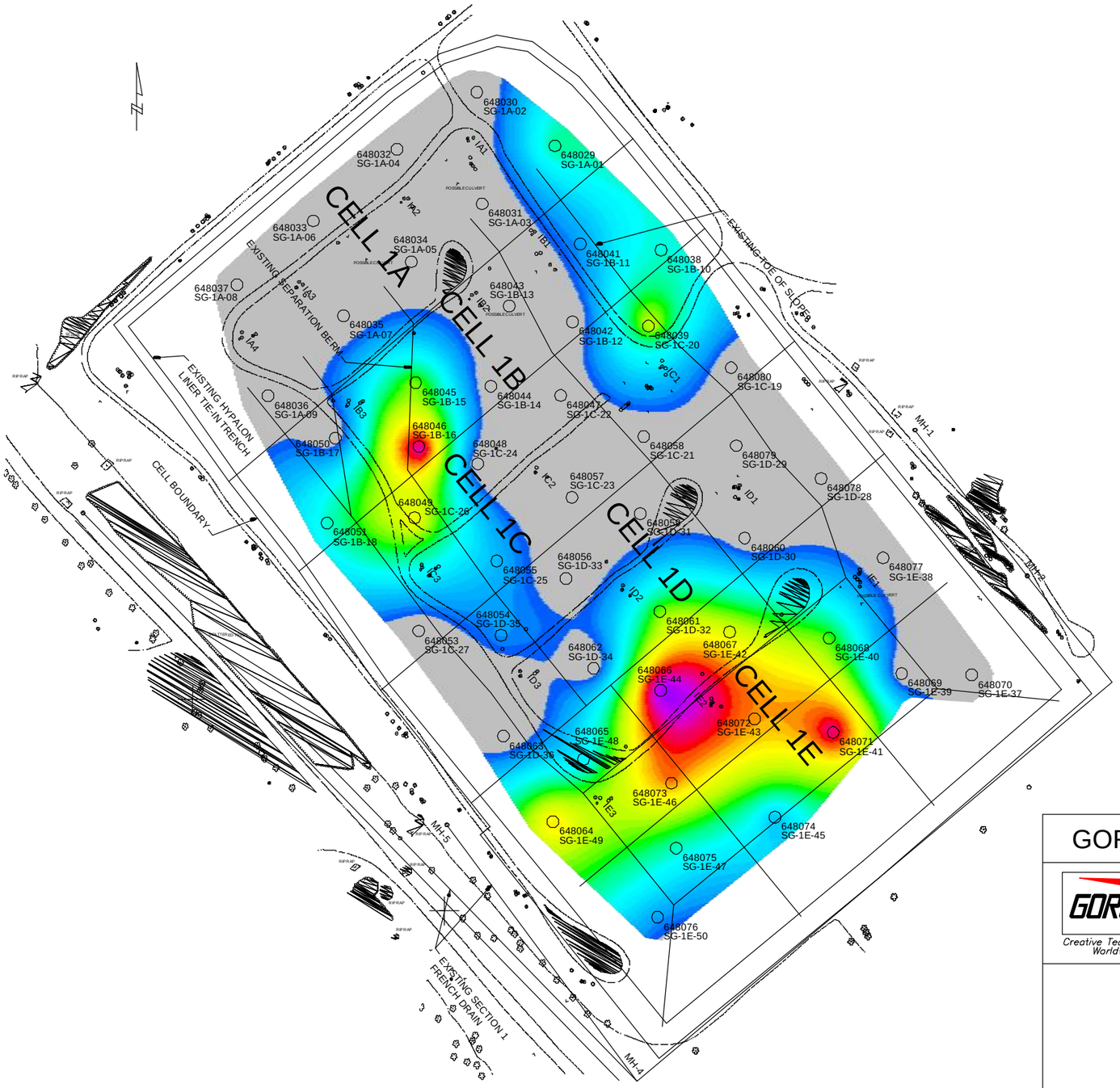
**100 CHESAPEAKE BOULEVARD**
**ELKTON, MD, USA 21921**
**USA**
**(410) 392-7600**

## AECOM, Greenville, SC
## PSCT Section I Cover, Pinewood, SC
## BTEX

| | | | |
|---|---|---|---|
| **DATE DRAWN: 29 Nov 2010** | **DRAWN BY: JW** | **ORIG. CAD: PSCT...DWG** | **SITE CODE: FRM** |
| **REV. DATE:** | **REV. #:** | **PROJECT NUMBER: 20784505** | |

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0.263
0.182
0.126
0.087
0.060
0.042
0.029
0.020

**PCE**
[µg]

Scale 1:2040

100 0 100 200 300 400

(feet)

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USA
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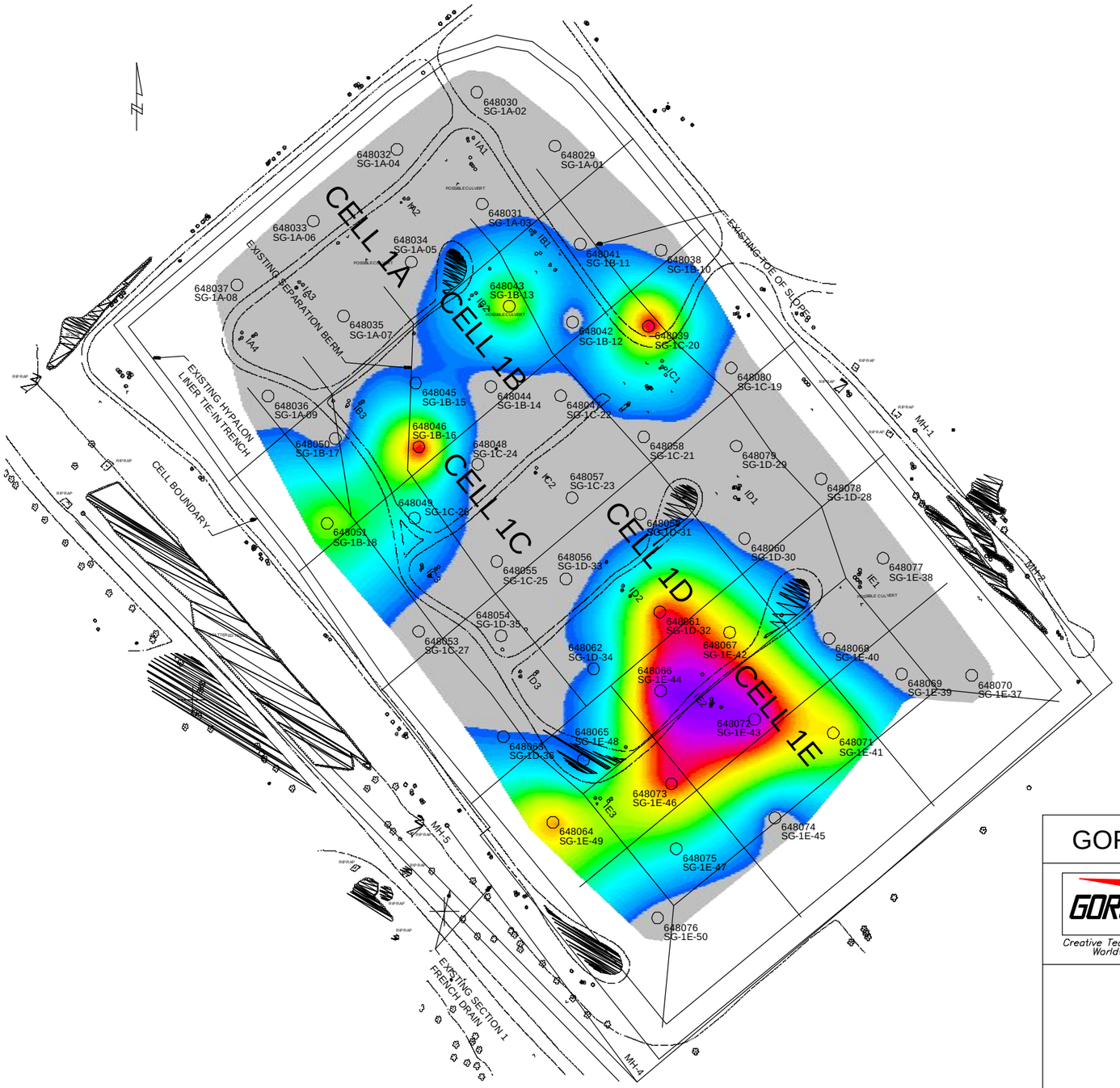
GORE Creative Technologies Worldwide

## AECOM, Greenville, SC
## PSCT Section I Cover, Pinewood, SC
## Tetrachloroethene

| | | | |
|---|---|---|---|
| DATE DRAWN: 29 Nov 2010 | DRAWN BY: JW | ORIG. CAD: PSCT...DWG | SITE CODE: FRM |
| REV. DATE: | REV. #: | PROJECT NUMBER: 20784505 | |

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0.176
0.122
0.085
0.059
0.041
0.029
0.020

**TCE**
[µg]

Scale 1:2040

100 0 100 200 300 400

(feet)



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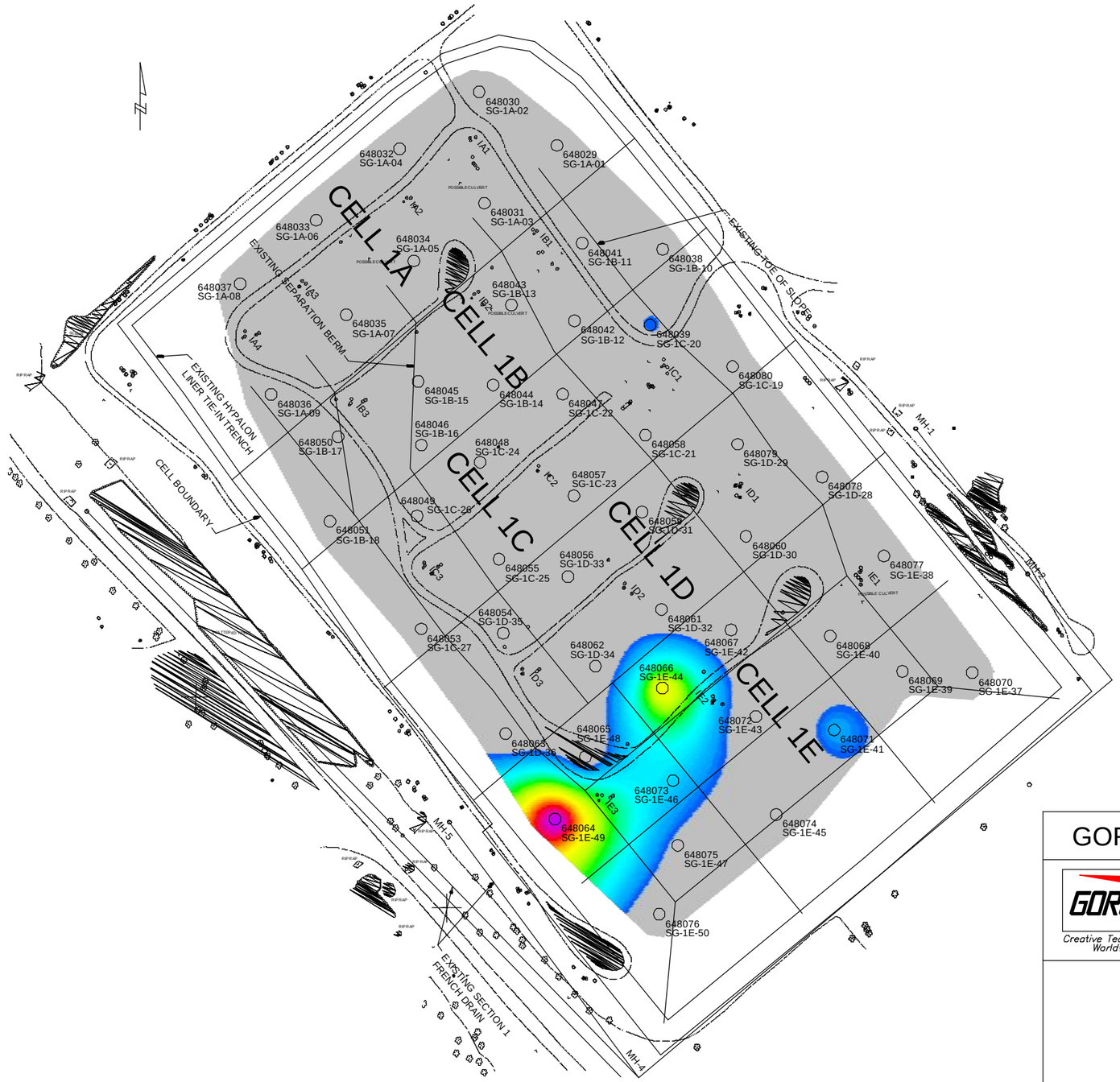
USA
(410) 392-7600

## AECOM, Greenville, SC
## PSCT Section I Cover, Pinewood, SC
## Trichloroethene

| | | | |
|---|---|---|---|
| **DATE DRAWN: 29 Nov 2010** | **DRAWN BY: JW** | **ORIG. CAD: PSCT...DWG** | **SITE CODE: FRM** |
| **REV. DATE:** | **REV. #:** | **PROJECT NUMBER: 20784505** | |




Scale 1:2040

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(feet)

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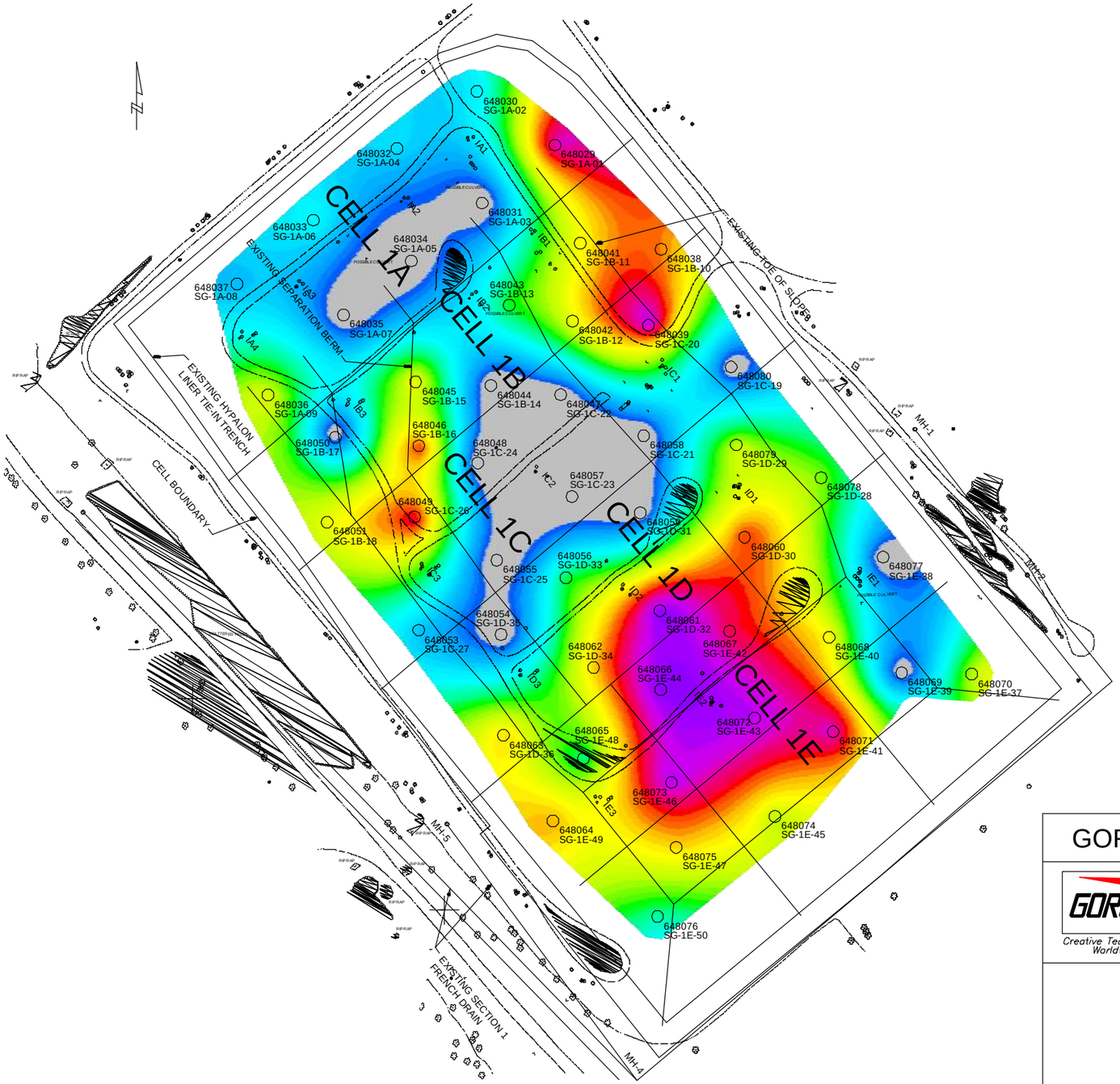
ELKTON, MD, USA 21921
USA
(410) 392-7600

## AECOM, Greenville, SC
## PSCT Section I Cover, Pinewood, SC
## 1,1,1-Trichloroethane

| | | | |
|---|---|---|---|
| DATE DRAWN: 29 Nov 2010 | DRAWN BY: JW | ORIG. CAD: PSCT...DWG | SITE CODE: FRM |
| REV. DATE: | REV. #: | PROJECT NUMBER: 20784505 | |

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0.062
0.042
0.029
0.020

**1,1-DCA**
[µg]

Scale 1:2040

100 0 100 200 300 400
(feet)



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USA
(410) 392-7600

## AECOM, Greenville, SC
## PSCT Section I Cover, Pinewood, SC
## 1,1-Dichloroethane

| | | | |
|---|---|---|---|
| DATE DRAWN: 29 Nov 2010 | DRAWN BY: JW | ORIG. CAD: PSCT...DWG | SITE CODE: FRM |
| REV. DATE: | REV. #: | PROJECT NUMBER: 20784505 | |

**W. L. Gore & Associates, Inc.**
100 Chesapeake Blvd. • P.O. Box 10
Elkton, MD 21922-0010
Phone: 410.392.7600 • 800.432.7998
Fax: 410.506.4780

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**Sales Offices:**
Europe: +49.89.4612.2198
San Francisco: 415.648.0438

Email: environmental@wlgore.com

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*Creative Technologies Worldwide*

LIT 139.0 08/14/07

# Appendix 2.6-1

GEL Laboratories, LLC Analytical Report

GEL Laboratories LLC
a member of The GEL Group INC

PO Box 30712 Charleston, SC 29417
2040 Savage Road Charleston, SC 29407
P 843.556.8171 F 843.766.1178

www.gel.com

November 29, 2010

Mr. David M. Welch
AECOM Water
10 Patewood Drive
Building VI, Suite 500
Greenville, South Carolina 29615

Re: Pinewood
Work Order: 266958

Dear Mr. Welch:

GEL Laboratories, LLC (GEL) appreciates the opportunity to provide the enclosed analytical results for the sample(s) we received on November 12, 2010. This original data report has been prepared and reviewed in accordance with GEL's standard operating procedures.

Our policy is to provide high quality, personalized analytical services to enable you to meet your analytical needs on time every time. We trust that you will find everything in order and to your satisfaction. If you have any questions, please do not hesitate to call me at (843) 556-8171, ext. 4300.

Sincerely,

Client Services Team
Project Manager

Enclosures

**GEL LABORATORIES LLC**
2040 Savage Road Charleston SC 29407 – (843) 556–8171 – www.gel.com

# Certificate of Analysis Report
for

AECM001 AECOM (P.O. 4561ACM)

Client SDG: 266958 GEL Work Order: 266958

**The Qualifiers in this report are defined as follows:**

* A quality control analyte recovery is outside of specified acceptance criteria

** Analyte is a surrogate compound

B For General Chemistry and Organic analysis the target analyte was detected in the associated blank.

E Organics––Concentration of the target analyte exceeds the instrument calibration range

J Value is estimated

U Analyte was analyzed for, but not detected above the MDL, MDA, or LOD.

Where the analytical method has been performed under NELAP certification, the analysis has met all of the requirements of the NELAC standard unless qualified on the Certificate of Analysis.

The designation ND, if present, appears in the result column when the analyte concentration is not detected above the detection limit.

This data report has been prepared and reviewed in accordance with GEL Laboratories LLC standard operating procedures. Please direct any questions to your Project Manager, Client Services Team.

Reviewed by 

# Certificate of Analysis

| | | | |
|---|---|---|---|
| Company : | AECOM Water | Report Date: November 29, 2010 | |
| Address : | 10 Patewood Drive<br>Building VI, Suite 500<br>Greenville, South Carolina 29615 | | |
| Contact: | Mr. David M. Welch | | |
| Project: | Pinewood | | |

| | | | |
|---|---|---|---|
| Client Sample ID: | SILC-1 | Project: | AECM00101 |
| Sample ID: | 266958001 | Client ID: | AECM001 |
| Matrix: | Ground Water | | |
| Collect Date: | 10-NOV-10 16:19 | | |
| Receive Date: | 12-NOV-10 | | |
| Collector: | Client | | |

| Parameter | Qualifier | Result | DL | RL | Units | DF | AnalystDate | Time | Batch | Method |
|---|---|---|---|---|---|---|---|---|---|---|
| **Volatile Organics** | | | | | | | | | | |
| *EPA 624 TTO Liquid "As Received"* | | | | | | | | | | |
| 1,1,1-Trichloroethane | U | ND | 0.325 | 1.00 | ug/L | 1 | RXD1 11/16/10 | 0003 | 1048933 | 1 |
| 1,1,2,2-Tetrachloroethane | U | ND | 0.250 | 1.00 | ug/L | 1 | | | | |
| 1,1,2-Trichloroethane | U | ND | 0.250 | 1.00 | ug/L | 1 | | | | |
| 1,1-Dichloroethane | | 14.7 | 0.300 | 1.00 | ug/L | 1 | | | | |
| 1,1-Dichloroethylene | U | ND | 0.300 | 1.00 | ug/L | 1 | | | | |
| 1,2-Dichloroethane | U | ND | 0.250 | 1.00 | ug/L | 1 | | | | |
| 1,2-Dichloropropane | U | ND | 0.250 | 1.00 | ug/L | 1 | | | | |
| 2-Chloroethylvinyl ether | U | ND | 1.50 | 5.00 | ug/L | 1 | | | | |
| Acrolein | U | ND | 1.25 | 5.00 | ug/L | 1 | | | | |
| Acrylonitrile | U | ND | 1.00 | 5.00 | ug/L | 1 | | | | |
| Benzene | | 1.19 | 0.300 | 1.00 | ug/L | 1 | | | | |
| Bromodichloromethane | U | ND | 0.250 | 1.00 | ug/L | 1 | | | | |
| Bromoform | U | ND | 0.250 | 1.00 | ug/L | 1 | | | | |
| Bromomethane | U | ND | 0.300 | 1.00 | ug/L | 1 | | | | |
| Carbon tetrachloride | U | ND | 0.300 | 1.00 | ug/L | 1 | | | | |
| Chlorobenzene | U | ND | 0.250 | 1.00 | ug/L | 1 | | | | |
| Chloroethane | U | ND | 0.300 | 1.00 | ug/L | 1 | | | | |
| Chloroform | U | ND | 0.250 | 1.00 | ug/L | 1 | | | | |
| Chloromethane | U | ND | 0.300 | 1.00 | ug/L | 1 | | | | |
| Dibromochloromethane | U | ND | 0.300 | 1.00 | ug/L | 1 | | | | |
| Ethylbenzene | U | ND | 0.250 | 1.00 | ug/L | 1 | | | | |
| Methylene chloride | U | ND | 2.00 | 2.00 | ug/L | 1 | | | | |
| Tetrachloroethylene | U | ND | 0.300 | 1.00 | ug/L | 1 | | | | |
| Toluene | BJ | 0.260 | 0.250 | 1.00 | ug/L | 1 | | | | |
| Trichloroethylene | U | ND | 0.250 | 1.00 | ug/L | 1 | | | | |
| Vinyl chloride | | 31.8 | 0.500 | 1.00 | ug/L | 1 | | | | |
| cis-1,3-Dichloropropylene | U | ND | 0.250 | 1.00 | ug/L | 1 | | | | |
| trans-1,2-Dichloroethylene | | 2.20 | 0.300 | 1.00 | ug/L | 1 | | | | |
| trans-1,3-Dichloropropylene | U | ND | 0.250 | 1.00 | ug/L | 1 | | | | |

**The following Analytical Methods were performed**

| Method | Description | Analyst Comments |
|---|---|---|
| 1 | EPA 624 SC_NPDES | |

| Surrogate/Tracer recovery | Test | Result | Nominal | Recovery% | Acceptable Limits |
|---|---|---|---|---|---|
| 1,2-Dichloroethane-d4 | EPA 624 TTO Liquid "As Received" | 53.4 ug/L | 50.0 | 107 | (71%-130%) |

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# Certificate of Analysis

| | | |
|---|---|---|
| Company : | AECOM Water | Report Date: November 29, 2010 |
| Address : | 10 Patewood Drive<br>Building VI, Suite 500<br>Greenville, South Carolina 29615 | |
| Contact: | Mr. David M. Welch | |
| Project: | Pinewood | |

| | | | |
|---|---|---|---|
| Client Sample ID: | SILC-1 | Project: | AECM00101 |
| Sample ID: | 266958001 | Client ID: | AECM001 |

| Parameter | Qualifier | Result | DL | RL | Units | DF | Analyst | Date | Time | Batch | Method |
|---|---|---|---|---|---|---|---|---|---|---|---|
| Bromofluorobenzene | | EPA 624 TTO Liquid "As Received" | | 48.6 | ug/L | 50.0 | 97.2 | | (80%-120%) | | |
| Toluene-d8 | | EPA 624 TTO Liquid "As Received" | | 49.3 | ug/L | 50.0 | 98.6 | | (80%-120%) | | |

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| Company : | AECOM Water | Report Date: November 29, 2010 |
| Address : | 10 Patewood Drive<br>Building VI, Suite 500<br>Greenville, South Carolina 29615 | |
| Contact: | Mr. David M. Welch | |
| Project: | Pinewood | |

| | | | |
|---|---|---|---|
| Client Sample ID: | SILC-2 | Project: | AECM00101 |
| Sample ID: | 266958002 | Client ID: | AECM001 |
| Matrix: | Ground Water | | |
| Collect Date: | 10-NOV-10 15:50 | | |
| Receive Date: | 12-NOV-10 | | |
| Collector: | Client | | |

| Parameter | Qualifier | Result | DL | RL | Units | DF | AnalystDate | Time | Batch | Method |
|---|---|---|---|---|---|---|---|---|---|---|
| **Volatile Organics** | | | | | | | | | | |
| *EPA 624 TTO Liquid "As Received"* | | | | | | | | | | |
| 1,1,1-Trichloroethane | U | ND | 0.325 | 1.00 | ug/L | 1 | RXD1 11/16/10 | 0057 | 1048933 | 1 |
| 1,1,2,2-Tetrachloroethane | J | 0.630 | 0.250 | 1.00 | ug/L | 1 | | | | |
| 1,1-Dichloroethylene | | 7.35 | 0.300 | 1.00 | ug/L | 1 | | | | |
| 1,2-Dichloroethane | | 11.1 | 0.250 | 1.00 | ug/L | 1 | | | | |
| 1,2-Dichloropropane | U | ND | 0.250 | 1.00 | ug/L | 1 | | | | |
| 2-Chloroethylvinyl ether | U | ND | 1.50 | 5.00 | ug/L | 1 | | | | |
| Acrolein | U | ND | 1.25 | 5.00 | ug/L | 1 | | | | |
| Acrylonitrile | U | ND | 1.00 | 5.00 | ug/L | 1 | | | | |
| Benzene | J | 0.320 | 0.300 | 1.00 | ug/L | 1 | | | | |
| Bromodichloromethane | U | ND | 0.250 | 1.00 | ug/L | 1 | | | | |
| Bromoform | U | ND | 0.250 | 1.00 | ug/L | 1 | | | | |
| Bromomethane | U | ND | 0.300 | 1.00 | ug/L | 1 | | | | |
| Carbon tetrachloride | U | ND | 0.300 | 1.00 | ug/L | 1 | | | | |
| Chlorobenzene | U | ND | 0.250 | 1.00 | ug/L | 1 | | | | |
| Chloroethane | U | ND | 0.300 | 1.00 | ug/L | 1 | | | | |
| Chloroform | J | 0.260 | 0.250 | 1.00 | ug/L | 1 | | | | |
| Chloromethane | U | ND | 0.300 | 1.00 | ug/L | 1 | | | | |
| Dibromochloromethane | U | ND | 0.300 | 1.00 | ug/L | 1 | | | | |
| Ethylbenzene | U | ND | 0.250 | 1.00 | ug/L | 1 | | | | |
| Methylene chloride | U | ND | 2.00 | 2.00 | ug/L | 1 | | | | |
| Tetrachloroethylene | | 1.39 | 0.300 | 1.00 | ug/L | 1 | | | | |
| Toluene | U | ND | 0.250 | 1.00 | ug/L | 1 | | | | |
| Trichloroethylene | | 7.05 | 0.250 | 1.00 | ug/L | 1 | | | | |
| Vinyl chloride | | 5.13 | 0.500 | 1.00 | ug/L | 1 | | | | |
| cis-1,3-Dichloropropylene | U | ND | 0.250 | 1.00 | ug/L | 1 | | | | |
| trans-1,2-Dichloroethylene | U | ND | 0.300 | 1.00 | ug/L | 1 | | | | |
| trans-1,3-Dichloropropylene | U | ND | 0.250 | 1.00 | ug/L | 1 | | | | |
| 1,1,2-Trichloroethane | | 307 | 1.25 | 5.00 | ug/L | 5 | RXD1 11/16/10 | 1332 | 1048933 | 2 |
| 1,1-Dichloroethane | | 305 | 1.50 | 5.00 | ug/L | 5 | | | | |

**The following Analytical Methods were performed**

| Method | Description | Analyst Comments |
|---|---|---|
| 1 | EPA 624 SC_NPDES | |
| 2 | EPA 624 SC_NPDES | |

| Surrogate/Tracer recovery | Test | Result | Nominal | Recovery% | Acceptable Limits |
|---|---|---|---|---|---|

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# Certificate of Analysis

Company : AECOM Water
Address : 10 Patewood Drive
Building VI, Suite 500
Greenville, South Carolina 29615
Contact: Mr. David M. Welch
Project: Pinewood

Report Date: November 29, 2010

Client Sample ID: SILC-2
Sample ID: 266958002

Project: AECM00101
Client ID: AECM001

| Parameter | Qualifier | Result | DL | RL | Units | DF | Analyst | Date | Time | Batch | Method |
|---|---|---|---|---|---|---|---|---|---|---|---|

| Surrogate/Tracer recovery | Test | Result | Nominal | Recovery% | Acceptable Limits |
|---|---|---|---|---|---|
| 1,2-Dichloroethane-d4 | EPA 624 TTO Liquid "As Received" | 52.6 ug/L | 50.0 | 105 | (71%-130%) |
| Bromofluorobenzene | EPA 624 TTO Liquid "As Received" | 49.1 ug/L | 50.0 | 98.1 | (80%-120%) |
| Toluene-d8 | EPA 624 TTO Liquid "As Received" | 48.6 ug/L | 50.0 | 97.2 | (80%-120%) |

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# Certificate of Analysis

| | | |
|---|---|---|
| Company : | AECOM Water | Report Date: November 29, 2010 |
| Address : | 10 Patewood Drive<br>Building VI, Suite 500<br>Greenville, South Carolina 29615 | |
| Contact: | Mr. David M. Welch | |
| Project: | Pinewood | |

| | | | |
|---|---|---|---|
| Client Sample ID: | SILC-4 | Project: | AECM00101 |
| Sample ID: | 266958003 | Client ID: | AECM001 |
| Matrix: | Ground Water | | |
| Collect Date: | 10-NOV-10 16:00 | | |
| Receive Date: | 12-NOV-10 | | |
| Collector: | Client | | |

| Parameter | Qualifier | Result | DL | RL | Units | DF | AnalystDate | Time | Batch | Method |
|---|---|---|---|---|---|---|---|---|---|---|
| **Volatile Organics** | | | | | | | | | | |
| *EPA 624 TTO Liquid "As Received"* | | | | | | | | | | |
| 1,1,1-Trichloroethane | U | ND | 0.325 | 1.00 | ug/L | 1 | RXD1 11/16/10 | 1304 | 1048933 | 1 |
| 1,1,2,2-Tetrachloroethane | U | ND | 0.250 | 1.00 | ug/L | 1 | | | | |
| 1,1,2-Trichloroethane | U | ND | 0.250 | 1.00 | ug/L | 1 | | | | |
| 1,1-Dichloroethane | | 12.3 | 0.300 | 1.00 | ug/L | 1 | | | | |
| 1,1-Dichloroethylene | J | 0.660 | 0.300 | 1.00 | ug/L | 1 | | | | |
| 1,2-Dichloroethane | U | ND | 0.250 | 1.00 | ug/L | 1 | | | | |
| 1,2-Dichloropropane | U | ND | 0.250 | 1.00 | ug/L | 1 | | | | |
| 2-Chloroethylvinyl ether | U | ND | 1.50 | 5.00 | ug/L | 1 | | | | |
| Acrolein | U | ND | 1.25 | 5.00 | ug/L | 1 | | | | |
| Acrylonitrile | U | ND | 1.00 | 5.00 | ug/L | 1 | | | | |
| Benzene | U | ND | 0.300 | 1.00 | ug/L | 1 | | | | |
| Bromodichloromethane | U | ND | 0.250 | 1.00 | ug/L | 1 | | | | |
| Bromoform | U | ND | 0.250 | 1.00 | ug/L | 1 | | | | |
| Bromomethane | U | ND | 0.300 | 1.00 | ug/L | 1 | | | | |
| Carbon tetrachloride | U | ND | 0.300 | 1.00 | ug/L | 1 | | | | |
| Chlorobenzene | U | ND | 0.250 | 1.00 | ug/L | 1 | | | | |
| Chloroethane | | 2.08 | 0.300 | 1.00 | ug/L | 1 | | | | |
| Chloroform | U | ND | 0.250 | 1.00 | ug/L | 1 | | | | |
| Chloromethane | U | ND | 0.300 | 1.00 | ug/L | 1 | | | | |
| Dibromochloromethane | U | ND | 0.300 | 1.00 | ug/L | 1 | | | | |
| Ethylbenzene | U | ND | 0.250 | 1.00 | ug/L | 1 | | | | |
| Methylene chloride | U | ND | 2.00 | 2.00 | ug/L | 1 | | | | |
| Tetrachloroethylene | U | ND | 0.300 | 1.00 | ug/L | 1 | | | | |
| Toluene | U | ND | 0.250 | 1.00 | ug/L | 1 | | | | |
| Trichloroethylene | U | ND | 0.250 | 1.00 | ug/L | 1 | | | | |
| Vinyl chloride | | 6.29 | 0.500 | 1.00 | ug/L | 1 | | | | |
| cis-1,3-Dichloropropylene | U | ND | 0.250 | 1.00 | ug/L | 1 | | | | |
| trans-1,2-Dichloroethylene | U | ND | 0.300 | 1.00 | ug/L | 1 | | | | |
| trans-1,3-Dichloropropylene | U | ND | 0.250 | 1.00 | ug/L | 1 | | | | |

**The following Analytical Methods were performed**

| Method | Description | Analyst Comments |
|---|---|---|
| 1 | EPA 624 SC_NPDES | |

| Surrogate/Tracer recovery | Test | Result | Nominal | Recovery% | Acceptable Limits |
|---|---|---|---|---|---|
| 1,2-Dichloroethane-d4 | EPA 624 TTO Liquid "As Received" | 52.8 ug/L | 50.0 | 106 | (71%-130%) |

# Certificate of Analysis

| | | |
|---|---|---|
| Company : | AECOM Water | Report Date: November 29, 2010 |
| Address : | 10 Patewood Drive<br>Building VI, Suite 500<br>Greenville, South Carolina 29615 | |
| Contact: | Mr. David M. Welch | |
| Project: | Pinewood | |

| | | | |
|---|---|---|---|
| Client Sample ID: | SILC-4 | Project: | AECM00101 |
| Sample ID: | 266958003 | Client ID: | AECM001 |

| Parameter | Qualifier | Result | DL | RL | Units | DF | Analyst | Date | Time | Batch | Method |
|---|---|---|---|---|---|---|---|---|---|---|---|
| Bromofluorobenzene | | EPA 624 TTO Liquid "As Received" | | 48.3 | ug/L | 50.0 | 96.5 | | (80%-120%) | | |
| Toluene-d8 | | EPA 624 TTO Liquid "As Received" | | 48.7 | ug/L | 50.0 | 97.4 | | (80%-120%) | | |

# Certificate of Analysis

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|---|---|---|
| Company : | AECOM Water | Report Date: November 29, 2010 |
| Address : | 10 Patewood Drive<br>Building VI, Suite 500<br>Greenville, South Carolina 29615 | |
| Contact: | Mr. David M. Welch | |
| Project: | Pinewood | |

| | | | |
|---|---|---|---|
| Client Sample ID: | SILC-5 | Project: | AECM00101 |
| Sample ID: | 266958004 | Client ID: | AECM001 |
| Matrix: | Ground Water | | |
| Collect Date: | 10-NOV-10 15:17 | | |
| Receive Date: | 12-NOV-10 | | |
| Collector: | Client | | |

| Parameter | Qualifier | Result | DL | RL | Units | DF | AnalystDate | Time | Batch | Method |
|---|---|---|---|---|---|---|---|---|---|---|
| **Volatile Organics** | | | | | | | | | | |
| *EPA 624 TTO Liquid "As Received"* | | | | | | | | | | |
| 1,1,1-Trichloroethane | U | ND | 0.325 | 1.00 | ug/L | 1 | RXD1 11/16/10 | 0153 | 1048933 | 1 |
| 1,1,2,2-Tetrachloroethane | U | ND | 0.250 | 1.00 | ug/L | 1 | | | | |
| 1,1,2-Trichloroethane | U | ND | 0.250 | 1.00 | ug/L | 1 | | | | |
| 1,1-Dichloroethylene | | 1.35 | 0.300 | 1.00 | ug/L | 1 | | | | |
| 1,2-Dichloroethane | | 6.30 | 0.250 | 1.00 | ug/L | 1 | | | | |
| 1,2-Dichloropropane | J | 0.410 | 0.250 | 1.00 | ug/L | 1 | | | | |
| 2-Chloroethylvinyl ether | U | ND | 1.50 | 5.00 | ug/L | 1 | | | | |
| Acrolein | U | ND | 1.25 | 5.00 | ug/L | 1 | | | | |
| Acrylonitrile | U | ND | 1.00 | 5.00 | ug/L | 1 | | | | |
| Benzene | U | ND | 0.300 | 1.00 | ug/L | 1 | | | | |
| Bromodichloromethane | U | ND | 0.250 | 1.00 | ug/L | 1 | | | | |
| Bromoform | U | ND | 0.250 | 1.00 | ug/L | 1 | | | | |
| Bromomethane | U | ND | 0.300 | 1.00 | ug/L | 1 | | | | |
| Carbon tetrachloride | U | ND | 0.300 | 1.00 | ug/L | 1 | | | | |
| Chlorobenzene | U | ND | 0.250 | 1.00 | ug/L | 1 | | | | |
| Chloroethane | U | ND | 0.300 | 1.00 | ug/L | 1 | | | | |
| Chloroform | U | ND | 0.250 | 1.00 | ug/L | 1 | | | | |
| Chloromethane | U | ND | 0.300 | 1.00 | ug/L | 1 | | | | |
| Dibromochloromethane | U | ND | 0.300 | 1.00 | ug/L | 1 | | | | |
| Ethylbenzene | U | ND | 0.250 | 1.00 | ug/L | 1 | | | | |
| Methylene chloride | U | ND | 2.00 | 2.00 | ug/L | 1 | | | | |
| Tetrachloroethylene | | 1.11 | 0.300 | 1.00 | ug/L | 1 | | | | |
| Toluene | U | ND | 0.250 | 1.00 | ug/L | 1 | | | | |
| Trichloroethylene | | 2.42 | 0.250 | 1.00 | ug/L | 1 | | | | |
| Vinyl chloride | U | ND | 0.500 | 1.00 | ug/L | 1 | | | | |
| cis-1,3-Dichloropropylene | U | ND | 0.250 | 1.00 | ug/L | 1 | | | | |
| trans-1,2-Dichloroethylene | J | 0.750 | 0.300 | 1.00 | ug/L | 1 | | | | |
| trans-1,3-Dichloropropylene | U | ND | 0.250 | 1.00 | ug/L | 1 | | | | |
| 1,1-Dichloroethane | | 286 | 1.50 | 5.00 | ug/L | 5 | RXD1 11/16/10 | 1400 | 1048933 | 2 |

**The following Analytical Methods were performed**

| Method | Description | Analyst Comments |
|---|---|---|
| 1 | EPA 624 SC_NPDES | |
| 2 | EPA 624 SC_NPDES | |

| Surrogate/Tracer recovery | Test | Result | Nominal | Recovery% | Acceptable Limits |
|---|---|---|---|---|---|

# Certificate of Analysis

Company : AECOM Water
Address : 10 Patewood Drive
Building VI, Suite 500
Greenville, South Carolina 29615
Contact: Mr. David M. Welch
Project: Pinewood

Report Date: November 29, 2010

Client Sample ID: SILC-5
Sample ID: 266958004

Project: AECM00101
Client ID: AECM001

| Parameter | Qualifier | Result | DL | RL | Units | DF | Analyst | Date | Time | Batch | Method |
|---|---|---|---|---|---|---|---|---|---|---|---|

| Surrogate/Tracer recovery | Test | Result | Nominal | Recovery% | Acceptable Limits |
|---|---|---|---|---|---|
| 1,2-Dichloroethane-d4 | EPA 624 TTO Liquid "As Received" | 53.2 ug/L | 50.0 | 106 | (71%-130%) |
| Bromofluorobenzene | EPA 624 TTO Liquid "As Received" | 48.6 ug/L | 50.0 | 97.1 | (80%-120%) |
| Toluene-d8 | EPA 624 TTO Liquid "As Received" | 49.5 ug/L | 50.0 | 99.1 | (80%-120%) |

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|---|---|---|
| Company : | AECOM Water | Report Date: November 29, 2010 |
| Address : | 10 Patewood Drive<br>Building VI, Suite 500<br>Greenville, South Carolina 29615 | |
| Contact: | Mr. David M. Welch | |
| Project: | Pinewood | |

| | | | |
|---|---|---|---|
| Client Sample ID: | PBFD-1 | Project: | AECM00101 |
| Sample ID: | 266958005 | Client ID: | AECM001 |
| Matrix: | Ground Water | | |
| Collect Date: | 10-NOV-10 17:09 | | |
| Receive Date: | 12-NOV-10 | | |
| Collector: | Client | | |

| Parameter | Qualifier | Result | DL | RL | Units | DF | AnalystDate | Time | Batch | Method |
|---|---|---|---|---|---|---|---|---|---|---|
| **Volatile Organics** | | | | | | | | | | |
| *EPA 624 TTO Liquid "As Received"* | | | | | | | | | | |
| 1,1,1-Trichloroethane | U | ND | 0.325 | 1.00 | ug/L | 1 | RXD1 11/16/10 | 0220 | 1048933 | 1 |
| 1,1,2,2-Tetrachloroethane | U | ND | 0.250 | 1.00 | ug/L | 1 | | | | |
| 1,1,2-Trichloroethane | U | ND | 0.250 | 1.00 | ug/L | 1 | | | | |
| 1,1-Dichloroethane | U | ND | 0.300 | 1.00 | ug/L | 1 | | | | |
| 1,1-Dichloroethylene | U | ND | 0.300 | 1.00 | ug/L | 1 | | | | |
| 1,2-Dichloroethane | U | ND | 0.250 | 1.00 | ug/L | 1 | | | | |
| 1,2-Dichloropropane | U | ND | 0.250 | 1.00 | ug/L | 1 | | | | |
| 2-Chloroethylvinyl ether | U | ND | 1.50 | 5.00 | ug/L | 1 | | | | |
| Acrolein | U | ND | 1.25 | 5.00 | ug/L | 1 | | | | |
| Acrylonitrile | U | ND | 1.00 | 5.00 | ug/L | 1 | | | | |
| Benzene | U | ND | 0.300 | 1.00 | ug/L | 1 | | | | |
| Bromodichloromethane | U | ND | 0.250 | 1.00 | ug/L | 1 | | | | |
| Bromoform | U | ND | 0.250 | 1.00 | ug/L | 1 | | | | |
| Bromomethane | U | ND | 0.300 | 1.00 | ug/L | 1 | | | | |
| Carbon tetrachloride | U | ND | 0.300 | 1.00 | ug/L | 1 | | | | |
| Chlorobenzene | U | ND | 0.250 | 1.00 | ug/L | 1 | | | | |
| Chloroethane | U | ND | 0.300 | 1.00 | ug/L | 1 | | | | |
| Chloroform | U | ND | 0.250 | 1.00 | ug/L | 1 | | | | |
| Chloromethane | U | ND | 0.300 | 1.00 | ug/L | 1 | | | | |
| Dibromochloromethane | U | ND | 0.300 | 1.00 | ug/L | 1 | | | | |
| Ethylbenzene | U | ND | 0.250 | 1.00 | ug/L | 1 | | | | |
| Methylene chloride | U | ND | 2.00 | 2.00 | ug/L | 1 | | | | |
| Tetrachloroethylene | U | ND | 0.300 | 1.00 | ug/L | 1 | | | | |
| Toluene | U | ND | 0.250 | 1.00 | ug/L | 1 | | | | |
| Trichloroethylene | U | ND | 0.250 | 1.00 | ug/L | 1 | | | | |
| Vinyl chloride | U | ND | 0.500 | 1.00 | ug/L | 1 | | | | |
| cis-1,3-Dichloropropylene | U | ND | 0.250 | 1.00 | ug/L | 1 | | | | |
| trans-1,2-Dichloroethylene | U | ND | 0.300 | 1.00 | ug/L | 1 | | | | |
| trans-1,3-Dichloropropylene | U | ND | 0.250 | 1.00 | ug/L | 1 | | | | |

**The following Analytical Methods were performed**

| Method | Description | Analyst Comments |
|---|---|---|
| 1 | EPA 624 SC_NPDES | |

| Surrogate/Tracer recovery | Test | Result | Nominal | Recovery% | Acceptable Limits |
|---|---|---|---|---|---|
| 1,2-Dichloroethane-d4 | EPA 624 TTO Liquid "As Received" | 51.6 ug/L | 50.0 | 103 | (71%-130%) |

# Certificate of Analysis

Company : AECOM Water
Address : 10 Patewood Drive
Building VI, Suite 500
Greenville, South Carolina 29615
Contact: Mr. David M. Welch
Project: Pinewood

Report Date: November 29, 2010

Client Sample ID: PBFD-1
Sample ID: 266958005

Project: AECM00101
Client ID: AECM001

| Parameter | Qualifier | Result | DL | RL | Units | DF | Analyst Date | Time | Batch | Method |
|---|---|---|---|---|---|---|---|---|---|---|
| Bromofluorobenzene | | EPA 624 TTO Liquid "As Received" | | 48.4 | ug/L | 50.0 | 96.7 | (80%-120%) | | |
| Toluene-d8 | | EPA 624 TTO Liquid "As Received" | | 49.6 | ug/L | 50.0 | 99.1 | (80%-120%) | | |

# Certificate of Analysis

Company : AECOM Water
Address : 10 Patewood Drive
Building VI, Suite 500
Greenville, South Carolina 29615
Contact: Mr. David M. Welch
Project: Pinewood

Report Date: November 29, 2010

Client Sample ID: PAFD-1
Sample ID: 266958006
Matrix: Ground Water
Collect Date: 10-NOV-10 17:25
Receive Date: 12-NOV-10
Collector: Client

Project: AECM00101
Client ID: AECM001

| Parameter | Qualifier | Result | DL | RL | Units | DF | AnalystDate | Time | Batch | Method |
|---|---|---|---|---|---|---|---|---|---|---|
| **Volatile Organics** | | | | | | | | | | |
| *EPA 624 TTO Liquid "As Received"* | | | | | | | | | | |
| 1,1,1-Trichloroethane | U | ND | 0.325 | 1.00 | ug/L | 1 | RXD1 11/16/10 | 0248 | 1048933 | 1 |
| 1,1,2,2-Tetrachloroethane | U | ND | 0.250 | 1.00 | ug/L | 1 | | | | |
| 1,1,2-Trichloroethane | U | ND | 0.250 | 1.00 | ug/L | 1 | | | | |
| 1,1-Dichloroethane | U | ND | 0.300 | 1.00 | ug/L | 1 | | | | |
| 1,1-Dichloroethylene | U | ND | 0.300 | 1.00 | ug/L | 1 | | | | |
| 1,2-Dichloroethane | U | ND | 0.250 | 1.00 | ug/L | 1 | | | | |
| 1,2-Dichloropropane | U | ND | 0.250 | 1.00 | ug/L | 1 | | | | |
| 2-Chloroethylvinyl ether | U | ND | 1.50 | 5.00 | ug/L | 1 | | | | |
| Acrolein | U | ND | 1.25 | 5.00 | ug/L | 1 | | | | |
| Acrylonitrile | U | ND | 1.00 | 5.00 | ug/L | 1 | | | | |
| Benzene | U | ND | 0.300 | 1.00 | ug/L | 1 | | | | |
| Bromodichloromethane | U | ND | 0.250 | 1.00 | ug/L | 1 | | | | |
| Bromoform | U | ND | 0.250 | 1.00 | ug/L | 1 | | | | |
| Bromomethane | U | ND | 0.300 | 1.00 | ug/L | 1 | | | | |
| Carbon tetrachloride | U | ND | 0.300 | 1.00 | ug/L | 1 | | | | |
| Chlorobenzene | U | ND | 0.250 | 1.00 | ug/L | 1 | | | | |
| Chloroethane | U | ND | 0.300 | 1.00 | ug/L | 1 | | | | |
| Chloroform | U | ND | 0.250 | 1.00 | ug/L | 1 | | | | |
| Chloromethane | U | ND | 0.300 | 1.00 | ug/L | 1 | | | | |
| Dibromochloromethane | U | ND | 0.300 | 1.00 | ug/L | 1 | | | | |
| Ethylbenzene | U | ND | 0.250 | 1.00 | ug/L | 1 | | | | |
| Methylene chloride | U | ND | 2.00 | 2.00 | ug/L | 1 | | | | |
| Tetrachloroethylene | U | ND | 0.300 | 1.00 | ug/L | 1 | | | | |
| Toluene | U | ND | 0.250 | 1.00 | ug/L | 1 | | | | |
| Trichloroethylene | U | ND | 0.250 | 1.00 | ug/L | 1 | | | | |
| Vinyl chloride | U | ND | 0.500 | 1.00 | ug/L | 1 | | | | |
| cis-1,3-Dichloropropylene | U | ND | 0.250 | 1.00 | ug/L | 1 | | | | |
| trans-1,2-Dichloroethylene | U | ND | 0.300 | 1.00 | ug/L | 1 | | | | |
| trans-1,3-Dichloropropylene | U | ND | 0.250 | 1.00 | ug/L | 1 | | | | |

**The following Analytical Methods were performed**

| Method | Description | Analyst Comments |
|---|---|---|
| 1 | EPA 624 SC_NPDES | |

| Surrogate/Tracer recovery | Test | Result | Nominal | Recovery% | Acceptable Limits |
|---|---|---|---|---|---|
| 1,2-Dichloroethane-d4 | EPA 624 TTO Liquid "As Received" | 52.4 ug/L | 50.0 | 105 | (71%-130%) |

# Certificate of Analysis

Company : AECOM Water
Address : 10 Patewood Drive
Building VI, Suite 500
Greenville, South Carolina 29615
Contact: Mr. David M. Welch
Project: Pinewood

Report Date: November 29, 2010

Client Sample ID: PAFD-1
Sample ID: 266958006

Project: AECM00101
Client ID: AECM001

| Parameter | Qualifier | Result | DL | RL | Units | DF | Analyst Date | Time | Batch | Method |
|---|---|---|---|---|---|---|---|---|---|---|
| Bromofluorobenzene | | EPA 624 TTO Liquid "As Received" | | 47.9 | ug/L | 50.0 | 95.9 | (80%-120%) | | |
| Toluene-d8 | | EPA 624 TTO Liquid "As Received" | | 49.7 | ug/L | 50.0 | 99.4 | (80%-120%) | | |

# Certificate of Analysis

| | | |
|---|---|---|
| Company : | AECOM Water | Report Date: November 29, 2010 |
| Address : | 10 Patewood Drive<br>Building VI, Suite 500<br>Greenville, South Carolina 29615 | |
| Contact: | Mr. David M. Welch | |
| Project: | Pinewood | |

| | | | |
|---|---|---|---|
| Client Sample ID: | PAFD-2 | Project: | AECM00101 |
| Sample ID: | 266958007 | Client ID: | AECM001 |
| Matrix: | Ground Water | | |
| Collect Date: | 10-NOV-10 14:15 | | |
| Receive Date: | 12-NOV-10 | | |
| Collector: | Client | | |

| Parameter | Qualifier | Result | DL | RL | Units | DF | AnalystDate | Time | Batch | Method |
|---|---|---|---|---|---|---|---|---|---|---|
| **Volatile Organics** | | | | | | | | | | |
| *EPA 624 TTO Liquid "As Received"* | | | | | | | | | | |
| 1,1,1-Trichloroethane | U | ND | 0.325 | 1.00 | ug/L | 1 | RXD1 11/16/10 | 0316 | 1048933 | 1 |
| 1,1,2,2-Tetrachloroethane | U | ND | 0.250 | 1.00 | ug/L | 1 | | | | |
| 1,1,2-Trichloroethane | U | ND | 0.250 | 1.00 | ug/L | 1 | | | | |
| 1,1-Dichloroethane | U | ND | 0.300 | 1.00 | ug/L | 1 | | | | |
| 1,1-Dichloroethylene | U | ND | 0.300 | 1.00 | ug/L | 1 | | | | |
| 1,2-Dichloroethane | U | ND | 0.250 | 1.00 | ug/L | 1 | | | | |
| 1,2-Dichloropropane | U | ND | 0.250 | 1.00 | ug/L | 1 | | | | |
| 2-Chloroethylvinyl ether | U | ND | 1.50 | 5.00 | ug/L | 1 | | | | |
| Acrolein | U | ND | 1.25 | 5.00 | ug/L | 1 | | | | |
| Acrylonitrile | U | ND | 1.00 | 5.00 | ug/L | 1 | | | | |
| Benzene | U | ND | 0.300 | 1.00 | ug/L | 1 | | | | |
| Bromodichloromethane | U | ND | 0.250 | 1.00 | ug/L | 1 | | | | |
| Bromoform | U | ND | 0.250 | 1.00 | ug/L | 1 | | | | |
| Bromomethane | U | ND | 0.300 | 1.00 | ug/L | 1 | | | | |
| Carbon tetrachloride | U | ND | 0.300 | 1.00 | ug/L | 1 | | | | |
| Chlorobenzene | U | ND | 0.250 | 1.00 | ug/L | 1 | | | | |
| Chloroethane | U | ND | 0.300 | 1.00 | ug/L | 1 | | | | |
| Chloroform | U | ND | 0.250 | 1.00 | ug/L | 1 | | | | |
| Chloromethane | U | ND | 0.300 | 1.00 | ug/L | 1 | | | | |
| Dibromochloromethane | U | ND | 0.300 | 1.00 | ug/L | 1 | | | | |
| Ethylbenzene | U | ND | 0.250 | 1.00 | ug/L | 1 | | | | |
| Methylene chloride | U | ND | 2.00 | 2.00 | ug/L | 1 | | | | |
| Tetrachloroethylene | U | ND | 0.300 | 1.00 | ug/L | 1 | | | | |
| Toluene | U | ND | 0.250 | 1.00 | ug/L | 1 | | | | |
| Trichloroethylene | U | ND | 0.250 | 1.00 | ug/L | 1 | | | | |
| Vinyl chloride | U | ND | 0.500 | 1.00 | ug/L | 1 | | | | |
| cis-1,3-Dichloropropylene | U | ND | 0.250 | 1.00 | ug/L | 1 | | | | |
| trans-1,2-Dichloroethylene | U | ND | 0.300 | 1.00 | ug/L | 1 | | | | |
| trans-1,3-Dichloropropylene | U | ND | 0.250 | 1.00 | ug/L | 1 | | | | |

**The following Analytical Methods were performed**

| Method | Description | Analyst Comments |
|---|---|---|
| 1 | EPA 624 SC_NPDES | |

| Surrogate/Tracer recovery | Test | Result | Nominal | Recovery% | Acceptable Limits |
|---|---|---|---|---|---|
| 1,2-Dichloroethane-d4 | EPA 624 TTO Liquid "As Received" | 51.9 ug/L | 50.0 | 104 | (71%-130%) |

# Certificate of Analysis

Company : AECOM Water
Address : 10 Patewood Drive
Building VI, Suite 500
Greenville, South Carolina 29615
Contact: Mr. David M. Welch
Project: Pinewood

Report Date: November 29, 2010

Client Sample ID: PAFD-2
Sample ID: 266958007

Project: AECM00101
Client ID: AECM001

| Parameter | Qualifier | Result | DL | RL | Units | DF | Analyst | Date | Time | Batch | Method |
|---|---|---|---|---|---|---|---|---|---|---|---|
| Bromofluorobenzene | | EPA 624 TTO Liquid "As Received" | | 48.2 | ug/L | 50.0 | | 96.5 | | (80%-120%) | |
| Toluene-d8 | | EPA 624 TTO Liquid "As Received" | | 49.1 | ug/L | 50.0 | | 98.2 | | (80%-120%) | |

## QC Summary

**Report Date: November 29, 2010**


**AECOM Water**
**10 Patewood Drive**
**Building VI, Suite 500**
**Greenville, South Carolina**
**Contact:** **Mr. David M. Welch**

**Workorder:** **266958**

| Parmname | NOM | | Sample | Qual | QC | Units | RPD% | REC% | Range | Anlst | Date Time |
|---|---|---|---|---|---|---|---|---|---|---|---|
| **Volatile-GC/MS** | | | | | | | | | | | |
| Batch 1048933 | | | | | | | | | | | |
| QC1202264666 266958001 DUP | | | | | | | | | | | |
| 1,1,1-Trichloroethane | | U | ND | U | ND | ug/L | N/A | | | RXD1 | 11/16/10 00:30 |
| 1,1,2,2-Tetrachloroethane | | U | ND | U | ND | ug/L | N/A | | | | |
| 1,1,2-Trichloroethane | | U | ND | U | ND | ug/L | N/A | | | | |
| 1,1-Dichloroethane | | | 14.7 | | 14.5 | ug/L | 1.65 | | | | |
| 1,1-Dichloroethylene | | U | ND | U | ND | ug/L | N/A | | | | |
| 1,2-Dichloroethane | | U | ND | U | ND | ug/L | N/A | | | | |
| 1,2-Dichloropropane | | U | ND | U | ND | ug/L | N/A | | | | |
| 2-Chloroethylvinyl ether | | U | ND | U | ND | ug/L | N/A | | | | |
| Acrolein | | U | ND | U | ND | ug/L | N/A | | | | |
| Acrylonitrile | | U | ND | U | ND | ug/L | N/A | | | | |
| Benzene | | | 1.19 | | 1.16 | ug/L | 2.55 ^ | | (+/-1.00) | | |
| Bromodichloromethane | | U | ND | U | ND | ug/L | N/A | | | | |
| Bromoform | | U | ND | U | ND | ug/L | N/A | | | | |
| Bromomethane | | U | ND | U | ND | ug/L | N/A | | | | |
| Carbon tetrachloride | | U | ND | U | ND | ug/L | N/A | | | | |
| Chlorobenzene | | U | ND | U | ND | ug/L | N/A | | | | |
| Chloroethane | | U | ND | U | ND | ug/L | N/A | | | | |
| Chloroform | | U | ND | U | ND | ug/L | N/A | | | | |
| Chloromethane | | U | ND | U | ND | ug/L | N/A | | | | |
| Dibromochloromethane | | U | ND | U | ND | ug/L | N/A | | | | |
| Ethylbenzene | | U | ND | U | ND | ug/L | N/A | | | | |
| Methylene chloride | | U | ND | U | ND | ug/L | N/A | | | | |
| Tetrachloroethylene | | U | ND | U | ND | ug/L | N/A | | | | |
| Toluene | | BJ | 0.260 | U | ND | ug/L | N/A ^ | | | | |
| Trichloroethylene | | U | ND | U | ND | ug/L | N/A | | | | |
| Vinyl chloride | | | 31.8 | | 30.5 | ug/L | 3.95 | | | | |
| cis-1,3-Dichloropropylene | | U | ND | U | ND | ug/L | N/A | | | | |
| trans-1,2-Dichloroethylene | | | 2.20 | | 2.13 | ug/L | 3.23 ^ | | (+/-1.00) | | |
| trans-1,3-Dichloropropylene | | U | ND | U | ND | ug/L | N/A | | | | |
| **1,2-Dichloroethane-d4 | 50.0 | | 53.4 | | 53.5 | ug/L | | 107 | (71%-130%) | | |
| **Bromofluorobenzene | 50.0 | | 48.6 | | 48.4 | ug/L | | 96.8 | (80%-120%) | | |
| **Toluene-d8 | 50.0 | | 49.3 | | 49.3 | ug/L | | 98.6 | (80%-120%) | | |
| QC1202264665 MB | | | | | | | | | | | |
| 1,1,1-Trichloroethane | | | | U | ND | ug/L | | | | | 11/15/10 13:15 |
| 1,1,2,2-Tetrachloroethane | | | | U | ND | ug/L | | | | | |
| 1,1,2-Trichloroethane | | | | U | ND | ug/L | | | | | |
| 1,1-Dichloroethane | | | | U | ND | ug/L | | | | | |

# QC Summary

**Workorder:** **266958**



| Parmname | NOM | Sample | Qual | QC | Units | RPD% | REC% | Range | Anlst | Date Time |
|---|---|---|---|---|---|---|---|---|---|---|
| **Volatile-GC/MS** | | | | | | | | | | |
| Batch 1048933 | | | | | | | | | | |
| 1,1-Dichloroethylene | | | U | ND | ug/L | | | | | |
| 1,2-Dichloroethane | | | U | ND | ug/L | | | | RXD1 | 11/15/10 13:15 |
| 1,2-Dichloropropane | | | U | ND | ug/L | | | | | |
| 2-Chloroethylvinyl ether | | | U | ND | ug/L | | | | | |
| Acrolein | | | U | ND | ug/L | | | | | |
| Acrylonitrile | | | U | ND | ug/L | | | | | |
| Benzene | | | U | ND | ug/L | | | | | |
| Bromodichloromethane | | | U | ND | ug/L | | | | | |
| Bromoform | | | U | ND | ug/L | | | | | |
| Bromomethane | | | U | ND | ug/L | | | | | |
| Carbon tetrachloride | | | U | ND | ug/L | | | | | |
| Chlorobenzene | | | U | ND | ug/L | | | | | |
| Chloroethane | | | U | ND | ug/L | | | | | |
| Chloroform | | | U | ND | ug/L | | | | | |
| Chloromethane | | | U | ND | ug/L | | | | | |
| Dibromochloromethane | | | U | ND | ug/L | | | | | |
| Ethylbenzene | | | U | ND | ug/L | | | | | |
| Methylene chloride | | | U | ND | ug/L | | | | | |
| Tetrachloroethylene | | | U | ND | ug/L | | | | | |
| Toluene | | | J | 0.300 | ug/L | | | | | |
| Trichloroethylene | | | U | ND | ug/L | | | | | |
| Vinyl chloride | | | U | ND | ug/L | | | | | |
| cis-1,3-Dichloropropylene | | | U | ND | ug/L | | | | | |
| trans-1,2-Dichloroethylene | | | U | ND | ug/L | | | | | |
| trans-1,3-Dichloropropylene | | | U | ND | ug/L | | | | | |
| **1,2-Dichloroethane-d4 | 50.0 | | | 52.8 | ug/L | | 106 | (71%-130%) | | |
| **Bromofluorobenzene | 50.0 | | | 48.4 | ug/L | | 96.8 | (80%-120%) | | |
| **Toluene-d8 | 50.0 | | | 49.3 | ug/L | | 98.6 | (80%-120%) | | |
| QC1202265445 MB | | | | | | | | | | |
| 1,1,1-Trichloroethane | | | U | ND | ug/L | | | | | 11/16/10 12:36 |
| 1,1,2,2-Tetrachloroethane | | | U | ND | ug/L | | | | | |
| 1,1,2-Trichloroethane | | | U | ND | ug/L | | | | | |
| 1,1-Dichloroethane | | | U | ND | ug/L | | | | | |
| 1,1-Dichloroethylene | | | U | ND | ug/L | | | | | |
| 1,2-Dichloroethane | | | U | ND | ug/L | | | | | |
| 1,2-Dichloropropane | | | U | ND | ug/L | | | | | |
| 2-Chloroethylvinyl ether | | | U | ND | ug/L | | | | | |
| Acrolein | | | U | ND | ug/L | | | | | |
| Acrylonitrile | | | U | ND | ug/L | | | | | |
| Benzene | | | U | ND | ug/L | | | | | |
| Bromodichloromethane | | | U | ND | ug/L | | | | | |
| Bromoform | | | U | ND | ug/L | | | | | |

# QC Summary

**Workorder:** **266958**



| Parmname | NOM | | Sample | Qual | QC | Units | RPD% | REC% | Range | Anlst | Date Time |
|---|---|---|---|---|---|---|---|---|---|---|---|
| **Volatile-GC/MS** | | | | | | | | | | | |
| Batch 1048933 | | | | | | | | | | | |
| Bromomethane | | | | U | ND | ug/L | | | | | |
| Carbon tetrachloride | | | | U | ND | ug/L | | | | RXD1 | 11/16/10 12:36 |
| Chlorobenzene | | | | U | ND | ug/L | | | | | |
| Chloroethane | | | | U | ND | ug/L | | | | | |
| Chloroform | | | | U | ND | ug/L | | | | | |
| Chloromethane | | | | U | ND | ug/L | | | | | |
| Dibromochloromethane | | | | U | ND | ug/L | | | | | |
| Ethylbenzene | | | | U | ND | ug/L | | | | | |
| Methylene chloride | | | | U | ND | ug/L | | | | | |
| Tetrachloroethylene | | | | U | ND | ug/L | | | | | |
| Toluene | | | | U | ND | ug/L | | | | | |
| Trichloroethylene | | | | U | ND | ug/L | | | | | |
| Vinyl chloride | | | | U | ND | ug/L | | | | | |
| cis-1,3-Dichloropropylene | | | | U | ND | ug/L | | | | | |
| trans-1,2-Dichloroethylene | | | | U | ND | ug/L | | | | | |
| trans-1,3-Dichloropropylene | | | | U | ND | ug/L | | | | | |
| **1,2-Dichloroethane-d4 | 50.0 | | | | 52.9 | ug/L | | 106 | (71%-130%) | | |
| **Bromofluorobenzene | 50.0 | | | | 48.6 | ug/L | | 97.2 | (80%-120%) | | |
| **Toluene-d8 | 50.0 | | | | 49.2 | ug/L | | 98.3 | (80%-120%) | | |
| QC1202264667 266958001 PS | | | | | | | | | | | |
| 1,1,1-Trichloroethane | 50.0 | U | ND | | 47.7 | ug/L | | 95.4 | (67%-127%) | | 11/16/10 03:44 |
| 1,1,2,2-Tetrachloroethane | 50.0 | U | ND | | 45.8 | ug/L | | 91.6 | (59%-129%) | | |
| 1,1,2-Trichloroethane | 50.0 | U | ND | | 48.3 | ug/L | | 96.7 | (67%-121%) | | |
| 1,1-Dichloroethane | 50.0 | | 14.7 | | 65.1 | ug/L | | 101 | (70%-120%) | | |
| 1,1-Dichloroethylene | 50.0 | U | ND | | 44.4 | ug/L | | 88.7 | (61%-123%) | | |
| 1,2-Dichloroethane | 50.0 | U | ND | | 52.1 | ug/L | | 104 | (65%-126%) | | |
| 1,2-Dichloropropane | 50.0 | U | ND | | 52.7 | ug/L | | 105 | (70%-121%) | | |
| 2-Chloroethylvinyl ether | 250 | U | ND | | 171 | ug/L | | 68.3 | (30%-191%) | | |
| Benzene | 50.0 | | 1.19 | | 49.2 | ug/L | | 96 | (68%-117%) | | |
| Bromodichloromethane | 50.0 | U | ND | | 52.8 | ug/L | | 106 | (72%-128%) | | |
| Bromoform | 50.0 | U | ND | | 42.3 | ug/L | | 84.5 | (66%-131%) | | |
| Bromomethane | 50.0 | U | ND | | 44.2 | ug/L | | 88.4 | (56%-135%) | | |
| Carbon tetrachloride | 50.0 | U | ND | | 49.4 | ug/L | | 98.8 | (66%-133%) | | |
| Chlorobenzene | 50.0 | U | ND | | 48.3 | ug/L | | 96.5 | (72%-115%) | | |
| Chloroethane | 50.0 | U | ND | | 44.1 | ug/L | | 88.2 | (65%-120%) | | |
| Chloroform | 50.0 | U | ND | | 49.6 | ug/L | | 99.1 | (69%-121%) | | |
| Chloromethane | 50.0 | U | ND | | 50.7 | ug/L | | 101 | (46%-129%) | | |
| Dibromochloromethane | 50.0 | U | ND | | 52.1 | ug/L | | 104 | (73%-128%) | | |
| Ethylbenzene | 50.0 | U | ND | | 45.9 | ug/L | | 91.8 | (64%-123%) | | |
| Methylene chloride | 50.0 | U | ND | | 49.1 | ug/L | | 98.2 | (64%-125%) | | |
| Tetrachloroethylene | 50.0 | U | ND | | 45.9 | ug/L | | 91.8 | (64%-117%) | | |
| Toluene | 50.0 | BJ | 0.260 | | 45.3 | ug/L | | 90.1 | (63%-118%) | | |

# QC Summary

**Workorder:** **266958**



| Parmname | NOM | | Sample | Qual | QC | Units | RPD% | REC% | Range | Anlst | Date Time |
|---|---|---|---|---|---|---|---|---|---|---|---|
| **Volatile-GC/MS** | | | | | | | | | | | |
| Batch 1048933 | | | | | | | | | | | |
| Trichloroethylene | 50.0 | U | ND | | 46.4 | ug/L | | 92.7 | (61%-128%) | | |
| Vinyl chloride | 50.0 | | 31.8 | | 74.0 | ug/L | | 84.5 | (53%-132%) | RXD1 | 11/16/10 03:44 |
| cis-1,3-Dichloropropylene | 50.0 | U | ND | | 52.8 | ug/L | | 106 | (70%-124%) | | |
| trans-1,2-Dichloroethylene | 50.0 | | 2.20 | | 50.2 | ug/L | | 95.9 | (65%-121%) | | |
| trans-1,3-Dichloropropylene | 50.0 | U | ND | | 51.4 | ug/L | | 103 | (68%-129%) | | |
| **1,2-Dichloroethane-d4 | 50.0 | | 53.4 | | 52.5 | ug/L | | 105 | (71%-130%) | | |
| **Bromofluorobenzene | 50.0 | | 48.6 | | 47.0 | ug/L | | 94 | (80%-120%) | | |
| **Toluene-d8 | 50.0 | | 49.3 | | 49.6 | ug/L | | 99.3 | (80%-120%) | | |

Notes:
The Qualifiers in this report are defined as follows:

- ** Analyte is a surrogate compound
- < Result is less than value reported
- > Result is greater than value reported
- A The TIC is a suspected aldol-condensation product
- B For General Chemistry and Organic analysis the target analyte was detected in the associated blank.
- C Analyte has been confirmed by GC/MS analysis
- D Results are reported from a diluted aliquot of the sample
- E Organics--Concentration of the target analyte exceeds the instrument calibration range
- F Estimated Value
- H Analytical holding time was exceeded
- J Value is estimated
- JNX Non Calibrated Compound
- M Matrix Related Failure
- N Organics--Presumptive evidence based on mass spectral library search to make a tentative identification of the analyte (TIC). Quantitation is based on nearest internal standard response factor
- N/A RPD or %Recovery limits do not apply.
- ND Analyte concentration is not detected above the detection limit
- NJ Consult Case Narrative, Data Summary package, or Project Manager concerning this qualifier
- P Organics--The concentrations between the primary and confirmation columns/detectors is >40% different. For HPLC, difference is also <70%
- Q One or more quality control criteria have not been met. Refer to the applicable narrative or DER.
- R Sample results are rejected
- U Analyte was analyzed for, but not detected above the MDL, MDA, or LOD.
- X Consult Case Narrative, Data Summary package, or Project Manager concerning this qualifier
- Y QC Samples were not spiked with this compound
- ^ RPD of sample and duplicate evaluated using +/-RL. Concentrations are <5X the RL. Qualifier Not Applicable for Radiochemistry.
- h Preparation or preservation holding time was exceeded

# QC Summary

**Workorder:** **266958**



| Parmname | NOM | Sample | Qual | QC | Units | RPD% | REC% | Range | Anlst | Date | Time |
|---|---|---|---|---|---|---|---|---|---|---|---|

N/A indicates that spike recovery limits do not apply when sample concentration exceeds spike conc. by a factor of 4 or more.
^ The Relative Percent Difference (RPD) obtained from the sample duplicate (DUP) is evaluated against the acceptance criteria when the sample is greater than five times (5X) the contract required detection limit (RL). In cases where either the sample or duplicate value is less than 5X the RL, a control limit of +/- the RL is used to evaluate the DUP result.
* Indicates that a Quality Control parameter was not within specifications.
For PS, PSD, and SDILT results, the values listed are the measured amounts, not final concentrations.

Where the analytical method has been performed under NELAP certification, the analysis has met all of the requirements of the NELAC standard unless qualified on the QC Summary.

**There are no "Data Exception Reports" associated with this analytical report.**

2.0101171098

Page: 1 of
Project #: ~~AECOM~~ AECM00101
GEL Quote #:
COC Number (1):
PO Number:

# GEL Chain of Custody and Analytical Request

**GEL Work Order Number:** 266958

GEL Laboratories, LLC
2040 Savage Road
Charleston, SC 29407
Phone: (843) 556-8171
Fax: (843) 766-1178

Client Name: AECOM Water  Phone #: (864) 234-3000
Project/Site Name: Pinewood  Fax #:
Address: 10 Patewood Dr., Bldg VI, Suite 500 Greenville, SC 29615
Collected by: A. Gupta / C. Sudderth  Send Results To: David Welch



**Sample Analysis Requested** (5) (Fill in the number of containers for each test)

| Sample ID (* For composites - indicate start and stop date/time) | *Date Collected (mm-dd-yy) | *Time Collected (Military) (hhmm) | QC Code (2) | Field Filtered (3) | Sample Matrix (4) | Should this sample be considered: Radioactive | Should this sample be considered: TSCA Regulated | Total number of containers | HA | VOCs 624 | VOCs 624 | <-- Preservative Type (6) |
|---|---|---|---|---|---|---|---|---|---|---|---|---|
| SILC-1 | 11/10/10 | 1619 | G | N | GW | N | N | 4 | 2 | 2 | | |
| SILC-2 | 11/10/10 | 1550 | G | N | GW | N | N | 2 | 2 | | | |
| SILC-4 | 11/10/10 | 1600 | G | N | GW | N | N | 4 | 2 | 2 | | |
| SILC-5 | 11/10/10 | 1517 | G | N | GW | N | N | 3 | 1 | 2 | | |
| PBFD-1 | 11/10/10 | 1709 | G | N | SW | N | N | 4 | 2 | 2 | | |
| PAFD-1 | 11/10/10 | 1725 | G | N | SW | N | N | 4 | 2 | 2 | | |
| PAFD-2 | 11/11/10 | 1415 | G | N | SW | N | N | 4 | 2 | 2 | | |
| | | | | | | | | | | | | |
| | | | | | | | | | | | | |
| | | | | | | | | | | | | |

**Comments**
Note: extra sample is required for sample specific QC

TAT Requested: Normal: ✓ Rush: Specify: (Subject to Surcharge)  Fax Results: Yes / No  Circle Deliverable: C of A / QC Summary / Level 1 / Level 2 / Level 3 / Level 4

***Remarks:*** *Are there any known hazards applicable to these samples? If so, please list the hazards*

Sample Collection Time Zone
(Eastern) Pacific
Central Other
Mountain

**Chain of Custody Signatures**

| | Relinquished By (Signed) | Date | Time | Received by (signed) | Date | Time |
|---|---|---|---|---|---|---|
| 1 | Charles K. Sudderth | 11/11/10 | 1630 | Steve Rucker | 11/11/10 | 1630 |
| 2 | [illegible] | 11/12/10 | | [illegible] | 111210 | 1415 |
| 3 | | | | | | |

**Sample Shipping and Delivery Details**

GEL PM:
Method of Shipment:  Date Shipped:
Airbill #:
Airbill #:

1.) Chain of Custody Number = Client Determined
2.) QC Codes: **N** = Normal Sample, **TB** = Trip Blank, **FD** = Field Duplicate, **EB** = Equipment Blank, **MS** = Matrix Spike Sample, **MSD** = Matrix Spike Duplicate Sample, **G** = Grab, **C** = Composite
3.) Field Filtered: For liquid matrices, indicate with a - **Y** - for yes the sample was field filtered or - **N** - for sample was not field filtered.
4.) Matrix Codes: **DW**=Drinking Water, **GW**=Groundwater, **SW**=Surface Water, **WW**=Waste Water, **W**=Water, **SO**=Soil, **SD**=Sediment, **SL**=Sludge, **SS**=Solid Waste, **O**=Oil, **F**=Filter, **P**=Wipe, **U**=Urine, **F**=Fecal, **N**=Nasal
5.) Sample Analysis Requested: Analytical method requested (i.e. **8260B**, **6010B/7470A**) and number of containers provided for each (i.e. *8260B* - **3**, *6010B/7470A* - **1**).
6.) Preservative Type: **HA** = Hydrochloric Acid, **NI** = Nitric Acid, **SH** = Sodium Hydroxide, **SA** = Sulfuric Acid, **AA** = Ascorbic Acid, **HX** = Hexane, **ST** = Sodium Thiosulfate, If no preservative is added = leave field blank

*For Lab Receiving Use Only*
*Custody Seal Intact?* YES NO
*Cooler Temp:* 5 C

**WHITE = LABORATORY**  **YELLOW = FILE**  **PINK = CLIENT**

GEL Laboratories LLC

# SAMPLE RECEIPT & REVIEW FORM

| | | | |
|---|---|---|---|
| **Client:** AECOM | | | **SDG/AR/COC/Work Order:** 266958 |
| **Received By:** tg | | | **Date Received:** 111210 |
| **Suspected Hazard Information** | **Yes** | **No** | *If Counts > x2 area background on samples not marked "radioactive", contact the Radiation Safety Group of further investigation. |
| COC/Samples marked as radioactive? | | ✓ | Maximum Counts Observed*: 10 |
| Classified Radioactive II or III by RSO? | | ✓ | |
| COC/Samples marked containing PCBs? | | ✓ | |
| Shipped as a DOT Hazardous? | | ✓ | Hazard Class Shipped: UN#: |
| Samples identified as Foreign Soil? | | ✓ | |

| | Sample Receipt Criteria | Yes | NA | No | Comments/Qualifiers (Required for Non-Conforming Items) |
|---|---|---|---|---|---|
| 1 | Shipping containers received intact and sealed? | ✓ | | | Circle Applicable: Seals broken Damaged container Leaking container Other (describe) |
| 2 | Samples requiring cold preservation within (0 ≤ 6 deg. C)? | ✓ | | | Preservation Method: 5 Ice bags Blue ice Dry ice None Other (describe) |
| 2a | Daily check performed and passed on IR temperature gun? | ✓ | | | Temperature Device Serial #: Secondary Temperature Device Serial # (If Applicable): 91050004 |
| 3 | Chain of custody documents included with shipment? | ✓ | | | |
| 4 | Sample containers intact and sealed? | ✓ | | | Circle Applicable: Seals broken Damaged container Leaking container Other (describe) |
| 5 | Samples requiring chemical preservation at proper pH? | ✓ | | | Sample ID's, containers affected and observed pH: If Preservation added, Lot#: |
| 6 | VOA vials free of headspace (defined as < 6mm bubble)? | ✓ | | | Sample ID's and containers affected: |
| 7 | Are Encore containers present? | | ✓ | | (If yes, immediately deliver to Volatiles laboratory) |
| 8 | Samples received within holding time? | ✓ | | | ID's and tests affected: |
| 9 | Sample ID's on COC match ID's on bottles? | ✓ | | | Sample ID's and containers affected: |
| 10 | Date & time on COC match date & time on bottles? | ✓ | | | Sample ID's affected: |
| 11 | Number of containers received match number indicated on COC? | ✓ | | | Sample ID's affected: |
| 12 | COC form is properly signed in relinquished/received sections? | ✓ | | | |
| 13 | Carrier and tracking number. | ✓ | | | Circle Applicable: FedEx Air FedEx Ground UPS Field Services Courier Other |

Comments (Use Continuation Form if needed):

PM (or PMA) review: Initials JMC Date 11/12/10 Page 1 of 1

**List of current GEL Certifications as of 29 November 2010**

| State | Certification |
|---|---|
| Arizona | AZ0668 |
| Arkansas | 88–0651 |
| CLIA | 42D0904046 |
| California – NELAP | 01151CA |
| Colorado | GEL |
| Connecticut | PH–0169 |
| Dept. of Navy | NFESC 413 |
| EPA Region 5 | WG–15J |
| Florida – NELAP | E87156 |
| Georgia | E87156 (FL/NELAP) |
| Georgia DW | 967 |
| Hawaii | N/A |
| ISO 17025 | 2567.01 |
| Idaho | SC00012 |
| Illinois – NELAP | 200029 |
| Indiana | C–SC–01 |
| Kansas – NELAP | E–10332 |
| Kentucky | 90129 |
| Louisiana – NELAP | 03046 |
| Maryland | 270 |
| Massachusetts | M–SC012 |
| Nevada | SC00012 |
| New Jersey – NELAP | SC002 |
| New Mexico | FL NELAP E87156 |
| New York – NELAP | 11501 |
| North Carolina | 233 |
| North Carolina DW | 45709 |
| Oklahoma | 9904 |
| Pennsylvania – NELAP | 68–00485 |
| South Carolina | 10120001/10120002 |
| Tennessee | TN 02934 |
| Texas – NELAP | T104704235–07B–TX |
| U.S. Dept. of Agriculture | S–52597 |
| Utah – NELAP | GEL |
| Vermont | VT87156 |
| Virginia | 00151 |
| Washington | C1641 |

# Appendix 2.8-1

NPDES Permit No. SC0042170

PSCT 06.50



D H E C
PROMOTE PROTECT PROSPER



CERTIFIED MAIL/RETURN RECEIPT REQUESTED

June 22, 2005

Mr. Thomas W. Devine
Principal
Kestrel Horizons, LLC
20-B Creekview Court
Greenville, SC 29615

Re: NPDES Permit No. SC0042170
Pinewood Site Custodial Trust
Sumter County

Dear Mr. Devine:

Enclosed is the National Pollutant Discharge Elimination system (NPDES) Permit for the above referenced facility. The Department of Health and Environmental Control (DHEC) will enforce all the provisions of the permit in an equitable and timely manner.

In order that you understand your responsibilities included in the provisions of this permit, particular attention should be given to the following sections:

1. PART III: This section contains all listings of effluent characteristics, discharge limitations, and groundwater, soil and sludge monitoring.
2. PART II.L.4: This section contains your responsibilities for reporting monitoring results. Preprinted Discharge Monitoring Report (DMR) and groundwater monitoring forms will be provided at a later date by DHEC for reporting monitoring results.
3. PART II.L.3: This section describes the specific requirements for an SC permit to be transferred to another party.
4. PART II.E: This section contains responsibilities for the proper operation and maintenance of your facility.
5. PART V: This section contains all the special requirements relative to your permit. Such items in this section include the certified operator required to operate your wastewater treatment plant, the day of the week on which monitoring shall occur, and sludge disposal requirements.

This permit, as issued, will become effective on the effective date specified on the permit, provided no appeal for an adjudicatory hearing is made. The issuance of this permit represents a final staff decision that may be appealed to the Administrative Law Court (ALC). Such appeal must be made pursuant to the amended Rules of Procedure for the Administrative Law Court that became effective on May 1, 2005. Pursuant to Rule 11 of the amended ALC Rules of Procedure, such appeal must be made by filing a request for a contested case hearing with the Clerk of the ALC within thirty (30) days after notice of this decision at the following address:

Clerk, Administrative Law Court
1205 Pendleton Street, Suite 224
PO Box 11667
Columbia, SC 29211

Pursuant to Rule 11(D), the following elements must, at a minimum, be included within the request:

1. The name of the party requesting the hearing and the issue(s) for which the hearing is requested;
2. The caption or other information sufficient to identify the decision, order, letter, determination, action, or inaction which is subject to the hearing;
3. A copy of the written agency decision, order, letter or determination, if any, which gave rise to the request;
4. The relief requested.

Furthermore, pursuant to ALC Rule 71, the Administrative Law Court requires that a party requesting a contested case hearing must submit a filing fee in the amount of $250.00 with the Administrative Law Court. A copy of a request for the contested case hearing must also be served on each party, including but not limited to, DHEC. Copies of a request for a contested case hearing should be mailed to the Clerk of the Board, DHEC, 2600 Bull Street, Columbia, SC 29201, (803) 898-3300.

If you have any questions about the technical aspects of this permit, please contact Mr. Butch Swygert (803) 898-4235. Information pertaining to adjudicatory matters may be obtained by contacting the Legal Office, SCDHEC, 2600 Bull Street, Columbia, SC 29201, or by calling them at (803)898-3350.

Sincerely,

Marion F. Sadler, Jr., Director
Industrial, Agricultural, and
Storm Water Permitting Division

Enclosure

cc: EPA
Ronnie Driggers, Wateree
Jaime Teraoka, WP Enforcement
Florence EQC Lab
Butch Swygert, BOW
NPDES Administration

D H E C

PROMOTE PROTECT PROSPER

South Carolina Department of Health
and Environmental Control

# *National Pollutant Discharge Elimination System Permit*

## for Discharge to Surface Waters

This Permit Certifies That

***PINEWOOD SITE CUSTODIAL TRUST***
has been granted permission to discharge from a facility located at

***8430 Camp MacBoykin Road***
***Pinewood, South Carolina***
***Sumter County***

to receiving waters named

***Unnamed Tributary to Lake Marion***

in accordance with limitations, monitoring requirements and other conditions set forth herein. This permit is issued in accordance with the provisions of the Pollution Control Act of South Carolina (S.C. Code Sections 48-1-10 *et seq.*, 1976), Regulation 61-9 and with the provisions of the Federal Clean Water Act (PL 92-500), as amended, 33 U.S.C. 1251 *et seq.*, the "Act."

**Marion F. Sadler, Jr., Director**
**Industrial, Agricultural, and Storm Water Permitting Division**
**Bureau of Water**

***Issue Date:*** **June 22, 2005** ***Expiration Date:*** **July 31, 2010**

***Effective Date:*** **August 1, 2005** ***Permit No.:*** **SC0042170**

## Table of Contents

**PART I. Definitions**

Any term not defined in this Part has the definition stated in the Pollution Control Act or in "Water Pollution Control Permits", R.61-9 or its normal meaning.

A. The "Act", or CWA, shall refer to the Clean Water Act (Formerly referred to as the Federal Water Pollution Control Act) Public Law 92-500, as amended.

B. "Adverse Impact" means a significant negative impact to land, water and associated resources resulting from a land disturbing activity. The negative impact includes increased risk of flooding; degradation of water quality; increased sedimentation; reduced groundwater recharge; negative impacts on aquatic organisms; negative impacts on wildlife and other resources; and threatened public health.

C. The "average" or "arithmetic mean" of any set of values is the summation of the individual values divided by the number of individual values.

D. "Basin" (or "Lagoon") means any in-ground or earthen structure designed to receive, treat, store, temporarily retain and/or allow for the infiltration/evaporation of wastewater.

E. "Best Management Practices" ("BMPs") means schedules of activities, prohibitions of practices, maintenance procedures, and other management practices to prevent or reduce the pollution of waters of South Carolina. BMPs also include treatment requirements, operating procedures, and practices to control plant site runoff, spillage or leaks, sludge or waste disposal, or drainage from raw material storage.

F. "Bypass" means the intentional diversion of waste streams from any portion of a treatment facility.

G. A "composite sample" shall be defined as one of the following four types:

1. An influent or effluent portion collected continuously over a specified period of time at a rate proportional to the flow.

2. A combination of not less than 8 influent or effluent grab samples collected at regular (equal) intervals over a specified period of time and composited by increasing the volume of each aliquot in proportion to flow. If continuous flow measurement is not used to composite in proportion to flow, the following method will be used: An instantaneous flow measurement should be taken each time a grab sample is collected. At the end of the sampling period, the instantaneous flow measurements should be summed to obtain a total flow. The instantaneous flow measurement can then be divided by the total flow to determine the percentage of each grab sample to be combined. These combined samples form the composite sample.

3. A combination of not less than 8 influent or effluent grab samples of equal volume but at variable time intervals that are inversely proportional to the volume of the flow. In other words, the time interval between aliquots is reduced as the volume of flow increases.

4. If the effluent flow varies by less than 15 percent, a combination of not less than 8 influent or effluent grab samples of constant (equal) volume collected at regular (equal) time intervals over a specified period of time.

All samples shall be properly preserved in accordance with Part II.J.4. Continuous flow or the sum of instantaneous flows measured and averaged for the specified compositing time period shall be used with composite results to calculate mass.

H. "Construction Activity" is defined as any land disturbing activity that is related to the operation and closure of the landfill cells, construction and maintenance of the first surge basin and demolition of existing wastewater structures.

I. "Daily maximum" is the highest average value recorded of samples collected on any single day during the calendar month.

J. "Daily minimum" is the lowest average value recorded of samples collected on any single day during the calendar month.

K. The "Department" or "DHEC" shall refer to the South Carolina Department of Health and Environmental Control.

L. "Final Stabilization" means the installation of vegetative or structural measures to establish a soil cover to reduce soil erosion by storm water runoff, wind, ice and gravity.

M. The "geometric mean" of any set of values is the Nth root of the product of the individual values where N is equal to the number of individual values. The geometric mean is equivalent to the antilog of the arithmetic mean of the logarithms of the individual values. For purposes of calculating the geometric mean, values of zero (0) shall be considered to be one (1).

N. A "grab sample" is an individual, discrete or single influent or effluent portion of at least 100 milliliters collected at a time representative of the discharge and over a period not exceeding 15 minutes and retained separately for analysis. Instantaneous flow measured at the time of grab sample collection shall be used to calculate quantity, unless a totalizer is used.

O. "Groundwater" means the water below the land surface found in fractured rock or various soil strata.

P. "Land Disturbing Activity" means any use of the land by any person that results in a change in the natural cover or topography that may cause erosion and contribute to sediment and alter the quality and quantity of storm water runoff.

Q. The "maximum or minimum" is the highest or lowest value, respectively, recorded of all samples collected during the calendar month. These terms may also be known as the instantaneous maximum or minimum.

R. The "monthly average", other than for fecal coliform, is the arithmetic mean of all samples collected in a calendar month period. The monthly average for fecal coliform bacteria is the geometric mean of all samples collected in a calendar month period. The monthly average loading is the arithmetic average of all individual loading determinations made during the month.

S. The "PCA" shall refer to the Pollution Control Act (Chapter 1, Title 48, Code of Laws of South Carolina).

T. The "practical quantitation limit" (PQL) is the concentration at which the entire analytical system must give a recognizable signal and acceptable calibration point. It is the concentration in a sample that is equivalent to the

concentration of the lowest calibration standard analyzed by a specific analytical procedure, assuming that all the method-specific sample weights, volumes, and processing steps have been followed.

U. "Quarter" is defined as the first three calendar months beginning with the month that this permit becomes effective and each group of three calendar months thereafter.

V. "Quarterly average" is the arithmetic mean of all samples collected in a quarter.

W. "Runoff coefficient" means the fraction of total rainfall that will appear at the conveyance as runoff.

X. "Severe property damage" means substantial physical damage to property, damage to the treatment facilities which causes them to become inoperable, or substantial and permanent loss of natural resources which can reasonably be expected to occur in the absence of a bypass. Severe property damage does not mean economic loss caused by delays in production.

Y. "Sludge" means industrial sludge. Industrial sludge is a solid, semi-solid, or liquid residue generated during the treatment of industrial wastewater in a treatment works. Industrial sludge includes, but is not limited to, industrial septage; scum or solids removed in primary, secondary, or advanced wastewater treatment processes; and a material derived from industrial sludge. Industrial sludge does not include ash generated during the firing of industrial sludge in an industrial sludge incinerator or grit and screenings generated during preliminary treatment of industrial wastewater in a treatment works. Industrial sludge by definition does not include sludge covered under 40 CFR Part 503 or R.61-9.503.

Z. "Storm Water"" means storm water runoff, snow melt runoff, and surface runoff and drainage.

AA. "Storm water Management" means, for:
1. quantitative control, a system of vegetative or structural measures, or both, that control the increased volume and rate of storm water runoff caused by manmade changes to the land;
2. qualitative control, a system of vegetative, structural, or other measures that reduce or eliminate pollutants that might otherwise be carried by storm water runoff.

BB. "Upset" means an exceptional incident in which there is unintentional and temporary noncompliance with technology based permit effluent limitations because of factors beyond the reasonable control of the permittee. An upset does not include noncompliance to the extent caused by operational error, improperly designed treatment facilities, inadequate treatment facilities, lack of preventive maintenance, or careless or improper operation.

CC. "Wastewater" means industrial wastewater. Industrial wastewater is wastewater generated from a federal facility, commercial or industrial process, including waste and wastewater from humans when generated at an industrial facility.

## PART II. Standard Conditions

A. Duty to comply

The permittee must comply with all conditions of the permit. Any permit noncompliance constitutes a violation of the Clean Water Act and the Pollution Control Act and is grounds for enforcement action; for permit termination, revocation and reissuance, or modification; or denial of a permit renewal application. The Department's approval of wastewater facility plans and specifications does not relieve the permittee of responsibility to meet permit limits.

1. The permittee shall comply with effluent standards or prohibitions established under section 307(a) of the Clean Water Act for toxic pollutants and with standards for sewage sludge use or disposal established under section 405(d) of the CWA within the time provided in the regulations that establish these standards or prohibitions or standards for sewage sludge use or disposal, even if the permit has not yet been modified to incorporate the requirement.

2. Failure to comply with permit conditions or the provisions of this permit may subject the permittee to civil penalties under S.C. Code Section 48-1-330 or criminal sanctions under S.C. Code Section 48-1-320. Sanctions for violations of the Federal Clean Water Act may be imposed in accordance with the provisions of 40 CFR Part 122.41(a)(2) and (3).

3. A person who violates any provision of this permit, a term, condition or schedule of compliance contained within this NPDES permit, or the State law is subject to the actions defined in the State law.

B. Duty to reapply

If the permittee wishes to continue an activity regulated by this permit after the expiration date of this permit, the permittee must apply for and obtain a new permit. A permittee with a currently effective permit shall submit a new application 180 days before the existing permit expires, unless permission for a later date has been granted by the Department. The Department shall not grant permission for applications to be submitted later than the expiration date of the existing permit.

C. Need to halt or reduce activity not a defense

It shall not be a defense for a permittee in an enforcement action that it would have been necessary to halt or reduce the permitted activity in order to maintain compliance with the conditions of this permit.

D. Duty to mitigate

The permittee shall take all reasonable steps to minimize or prevent any discharge or sludge use or disposal in violation of this permit which has a reasonable likelihood of adversely affecting human health or the environment.

E. Proper operation and maintenance

1. The permittee shall at all times properly operate and maintain in good working order and operate as efficiently as possible all facilities and systems of treatment and control (and related appurtenances) which are installed or used by the permittee to achieve compliance with the terms and conditions of this permit. Proper operation and maintenance includes effective performance based on design facility removals, adequate funding, adequate operator staffing and training and also includes adequate laboratory controls and appropriate quality assurance procedures. This provision requires the operation of back-up or auxiliary facilities or similar systems which are installed by a permittee only when the operation is necessary to achieve compliance with the conditions of the permit.

2. Power Failures. In order to maintain compliance with effluent limitations and prohibitions of this permit, the permittee shall either:

   a. provide an alternative power source sufficient to operate the wastewater control facilities;

   b. or have a plan of operation which will halt, reduce, or otherwise control production and/or all discharges upon the reduction, loss, or failure of the primary source of power to the wastewater control facilities.

3. The permittee shall develop and maintain at the facility a complete Operations and Maintenance Manual for the waste treatment facilities and/or land application system. The manual shall be made available for on-site review during normal working hours. The manual shall contain operation and maintenance instructions for all equipment and appurtenances associated with the waste treatment facilities and land application system. The manual shall contain a general description of the treatment process(es), the operational procedures to meet the requirements of E.1 above, and the corrective action to be taken should operating difficulties be encountered.

4. The permittee shall provide for the performance of weekly treatment facility inspections by a certified operator of the appropriate grade as defined in Part V.E.3 of this permit. The Department made exceptions to the daily operator requirement in accordance with R.61-9.122.41(e)(3)(ii). The inspections shall include, but should not necessarily be limited to, areas which require visual observation to determine efficient operation and for which immediate corrective measures can be taken using the O & M manual as a guide. All inspections shall be recorded and shall include the date, time, and name of the person making the inspection, corrective measures taken, and routine equipment maintenance, repair, or replacement performed. The permittee shall maintain all records of inspections at the permitted facility as required by the permit, and the records shall be made available for on-site review during normal working hours.

5. The name and grade of the operator of record shall be submitted to DHEC/Bureau of Water/Water Enforcement Division prior to placing the facility into operation. A roster of operators associated with the facility's operation and their certification grades shall also be submitted with the name of the "operator-in-charge." Any changes in operator or operators shall be submitted to the Department as they occur.

F. Permit actions

This permit may be modified, revoked and reissued, or terminated for cause. The filing of a request by the permittee for a permit modification, revocation and reissuance, or termination, or a notification of planned changes or anticipated noncompliance does not stay any permit condition.

G. Property rights

This permit does not convey any property rights of any sort, or any exclusive privilege nor does it authorize any injury to persons or property or invasion of other private rights, or any infringement of State or local law or regulations.

H. Duty to provide information

The permittee shall furnish to the Department, within a reasonable time, any information which the Department may request to determine whether cause exists for modifying, revoking and reissuing, or terminating this permit or to determine compliance with this permit. The permittee shall also furnish to the Department upon request, copies of records required to be kept by this permit.

I. Inspection and entry

The permittee shall allow the Department, or an authorized representative (including an authorized contractor acting as a representative of the Department), upon presentation of credentials and other documents as may be required by law, to:

1. Enter upon the permittee's premises where a regulated facility or activity is located or conducted, or where records must be kept under the conditions of this permit;

2. Have access to and copy, at reasonable times, any records that must be kept under the conditions of this permit;

3. Inspect at reasonable times any facilities, equipment (including monitoring and control equipment), practices, or operations regulated or required under this permit; and

4. Sample or monitor at reasonable times, for the purposes of assuring permit compliance or as otherwise authorized by the Clean Water Act and Pollution Control Act, any substances or parameters at any location.

J. Monitoring and records

1. a. (1) Samples and measurements taken for the purpose of monitoring shall be representative of the monitored activity.

(2) Samples shall be reasonably distributed in time, while maintaining representative sampling.

(3) No analysis, which is otherwise valid, shall be terminated for the purpose of preventing the analysis from showing a permit or water quality violation.

b. Flow Measurements.

(1) Where primary flow meters are required, appropriate flow measurement devices and methods consistent with accepted scientific practices shall be present and used to ensure the accuracy and reliability of measurements of the volume of monitored discharges. The devices shall be installed,

calibrated and maintained to ensure that the accuracy of the measurements are consistent with the accepted capability of that type of device. Devices selected shall be capable of measuring flows with a maximum deviation of less than 10% from the true discharge rates throughout the range of expected discharge volumes. The primary flow device, where required, must be accessible to the use of a continuous flow recorder.

(2) Where permits require an estimate of flow, the permittee shall maintain at the permitted facility a record of the method(s) used in estimating the discharge flow (e.g., pump curves, production charts, water use records) for the outfall(s) designated on limits pages to monitor flow by an estimate.

(3) Records of any necessary calibrations must be kept.

2. Except for records of monitoring information required by this permit related to the permittee's sewage sludge use and disposal activities, which shall be retained for a period of at least five years (or longer as required by R.61-9.503 or R.61-9.504), the permittee shall retain records of all monitoring information, including all calibration and maintenance records and all original strip chart recordings for continuous monitoring instrumentation, copies of all reports required by this permit, and records of all data used to complete the application for this permit, for a period of at least 3 years from the date of the sample, measurement, report or application. This period may be extended by request of the Department at any time.

3. Records of monitoring information shall include:

   a. The date, exact place, and time of sampling or measurements;

   b. The individual(s) who performed the sampling or measurements;

   c. The date(s) analyses were performed;

   d. The individual(s) who performed the analyses;

   e. The analytical techniques or methods used; and

   f. The results of such analyses.

4. a. Analyses for required monitoring must be conducted according to test procedures approved under 40 CFR Part 136, equivalent test procedures approved by DHEC's Division of Laboratory Certification or other test procedures that have been specified in the permit.

   In the case of sludge use or disposal, analysis for required monitoring must be conducted according to test procedures approved under 40 CFR Part 136, test procedures specified in R.61-9.503 or R.61-9.504, equivalent test procedures approved by DHEC's Division of Laboratory Certification or other test procedures that have been specified in the permit.

   b. Unless addressed elsewhere in this permit, the permittee shall use a sufficiently sensitive analytical method that achieves a value below the derived permit limit stated in Part III. If more than one method of analysis is approved for use, the Department recommends for reasonable potential determinations that the permittee use the method having the lowest practical quantitation limit (PQL) unless otherwise

specified in Part V of the permit. For the purposes of reporting analytical data on the Discharge Monitoring Report (DMR):

(1) Analytical results below the PQL conducted using a method in accordance with Part II.J.4.a above shall be reported as zero (0). Zero (0) shall also be used to average results which are below the PQL. When zero (0) is reported or used to average results, the permittee shall report, in the "Comment Section" or in an attachment to the DMR, the analytical method used, the PQL achieved, and the number of times results below the PQL were reported as zero (0).

(2) Analytical results above the PQL conducted using a method in accordance with Part II.J.4.a shall be reported as the value achieved. When averaging results using a value containing a "less than," the average shall be calculated using the value and reported as "less than" the average of all results collected.

(3) Mass values shall be calculated using the flow taken at the time of the sample and either the concentration value actually achieved or the value as determined from the procedures in (1) or (2) above, as appropriate.

5. The PCA provides that any person who falsifies, tampers with, or knowingly renders inaccurate any monitoring device or method required to be maintained under this permit shall, upon conviction, be punished by a fine of not more than $25,000 or by imprisonment for not more than 2 years, or both. If a conviction of a person is for a violation committed after a first conviction of such person under this paragraph, punishment provided by the Clean Water Act is also by imprisonment of not more than 4 years.

K. Signatory requirement.

1. All applications, reports, or information submitted to the Department shall be signed and certified.

a. Applications. All permit applications shall be signed as follows:

(1) For a corporation: by a responsible corporate officer. For the purpose of this section, a responsible corporate officer means:

(a) A president, secretary, treasurer, or vice-president of the corporation in charge of a principal business function, or any other person who performs similar policy or decision-making functions for the corporation, or

(b) The manager of one or more manufacturing, production, or operating facilities, provided the manager is authorized to make management decisions which govern the operation of the regulated facility including having the explicit or implicit duty of making major capital investment recommendations, and initiating and directing other comprehensive measures to assure long term environmental compliance with environmental laws and regulations; the manager can ensure that the necessary systems are established or actions taken to gather complete and accurate information for permit application requirements; and where authority to sign documents has been assigned or delegated to the manager in accordance with corporate procedures.

(2) For a partnership or sole proprietorship: by a general partner or the proprietor, respectively; or

(3) For a municipality, State, Federal, or other public agency or public facility: By either a principal executive officer, mayor, or other duly authorized employee or ranking elected official. For purposes of this section, a principal executive officer of a Federal agency includes:

(a) The chief executive officer of the agency, or

(b) A senior executive officer having responsibility for the overall operations of a principal geographic unit of the agency (e.g., Regional Administrator, Region IV, EPA).

b. All reports required by permits, and other information requested by the Department, shall be signed by a person described in Part II.K.1.a of this section, or by a duly authorized representative of that person. A person is a duly authorized representative only if:

(1) The authorization is made in writing by a person described in Part II.K.1.a of this section;

(2) The authorization specifies either an individual or a position having responsibility for the overall operation of the regulated facility or activity such as the position of plant manager, operator of a well or a well field, superintendent, position of equivalent responsibility, or an individual or position having overall responsibility for environmental matters for the company. (A duly authorized representative may thus be either a named individual or any individual occupying a named position.) and,

(3) The written authorization is submitted to the Department.

c. Changes to authorization. If an authorization under Part II.K.1.b of this section is no longer accurate because a different individual or position has responsibility for the overall operation of the facility, a new authorization satisfying the requirements of Part II.K.1.b of this section must be submitted to the Department prior to or together with any reports, information, or applications to be signed by an authorized representative.

d. Certification. Any person signing a document under Part II.K.1.a or b of this section shall make the following certification: "I certify under penalty of law that this document and all attachments were prepared under my direction or supervision in accordance with a system designed to assure that qualified personnel properly gather and evaluate the information submitted. Based on my inquiry of the person or persons who manage the system, or those persons directly responsible for gathering the information, the information submitted is, to the best of my knowledge and belief, true, accurate, and complete. I am aware that there are significant penalties for submitting false information, including the possibility of fine and imprisonment for knowing violations."

2. The PCA provides that any person who knowingly makes any false statement, representation, or certification in any record or other document submitted or required to be maintained under this permit, including monitoring reports or reports of compliance or non-compliance shall, upon conviction, be punished by a fine of not more than $25,000 per violation, or by imprisonment for not more than two years per violation, or by both.

L. Reporting requirements

1. Planned changes.

The permittee shall give written notice to DHEC/Bureau of Water/Industrial, Agricultural and Storm Water Permitting Division as soon as possible of any planned physical alterations or additions to the permitted facility. Notice is required only when:

a. The alteration or addition to a permitted facility may meet one of the criteria for determining whether a facility is a new source in R 61-9.122.29(b); or

b. The alteration or addition could significantly change the nature or increase the quantity of pollutants discharged. This notification applies to pollutants which are subject neither to effluent limitations in the permit, nor to notification requirements under Part II.L.8 of this section.

c. The alteration or addition results in a significant change in the permittee's sewage sludge or industrial sludge use or disposal practices, and such alteration, addition, or change may justify the application of permit conditions that are different from or absent in the existing permit, including notification of additional use or disposal sites not reported during the permit application process or not reported pursuant to an approved land application plan (included in the NPDES permit directly or by reference);

2. Anticipated noncompliance.

The permittee shall give advance notice to the DHEC/Bureau of Water/Water Enforcement Division of any planned changes in the permitted facility or activity which may result in noncompliance with permit requirements.

3. Transfers.

This permit is not transferable to any person except after written notice to the DHEC/Bureau of Water/NPDES Administration. The Department may require modification or revocation and reissuance of the permit to change the name of permittee and incorporate such other requirements as may be necessary under the Pollution Control Act and the Clean Water Act.

a. Transfers by modification. Except as provided in paragraph b of this section, a permit may be transferred by the permittee to a new owner or operator only if the permit has been modified or revoked and reissued (under R.61-9.122.62(e)(2)), or a minor modification made (under R.61-9.122.63(d)), to identify the new permittee and incorporate such other requirements as may be necessary under CWA.

b. Other transfers. As an alternative to transfers under paragraph a of this section, any NPDES permit may be transferred to a new permittee if:

(1) The current permittee notifies the Department at least 30 days in advance of the proposed transfer date in Part II.L.3.b(2) of this section;

(2) The notice includes U.S. EPA NPDES Application Form 1 and a written agreement between the existing and new permittees containing a specific date for transfer of permit responsibility, coverage, and liability between them; and

(3) Permits are non-transferable except with prior consent of the Department. A modification under this section is a minor modification which does not require public notice.

4. Monitoring reports. Monitoring results shall be reported at the intervals specified elsewhere in this permit.

a. Monitoring results must be reported on a Discharge Monitoring Report (DMR) or forms provided or specified by the Department for reporting results of monitoring of sludge use or disposal practices including the following:

(1) Effluent Monitoring: Effluent monitoring results obtained at the required frequency shall be reported on a Discharge Monitoring Report Form (EPA Form 3320-1). The DMR is due postmarked no later than the 28th day of the month following the end of the monitoring period. One original and one copy of the Discharge Monitoring Reports (DMRs) shall be submitted to:

S.C. Department of Health and Environmental Control
Bureau of Water/Compliance Assurance Division
Permit and Data Administration Section
2600 Bull Street
Columbia, South Carolina 29201

(2) Sludge, Biosolids and/or Soil Monitoring: Sludge, biosolids and/or soil monitoring results obtained at the required frequency shall be reported in a laboratory format postmarked no later than the 28th day of the month following the end of the monitoring period. Two copies of these results shall be submitted to:

S.C. Department of Health and Environmental Control
Bureau of Water/Water Enforcement Division
Water Pollution Enforcement Section
2600 Bull Street
Columbia, South Carolina 29201

(3) All other reports required by this permit shall be submitted at the frequency specified elsewhere in the permit to:
S.C. Department of Health and Environmental Control
Bureau of Water/Water Enforcement Division
Water Pollution Enforcement Section
2600 Bull Street
Columbia, South Carolina 29201

b. If the permittee monitors any pollutant more frequently than required by the permit using test procedures approved under 40 CFR Part 136 or, in the case of sludge use or disposal, approved under 40 CFR Part 136 unless otherwise specified in R.61-9.503 or R.61-9.504, or as specified in the permit, all valid results of this monitoring shall be included in the calculation and reporting of the data submitted in the

DMR or sludge reporting form specified by the Department. The permittee has sole responsibility for scheduling analyses, other than for the sample date specified in Part V, so as to ensure there is sufficient opportunity to complete and report the required number of valid results for each monitoring period.

c. Calculations for all limitations which require averaging of measurements shall utilize an arithmetic mean unless otherwise specified by the Department in the permit.

5. Twenty-four hour reporting

a. The permittee shall report any non-compliance, which may endanger health or the environment. Any information shall be provided orally to local DHEC office within 24 hours from the time the permittee becomes aware of the circumstances. During normal working hours call:

| County | EQC District | Phone No. |
|---|---|---|
| Anderson, Oconee | Appalachia I | 864-260-5569 |
| Greenville, Pickens | Appalachia II | 864-241-1090 |
| Cherokee, Spartanburg, Union | Appalachia III | 864-596-3800 |
| Chester, Lancaster, York | Catawba | 803-285-7461 |
| Fairfield, Lexington, Newberry, Richland | Central Midlands | 803-896-0620 |
| Aiken, Allendale, Bamberg, Barnwell, Calhoun, Orangeburg | Edisto Savannah | 803-641-7670 |
| Beaufort, Colleton, Hampton, Jasper | Low Country | 843-846-1030 |
| Chesterfield, Darlington, Dillon, Florence, Marion, Marlboro | Pee Dee | 843-661-4825 |
| Berkeley, Charleston, Dorchester | Trident | 843-740-1590 |
| Abbeville, Edgefield, Greenwood, Laurens, McCormick, Saluda | Upper Savannah | 864-223-0333 |
| Georgetown, Horry, Williamsburg | Waccamaw | 843-238-4378 |
| Clarendon, Kershaw, Lee, Sumter | Wateree | 803-778-1531 |

*After-hour reporting should be made to the 24-Hour Emergency Response telephone number 803-253-6488 or 1-888-481-0125 outside of the Columbia area.

A written submission shall also be provided to the address in Part II.L.4.a(4) within 5 days of the time the permittee becomes aware of the circumstances. The written submission shall contain a description of

the noncompliance and its cause; the period of noncompliance, including exact dates and times, and if the noncompliance has not been corrected, the anticipated time it is expected to continue; and steps taken or planned to reduce, eliminate, and prevent reoccurrence of the noncompliance.

b. The following shall be included as information which must be reported within 24 hours under this paragraph.

(1) Any unanticipated bypass which exceeds any effluent limitation in the permit. (See R.61-9.122.44(g)).

(2) Any upset which exceeds any effluent limitation in the permit.

(3) Violation of a maximum daily discharge limitation for any of the pollutants listed by the Department in the permit to be reported within 24 hours (See R 61-9.122.44(g)). If the permit contains maximum limitations for any of the pollutants listed below, a violation of the maximum limitations shall be reported orally to the DHEC/Bureau of Water/Water Enforcement Division within 24 hours or the next business day.

(a) Whole Effluent Toxicity (WET),
(b) tributyl tin (TBT), and
(c) any of the following bioaccumulative pollutants:

| | |
|---|---|
| $\alpha$ BHC | Mercury |
| $\beta$ BHC | Mirex |
| $\delta$ BHC (Lindane) | Octachlorostyrene |
| BHC | PCBs |
| Chlordane | Pentachlorobenzene |
| DDD | Photomirex |
| DDE | 1,2,3,4-Tetrachlorobenzene |
| DDT | 1,2,4,5-Tetrachlorobenzene |
| Dieldrin | 2,3,7,8-TCDD |
| Hexachlorobenzene | Toxaphene |
| Hexachlorobutadiene | |

c. The Department may waive the written report on a case-by-case basis for reports under Part II.L.5.b of this section if the oral report has been received within 24 hours.

6. Other noncompliance.

The permittee shall report all instances of noncompliance not reported under Part II.L.4 and 5 of this section and Part IV at the time monitoring reports are submitted. The reports shall contain the information listed in Part II.L.5 of this section.

7. Other information.

Where the permittee becomes aware that it failed to submit any relevant facts in a permit application, or submitted incorrect information in a permit application or in any report to the Department, it shall promptly submit such facts or information to the Industrial, Agricultural and Storm Water Permitting Division. This

information may result in permit modification, revocation and reissuance, or termination in accordance with Regulation 61-9.

8. Existing manufacturing, commercial, mining, and silvicultural dischargers.

In addition to the reporting requirements under Part II.L.1-7 of this section, all existing manufacturing, commercial, mining, and silvicultural dischargers must notify the DHEC/Bureau of Water/Water Enforcement Division of the Department as soon as they know or have reason to believe:

a. That any activity has occurred or will occur which would result in the discharge on a routine or frequent basis, of any toxic pollutant which is not limited in the permit, if that discharge will exceed the highest of the following "notification levels":

(1) One hundred micrograms per liter (100 μg/l);

(2) Two hundred micrograms per liter (200 μg/l) for acrolein and acrylonitrile; five hundred micrograms per liter (500 μg/l) for 2,4-dinitrophenol and for 2-methyl-4,6-dinitrophenol; and one milligram per liter (1 mg/l) for antimony;

(3) Five (5) times the maximum concentration value reported for that pollutant in the permit application; or

(4) The level established by the Department in accordance with section R.61-9.122.44(f).

b. That any activity has occurred or will occur which would result in any discharge, on a non-routine or infrequent basis, of a toxic pollutant which is not limited in the permit, if that discharge will exceed in the highest of the following "notification levels":

(1) Five hundred micrograms per liter (500 μg/l);

(2) One milligram per liter (1 mg/l) for antimony;

(3) Ten (10) times the maximum concentration value reported for that pollutant in the permit application in accordance with R.61-9.122.21(g)(7).

(4) The level established by the Department in accordance with section R.61-9.122.44(f).

M. Bypass

1. Bypass not exceeding limitations. The permittee may allow any bypass to occur which does not cause effluent limitations to be exceeded but only if it also is for essential maintenance to assure efficient operation. These bypasses are not subject to the provisions of Part II.M.2 and 3 of this section.

2. Notice.
   a. Anticipated bypass. If the permittee knows in advance of the need for a bypass, it shall submit prior notice, if possible, at least ten days before the date of the bypass to the DHEC/Bureau of Water/ Industrial, Agricultural and Storm Water Permitting Division.

b. Unanticipated bypass. The permittee shall submit notice of an unanticipated bypass as required in Part II.L.5 of this section.

3. Prohibition of bypass

a. Bypass is prohibited, and the Department may take enforcement action against a permittee for bypass, unless:

(1) Bypass was unavoidable to prevent loss of life, personal injury, or severe property damage;

(2) There were no feasible alternatives to the bypass, such as the use of auxiliary treatment facilities, retention of untreated wastes, or maintenance during normal periods of equipment downtime. This condition is not satisfied if adequate back-up equipment should have been installed in the exercise of reasonable engineering judgment to prevent a bypass which occurred during normal periods of equipment downtime or preventive maintenance; and

(3) The permittee submitted notices as required under Part II.M.2 of this section.

b. The Department may approve an anticipated bypass, after considering its adverse effects, if the Department determines that it will meet the three conditions listed above in Part II.M.3.a of this section.

N. Upset

1. Effect of an upset. An upset constitutes an affirmative defense to an action brought for noncompliance with such technology based permit effluent limitations if the requirements of Part II.N.2 of this section are met. No determination made during administrative review of claims that noncompliance was caused by upset, and before an action for noncompliance, is final administrative action subject to judicial review.

2. Conditions necessary for a demonstration of upset. A permittee who wishes to establish the affirmative defense of upset shall demonstrate, through properly signed, contemporaneous operating logs, or other relevant evidence that:

a. An upset occurred and that the permittee can identify the cause(s) of the upset;

b. The permitted facility was at the time being properly operated; and

c. The permittee submitted notice of the upset as required in Part II.L.5.b(2) of this section.

d. The permittee complied with any remedial measures required under Part II.D of this section.

3. Burden of proof. In any enforcement proceeding, the permittee seeking to establish the occurrence of an upset has the burden of proof.

O. Misrepresentation of Information

1. Any person making application for a NPDES discharge permit or filing any record, report, or other document pursuant to a regulation of the Department, shall certify that all information contained in such document is true. All application facts certified to by the applicant shall be considered valid conditions of the permit issued pursuant to the application.

2. Any person who knowingly makes any false statement, representation, or certification in any application, record, report, or other documents filed with the Department pursuant to the State law, and the rules and regulations pursuant to that law, shall be deemed to have violated a permit condition and shall be subject to the penalties provided for pursuant to 48-1-320 or 48-1-330.

## Part III. Limitations and Monitoring Requirements

A. Effluent Limitations and Monitoring Requirements

1. Outfall 001/Interim Limits

a. During the period beginning on the effective date of this permit and lasting through July 31, 2007, the permittee is authorized to discharge from outfall serial number 001: Storm water runoff from sub-watersheds 101, 102, 103, 105, 106, 107, 109, 111, 112, 115B, 116 and 121 and groundwater from French drains.

Such discharge shall be limited and monitored by the permittee as specified below:

| EFFLUENT CHARACTERISTICS | DISCHARGE LIMITATIONS | | | | MONITORING REQUIREMENTS | |
|---|---|---|---|---|---|---|
| | Mass | | Concentration | | | |
| | Monthly Average | Daily Maximum | Monthly Average | Daily Maximum | Sampling Frequency | Sample Type |
| Flow | MR[1], MGD | MR[1], MGD | - | - | 1/Month | Instantaneous[2] |
| pH | - | - | Min MR[1] su, Max MR[1] su[3] | | 1/Month | Grab |
| Total Suspended Solids | - | - | MR[1] mg/l | MR[1] mg/l | 1/Month | Grab |
| Total Arsenic[4] | - | - | MR[1] µg/l | MR[1] µg/l | 1/Month | Grab |
| Total Cadmium[4] | - | - | MR[1] µg/l | MR[1] µg/l | 1/Month | Grab |
| Total Lead[4] | - | - | MR[1] µg/l | MR[1] µg/l | 1/Month | Grab |
| Total Mercury[4] | - | - | MR[1] µg/l | MR[1] µg/l | 1/Month | Grab |
| Total Silver[4] | - | - | MR[1] µg/l | MR[1] µg/l | 1/Month | Grab |
| Chlordane[4] | - | - | MR[1] µg/l | MR[1] µg/l | 1/Month | Grab |
| Heptachlor[4] | - | - | MR[1] µg/l | MR[1] µg/l | 1/Month | Grab |
| Toxaphene[4] | - | - | MR[1] µg/l | MR[1] µg/l | 1/Month | Grab |
| Endrin[4] | - | - | MR[1] µg/l | MR[1] µg/l | 1/Month | Grab |

Outfall 001/Interim Limits Con't

| EFFLUENT CHARACTERISTICS | DISCHARGE LIMITATIONS | | | | MONITORING REQUIREMENTS | |
|---|---|---|---|---|---|---|
| | Mass | | Concentration | | | |
| | Monthly Average | Daily Maximum | Monthly Average | Daily Maximum | Sampling Frequency | Sample Type |
| Lindane[4] | - | - | MR[1] µg/l | MR[1] µg/l | 1/Month | Grab |
| Methoxychlor[4] | - | - | MR[1] µg/l | MR[1] µg/l | 1/Month | Grab |
| 2,4-Dichlorophenoxyacetic acid[4] | - | - | MR[1] µg/l | MR[1] µg/l | 1/Month | Grab |
| 2,4,5-Trichlorophenoxyacetic acid[4] | - | - | MR[1] µg/l | MR[1] µg/l | 1/Month | Grab |
| | | | | | | |

[1]MR: Monitor and Report
[2]See Part II.J.1
[3]See Part I.Q.
[4]See Part V.A.4.

Samples taken in compliance with the monitoring requirements specified above shall be taken at the following location(s): after treatment in Pond A but prior to mixing with the receiving stream. All samples shall be taken during the occurrence of a discharge from the outfall structure, but need not be more than once per month.

Outfall 001/Final Limits

b. During the period beginning on or before August 1, 2007 and lasting through the expiration date, the permittee is authorized to discharge from outfall serial number 001: Storm water runoff from sub-watersheds 101, 102, 103, 105, 106, 107, 109, 111, 112, 115B, 116 and 121and groundwater from French drains.

Such discharge shall be limited and monitored by the permittee as specified below:

| EFFLUENT CHARACTERISTICS | DISCHARGE LIMITATIONS | | | | MONITORING REQUIREMENTS | |
|---|---|---|---|---|---|---|
| | Mass | | Concentration | | | |
| | Monthly Average | Daily Maximum | Monthly Average | Daily Maximum | Sampling Frequency | Sample Type |
| Flow | MR[1], MGD | MR[1], MGD | - | - | 1/Month | Instantaneous[2] |
| pH | - | - | Min MR[1] su, Max MR[1] su[3] | | 1/Month | Grab |
| Total Suspended Solids | - | - | MR[1] mg/l | MR[1] mg/l | 1/Month | Grab |
| Total Arsenic[4] | - | - | MR[1] µg/l | MR[1] µg/l | 1/Month | Grab |
| Total Cadmium[4] | - | - | 0.34 µg/l | 1.9 µg/l | 1/Month | Grab |
| Total Lead[4] | - | - | 3.4 µg/l | 88 µg/l | 1/Month | Grab |
| Total Mercury[4] | - | - | MR[1] µg/l | MR[1] µg/l | 1/Month | Grab |
| Total Silver[4] | - | - | MR[1] µg/l | 0.19 µg/l | 1/Month | Grab |
| Chlordane[4] | - | - | MR[1] µg/l | MR[1] µg/l | 1/Month | Grab |
| Heptachlor[4] | - | - | MR[1] µg/l | MR[1] µg/l | 1/Month | Grab |
| Toxaphene[4] | - | - | MR[1] µg/l | MR[1] µg/l | 1/Month | Grab |
| Endrin[4] | - | - | MR[1] µg/l | MR[1] µg/l | 1/Month | Grab |

Outfall 001/Final Limits/ Con't

| EFFLUENT CHARACTERISTICS | DISCHARGE LIMITATIONS | | | | MONITORING REQUIREMENTS | |
|---|---|---|---|---|---|---|
| | Mass | | Concentration | | | |
| | Monthly Average | Daily Maximum | Monthly Average | Daily Maximum | Sampling Frequency | Sample Type |
| Lindane[4] | - | - | MR[1] µg/l | MR[1] µg/l | 1/Month | Grab |
| Methoxychlor[4] | - | - | MR[1] µg/l | MR[1] µg/l | 1/Month | Grab |
| 2,4-Dichlorophenoxyacetic acid[4] | - | - | MR[1] µg/l | MR[1] µg/l | 1/Month | Grab |
| 2,4,5-Trichlorophenoxyacetic acid[4] | - | - | MR[1] µg/l | MR[1] µg/l | 1/Month | Grab |
| | | | | | | |

[1]MR: Monitor and Report
[2]See Part II.J.1
[3]See Part I.Q.
[4]See Part V.A.4

Samples taken in compliance with the monitoring requirements specified above shall be taken at the following location(s): after treatment in Pond A but prior to mixing with the receiving stream. All samples shall be taken during the occurrence of a discharge from the outfall structure, but need not be more than once per month.

2. Outfall 01A/Final Limits

a. During the period beginning on the effective date of this permit and lasting through the expiration date, the permittee is authorized to discharge from outfall serial number 01A: Treated groundwater from French drains and treated storm water.

Such discharge shall be limited and monitored by the permittee as specified below:

| EFFLUENT CHARACTERISTICS | DISCHARGE LIMITATIONS | | | | MONITORING REQUIREMENTS | |
|---|---|---|---|---|---|---|
| | Mass | | Concentration | | | |
| | Monthly Average | Daily Maximum | Monthly Average | Daily Maximum | Sampling Frequency | Sample Type |
| Flow | MR[1], MGD | MR[1], MGD | - | - | 1/Month | Estimate[2] |
| Tetrachloroethylene | - | - | MR[1] µg/l | 17 µg/l | 1/Month | Grab |

[1]MR: Monitor and Report

REPLACED 7/29/05

Samples taken in compliance with the monitoring requirements specified above shall be taken at the following location(s): after treatment in the air stripper but prior to mixing with any other waste streams.

2. Outfall 01A/Final Limits

a. During the period beginning on the effective date of this permit and lasting through the expiration date, the permittee is authorized to discharge from outfall serial number 01A: Treated groundwater from French drains and treated storm water.

Such discharge shall be limited and monitored by the permittee as specified below:

| EFFLUENT CHARACTERISTICS | DISCHARGE LIMITATIONS | | | | MONITORING REQUIREMENTS | |
|---|---|---|---|---|---|---|
| | Mass | | Concentration | | | |
| | Monthly Average | Daily Maximum | Monthly Average | Daily Maximum | Sampling Frequency | Sample Type |
| Flow | MR[1], MGD | MR[1], MGD | - | - | 1/Month | Estimate[2] |
| Tetrachloroethylene | - | - | MR[1] µg/l | 17 µg/l | 1/Month | Grab |

[1]MR: Monitor and Report

Samples taken in compliance with the monitoring requirements specified above shall be taken at the following location(s): after treatment in the air stripper/aerated ponds but prior to mixing with any other waste streams.

Outfall 002/Final Limits

b. During the period beginning on the effective date of this permit and lasting through the expiration date, the permittee is authorized to discharge from outfall serial number 002: Storm water runoff from sub-watersheds 108, 114, 115A, 119 and 123 and groundwater from French drains.

Such discharge shall be limited and monitored by the permittee as specified below:

| EFFLUENT CHARACTERISTICS | DISCHARGE LIMITATIONS | | | | MONITORING REQUIREMENTS | |
|---|---|---|---|---|---|---|
| | Mass | | Concentration | | | |
| | Monthly Average | Daily Maximum | Monthly Average | Daily Maximum | Sampling Frequency | Sample Type |
| Flow | MR[1], MGD | MR[1], MGD | - | - | 1/Month | Instantaneous[2] |
| PH | - | - | Min MR[1] su, Max MR[1] su[3] | | 1/Month | Grab |
| Total Suspended Solids | - | - | MR[1] mg/l | MR[1] mg/l | 1/Month | Grab |
| Total Arsenic[4] | - | - | MR[1] µg/l | MR[1] µg/l | 1/Month | Grab |
| Total Cadmium[4] | - | - | MR[1] µg/l | MR[1] µg/l | 1/Month | Grab |
| Total Lead[4] | - | - | MR[1] µg/l | MR[1] µg/l | 1/Month | Grab |
| Total Mercury[4] | - | - | MR[1] µg/l | MR[1] µg/l | 1/Month | Grab |
| Total Silver[4] | - | - | MR[1] µg/l | MR[1] µg/l | 1/Month | Grab |
| Chlordane[4] | - | - | MR[1] µg/l | MR[1] µg/l | 1/Month | Grab |
| Heptachlor[4] | - | - | MR[1] µg/l | MR[1] µg/l | 1/Month | Grab |
| Toxaphene[4] | - | - | MR[1] µg/l | MR[1] µg/l | 1/Month | Grab |
| Endrin[4] | - | - | MR[1] µg/l | MR[1] µg/l | 1/Month | Grab |
| Lindane[4] | - | - | MR[1] µg/l | MR[1] µg/l | 1/Month | Grab |
| Methoxychlor[4] | - | - | MR[1] µg/l | MR[1] µg/l | 1/Month | Grab |
| 2,4-Dichlorophenoxyacetic acid[4] | - | - | MR[1] µg/l | MR[1] µg/l | 1/Month | Grab |
| 2,4,5-Trichlorophenoxyacetic acid[4] | - | - | MR[1] µg/l | MR[1] µg/l | 1/Month | Grab |

Outfall 002/Final Limits Con't

[1]MR: Monitor and Report
[2]See Part II.J.1
[3]See Part I.Q.
[4]See Part V.A.4

Samples taken in compliance with the monitoring requirements specified above shall be taken at the following location(s): after treatment in Pond B but prior to mixing with the receiving stream. All samples shall be taken during the occurrence of a discharge from the outfall structure, but need not be more than once per month.

3. Outfall 02A/Final Limits

a. During the period beginning on the effective date of this permit and lasting through the effective date of this permit, the permittee is authorized to discharge from outfall serial number 02A: Storm water runoff from sub-watershed 120 and off-site runoff through Touchberry Creek.

Such discharge shall be limited and monitored by the permittee as specified below:

| EFFLUENT CHARACTERISTICS | DISCHARGE LIMITATIONS | | | | MONITORING REQUIREMENTS | |
|---|---|---|---|---|---|---|
| | Mass | | Concentration | | | |
| | Monthly Average | Daily Maximum | Monthly Average | Daily Maximum | Sampling Frequency | Sample Type |
| Flow | MR[1], MGD | MR[1], MGD | - | - | 1/Quarter | Instantaneous[2] |
| PH | - | - | Min MR[1] su, Max MR[1] su[3] | | 1/Quarter | Grab |
| Total Suspended Solids | - | - | MR[1] mg/l | MR[1] mg/l | 1/Quarter | Grab |
| Total Arsenic[4] | - | - | MR[1] µg/l | MR[1] µg/l | 1/Quarter | Grab |
| Total Cadmium[4] | - | - | MR[1] µg/l | MR[1] µg/l | 1/Quarter | Grab |
| Total Lead[4] | - | - | MR[1] µg/l | MR[1] µg/l | 1/Quarter | Grab |
| Total Mercury[4] | - | - | MR[1] µg/l | MR[1] µg/l | 1/Quarter | Grab |
| Total Silver[4] | - | - | MR[1] µg/l | MR[1] µg/l | 1/Quarter | Grab |
| Chlordane[4] | - | - | MR[1] µg/l | MR[1] µg/l | 1/Quarter | Grab |
| Heptachlor[4] | - | - | MR[1] µg/l | MR[1] µg/l | 1/Quarter | Grab |
| Toxaphene[4] | - | - | MR[1] µg/l | MR[1] µg/l | 1/Quarter | Grab |
| Endrin[4] | - | - | MR[1] µg/l | MR[1] µg/l | 1/Quarter | Grab |

Outfall 02A/Final Limits Con't

| EFFLUENT CHARACTERISTICS | DISCHARGE LIMITATIONS | | | | MONITORING REQUIREMENTS | |
|---|---|---|---|---|---|---|
| | Mass | | Concentration | | | |
| | Monthly Average | Daily Maximum | Monthly Average | Daily Maximum | Sampling Frequency | Sample Type |
| Lindane[4] | - | - | MR[1] µg/l | MR[1] µg/l | 1/Quarter | Grab |
| Methoxychlor[4] | - | - | MR[1] µg/l | MR[1] µg/l | 1/Quarter | Grab |
| 2,4-Dichlorophenoxyacetic acid[4] | - | - | MR[1] µg/l | MR[1] µg/l | 1/Quarter | Grab |
| 2,4,5-Trichlorophenoxyacetic acid[4] | - | - | MR[1] µg/l | MR[1] µg/l | 1/Quarter | Grab |

[1]MR: Monitor and Report
[2]See Part II.J.1
[3]See Part I.Q.
[4]See Part V.A.4

Samples taken in compliance with the monitoring requirements specified above shall be taken at the following location(s): at or near the outfall, but prior to mixing with storm water from sub-watersheds 117 and 118.

B. Whole Effluent Toxicity and Other Biological Limitations and Monitoring Requirements

1. See Part V.B.1.

C. Groundwater Monitoring Requirements

N/A

D. Sludge Monitoring Requirements

N/A

E. Soil Monitoring Requirements

N/A

**Part IV. Schedule of Compliance**

A. Schedule(s)

1. For the final limits at Outfalls 001, 002, and 02A:

   a. On or before August 1, 2005, the permittee shall submit three (3) copies of a Preliminary Engineering Report (PER), in accordance with South Carolina Regulation 61-67 (*Standards for Wastewater Facility Construction*), which describes how the facility will attain compliance with the limitations set forth for in the final limits for discharges 001, 002 and 02A. The limit may be met simply using the BMPs and/or other measures being used to remove or reduce pollutant concentrations as required in Part V of this permit.

   The permittee has notified the Department that the landfill closure will be completed within the next twenty-four months. In lieu of the PER, the permittee may submit a letter detailing the close out schedule and any remaining wastewater or storm water discharges that may require permitting after closure.

   b. On or before August 1, 2006 and after receiving PER approval from the Department, the permittee shall submit three (3) copies of the Final Engineering Report (FER), three (3) complete copies of the Construction Permit Application for Wastewater Treatment facilities, and three (3) copies of the plans and specifications along with supporting calculations, in accordance with South Carolina Regulation 61-67 describing how the facility will attain compliance with the final limitations set forth for discharges 001, 002 and 02A or the permittee may submit a progress report on the close out of the facility. If the information supplied in the PER required above does not require a construction permit, this item becomes void.

   c. On or before August 1, 2007, the permittee shall comply with the final limitations of this permit.

   d. Submit interim reports of progress describing the events taking place to remove or reduce pollutant concentrations shall be submitted to the Department every nine (9) months after the permit effective date until final limits are complied with. The last date may not be a full nine months.

B. Reports of compliance or noncompliance with, or any progress reports on, interim and final requirements contained in any compliance schedule of this permit shall be submitted no later than 14 days following each scheduled date.

## Part V. Other Requirements

A. Effluent Requirements

1. There shall be no discharge of floating solids or visible foam in other than trace amounts, nor shall the effluent cause a visible sheen on the receiving waters.

2. Pinewood Site Custodial Trust has permission to transport and dispose of contaminated storm water and groundwater to the Berkeley County Water & Sanitation Authority's Goose Creek Lower Berkeley Regional Plant (NPDES Permit No. SC0046060). The permittee must notify the Department prior to discontinuing disposing contaminated storm water and groundwater to the above reference POTW in order to obtain approval for a new disposal site.

3. The permittee has received pilot study approval to treat contaminated groundwater from French drains located on site. Approval is valid until July 1, 2005 unless the permittee obtains a Permit To Construct for this WWTP prior to July 1, 2005. The concentration of tetrachloroethylene (PCE) in the air stripper effluent must not exceed 17 ppb. The treated effluent will be combined with the storm water entering treatment Pond A (Outfall 001). Quarterly reports of treatability data must be submitted until the pilot project is abandoned.

4. The permittee shall use a sufficiently sensitive analytical method that achieves a value below the derived permit limit stated in Part III. The Department recommends that the permittee use a method that will achieve the PQL specified below or a lower PQL. Use of the appropriate PQL may lend value in demonstration of "no reasonable potential" later based on the statistics used to determine reasonable potential. The permittee must use the PQL specified below or a lower PQL to show permit compliance where either

   a. the derived permit limit in Part III for the parameter of concern is at or below the PQL specified below, or

   b. Part III contains only monitoring and reporting (MR) for the parameter of concern.

| Parameter | Analytical Method | PQL |
|---|---|---|
| Total Arsenic | EPA Method 200.8 or 200.9<br>Standard method 3113B | 0.0050 mg/l |
| Total Cadmium | EPA Method 200.8 or 200.9<br>Standard method 3113B | 0.00010 mg/l |
| Total Lead | EPA Method 200.8 or 200.9<br>Standard method 3113B | 0.0020 mg/l |
| Total Silver | EPA Method 200.8 or 200.9<br>Standard Method 3113B | 0.0050 mg/l |
| Total Mercury | EPA Method 1669/1631C | 0.0005 ug/l |

| | | |
|---|---|---|
| Chlordane | EPA Method 608 or 8081A | 0.50 µg/l |
| Heptachlor | EPA Method 608 or 8081A | 0.050 µg/l |
| Toxaphene | EPA Method 608 or 8081A | 0.50 µg/l |
| Endrin | EPA Method 608 or 8081A | 0.050 µg/l |
| Lindane | EPA Method 608 or 8081A | 0.050 µg/l |
| Methoxychlor | EPA Method 608 or 8081A | 0.50 µg/l |
| Tetrachloroethylene (PCE) | EPA Method 624, 1624B or 8260B | 2.0 µg/l |
| 2,4-Dichlorophenoxyacetic acid | EPA Method 6640B or 8151A | 0.050 µg/l |
| 2,4,5-Trichlorophenoxyacetic acid | EPA Method 6640B or 8151A | 0.025 µg/l |

B. Whole Effluent Toxicity and Other Biological Requirements

1. Instream Macroinvertebrate Assessment

a. The permittee shall conduct an instream macroinvertebrate survey twice per year.

(1) Instream macroinvertebrate assessments are used to detect biological impacts due to point source discharges or to determine ambient instream conditions, including non-point source impacts. The permittee shall use the following documents as guidance for writing proposed biological studies:

(a) EPA publication entitled, "Revision to Rapid Bioassessment Protocols for Use in Streams and Rivers: Periphyton, Benthic Macroinvertebrates, and Fish," by Barbour M.T., J. Gerritsen, B.D. Snyder, and J.B. Stribling (EPA 841-B-99-002) and

(b) "South Carolina Department of Health and Environmental/Control Standard Operating and Quality Control Procedures for Macroinvertebrate Sampling," Water Monitoring, Assessment, and Protection Division, Aquatic Biology Section, Columbia, SC, SCDHEC Document #004-98.

(2) The assessments should be conducted during late summer (mid-August thru September) and late winter (February thru mid-March).

c. The results of the instream assessments must be submitted to the Department within 90 days after completion of the sampling.

C. Groundwater Requirements

N/A

D. Sludge Requirements

N/A

E. Other Conditions

1. The permittee shall maintain an all weather access road to the air stripper, storm water ponds and appurtenances at all times.

2. All waste oil and solid and hazardous waste shall be disposed of in accordance with the rules and regulations of SCDHEC's Bureau of Land & Waste Management.

3. The air stripper has been assigned a classification of Group I-PC (Physical/Chemical) in Permit to Construct No. 18,920-IW issued by the Department on February 11, 2005. This classification corresponds to an operator with a Grade D-PC.

4. In order to eliminate sampling at Outfall 02A, the permittee may choose to sample at a location prior to the point at which the flow from sub-watershed 120 or any other discharge generated on the landfill site combines with Touchberry Creek. If that sampling data shows that the water coming from off-site contains the same pollutants at the similar levels, sampling for those parameters may be discontinued for this outfall. If the decision is made to pursue this option,

   a. Prior to any off-site sampling, the permittee shall submit to the Department for approval
      (1) the location of the off-site sample point, including a map showing the location of the existing and proposed discharges and
      (2) a plan for timing of the sampling of the existing discharge and the proposed discharge which will take into account the time of travel between the two points and the size of the rain event needed to generate a discharge to make the best correlation between the two points.

   b. The permittee shall provide at least 10 samples spread over a full year from each sampling location. Any sampling conducted at Outfall 02A more frequently than required by Part III of this permit must be reported on the DMRs in accordance with Part II.L.4(b).

   c. Upon completion of the sampling, the permittee may submit the summarized data with a request for permit modification for those parameters that are present due to the off-site water.

   d. If this additional sampling is not provided or if it does not demonstrate that the pollutants come from off-site, then the final limits will go into effect after the time allowed in the schedule of compliance in Part IV of this permit.

   e. If the sampling data shows that sampling may be discontinued for any parameters or if the data shows that additional requirements are needed, this permit may be reopened to remove or add conditions.

F. Storm Water Related to Landfill Construction Activity

1. Storm Water Pollution Prevention Plan (SWPPP)

a. A SWPPP must be developed for all landfill closure construction activities. A qualified individual must prepare such SWPPP in accordance with good engineering practices. The SWPPP must be prepared, amended when necessary, certified, and stamped by a qualified individual who is licensed as follows:

Registered professional engineers as described in Title 40, Chapter 22;
Registered landscape architects as described in Title 40, Chapter 28, Section 10, item (b);
Tier B land surveyors as described in Title 40, Chapter 22; or
Federal government employees as described by Title 40, Chapter 22, Section 280(A)(3).

b. Contractors

(1) The SWPPP must clearly identify for each measure identified in the plan, the contractor(s) and/or subcontractor(s) that will implement the measure. All contractors and subcontractors identified in the plan must sign a copy of the certification statement below. All signed certifications must be included in the SWPPP.

(2) Certification Statement. All contractors and subcontractors whose activities at the landfill may impact storm water discharges or controls at the site along the duration of the landfill closure construction activities, shall sign a copy of the certification statement given below:

"I certify by my signature below that I have read and accept the terms and conditions of the Storm Water Pollution Prevention Plan (SWPPP) as required by this NPDES permit for which I have been contracted to perform construction-related professional services. I understand that I, and my company, as the case may be, are legally accountable to the SC Department of Health and Environmental Control (DHEC), under the authorities of the CWA and the SC Pollution Control Act, to ensure compliance with the terms and conditions of the SWPPP."

(3) The date of the signature, the title of the person providing the signature, and the name, address, and telephone number of the contracted firm, shall also be provided. In the event the SWPPP is amended, such amendments should be incorporated into the plan and the contractors and subcontractors should acknowledge by signature and date.

(4) Copies of all contractor certifications shall be retained with the SWPPP.

c. Contents of Plan. The SWPPP shall include the following items:

(1) Site Description. The SWPPP shall provide a description of pollutant sources and other information as indicated:

(a) Estimates of the total area of the site and the total area of the site that is expected to be disturbed by excavation, grading, or other construction activities; and

(b) A legible site map, showing the entire site, identifying:

(1) Direction(s) of storm water flow and approximate slopes anticipated after major grading activities;
(2) Areas of soil disturbance and areas that will not be disturbed;
(3) Locations of structural and nonstructural BMPs identified in the SWPPP;
(4) Locations where stabilization practices are expected to occur;
(5) Except for rolloffs, locations of off-site material, waste, borrow or construction equipment storage areas;
(6) Locations of all waters of the state of South Carolina (including wetlands);
(7) Locations where storm water discharges to a surface water; and
(8) Areas where final stabilization has been accomplished.

(2) Controls. The SWPPP shall include a description of all pollution control measures (i.e, BMPs) that will be implemented at the landfill related to construction activity. The plan will clearly describe for each major activity appropriate control measures and the general sequence during the construction process in which the measures will be implemented. The SWPPP shall include the following minimum components:

(a) A description of interim and permanent stabilization practices, including site-specific scheduling of the implementation of the practices. Site plans should ensure that disturbed portions of the site are stabilized. Stabilization practices may include: temporary seeding, permanent seeding, mulching, geotextiles, sod stabilization, vegetative buffer strips, protection of trees, preservation of mature vegetation, and other appropriate measures. A record of the dates when major grading activities occur, when construction activities temporarily or permanently cease on a portion of the site, and when stabilization measures are initiated shall be included in the plan. Stabilization measures shall be initiated as soon as practicable in portions of the site where construction activities have temporarily or permanently ceased

(b) A description of structural practices to divert flows from exposed soils, retain/detain flows or otherwise limit runoff and the discharge of pollutants from exposed areas of the site. Such practices may include silt fences, earth dikes, drainage swales, sediment traps, check dams, subsurface drains, pipe slope drains, level spreaders, storm drain inlet protection, rock outlet protection, reinforced soil retaining systems, gabions, and temporary or permanent sediment basins. Structural practices should be placed on upland soils to the degree attainable. The installation of these devices may be subject to Section 404 of the CWA.

(1) Sediment Basins: For common drainage locations that serve an area with 10 or more acres disturbed at one time, a temporary (or permanent) sediment basin that provides storage for a calculated volume of runoff from the drainage area from at least a 10-year, 24-hour storm, or equivalent control measures, must be provided where attainable until final stabilization of the site. Where no such calculation has been performed, a temporary (or permanent) sediment basin providing at least 3,600 cubic feet of storage per acre drained, or equivalent control measures, must be provided where attainable until final stabilization of the site. When computing the number of acres draining into a common location, it is not necessary to include flows from offsite areas and flows from on-site areas that are either undisturbed or

have undergone final stabilization where such flows are diverted around both the disturbed area and the sediment basin. In determining whether installing a sediment basin is attainable, factors such as site soils, slope, available area on-site, etc. shall be considered.

(2) For drainage locations that serve 10 or more disturbed acres at one time where a temporary sediment basin or equivalent controls are not attainable, smaller sediment basins and/or sediment traps should be used. At a minimum, silt fences, vegetative buffer strips, or equivalent sediment controls are required for all down slope boundaries (and for those side slope boundaries deemed appropriate as dictated by individual site conditions).

(3) For drainage locations that serve less than 10 acres, smaller sediment basins and/or sediment traps, silt fences or equivalent sediment controls are required for all sideslope and downslope boundaries of the construction area unless a sediment basin providing storage for 3,600 cubic feet of storage per acre drained is provided.

(4) Velocity dissipation devices shall be placed at discharge locations and along the length of any outfall channel as necessary to provide a non-erosive velocity flow from the structure to a water course so that the natural physical and biological characteristics and functions are maintained and protected (e.g. no significant changes in the hydrological regime of the receiving water).

(c) A description of measures that will be installed during the landfill closure construction to control pollutants in storm water discharges that will occur after construction operations have been completed. Structural measures should be placed on upland soils to the degree attainable. The installation of these devices may be subject to Section 404 of the CWA.

(d) Off-site vehicle tracking of sediments and the generation of dust shall be minimized.

(e) The plan shall address the proper application rates and methods for the use of fertilizers and pesticides at the construction site and set forth how these procedures will be implemented and enforced.

(f) If sediment escapes the construction site, off-site accumulations of sediment must be removed at a frequency sufficient to minimize off-site impacts unless DHEC agrees that it is appropriate to leave the off-site accumulations in place.

2. Maintenance of Controls

(a) All erosion and sediment control measures and other protective measures identified in the SWPPP must be maintained in effective operating condition. If site inspections identify Best Management Practices (BMPs) that are not operating effectively, maintenance must be performed as soon as possible and before the next storm event whenever practicable to maintain the continued effectiveness of storm water controls.

(b) If existing BMPs need to be modified or if additional BMPs are necessary for any reason, implementation must be completed before the next storm event whenever practicable. If implementation before the next storm event is impracticable, the situation must be documented in the SWPPP and alternative BMPs must be implemented as soon as possible.

(c) Sediment from sediment traps or sedimentation ponds must be removed as indicated in the SWPPP or when design capacity has been reduced by 50 percent, which ever comes first.

3. Other Applicable Programs

The SWPPP must be consistent with all applicable federal, state, or local requirements for soil and erosion control and storm water management, including updates to the SWPPP as necessary to reflect any revisions to applicable federal, state, or local requirements for soil and erosion control.

4. Inspections

(a) Inspections must be conducted at a minimum in accordance with one of the two schedules listed below. You must specify in your SWPPP which schedule you will be following.

(1) At least once every 7 calendar days, or
(2) At least once every 14 calendar days and within 24 hours of the end of a storm event of 0.5 inches or greater.

(b) Inspection frequency may be reduced to at least once every month if the entire site is temporarily stabilized.

(c) Inspections must be conducted by qualified personnel. "Qualified personnel" means a person(s) knowledgeable in the principles and practice of erosion and sediment controls who possesses the skills to assess conditions at the construction site that could impact storm water quality and to assess the effectiveness of any sediment and erosion control measures selected to control the quality of storm water discharges from the construction activity. This person must be either the preparer of the SWPPP or an individual who is under the direct supervision of the preparer of the approved SWPPP and who meets the requirements in this paragraph or an individual who has been certified under Clemson University's Certified Storm Water Construction Inspection Program. Inspections may also be conducted by a person with a registration equivalent to the registration of the preparer of the SWPPP and who meets the qualifications of this paragraph or an individual who is under the direct supervision of the equivalent person and who meets the requirements in this paragraph.

(d) Inspections must include all areas of the site disturbed by construction activity and areas used for storage of materials that are exposed to precipitation. Inspectors must look for evidence of, or the potential for, pollutants entering the storm water conveyance system. Sedimentation and erosion control measures identified in the SWPPP must be observed to ensure proper operation. Discharge locations must be inspected to ascertain whether erosion control measures are effective in preventing significant impacts to waters of the state of South Carolina, where accessible. Where discharge locations are inaccessible, nearby downstream locations must be inspected to the extent that such inspections are practicable. Locations where vehicles enter or exit the site must be inspected for

evidence of off-site sediment tracking.

(e) For each inspection required above, you must complete an inspection report. At a minimum, the inspection report must include:

(1) The inspection date;

(2) Names, titles, and, if not previously given in an inspection report, the qualifications of personnel making the inspection unless they have changed;

(3) Weather information for the period since the last inspection (or since commencement of construction activity if the first inspection) including a best estimate of the beginning of each storm event, duration of each storm event, approximate amount of rainfall for each storm event (in inches), and whether you know if any discharges occurred;

(4) Weather information and a description of any discharges occurring at the time of the inspection;

(5) Location(s) of discharges of sediment or other pollutants from the site;

(6) Location(s) of BMPs that need maintenance;

(7) Location(s) of BMPs that failed to operate as designed or proved inadequate for a particular location;

(8) Location(s) where additional BMPs are needed that did not exist at the time of inspection; and

(9) Corrective action required including any changes to the SWPPP necessary and implementation dates.

A record of each inspection and of any actions taken in accordance with this Part must be retained as part of the SWPPP for at least three years. The inspection reports must identify any incidents of non-compliance with the permit conditions. Where a report does not identify any incidents of non-compliance, the report must contain a certification that the construction areas are in compliance with the SWPPP and the permit. The report must be signed in accordance with §122.22 of SC Regulation 61-9.

(f) A quarterly report must be submitted which includes the following information, at a minimum:

(1) A summary of the results of the inspections conducted during the quarter;

(2) A listing of all deficiencies noted during inspections with the date the deficiency was noted;

(3) For each deficiency noted that required corrective action:

(a) A listing of the name(s), address(es), and telephone number(s) of the party or parties responsible; and
(b) A statement whether this deficiency was listed in the previous quarterly report;

(4) A listing of the corrective actions that were taken to remedy any deficiencies noted and the date the corrective actions were completed;

(5) A statement on whether or not the SWPPP was updated to deal with any deficiencies noted;

(6) A copy of each inspection conducted during the quarter attached in an appendix to the quarterly report; and

(7) A copy of the signed and dated certifications by all contractors involved in site landfill construction activities with each contractor's responsibilities indicated.

5. Maintaining an Updated SWPPP

(a) The SWPPP, including the site map, must be amended whenever there is a change in design, construction, operation, or maintenance at the site that has or could have a significant effect on the discharge of pollutants to the waters of the state of South Carolina that has not been previously addressed in the SWPPP.

(b) The SWPPP must be amended if, during inspections or investigations by site staff, or by local, state, or federal officials, it is determined that the SWPPP is ineffective in eliminating or significantly minimizing pollutants in storm water discharges from the construction site.

(c) Based on the results of an inspection, the SWPPP must be modified as necessary to include additional or modified BMPs designed to correct problems identified. Revisions to the SWPPP must be completed within seven (7) calendar days following the inspection. Implementation of these additional or modified BMPs must be accomplished as described in F.3 above.

6. Signature, Review and Making SWPPPs Available

(a) A copy of the SWPPP must be retained at the landfill until the date of final stabilization.

(b) SWPPPs must be made available upon request by EPA; DHEC; any local agency approving sediment and erosion plans, grading plans, or storm water management plans; and local government officials. The copy of the SWPPP that is required to be kept on-site or locally available must be made available, in its entirety, to DHEC or the EPA staff for review and copying at the time of an on-site inspection.

(c) All SWPPPs must be signed and certified in accordance with §122.22 of SC Regulation 61-9.

7. Final Stabilization

Where a site has been finally stabilized and all storm water discharges from landfill closure construction activities are eliminated, the permittee must submit a letter to the Department signed in accordance with §122.22 of SC Regulation 61-9. The letter shall include the following information:

(a) The NPDES Permit Number, Name of the Permittee and County of the Discharges,

(b) An indication of whether the storm water discharges associated with landfill closure construction activity have been eliminated; and

(c) A discussion of the remaining discharges to the permitted outfall structures.

For the purposes of this certification, elimination of storm water discharges associated with construction activity means that all disturbed soils at the landfill have been finally stabilized and temporary erosion and sediment control measures have been removed or will be removed at an appropriate time, or that all storm water discharges associated with landfill closure construction activities have otherwise been eliminated.

# Appendix 3.2-1
# Storm Water Modeling Results

Culvert Master

Pond Pack – 10 Year Event

Pond Pack – 25 Year Event

# Culvert Master

# Culvert Calculator Report
# J-13 (Existing)

Solve For: Discharge

| Culvert Summary | | | | | |
|---|---|---|---|---|---|
| Allowable HW Elevation | 133.19 | ft | Headwater Depth/Height | 1.00 | |
| Computed Headwater Elevation | 133.19 | ft | Discharge | 3.59 | cfs |
| Inlet Control HW Elev. | 133.07 | ft | Tailwater Elevation | 0.00 | ft |
| Outlet Control HW Elev. | 133.19 | ft | Control Type | Entrance Control | |

| Grades | | | | | |
|---|---|---|---|---|---|
| Upstream Invert | 131.94 | ft | Downstream Invert | 130.05 | ft |
| Length | 30.00 | ft | Constructed Slope | 0.063000 | ft/ft |

| Hydraulic Profile | | | | | |
|---|---|---|---|---|---|
| Profile | S2 | | Depth, Downstream | 0.41 | ft |
| Slope Type | Steep | | Normal Depth | 0.38 | ft |
| Flow Regime | Supercritical | | Critical Depth | 0.77 | ft |
| Velocity Downstream | 10.23 | ft/s | Critical Slope | 0.005491 | ft/ft |

| Section | | | | | |
|---|---|---|---|---|---|
| Section Shape | Circular | | Mannings Coefficient | 0.012 | |
| Section Material | Corrugated HDPE (Smooth Interior) | | Span | 1.25 | ft |
| Section Size | 15 inch | | Rise | 1.25 | ft |
| Number Sections | 1 | | | | |

| Outlet Control Properties | | | | | |
|---|---|---|---|---|---|
| Outlet Control HW Elev. | 133.19 | ft | Upstream Velocity Head | 0.32 | ft |
| Ke | 0.50 | | Entrance Loss | 0.16 | ft |

| Inlet Control Properties | | | | | |
|---|---|---|---|---|---|
| Inlet Control HW Elev. | 133.07 | ft | Flow Control | N/A | |
| Inlet Type | Square edge w/headwall | | Area Full | 1.2 | ft² |
| K | 0.00980 | | HDS 5 Chart | 1 | |
| M | 2.00000 | | HDS 5 Scale | 1 | |
| C | 0.03980 | | Equation Form | 1 | |
| Y | 0.67000 | | | | |

# Culvert Calculator Report
# J-17 (Existing)

Solve For: Discharge

| Culvert Summary | | | | | |
|---|---|---|---|---|---|
| Allowable HW Elevation | 137.00 | ft | Headwater Depth/Height | 1.00 | |
| Computed Headwater Elevation | 137.00 | ft | Discharge | 3.59 | cfs |
| Inlet Control HW Elev. | 136.91 | ft | Tailwater Elevation | 0.00 | ft |
| Outlet Control HW Elev. | 137.00 | ft | Control Type | Entrance Control | |

| Grades | | | | | |
|---|---|---|---|---|---|
| Upstream Invert | 135.75 | ft | Downstream Invert | 134.90 | ft |
| Length | 40.00 | ft | Constructed Slope | 0.021250 | ft/ft |

| Hydraulic Profile | | | | | |
|---|---|---|---|---|---|
| Profile | S2 | | Depth, Downstream | 0.53 | ft |
| Slope Type | Steep | | Normal Depth | 0.51 | ft |
| Flow Regime | Supercritical | | Critical Depth | 0.77 | ft |
| Velocity Downstream | 7.28 | ft/s | Critical Slope | 0.005491 | ft/ft |

| Section | | | | | |
|---|---|---|---|---|---|
| Section Shape | Circular | | Mannings Coefficient | 0.012 | |
| Section Material | Corrugated HDPE (Smooth Interior) | | Span | 1.25 | ft |
| Section Size | 15 inch | | Rise | 1.25 | ft |
| Number Sections | 1 | | | | |

| Outlet Control Properties | | | | | |
|---|---|---|---|---|---|
| Outlet Control HW Elev. | 137.00 | ft | Upstream Velocity Head | 0.32 | ft |
| Ke | 0.50 | | Entrance Loss | 0.16 | ft |

| Inlet Control Properties | | | | | |
|---|---|---|---|---|---|
| Inlet Control HW Elev. | 136.91 | ft | Flow Control | N/A | |
| Inlet Type | Square edge w/headwall | | Area Full | 1.2 | ft² |
| K | 0.00980 | | HDS 5 Chart | 1 | |
| M | 2.00000 | | HDS 5 Scale | 1 | |
| C | 0.03980 | | Equation Form | 1 | |
| Y | 0.67000 | | | | |

# Culvert Calculator Report
# J-19 (Existing)

Solve For: Discharge

| Culvert Summary | | | | | |
|---|---|---|---|---|---|
| Allowable HW Elevation | 138.46 | ft | Headwater Depth/Height | 1.00 | |
| Computed Headwater Elevation | 138.46 | ft | Discharge | 3.59 | cfs |
| Inlet Control HW Elev. | 138.36 | ft | Tailwater Elevation | 0.00 | ft |
| Outlet Control HW Elev. | 138.46 | ft | Control Type | Entrance Control | |

| Grades | | | | | |
|---|---|---|---|---|---|
| Upstream Invert | 137.21 | ft | Downstream Invert | 135.55 | ft |
| Length | 40.00 | ft | Constructed Slope | 0.041500 | ft/ft |

| Hydraulic Profile | | | | | |
|---|---|---|---|---|---|
| Profile | S2 | | Depth, Downstream | 0.44 | ft |
| Slope Type | Steep | | Normal Depth | 0.43 | ft |
| Flow Regime | Supercritical | | Critical Depth | 0.77 | ft |
| Velocity Downstream | 9.19 | ft/s | Critical Slope | 0.005491 | ft/ft |

| Section | | | | | |
|---|---|---|---|---|---|
| Section Shape | Circular | | Mannings Coefficient | 0.012 | |
| Section Material | Corrugated HDPE (Smooth Interior) | | Span | 1.25 | ft |
| Section Size | 15 inch | | Rise | 1.25 | ft |
| Number Sections | 1 | | | | |

| Outlet Control Properties | | | | | |
|---|---|---|---|---|---|
| Outlet Control HW Elev. | 138.46 | ft | Upstream Velocity Head | 0.32 | ft |
| Ke | 0.50 | | Entrance Loss | 0.16 | ft |

| Inlet Control Properties | | | | | |
|---|---|---|---|---|---|
| Inlet Control HW Elev. | 138.36 | ft | Flow Control | N/A | |
| Inlet Type | Square edge w/headwall | | Area Full | 1.2 | ft² |
| K | 0.00980 | | HDS 5 Chart | 1 | |
| M | 2.00000 | | HDS 5 Scale | 1 | |
| C | 0.03980 | | Equation Form | 1 | |
| Y | 0.67000 | | | | |

# Culvert Calculator Report
# J-21 (Existing)

Solve For: Discharge

| Culvert Summary | | | | | |
|---|---|---|---|---|---|
| Allowable HW Elevation | 119.75 | ft | Headwater Depth/Height | 2.09 | |
| Computed Headwater Elevation | 119.75 | ft | Discharge | 12.95 | cfs |
| Inlet Control HW Elev. | 119.75 | ft | Tailwater Elevation | 0.00 | ft |
| Outlet Control HW Elev. | 119.71 | ft | Control Type | Inlet Control | |

| Grades | | | | | |
|---|---|---|---|---|---|
| Upstream Invert | 116.61 | ft | Downstream Invert | 116.52 | ft |
| Length | 33.00 | ft | Constructed Slope | 0.002727 | ft/ft |

| Hydraulic Profile | | | | | |
|---|---|---|---|---|---|
| Profile | CompositeM2PressureProfile | | Depth, Downstream | 1.35 | ft |
| Slope Type | Mild | | Normal Depth | N/A | ft |
| Flow Regime | Subcritical | | Critical Depth | 1.35 | ft |
| Velocity Downstream | 7.73 | ft/s | Critical Slope | 0.013384 | ft/ft |

| Section | | | | | |
|---|---|---|---|---|---|
| Section Shape | Circular | | Mannings Coefficient | 0.013 | |
| Section Material | Concrete | | Span | 1.50 | ft |
| Section Size | 18 inch | | Rise | 1.50 | ft |
| Number Sections | 1 | | | | |

| Outlet Control Properties | | | | | |
|---|---|---|---|---|---|
| Outlet Control HW Elev. | 119.71 | ft | Upstream Velocity Head | 0.83 | ft |
| Ke | 0.50 | | Entrance Loss | 0.42 | ft |

| Inlet Control Properties | | | | | |
|---|---|---|---|---|---|
| Inlet Control HW Elev. | 119.75 | ft | Flow Control | N/A | |
| Inlet Type | Square edge w/headwall | | Area Full | 1.8 | ft² |
| K | 0.00980 | | HDS 5 Chart | 1 | |
| M | 2.00000 | | HDS 5 Scale | 1 | |
| C | 0.03980 | | Equation Form | 1 | |
| Y | 0.67000 | | | | |

# Culvert Calculator Report
# J-21 (Proposed)

Solve For: Discharge

| Culvert Summary | | | | | |
|---|---|---|---|---|---|
| Allowable HW Elevation | 119.11 | ft | Headwater Depth/Height | 1.25 | |
| Computed Headwater Elevation | 119.11 | ft | Discharge | 16.54 | cfs |
| Inlet Control HW Elev. | 119.06 | ft | Tailwater Elevation | 0.00 | ft |
| Outlet Control HW Elev. | 119.11 | ft | Control Type | Outlet Control | |

| Grades | | | | | |
|---|---|---|---|---|---|
| Upstream Invert | 116.61 | ft | Downstream Invert | 116.52 | ft |
| Length | 33.00 | ft | Constructed Slope | 0.002727 | ft/ft |

| Hydraulic Profile | | | | | |
|---|---|---|---|---|---|
| Profile | M2 | | Depth, Downstream | 1.47 | ft |
| Slope Type | Mild | | Normal Depth | N/A | ft |
| Flow Regime | Subcritical | | Critical Depth | 1.47 | ft |
| Velocity Downstream | 6.70 | ft/s | Critical Slope | 0.006785 | ft/ft |

| Section | | | | | |
|---|---|---|---|---|---|
| Section Shape | Circular | | Mannings Coefficient | 0.013 | |
| Section Material | Concrete | | Span | 2.00 | ft |
| Section Size | 24 inch | | Rise | 2.00 | ft |
| Number Sections | 1 | | | | |

| Outlet Control Properties | | | | | |
|---|---|---|---|---|---|
| Outlet Control HW Elev. | 119.11 | ft | Upstream Velocity Head | 0.50 | ft |
| Ke | 0.50 | | Entrance Loss | 0.25 | ft |

| Inlet Control Properties | | | | | |
|---|---|---|---|---|---|
| Inlet Control HW Elev. | 119.06 | ft | Flow Control | Transition | |
| Inlet Type | Square edge w/headwall | | Area Full | 3.1 | ft² |
| K | 0.00980 | | HDS 5 Chart | 1 | |
| M | 2.00000 | | HDS 5 Scale | 1 | |
| C | 0.03980 | | Equation Form | 1 | |
| Y | 0.67000 | | | | |

# Culvert Calculator Report
# J-27 (Existing)

Solve For: Discharge

| Culvert Summary | | | | | |
|---|---|---|---|---|---|
| Allowable HW Elevation | 138.46 | ft | Headwater Depth/Height | 1.00 | |
| Computed Headwater Elevation | 138.46 | ft | Discharge | 3.59 | cfs |
| Inlet Control HW Elev. | 138.37 | ft | Tailwater Elevation | 0.00 | ft |
| Outlet Control HW Elev. | 138.46 | ft | Control Type | Entrance Control | |

| Grades | | | | | |
|---|---|---|---|---|---|
| Upstream Invert | 137.21 | ft | Downstream Invert | 136.30 | ft |
| Length | 40.00 | ft | Constructed Slope | 0.022750 | ft/ft |

| Hydraulic Profile | | | | | |
|---|---|---|---|---|---|
| Profile | S2 | | Depth, Downstream | 0.52 | ft |
| Slope Type | Steep | | Normal Depth | 0.50 | ft |
| Flow Regime | Supercritical | | Critical Depth | 0.77 | ft |
| Velocity Downstream | 7.45 | ft/s | Critical Slope | 0.005491 | ft/ft |

| Section | | | | | |
|---|---|---|---|---|---|
| Section Shape | Circular | | Mannings Coefficient | 0.012 | |
| Section Material | Corrugated HDPE (Smooth Interior) | | Span | 1.25 | ft |
| Section Size | 15 inch | | Rise | 1.25 | ft |
| Number Sections | 1 | | | | |

| Outlet Control Properties | | | | | |
|---|---|---|---|---|---|
| Outlet Control HW Elev. | 138.46 | ft | Upstream Velocity Head | 0.32 | ft |
| Ke | 0.50 | | Entrance Loss | 0.16 | ft |

| Inlet Control Properties | | | | | |
|---|---|---|---|---|---|
| Inlet Control HW Elev. | 138.37 | ft | Flow Control | N/A | |
| Inlet Type | Square edge w/headwall | | Area Full | 1.2 | ft² |
| K | 0.00980 | | HDS 5 Chart | 1 | |
| M | 2.00000 | | HDS 5 Scale | 1 | |
| C | 0.03980 | | Equation Form | 1 | |
| Y | 0.67000 | | | | |

# Culvert Calculator Report
# J-31 (Existing)

Solve For: Discharge

| Culvert Summary | | | | | |
|---|---|---|---|---|---|
| Allowable HW Elevation | 138.08 | ft | Headwater Depth/Height | 1.00 | |
| Computed Headwater Elevation | 138.08 | ft | Discharge | 3.59 | cfs |
| Inlet Control HW Elev. | 137.99 | ft | Tailwater Elevation | 0.00 | ft |
| Outlet Control HW Elev. | 138.08 | ft | Control Type | Entrance Control | |

| Grades | | | | | |
|---|---|---|---|---|---|
| Upstream Invert | 136.83 | ft | Downstream Invert | 135.98 | ft |
| Length | 40.00 | ft | Constructed Slope | 0.021250 | ft/ft |

| Hydraulic Profile | | | | | |
|---|---|---|---|---|---|
| Profile | S2 | | Depth, Downstream | 0.53 | ft |
| Slope Type | Steep | | Normal Depth | 0.51 | ft |
| Flow Regime | Supercritical | | Critical Depth | 0.77 | ft |
| Velocity Downstream | 7.28 | ft/s | Critical Slope | 0.005491 | ft/ft |

| Section | | | | | |
|---|---|---|---|---|---|
| Section Shape | Circular | | Mannings Coefficient | 0.012 | |
| Section Material | Corrugated HDPE (Smooth Interior) | | Span | 1.25 | ft |
| Section Size | 15 inch | | Rise | 1.25 | ft |
| Number Sections | 1 | | | | |

| Outlet Control Properties | | | | | |
|---|---|---|---|---|---|
| Outlet Control HW Elev. | 138.08 | ft | Upstream Velocity Head | 0.32 | ft |
| Ke | 0.50 | | Entrance Loss | 0.16 | ft |

| Inlet Control Properties | | | | | |
|---|---|---|---|---|---|
| Inlet Control HW Elev. | 137.99 | ft | Flow Control | N/A | |
| Inlet Type | Square edge w/headwall | | Area Full | 1.2 | ft² |
| K | 0.00980 | | HDS 5 Chart | 1 | |
| M | 2.00000 | | HDS 5 Scale | 1 | |
| C | 0.03980 | | Equation Form | 1 | |
| Y | 0.67000 | | | | |

# Culvert Calculator Report
# J-33 (Existing)

Solve For: Discharge

| Culvert Summary | | | | | |
|---|---|---|---|---|---|
| Allowable HW Elevation | 131.18 | ft | Headwater Depth/Height | 1.00 | |
| Computed Headwater Elevation | 131.18 | ft | Discharge | 4.11 | cfs |
| Inlet Control HW Elev. | 131.07 | ft | Tailwater Elevation | 0.00 | ft |
| Outlet Control HW Elev. | 131.18 | ft | Control Type | Entrance Control | |

| Grades | | | | | |
|---|---|---|---|---|---|
| Upstream Invert | 130.18 | ft | Downstream Invert | 126.27 | ft |
| Length | 40.00 | ft | Constructed Slope | 0.097750 | ft/ft |

| Hydraulic Profile | | | | | |
|---|---|---|---|---|---|
| Profile | S2 | | Depth, Downstream | 0.28 | ft |
| Slope Type | Steep | | Normal Depth | 0.28 | ft |
| Flow Regime | Supercritical | | Critical Depth | 0.61 | ft |
| Velocity Downstream | 11.46 | ft/s | Critical Slope | 0.005918 | ft/ft |

| Section | | | | | |
|---|---|---|---|---|---|
| Section Shape | Circular | | Mannings Coefficient | 0.012 | |
| Section Material | Corrugated HDPE (Smooth Interior) | | Span | 1.00 | ft |
| Section Size | 12 inch | | Rise | 1.00 | ft |
| Number Sections | 2 | | | | |

| Outlet Control Properties | | | | | |
|---|---|---|---|---|---|
| Outlet Control HW Elev. | 131.18 | ft | Upstream Velocity Head | 0.26 | ft |
| Ke | 0.50 | | Entrance Loss | 0.13 | ft |

| Inlet Control Properties | | | | | |
|---|---|---|---|---|---|
| Inlet Control HW Elev. | 131.07 | ft | Flow Control | N/A | |
| Inlet Type | Square edge w/headwall | | Area Full | 1.6 | ft² |
| K | 0.00980 | | HDS 5 Chart | 1 | |
| M | 2.00000 | | HDS 5 Scale | 1 | |
| C | 0.03980 | | Equation Form | 1 | |
| Y | 0.67000 | | | | |

# Culvert Calculator Report
# J-33 (Proposed)

Solve For: Discharge

| Culvert Summary | | | | | |
|---|---|---|---|---|---|
| Allowable HW Elevation | 131.68 | ft | Headwater Depth/Height | 1.00 | |
| Computed Headwater Elevation | 131.68 | ft | Discharge | 11.33 | cfs |
| Inlet Control HW Elev. | 131.51 | ft | Tailwater Elevation | 0.00 | ft |
| Outlet Control HW Elev. | 131.68 | ft | Control Type | Entrance Control | |

| Grades | | | | | |
|---|---|---|---|---|---|
| Upstream Invert | 130.18 | ft | Downstream Invert | 126.27 | ft |
| Length | 40.00 | ft | Constructed Slope | 0.097750 | ft/ft |

| Hydraulic Profile | | | | | |
|---|---|---|---|---|---|
| Profile | S2 | | Depth, Downstream | 0.43 | ft |
| Slope Type | Steep | | Normal Depth | 0.40 | ft |
| Flow Regime | Supercritical | | Critical Depth | 0.92 | ft |
| Velocity Downstream | 13.61 | ft/s | Critical Slope | 0.005162 | ft/ft |

| Section | | | | | |
|---|---|---|---|---|---|
| Section Shape | Circular | | Mannings Coefficient | 0.012 | |
| Section Material | Corrugated HDPE (Smooth Interior) | | Span | 1.50 | ft |
| Section Size | 18 inch | | Rise | 1.50 | ft |
| Number Sections | 2 | | | | |

| Outlet Control Properties | | | | | |
|---|---|---|---|---|---|
| Outlet Control HW Elev. | 131.68 | ft | Upstream Velocity Head | 0.39 | ft |
| Ke | 0.50 | | Entrance Loss | 0.19 | ft |

| Inlet Control Properties | | | | | |
|---|---|---|---|---|---|
| Inlet Control HW Elev. | 131.51 | ft | Flow Control | Unsubmerged | |
| Inlet Type | Square edge w/headwall | | Area Full | 3.5 | ft² |
| K | 0.00980 | | HDS 5 Chart | 1 | |
| M | 2.00000 | | HDS 5 Scale | 1 | |
| C | 0.03980 | | Equation Form | 1 | |
| Y | 0.67000 | | | | |

# Culvert Calculator Report
# J-36 (Existing)

Solve For: Discharge

| Culvert Summary | | | | | |
|---|---|---|---|---|---|
| Allowable HW Elevation | 121.54 | ft | Headwater Depth/Height | 2.00 | |
| Computed Headwater Elevation | 121.54 | ft | Discharge | 2.90 | cfs |
| Inlet Control HW Elev. | 120.86 | ft | Tailwater Elevation | 0.00 | ft |
| Outlet Control HW Elev. | 121.54 | ft | Control Type | Outlet Control | |

| Grades | | | | | |
|---|---|---|---|---|---|
| Upstream Invert | 119.54 | ft | Downstream Invert | 119.38 | ft |
| Length | 40.00 | ft | Constructed Slope | 0.004000 | ft/ft |

| Hydraulic Profile | | | | | |
|---|---|---|---|---|---|
| Profile | CompositeM2PressureProfile | | Depth, Downstream | 0.73 | ft |
| Slope Type | Mild | | Normal Depth | N/A | ft |
| Flow Regime | Subcritical | | Critical Depth | 0.73 | ft |
| Velocity Downstream | 4.72 | ft/s | Critical Slope | 0.028936 | ft/ft |

| Section | | | | | |
|---|---|---|---|---|---|
| Section Shape | Circular | | Mannings Coefficient | 0.024 | |
| Section Material | CMP | | Span | 1.00 | ft |
| Section Size | 12 inch | | Rise | 1.00 | ft |
| Number Sections | 1 | | | | |

| Outlet Control Properties | | | | | |
|---|---|---|---|---|---|
| Outlet Control HW Elev. | 121.54 | ft | Upstream Velocity Head | 0.21 | ft |
| Ke | 0.90 | | Entrance Loss | 0.19 | ft |

| Inlet Control Properties | | | | | |
|---|---|---|---|---|---|
| Inlet Control HW Elev. | 120.86 | ft | Flow Control | N/A | |
| Inlet Type | Projecting | | Area Full | 0.8 | ft² |
| K | 0.03400 | | HDS 5 Chart | 2 | |
| M | 1.50000 | | HDS 5 Scale | 3 | |
| C | 0.05530 | | Equation Form | 1 | |
| Y | 0.54000 | | | | |

# Culvert Calculator Report
# J-36 (Proposed)

Solve For: Discharge

| Culvert Summary | | | | | |
|---|---|---|---|---|---|
| Allowable HW Elevation | 121.54 | ft | Headwater Depth/Height | 1.33 | |
| Computed Headwater Elevation | 121.54 | ft | Discharge | 6.61 | cfs |
| Inlet Control HW Elev. | 121.24 | ft | Tailwater Elevation | 0.00 | ft |
| Outlet Control HW Elev. | 121.54 | ft | Control Type | Outlet Control | |

| Grades | | | | | |
|---|---|---|---|---|---|
| Upstream Invert | 119.54 | ft | Downstream Invert | 119.38 | ft |
| Length | 40.00 | ft | Constructed Slope | 0.004000 | ft/ft |

| Hydraulic Profile | | | | | |
|---|---|---|---|---|---|
| Profile | CompositeM2PressureProfile | | Depth, Downstream | 0.99 | ft |
| Slope Type | Mild | | Normal Depth | N/A | ft |
| Flow Regime | Subcritical | | Critical Depth | 0.99 | ft |
| Velocity Downstream | 5.31 | ft/s | Critical Slope | 0.022303 | ft/ft |

| Section | | | | | |
|---|---|---|---|---|---|
| Section Shape | Circular | | Mannings Coefficient | 0.024 | |
| Section Material | CMP | | Span | 1.50 | ft |
| Section Size | 18 inch | | Rise | 1.50 | ft |
| Number Sections | 1 | | | | |

| Outlet Control Properties | | | | | |
|---|---|---|---|---|---|
| Outlet Control HW Elev. | 121.54 | ft | Upstream Velocity Head | 0.22 | ft |
| Ke | 0.90 | | Entrance Loss | 0.20 | ft |

| Inlet Control Properties | | | | | |
|---|---|---|---|---|---|
| Inlet Control HW Elev. | 121.24 | ft | Flow Control | Unsubmerged | |
| Inlet Type | Projecting | | Area Full | 1.8 | ft² |
| K | 0.03400 | | HDS 5 Chart | 2 | |
| M | 1.50000 | | HDS 5 Scale | 3 | |
| C | 0.05530 | | Equation Form | 1 | |
| Y | 0.54000 | | | | |

# Culvert Calculator Report
# J-41 (Proposed)

Solve For: Discharge

| Culvert Summary | | | | | |
|---|---|---|---|---|---|
| Allowable HW Elevation | 135.16 | ft | Headwater Depth/Height | 1.00 | |
| Computed Headwater Elevation | 135.16 | ft | Discharge | 5.75 | cfs |
| Inlet Control HW Elev. | 135.08 | ft | Tailwater Elevation | 0.00 | ft |
| Outlet Control HW Elev. | 135.16 | ft | Control Type | Outlet Control | |

| Grades | | | | | |
|---|---|---|---|---|---|
| Upstream Invert | 133.66 | ft | Downstream Invert | 133.56 | ft |
| Length | 40.00 | ft | Constructed Slope | 0.002500 | ft/ft |

| Hydraulic Profile | | | | | |
|---|---|---|---|---|---|
| Profile | M2 | | Depth, Downstream | 0.93 | ft |
| Slope Type | Mild | | Normal Depth | 1.24 | ft |
| Flow Regime | Subcritical | | Critical Depth | 0.93 | ft |
| Velocity Downstream | 5.03 | ft/s | Critical Slope | 0.005202 | ft/ft |

| Section | | | | | |
|---|---|---|---|---|---|
| Section Shape | Circular | | Mannings Coefficient | 0.012 | |
| Section Material | Corrugated HDPE (Smooth Interior) | | Span | 1.50 | ft |
| Section Size | 18 inch | | Rise | 1.50 | ft |
| Number Sections | 1 | | | | |

| Outlet Control Properties | | | | | |
|---|---|---|---|---|---|
| Outlet Control HW Elev. | 135.16 | ft | Upstream Velocity Head | 0.27 | ft |
| Ke | 0.50 | | Entrance Loss | 0.13 | ft |

| Inlet Control Properties | | | | | |
|---|---|---|---|---|---|
| Inlet Control HW Elev. | 135.08 | ft | Flow Control | Unsubmerged | |
| Inlet Type | Square edge w/headwall | | Area Full | 1.8 | ft² |
| K | 0.00980 | | HDS 5 Chart | 1 | |
| M | 2.00000 | | HDS 5 Scale | 1 | |
| C | 0.03980 | | Equation Form | 1 | |
| Y | 0.67000 | | | | |

# Culvert Calculator Report
# J-43 (Existing)

Solve For: Discharge

| Culvert Summary | | | | | |
|---|---|---|---|---|---|
| Allowable HW Elevation | 130.85 | ft | Headwater Depth/Height | 1.00 | |
| Computed Headwater Elevation | 130.85 | ft | Discharge | 4.11 | cfs |
| Inlet Control HW Elev. | 130.76 | ft | Tailwater Elevation | 0.00 | ft |
| Outlet Control HW Elev. | 130.85 | ft | Control Type | Entrance Control | |

| Grades | | | | | |
|---|---|---|---|---|---|
| Upstream Invert | 129.85 | ft | Downstream Invert | 127.73 | ft |
| Length | 40.00 | ft | Constructed Slope | 0.053000 | ft/ft |

| Hydraulic Profile | | | | | |
|---|---|---|---|---|---|
| Profile | S2 | | Depth, Downstream | 0.33 | ft |
| Slope Type | Steep | | Normal Depth | 0.33 | ft |
| Flow Regime | Supercritical | | Critical Depth | 0.61 | ft |
| Velocity Downstream | 9.07 | ft/s | Critical Slope | 0.005918 | ft/ft |

| Section | | | | | |
|---|---|---|---|---|---|
| Section Shape | Circular | | Mannings Coefficient | 0.012 | |
| Section Material | Corrugated HDPE (Smooth Interior) | | Span | 1.00 | ft |
| Section Size | 12 inch | | Rise | 1.00 | ft |
| Number Sections | 2 | | | | |

| Outlet Control Properties | | | | | |
|---|---|---|---|---|---|
| Outlet Control HW Elev. | 130.85 | ft | Upstream Velocity Head | 0.26 | ft |
| Ke | 0.50 | | Entrance Loss | 0.13 | ft |

| Inlet Control Properties | | | | | |
|---|---|---|---|---|---|
| Inlet Control HW Elev. | 130.76 | ft | Flow Control | N/A | |
| Inlet Type | Square edge w/headwall | | Area Full | 1.6 | ft² |
| K | 0.00980 | | HDS 5 Chart | 1 | |
| M | 2.00000 | | HDS 5 Scale | 1 | |
| C | 0.03980 | | Equation Form | 1 | |
| Y | 0.67000 | | | | |

# Culvert Calculator Report
# J-43 (Proposed)

Solve For: Discharge

| Culvert Summary | | | | | |
|---|---|---|---|---|---|
| Allowable HW Elevation | 132.35 | ft | Headwater Depth/Height | 1.00 | |
| Computed Headwater Elevation | 132.35 | ft | Discharge | 40.62 | cfs |
| Inlet Control HW Elev. | 132.13 | ft | Tailwater Elevation | 0.00 | ft |
| Outlet Control HW Elev. | 132.35 | ft | Control Type | Entrance Control | |

| Grades | | | | | |
|---|---|---|---|---|---|
| Upstream Invert | 129.85 | ft | Downstream Invert | 127.73 | ft |
| Length | 40.00 | ft | Constructed Slope | 0.053000 | ft/ft |

| Hydraulic Profile | | | | | |
|---|---|---|---|---|---|
| Profile | S2 | | Depth, Downstream | 0.88 | ft |
| Slope Type | Steep | | Normal Depth | 0.76 | ft |
| Flow Regime | Supercritical | | Critical Depth | 1.53 | ft |
| Velocity Downstream | 13.10 | ft/s | Critical Slope | 0.004356 | ft/ft |

| Section | | | | | |
|---|---|---|---|---|---|
| Section Shape | Circular | | Mannings Coefficient | 0.012 | |
| Section Material | Corrugated HDPE (Smooth Interior) | | Span | 2.50 | ft |
| Section Size | 30 inch | | Rise | 2.50 | ft |
| Number Sections | 2 | | | | |

| Outlet Control Properties | | | | | |
|---|---|---|---|---|---|
| Outlet Control HW Elev. | 132.35 | ft | Upstream Velocity Head | 0.65 | ft |
| Ke | 0.50 | | Entrance Loss | 0.32 | ft |

| Inlet Control Properties | | | | | |
|---|---|---|---|---|---|
| Inlet Control HW Elev. | 132.13 | ft | Flow Control | Unsubmerged | |
| Inlet Type | Square edge w/headwall | | Area Full | 9.8 | ft² |
| K | 0.00980 | | HDS 5 Chart | 1 | |
| M | 2.00000 | | HDS 5 Scale | 1 | |
| C | 0.03980 | | Equation Form | 1 | |
| Y | 0.67000 | | | | |

# Culvert Calculator Report
# J-60 (Existing)

Solve For: Discharge

| Culvert Summary | | | | | |
|---|---|---|---|---|---|
| Allowable HW Elevation | 117.62 | ft | Headwater Depth/Height | 1.00 | |
| Computed Headwater Elevation | 117.62 | ft | Discharge | 5.66 | cfs |
| Inlet Control HW Elev. | 117.43 | ft | Tailwater Elevation | 0.00 | ft |
| Outlet Control HW Elev. | 117.62 | ft | Control Type | Entrance Control | |

| Grades | | | | | |
|---|---|---|---|---|---|
| Upstream Invert | 116.12 | ft | Downstream Invert | 110.99 | ft |
| Length | 40.00 | ft | Constructed Slope | 0.128250 | ft/ft |

| Hydraulic Profile | | | | | |
|---|---|---|---|---|---|
| Profile | S2 | | Depth, Downstream | 0.41 | ft |
| Slope Type | Steep | | Normal Depth | 0.39 | ft |
| Flow Regime | Supercritical | | Critical Depth | 0.92 | ft |
| Velocity Downstream | 14.63 | ft/s | Critical Slope | 0.006064 | ft/ft |

| Section | | | | | |
|---|---|---|---|---|---|
| Section Shape | Circular | | Mannings Coefficient | 0.013 | |
| Section Material | Concrete | | Span | 1.50 | ft |
| Section Size | 18 inch | | Rise | 1.50 | ft |
| Number Sections | 1 | | | | |

| Outlet Control Properties | | | | | |
|---|---|---|---|---|---|
| Outlet Control HW Elev. | 117.62 | ft | Upstream Velocity Head | 0.39 | ft |
| Ke | 0.50 | | Entrance Loss | 0.19 | ft |

| Inlet Control Properties | | | | | |
|---|---|---|---|---|---|
| Inlet Control HW Elev. | 117.43 | ft | Flow Control | N/A | |
| Inlet Type | Square edge w/headwall | | Area Full | 1.8 | ft² |
| K | 0.00980 | | HDS 5 Chart | 1 | |
| M | 2.00000 | | HDS 5 Scale | 1 | |
| C | 0.03980 | | Equation Form | 1 | |
| Y | 0.67000 | | | | |

# Culvert Calculator Report
# J-60 (Proposed)

Solve For: Discharge

| Culvert Summary | | | | | |
|---|---|---|---|---|---|
| Allowable HW Elevation | 118.12 | ft | Headwater Depth/Height | 1.00 | |
| Computed Headwater Elevation | 118.12 | ft | Discharge | 11.63 | cfs |
| Inlet Control HW Elev. | 117.87 | ft | Tailwater Elevation | 0.00 | ft |
| Outlet Control HW Elev. | 118.12 | ft | Control Type | Entrance Control | |

| Grades | | | | | |
|---|---|---|---|---|---|
| Upstream Invert | 116.12 | ft | Downstream Invert | 110.99 | ft |
| Length | 40.00 | ft | Constructed Slope | 0.128250 | ft/ft |

| Hydraulic Profile | | | | | |
|---|---|---|---|---|---|
| Profile | S2 | | Depth, Downstream | 0.56 | ft |
| Slope Type | Steep | | Normal Depth | 0.51 | ft |
| Flow Regime | Supercritical | | Critical Depth | 1.22 | ft |
| Velocity Downstream | 16.30 | ft/s | Critical Slope | 0.005510 | ft/ft |

| Section | | | | | |
|---|---|---|---|---|---|
| Section Shape | Circular | | Mannings Coefficient | 0.013 | |
| Section Material | Concrete | | Span | 2.00 | ft |
| Section Size | 24 inch | | Rise | 2.00 | ft |
| Number Sections | 1 | | | | |

| Outlet Control Properties | | | | | |
|---|---|---|---|---|---|
| Outlet Control HW Elev. | 118.12 | ft | Upstream Velocity Head | 0.52 | ft |
| Ke | 0.50 | | Entrance Loss | 0.26 | ft |

| Inlet Control Properties | | | | | |
|---|---|---|---|---|---|
| Inlet Control HW Elev. | 117.87 | ft | Flow Control | Unsubmerged | |
| Inlet Type | Square edge w/headwall | | Area Full | 3.1 | ft² |
| K | 0.00980 | | HDS 5 Chart | 1 | |
| M | 2.00000 | | HDS 5 Scale | 1 | |
| C | 0.03980 | | Equation Form | 1 | |
| Y | 0.67000 | | | | |

# Culvert Calculator Report
# J-64 (Existing)

Solve For: Discharge

| Culvert Summary | | | | | |
|---|---|---|---|---|---|
| Allowable HW Elevation | 115.70 | ft | Headwater Depth/Height | 1.00 | |
| Computed Headwater Elevation | 115.70 | ft | Discharge | 5.66 | cfs |
| Inlet Control HW Elev. | 115.57 | ft | Tailwater Elevation | 0.00 | ft |
| Outlet Control HW Elev. | 115.70 | ft | Control Type | Entrance Control | |

| Grades | | | | | |
|---|---|---|---|---|---|
| Upstream Invert | 114.20 | ft | Downstream Invert | 112.44 | ft |
| Length | 40.00 | ft | Constructed Slope | 0.044000 | ft/ft |

| Hydraulic Profile | | | | | |
|---|---|---|---|---|---|
| Profile | S2 | | Depth, Downstream | 0.54 | ft |
| Slope Type | Steep | | Normal Depth | 0.52 | ft |
| Flow Regime | Supercritical | | Critical Depth | 0.92 | ft |
| Velocity Downstream | 9.82 | ft/s | Critical Slope | 0.006064 | ft/ft |

| Section | | | | | |
|---|---|---|---|---|---|
| Section Shape | Circular | | Mannings Coefficient | 0.013 | |
| Section Material | Concrete | | Span | 1.50 | ft |
| Section Size | 18 inch | | Rise | 1.50 | ft |
| Number Sections | 1 | | | | |

| Outlet Control Properties | | | | | |
|---|---|---|---|---|---|
| Outlet Control HW Elev. | 115.70 | ft | Upstream Velocity Head | 0.39 | ft |
| Ke | 0.50 | | Entrance Loss | 0.19 | ft |

| Inlet Control Properties | | | | | |
|---|---|---|---|---|---|
| Inlet Control HW Elev. | 115.57 | ft | Flow Control | N/A | |
| Inlet Type | Square edge w/headwall | | Area Full | 1.8 | ft² |
| K | 0.00980 | | HDS 5 Chart | 1 | |
| M | 2.00000 | | HDS 5 Scale | 1 | |
| C | 0.03980 | | Equation Form | 1 | |
| Y | 0.67000 | | | | |

# Pond Pack – 10 Year Event

# Table of Contents

# Table of Contents

Subsection: Master Network Summary

## Catchments Summary

| Label | Scenario | Return Event (years) | Hydrograph Volume (ac-ft) | Time to Peak (hours) | Peak Flow ($ft^3/s$) |
|---|---|---|---|---|---|
| CM-10 | Pre Dev 10 yr | 10 | 0.244 | 11.940 | 4.45 |
| CM-11 | Pre Dev 10 yr | 10 | 0.095 | 11.925 | 1.78 |
| CM-12 | Pre Dev 10 yr | 10 | 0.089 | 11.935 | 1.63 |
| CM-13 | Pre Dev 10 yr | 10 | 0.203 | 12.010 | 3.27 |
| CM-14 | Pre Dev 10 yr | 10 | 1.169 | 12.010 | 18.96 |
| CM-16 | Pre Dev 10 yr | 10 | 0.054 | 11.935 | 1.00 |
| CM-17 | Pre Dev 10 yr | 10 | 0.132 | 12.120 | 1.48 |
| CM-18 | Pre Dev 10 yr | 10 | 0.464 | 11.995 | 7.67 |
| CM-19 | Pre Dev 10 yr | 10 | 0.095 | 11.995 | 1.58 |
| CM-21 | Pre Dev 10 yr | 10 | 0.158 | 12.005 | 2.55 |
| CM-29 | Pre Dev 10 yr | 10 | 1.117 | 12.050 | 16.38 |
| CM-3 | Pre Dev 10 yr | 10 | 0.118 | 11.930 | 2.20 |
| CM-5 | Pre Dev 10 yr | 10 | 0.036 | 11.930 | 0.68 |
| CM-6 | Pre Dev 10 yr | 10 | 0.085 | 11.970 | 1.44 |
| CM-7 | Pre Dev 10 yr | 10 | 0.401 | 12.030 | 6.11 |
| CM-8 | Pre Dev 10 yr | 10 | 0.070 | 11.960 | 1.20 |
| CM-9 | Pre Dev 10 yr | 10 | 0.076 | 12.000 | 1.23 |

## Node Summary

| Label | Scenario | Return Event (years) | Hydrograph Volume (ac-ft) | Time to Peak (hours) | Peak Flow ($ft^3/s$) |
|---|---|---|---|---|---|
| J-129 | Pre Dev 10 yr | 10 | 1.117 | 12.050 | 16.38 |
| J-13 | Pre Dev 10 yr | 10 | 0.118 | 11.930 | 2.20 |
| J-17 | Pre Dev 10 yr | 10 | 0.036 | 11.930 | 0.68 |
| J-18 | Pre Dev 10 yr | 10 | 0.036 | 11.930 | 0.68 |
| J-19 | Pre Dev 10 yr | 10 | 0.085 | 11.970 | 1.44 |
| J-20 | Pre Dev 10 yr | 10 | 0.085 | 11.970 | 1.44 |
| J-21 | Pre Dev 10 yr | 10 | 0.822 | 12.015 | 12.55 |
| J-27 | Pre Dev 10 yr | 10 | 0.070 | 11.960 | 1.20 |
| J-28 | Pre Dev 10 yr | 10 | 0.070 | 11.960 | 1.20 |
| J-31 | Pre Dev 10 yr | 10 | 0.076 | 12.000 | 1.23 |
| J-32 | Pre Dev 10 yr | 10 | 0.076 | 12.000 | 1.23 |
| J-33 | Pre Dev 10 yr | 10 | 0.390 | 11.950 | 6.71 |
| J-35 | Pre Dev 10 yr | 10 | 0.118 | 11.930 | 2.20 |
| J-36 | Pre Dev 10 yr | 10 | 0.212 | 11.925 | 3.98 |
| J-39 | Pre Dev 10 yr | 10 | 0.522 | 12.025 | 8.01 |
| J-41 | Pre Dev 10 yr | 10 | 0.203 | 12.010 | 3.27 |
| J-42 | Pre Dev 10 yr | 10 | 0.203 | 12.010 | 3.27 |
| J-43 | Pre Dev 10 yr | 10 | 1.372 | 12.010 | 22.22 |
| J-52 | Pre Dev 10 yr | 10 | 0.054 | 11.935 | 1.00 |
| J-53 | Pre Dev 10 yr | 10 | 0.054 | 11.935 | 1.00 |
| J-59 | Pre Dev 10 yr | 10 | 0.464 | 11.995 | 7.67 |
| J-60 | Pre Dev 10 yr | 10 | 0.463 | 12.005 | 7.64 |

Subsection: Master Network Summary

## Node Summary

| Label | Scenario | Return Event (years) | Hydrograph Volume (ac-ft) | Time to Peak (hours) | Peak Flow ($ft^3/s$) |
|---|---|---|---|---|---|
| J-62 | Pre Dev 10 yr | 10 | 0.559 | 12.005 | 9.21 |
| J-64 | Pre Dev 10 yr | 10 | 0.158 | 12.025 | 2.53 |
| J-66 | Pre Dev 10 yr | 10 | 0.158 | 12.005 | 2.55 |
| O-10 | Pre Dev 10 yr | 10 | 0.158 | 12.025 | 2.53 |
| O-12 | Pre Dev 10 yr | 10 | 0.390 | 11.950 | 6.71 |
| O-13 | Pre Dev 10 yr | 10 | 1.372 | 12.010 | 22.22 |
| O-14 | Pre Dev 10 yr | 10 | 1.116 | 12.060 | 16.26 |
| O-5 | Pre Dev 10 yr | 10 | 0.822 | 12.015 | 12.55 |
| O-8 | Pre Dev 10 yr | 10 | 0.186 | 12.025 | 2.02 |
| O-9 | Pre Dev 10 yr | 10 | 0.559 | 12.005 | 9.21 |

Subsection: Unit Hydrograph Equations

## Unit Hydrograph Method (Computational Notes)
## Definition of Terms

| | |
|---|---|
| At | Total area (acres): At = Ai+Ap |
| Ai | Impervious area (acres) |
| Ap | Pervious area (acres) |
| CNi | Runoff curve number for impervious area |
| CNp | Runoff curve number for pervious area |
| fLoss | f loss constant infiltration (depth/time) |
| gKs | Saturated Hydraulic Conductivity (depth/time) |
| Md | Volumetric Moisture Deficit |
| Psi | Capillary Suction (length) |
| hK | Horton Infiltration Decay Rate (time^-1) |
| fo | Initial Infiltration Rate (depth/time) |
| fc | Ultimate(capacity)Infiltration Rate (depth/time) |
| Ia | Initial Abstraction (length) |
| dt | Computational increment (duration of unit excess rainfall)<br>Default dt is smallest value of 0.1333Tc, rtm, and th<br>(Smallest dt is then adjusted to match up with Tp) |
| UDdt | User specified override computational main time increment<br>(only used if UDdt is => .1333Tc) |
| D(t) | Point on distribution curve (fraction of P) for time step t |
| K | 2 / (1 + (Tr/Tp)): default K = 0.75: (for Tr/Tp = 1.67) |
| Ks | Hydrograph shape factor = Unit Conversions * K: = ((1hr/3600sec) *<br>(1ft/12in) * ((5280ft)**2/sq.mi)) * K<br>Default Ks = 645.333 * 0.75 = 484 |
| Lag | Lag time from center of excess runoff (dt) to Tp: Lag = 0.6Tc |
| P | Total precipitation depth, inches |
| Pa(t) | Accumulated rainfall at time step t |
| Pi(t) | Incremental rainfall at time step t |
| qp | Peak discharge (cfs) for 1in. runoff, for 1hr, for 1 sq.mi. = (Ks * A * Q) /<br>Tp (where Q = 1in. runoff, A=sq.mi.) |
| Qu(t) | Unit hydrograph ordinate (cfs) at time step t |
| Q(t) | Final hydrograph ordinate (cfs) at time step t |
| Rai(t) | Accumulated runoff (inches) at time step t for impervious area |
| Rap(t) | Accumulated runoff (inches) at time step t for pervious area |
| Rii(t) | Incremental runoff (inches) at time step t for impervious area |
| Rip(t) | Incremental runoff (inches) at time step t for pervious area |
| R(t) | Incremental weighted total runoff (inches) |
| Rtm | Time increment for rainfall table |
| Si | S for impervious area: Si = (1000/CNi) - 10 |
| Sp | S for pervious area: Sp = (1000/CNp) - 10 |
| t | Time step (row) number |
| Tc | Time of concentration |
| Tb | Time (hrs) of entire unit hydrograph: Tb = Tp + Tr |
| Tp | Time (hrs) to peak of a unit hydrograph: Tp = (dt/2) + Lag |
| Tr | Time (hrs) of receding limb of unit hydrograph: Tr = ratio of Tp |

Subsection: Unit Hydrograph Equations

## Unit Hydrograph Method
## Computational Notes
## Precipitation

| | |
|---|---|
| Column (1) | Time for time step t |
| Column (2) | D(t) = Point on distribution curve for time step t |
| Column (3) | Pi(t) = Pa(t) - Pa(t-1): Col.(4) - Preceding Col.(4) |
| Column (4) | Pa(t) = D(t) x P: Col.(2) x P |

## Pervious Area Runoff (using SCS Runoff CN Method)

| | |
|---|---|
| Column (5) | Rap(t) = Accumulated pervious runoff for time step t<br>If (Pa(t) is <= 0.2Sp) then use: Rap(t) = 0.0<br>If (Pa(t) is > 0.2Sp) then use:<br><br>Rap(t) = (Col.(4)-0.2Sp)**2 / (Col.(4)+0.8Sp) |
| Column (6) | Rip(t) = Incremental pervious runoff for time step t<br>Rip(t) = Rap(t) - Rap(t-1)<br>Rip(t) = Col.(5) for current row - Col.(5) for preceding row. |

## Impervious Area Runoff

| | |
|---|---|
| Column (7 & 8)... | Did not specify to use impervious areas. |

## Incremental Weighted Runoff

| | |
|---|---|
| Column (9) | R(t) = (Ap/At) x Rip(t) + (Ai/At) x Rii(t)<br>R(t) = (Ap/At) x Col.(6) + (Ai/At) x Col.(8) |

## SCS Unit Hydrograph Method

| | |
|---|---|
| Column (10) | Q(t) is computed with the SCS unit hydrograph method using R(t) and Qu(t). |

| | |
|---|---|
| Storm Event | 10 yr |
| Return Event | 10 years |
| Duration | 24.000 hours |
| Depth | 5.8 in |
| Time of Concentration (Composite) | 0.101 hours |
| Scaled Area | 1.148 acres |

| | |
|---|---|
| Computational Time Increment | 0.013 hours |
| Time to Peak (Computed) | 11.940 hours |
| Flow (Peak, Computed) | 4.45 ft³/s |
| Output Increment | 0.005 hours |
| Time to Flow (Peak Interpolated Output) | 11.940 hours |
| Flow (Peak Interpolated Output) | 4.45 ft³/s |

| Drainage Area | |
|---|---|
| SCS CN (Composite) | 69.000 |
| Scaled Area | 1.148 acres |
| Maximum Retention (Pervious) | 4.5 in |
| Maximum Retention (Pervious, 20 percent) | 0.9 in |

| Cumulative Runoff | |
|---|---|
| Cumulative Runoff Depth (Pervious) | 2.6 in |
| Runoff Volume (Pervious) | 0.245 ac-ft |

| Hydrograph Volume (Area under Hydrograph curve) | |
|---|---|
| Volume | 0.244 ac-ft |

| SCS Unit Hydrograph Parameters | |
|---|---|
| Time of Concentration (Composite) | 0.101 hours |
| Computational Time Increment | 0.013 hours |
| Unit Hydrograph Shape Factor | 483.432 |
| K Factor | 0.749 |
| Receding/Rising, Tr/Tp | 1.670 |
| Unit peak, qp | 12.90 ft³/s |
| Unit peak time, Tp | 0.067 hours |

| SCS Unit Hydrograph Parameters | |
|---|---|
| Unit receding limb, Tr | 0.269 hours |
| Total unit time, Tb | 0.336 hours |

| | |
|---|---|
| Storm Event | 10 yr |
| Return Event | 10 years |
| Duration | 24.000 hours |
| Depth | 5.8 in |
| Time of Concentration (Composite) | 0.083 hours |
| Scaled Area | 0.445 acres |

| | |
|---|---|
| Computational Time Increment | 0.011 hours |
| Time to Peak (Computed) | 11.922 hours |
| Flow (Peak, Computed) | 1.78 ft³/s |
| Output Increment | 0.005 hours |
| Time to Flow (Peak Interpolated Output) | 11.925 hours |
| Flow (Peak Interpolated Output) | 1.78 ft³/s |

| Drainage Area | |
|---|---|
| SCS CN (Composite) | 69.000 |
| Scaled Area | 0.445 acres |
| Maximum Retention (Pervious) | 4.5 in |
| Maximum Retention (Pervious, 20 percent) | 0.9 in |

| Cumulative Runoff | |
|---|---|
| Cumulative Runoff Depth (Pervious) | 2.6 in |
| Runoff Volume (Pervious) | 0.095 ac-ft |

| Hydrograph Volume (Area under Hydrograph curve) | |
|---|---|
| Volume | 0.095 ac-ft |

| SCS Unit Hydrograph Parameters | |
|---|---|
| Time of Concentration (Composite) | 0.083 hours |
| Computational Time Increment | 0.011 hours |
| Unit Hydrograph Shape Factor | 483.432 |
| K Factor | 0.749 |
| Receding/Rising, Tr/Tp | 1.670 |
| Unit peak, qp | 6.05 ft³/s |
| Unit peak time, Tp | 0.056 hours |

| SCS Unit Hydrograph Parameters | |
|---|---|
| Unit receding limb, Tr | 0.222 hours |
| Total unit time, Tb | 0.278 hours |

| | |
|---|---|
| Storm Event | 10 yr |
| Return Event | 10 years |
| Duration | 24.000 hours |
| Depth | 5.8 in |
| Time of Concentration (Composite) | 0.096 hours |
| Scaled Area | 0.416 acres |

| | |
|---|---|
| Computational Time Increment | 0.013 hours |
| Time to Peak (Computed) | 11.936 hours |
| Flow (Peak, Computed) | 1.63 ft³/s |
| Output Increment | 0.005 hours |
| Time to Flow (Peak Interpolated Output) | 11.935 hours |
| Flow (Peak Interpolated Output) | 1.63 ft³/s |

| Drainage Area | |
|---|---|
| SCS CN (Composite) | 69.000 |
| Scaled Area | 0.416 acres |
| Maximum Retention (Pervious) | 4.5 in |
| Maximum Retention (Pervious, 20 percent) | 0.9 in |

| Cumulative Runoff | |
|---|---|
| Cumulative Runoff Depth (Pervious) | 2.6 in |
| Runoff Volume (Pervious) | 0.089 ac-ft |

| Hydrograph Volume (Area under Hydrograph curve) | |
|---|---|
| Volume | 0.089 ac-ft |

| SCS Unit Hydrograph Parameters | |
|---|---|
| Time of Concentration (Composite) | 0.096 hours |
| Computational Time Increment | 0.013 hours |
| Unit Hydrograph Shape Factor | 483.432 |
| K Factor | 0.749 |
| Receding/Rising, Tr/Tp | 1.670 |
| Unit peak, qp | 4.93 ft³/s |
| Unit peak time, Tp | 0.064 hours |

| SCS Unit Hydrograph Parameters | |
|---|---|
| Unit receding limb, Tr | 0.255 hours |
| Total unit time, Tb | 0.319 hours |

| | |
|---|---|
| Storm Event | 10 yr |
| Return Event | 10 years |
| Duration | 24.000 hours |
| Depth | 5.8 in |
| Time of Concentration (Composite) | 0.182 hours |
| Scaled Area | 0.955 acres |

| | |
|---|---|
| Computational Time Increment | 0.024 hours |
| Time to Peak (Computed) | 12.012 hours |
| Flow (Peak, Computed) | 3.27 ft³/s |
| Output Increment | 0.005 hours |
| Time to Flow (Peak Interpolated Output) | 12.010 hours |
| Flow (Peak Interpolated Output) | 3.27 ft³/s |

| Drainage Area | |
|---|---|
| SCS CN (Composite) | 69.000 |
| Scaled Area | 0.955 acres |
| Maximum Retention (Pervious) | 4.5 in |
| Maximum Retention (Pervious, 20 percent) | 0.9 in |

| Cumulative Runoff | |
|---|---|
| Cumulative Runoff Depth (Pervious) | 2.6 in |
| Runoff Volume (Pervious) | 0.204 ac-ft |

| Hydrograph Volume (Area under Hydrograph curve) | |
|---|---|
| Volume | 0.203 ac-ft |

| SCS Unit Hydrograph Parameters | |
|---|---|
| Time of Concentration (Composite) | 0.182 hours |
| Computational Time Increment | 0.024 hours |
| Unit Hydrograph Shape Factor | 483.432 |
| K Factor | 0.749 |
| Receding/Rising, Tr/Tp | 1.670 |
| Unit peak, qp | 5.94 ft³/s |
| Unit peak time, Tp | 0.121 hours |

| SCS Unit Hydrograph Parameters | |
|---|---|
| Unit receding limb, Tr | 0.485 hours |
| Total unit time, Tb | 0.607 hours |

| | |
|---|---|
| Storm Event | 10 yr |
| Return Event | 10 years |
| Duration | 24.000 hours |
| Depth | 5.8 in |
| Time of Concentration (Composite) | 0.177 hours |
| Scaled Area | 5.502 acres |

| | |
|---|---|
| Computational Time Increment | 0.024 hours |
| Time to Peak (Computed) | 12.009 hours |
| Flow (Peak, Computed) | 18.97 ft³/s |
| Output Increment | 0.005 hours |
| Time to Flow (Peak Interpolated Output) | 12.010 hours |
| Flow (Peak Interpolated Output) | 18.96 ft³/s |

| Drainage Area | |
|---|---|
| SCS CN (Composite) | 69.000 |
| Scaled Area | 5.502 acres |
| Maximum Retention (Pervious) | 4.5 in |
| Maximum Retention (Pervious, 20 percent) | 0.9 in |

| Cumulative Runoff | |
|---|---|
| Cumulative Runoff Depth (Pervious) | 2.6 in |
| Runoff Volume (Pervious) | 1.173 ac-ft |

| Hydrograph Volume (Area under Hydrograph curve) | |
|---|---|
| Volume | 1.169 ac-ft |

| SCS Unit Hydrograph Parameters | |
|---|---|
| Time of Concentration (Composite) | 0.177 hours |
| Computational Time Increment | 0.024 hours |
| Unit Hydrograph Shape Factor | 483.432 |
| K Factor | 0.749 |
| Receding/Rising, Tr/Tp | 1.670 |
| Unit peak, qp | 35.23 ft³/s |
| Unit peak time, Tp | 0.118 hours |

| SCS Unit Hydrograph Parameters | |
|---|---|
| Unit receding limb, Tr | 0.472 hours |
| Total unit time, Tb | 0.590 hours |

| | |
|---|---|
| Storm Event | 10 yr |
| Return Event | 10 years |
| Duration | 24.000 hours |
| Depth | 5.8 in |
| Time of Concentration (Composite) | 0.093 hours |
| Scaled Area | 0.255 acres |

| | |
|---|---|
| Computational Time Increment | 0.012 hours |
| Time to Peak (Computed) | 11.936 hours |
| Flow (Peak, Computed) | 1.00 ft³/s |
| Output Increment | 0.005 hours |
| Time to Flow (Peak Interpolated Output) | 11.935 hours |
| Flow (Peak Interpolated Output) | 1.00 ft³/s |

| Drainage Area | |
|---|---|
| SCS CN (Composite) | 69.000 |
| Scaled Area | 0.255 acres |
| Maximum Retention (Pervious) | 4.5 in |
| Maximum Retention (Pervious, 20 percent) | 0.9 in |

| Cumulative Runoff | |
|---|---|
| Cumulative Runoff Depth (Pervious) | 2.6 in |
| Runoff Volume (Pervious) | 0.054 ac-ft |

| Hydrograph Volume (Area under Hydrograph curve) | |
|---|---|
| Volume | 0.054 ac-ft |

| SCS Unit Hydrograph Parameters | |
|---|---|
| Time of Concentration (Composite) | 0.093 hours |
| Computational Time Increment | 0.012 hours |
| Unit Hydrograph Shape Factor | 483.432 |
| K Factor | 0.749 |
| Receding/Rising, Tr/Tp | 1.670 |
| Unit peak, qp | 3.09 ft³/s |
| Unit peak time, Tp | 0.062 hours |

| SCS Unit Hydrograph Parameters | |
|---|---|
| Unit receding limb, Tr | 0.249 hours |
| Total unit time, Tb | 0.311 hours |

| | |
|---|---|
| Storm Event | 10 yr |
| Return Event | 10 years |
| Duration | 24.000 hours |
| Depth | 5.8 in |
| Time of Concentration (Composite) | 0.417 hours |
| Scaled Area | 0.622 acres |

| | |
|---|---|
| Computational Time Increment | 0.056 hours |
| Time to Peak (Computed) | 12.116 hours |
| Flow (Peak, Computed) | 1.48 ft³/s |
| Output Increment | 0.005 hours |
| Time to Flow (Peak Interpolated Output) | 12.120 hours |
| Flow (Peak Interpolated Output) | 1.48 ft³/s |

| Drainage Area | |
|---|---|
| SCS CN (Composite) | 69.000 |
| Scaled Area | 0.622 acres |
| Maximum Retention (Pervious) | 4.5 in |
| Maximum Retention (Pervious, 20 percent) | 0.9 in |

| Cumulative Runoff | |
|---|---|
| Cumulative Runoff Depth (Pervious) | 2.6 in |
| Runoff Volume (Pervious) | 0.132 ac-ft |

| Hydrograph Volume (Area under Hydrograph curve) | |
|---|---|
| Volume | 0.132 ac-ft |

| SCS Unit Hydrograph Parameters | |
|---|---|
| Time of Concentration (Composite) | 0.417 hours |
| Computational Time Increment | 0.056 hours |
| Unit Hydrograph Shape Factor | 483.432 |
| K Factor | 0.749 |
| Receding/Rising, Tr/Tp | 1.670 |
| Unit peak, qp | 1.69 ft³/s |
| Unit peak time, Tp | 0.278 hours |

| SCS Unit Hydrograph Parameters | |
|---|---|
| Unit receding limb, Tr | 1.112 hours |
| Total unit time, Tb | 1.389 hours |

| | |
|---|---|
| Storm Event | 10 yr |
| Return Event | 10 years |
| Duration | 24.000 hours |
| Depth | 5.8 in |
| Time of Concentration (Composite) | 0.163 hours |
| Scaled Area | 2.182 acres |

| | |
|---|---|
| Computational Time Increment | 0.022 hours |
| Time to Peak (Computed) | 11.996 hours |
| Flow (Peak, Computed) | 7.68 ft³/s |
| Output Increment | 0.005 hours |
| Time to Flow (Peak Interpolated Output) | 11.995 hours |
| Flow (Peak Interpolated Output) | 7.67 ft³/s |

| Drainage Area | |
|---|---|
| SCS CN (Composite) | 69.000 |
| Scaled Area | 2.182 acres |
| Maximum Retention (Pervious) | 4.5 in |
| Maximum Retention (Pervious, 20 percent) | 0.9 in |

| Cumulative Runoff | |
|---|---|
| Cumulative Runoff Depth (Pervious) | 2.6 in |
| Runoff Volume (Pervious) | 0.465 ac-ft |

| Hydrograph Volume (Area under Hydrograph curve) | |
|---|---|
| Volume | 0.464 ac-ft |

| SCS Unit Hydrograph Parameters | |
|---|---|
| Time of Concentration (Composite) | 0.163 hours |
| Computational Time Increment | 0.022 hours |
| Unit Hydrograph Shape Factor | 483.432 |
| K Factor | 0.749 |
| Receding/Rising, Tr/Tp | 1.670 |
| Unit peak, qp | 15.20 ft³/s |
| Unit peak time, Tp | 0.108 hours |

| SCS Unit Hydrograph Parameters | |
|---|---|
| Unit receding limb, Tr | 0.434 hours |
| Total unit time, Tb | 0.542 hours |

| | |
|---|---|
| Storm Event | 10 yr |
| Return Event | 10 years |
| Duration | 24.000 hours |
| Depth | 5.8 in |
| Time of Concentration (Composite) | 0.163 hours |
| Scaled Area | 0.449 acres |

| | |
|---|---|
| Computational Time Increment | 0.022 hours |
| Time to Peak (Computed) | 11.996 hours |
| Flow (Peak, Computed) | 1.58 ft³/s |
| Output Increment | 0.005 hours |
| Time to Flow (Peak Interpolated Output) | 11.995 hours |
| Flow (Peak Interpolated Output) | 1.58 ft³/s |

| Drainage Area | |
|---|---|
| SCS CN (Composite) | 69.000 |
| Scaled Area | 0.449 acres |
| Maximum Retention (Pervious) | 4.5 in |
| Maximum Retention (Pervious, 20 percent) | 0.9 in |

| Cumulative Runoff | |
|---|---|
| Cumulative Runoff Depth (Pervious) | 2.6 in |
| Runoff Volume (Pervious) | 0.096 ac-ft |

| Hydrograph Volume (Area under Hydrograph curve) | |
|---|---|
| Volume | 0.095 ac-ft |

| SCS Unit Hydrograph Parameters | |
|---|---|
| Time of Concentration (Composite) | 0.163 hours |
| Computational Time Increment | 0.022 hours |
| Unit Hydrograph Shape Factor | 483.432 |
| K Factor | 0.749 |
| Receding/Rising, Tr/Tp | 1.670 |
| Unit peak, qp | 3.13 ft³/s |
| Unit peak time, Tp | 0.108 hours |

| SCS Unit Hydrograph Parameters | |
|---|---|
| Unit receding limb, Tr | 0.434 hours |
| Total unit time, Tb | 0.542 hours |

| | |
|---|---|
| Storm Event | 10 yr |
| Return Event | 10 years |
| Duration | 24.000 hours |
| Depth | 5.8 in |
| Time of Concentration (Composite) | 0.182 hours |
| Scaled Area | 0.744 acres |

| | |
|---|---|
| Computational Time Increment | 0.024 hours |
| Time to Peak (Computed) | 12.005 hours |
| Flow (Peak, Computed) | 2.55 ft³/s |
| Output Increment | 0.005 hours |
| Time to Flow (Peak Interpolated Output) | 12.005 hours |
| Flow (Peak Interpolated Output) | 2.55 ft³/s |

| Drainage Area | |
|---|---|
| SCS CN (Composite) | 69.000 |
| Scaled Area | 0.744 acres |
| Maximum Retention (Pervious) | 4.5 in |
| Maximum Retention (Pervious, 20 percent) | 0.9 in |

| Cumulative Runoff | |
|---|---|
| Cumulative Runoff Depth (Pervious) | 2.6 in |
| Runoff Volume (Pervious) | 0.159 ac-ft |

| Hydrograph Volume (Area under Hydrograph curve) | |
|---|---|
| Volume | 0.158 ac-ft |

| SCS Unit Hydrograph Parameters | |
|---|---|
| Time of Concentration (Composite) | 0.182 hours |
| Computational Time Increment | 0.024 hours |
| Unit Hydrograph Shape Factor | 483.432 |
| K Factor | 0.749 |
| Receding/Rising, Tr/Tp | 1.670 |
| Unit peak, qp | 4.64 ft³/s |
| Unit peak time, Tp | 0.121 hours |

| SCS Unit Hydrograph Parameters | |
|---|---|
| Unit receding limb, Tr | 0.485 hours |
| Total unit time, Tb | 0.606 hours |

| | |
|---|---|
| Storm Event | 10 yr |
| Return Event | 10 years |
| Duration | 24.000 hours |
| Depth | 5.8 in |
| Time of Concentration (Composite) | 0.244 hours |
| Scaled Area | 5.261 acres |

| | |
|---|---|
| Computational Time Increment | 0.032 hours |
| Time to Peak (Computed) | 12.052 hours |
| Flow (Peak, Computed) | 16.40 ft³/s |
| Output Increment | 0.005 hours |
| Time to Flow (Peak Interpolated Output) | 12.050 hours |
| Flow (Peak Interpolated Output) | 16.38 ft³/s |

| Drainage Area | |
|---|---|
| SCS CN (Composite) | 69.000 |
| Scaled Area | 5.261 acres |
| Maximum Retention (Pervious) | 4.5 in |
| Maximum Retention (Pervious, 20 percent) | 0.9 in |

| Cumulative Runoff | |
|---|---|
| Cumulative Runoff Depth (Pervious) | 2.6 in |
| Runoff Volume (Pervious) | 1.121 ac-ft |

| Hydrograph Volume (Area under Hydrograph curve) | |
|---|---|
| Volume | 1.117 ac-ft |

| SCS Unit Hydrograph Parameters | |
|---|---|
| Time of Concentration (Composite) | 0.244 hours |
| Computational Time Increment | 0.032 hours |
| Unit Hydrograph Shape Factor | 483.432 |
| K Factor | 0.749 |
| Receding/Rising, Tr/Tp | 1.670 |
| Unit peak, qp | 24.46 ft³/s |
| Unit peak time, Tp | 0.162 hours |

| SCS Unit Hydrograph Parameters | |
|---|---|
| Unit receding limb, Tr | 0.650 hours |
| Total unit time, Tb | 0.812 hours |

| | |
|---|---|
| Storm Event | 10 yr |
| Return Event | 10 years |
| Duration | 24.000 hours |
| Depth | 5.8 in |
| Time of Concentration (Composite) | 0.086 hours |
| Scaled Area | 0.553 acres |

| | |
|---|---|
| Computational Time Increment | 0.012 hours |
| Time to Peak (Computed) | 11.928 hours |
| Flow (Peak, Computed) | 2.20 ft³/s |
| Output Increment | 0.005 hours |
| Time to Flow (Peak Interpolated Output) | 11.930 hours |
| Flow (Peak Interpolated Output) | 2.20 ft³/s |

| Drainage Area | |
|---|---|
| SCS CN (Composite) | 69.000 |
| Scaled Area | 0.553 acres |
| Maximum Retention (Pervious) | 4.5 in |
| Maximum Retention (Pervious, 20 percent) | 0.9 in |

| Cumulative Runoff | |
|---|---|
| Cumulative Runoff Depth (Pervious) | 2.6 in |
| Runoff Volume (Pervious) | 0.118 ac-ft |

| Hydrograph Volume (Area under Hydrograph curve) | |
|---|---|
| Volume | 0.118 ac-ft |

| SCS Unit Hydrograph Parameters | |
|---|---|
| Time of Concentration (Composite) | 0.086 hours |
| Computational Time Increment | 0.012 hours |
| Unit Hydrograph Shape Factor | 483.432 |
| K Factor | 0.749 |
| Receding/Rising, Tr/Tp | 1.670 |
| Unit peak, qp | 7.26 ft³/s |
| Unit peak time, Tp | 0.058 hours |

| SCS Unit Hydrograph Parameters | |
|---|---|
| Unit receding limb, Tr | 0.230 hours |
| Total unit time, Tb | 0.288 hours |

| | |
|---|---|
| Storm Event | 10 yr |
| Return Event | 10 years |
| Duration | 24.000 hours |
| Depth | 5.8 in |
| Time of Concentration (Composite) | 0.089 hours |
| Scaled Area | 0.171 acres |

| | |
|---|---|
| Computational Time Increment | 0.012 hours |
| Time to Peak (Computed) | 11.929 hours |
| Flow (Peak, Computed) | 0.68 ft³/s |
| Output Increment | 0.005 hours |
| Time to Flow (Peak Interpolated Output) | 11.930 hours |
| Flow (Peak Interpolated Output) | 0.68 ft³/s |

| Drainage Area | |
|---|---|
| SCS CN (Composite) | 69.000 |
| Scaled Area | 0.171 acres |
| Maximum Retention (Pervious) | 4.5 in |
| Maximum Retention (Pervious, 20 percent) | 0.9 in |

| Cumulative Runoff | |
|---|---|
| Cumulative Runoff Depth (Pervious) | 2.6 in |
| Runoff Volume (Pervious) | 0.036 ac-ft |

| Hydrograph Volume (Area under Hydrograph curve) | |
|---|---|
| Volume | 0.036 ac-ft |

| SCS Unit Hydrograph Parameters | |
|---|---|
| Time of Concentration (Composite) | 0.089 hours |
| Computational Time Increment | 0.012 hours |
| Unit Hydrograph Shape Factor | 483.432 |
| K Factor | 0.749 |
| Receding/Rising, Tr/Tp | 1.670 |
| Unit peak, qp | 2.18 ft³/s |
| Unit peak time, Tp | 0.059 hours |

| SCS Unit Hydrograph Parameters | |
|---|---|
| Unit receding limb, Tr | 0.237 hours |
| Total unit time, Tb | 0.296 hours |

| | |
|---|---|
| Storm Event | 10 yr |
| Return Event | 10 years |
| Duration | 24.000 hours |
| Depth | 5.8 in |
| Time of Concentration (Composite) | 0.142 hours |
| Scaled Area | 0.399 acres |

| | |
|---|---|
| Computational Time Increment | 0.019 hours |
| Time to Peak (Computed) | 11.967 hours |
| Flow (Peak, Computed) | 1.44 ft³/s |
| Output Increment | 0.005 hours |
| Time to Flow (Peak Interpolated Output) | 11.970 hours |
| Flow (Peak Interpolated Output) | 1.44 ft³/s |

| Drainage Area | |
|---|---|
| SCS CN (Composite) | 69.000 |
| Scaled Area | 0.399 acres |
| Maximum Retention (Pervious) | 4.5 in |
| Maximum Retention (Pervious, 20 percent) | 0.9 in |

| Cumulative Runoff | |
|---|---|
| Cumulative Runoff Depth (Pervious) | 2.6 in |
| Runoff Volume (Pervious) | 0.085 ac-ft |

| Hydrograph Volume (Area under Hydrograph curve) | |
|---|---|
| Volume | 0.085 ac-ft |

| SCS Unit Hydrograph Parameters | |
|---|---|
| Time of Concentration (Composite) | 0.142 hours |
| Computational Time Increment | 0.019 hours |
| Unit Hydrograph Shape Factor | 483.432 |
| K Factor | 0.749 |
| Receding/Rising, Tr/Tp | 1.670 |
| Unit peak, qp | 3.19 ft³/s |
| Unit peak time, Tp | 0.095 hours |

| SCS Unit Hydrograph Parameters | |
|---|---|
| Unit receding limb, Tr | 0.378 hours |
| Total unit time, Tb | 0.473 hours |

| | |
|---|---|
| Storm Event | 10 yr |
| Return Event | 10 years |
| Duration | 24.000 hours |
| Depth | 5.8 in |
| Time of Concentration (Composite) | 0.222 hours |
| Scaled Area | 1.886 acres |

| | |
|---|---|
| Computational Time Increment | 0.030 hours |
| Time to Peak (Computed) | 12.030 hours |
| Flow (Peak, Computed) | 6.11 ft³/s |
| Output Increment | 0.005 hours |
| Time to Flow (Peak Interpolated Output) | 12.030 hours |
| Flow (Peak Interpolated Output) | 6.11 ft³/s |

| Drainage Area | |
|---|---|
| SCS CN (Composite) | 69.000 |
| Scaled Area | 1.886 acres |
| Maximum Retention (Pervious) | 4.5 in |
| Maximum Retention (Pervious, 20 percent) | 0.9 in |

| Cumulative Runoff | |
|---|---|
| Cumulative Runoff Depth (Pervious) | 2.6 in |
| Runoff Volume (Pervious) | 0.402 ac-ft |

| Hydrograph Volume (Area under Hydrograph curve) | |
|---|---|
| Volume | 0.401 ac-ft |

| SCS Unit Hydrograph Parameters | |
|---|---|
| Time of Concentration (Composite) | 0.222 hours |
| Computational Time Increment | 0.030 hours |
| Unit Hydrograph Shape Factor | 483.432 |
| K Factor | 0.749 |
| Receding/Rising, Tr/Tp | 1.670 |
| Unit peak, qp | 9.64 ft³/s |
| Unit peak time, Tp | 0.148 hours |

| SCS Unit Hydrograph Parameters | |
|---|---|
| Unit receding limb, Tr | 0.591 hours |
| Total unit time, Tb | 0.739 hours |

| | |
|---|---|
| Storm Event | 10 yr |
| Return Event | 10 years |
| Duration | 24.000 hours |
| Depth | 5.8 in |
| Time of Concentration (Composite) | 0.129 hours |
| Scaled Area | 0.327 acres |

| | |
|---|---|
| Computational Time Increment | 0.017 hours |
| Time to Peak (Computed) | 11.960 hours |
| Flow (Peak, Computed) | 1.20 ft³/s |
| Output Increment | 0.005 hours |
| Time to Flow (Peak Interpolated Output) | 11.960 hours |
| Flow (Peak Interpolated Output) | 1.20 ft³/s |

| Drainage Area | |
|---|---|
| SCS CN (Composite) | 69.000 |
| Scaled Area | 0.327 acres |
| Maximum Retention (Pervious) | 4.5 in |
| Maximum Retention (Pervious, 20 percent) | 0.9 in |

| Cumulative Runoff | |
|---|---|
| Cumulative Runoff Depth (Pervious) | 2.6 in |
| Runoff Volume (Pervious) | 0.070 ac-ft |

| Hydrograph Volume (Area under Hydrograph curve) | |
|---|---|
| Volume | 0.070 ac-ft |

| SCS Unit Hydrograph Parameters | |
|---|---|
| Time of Concentration (Composite) | 0.129 hours |
| Computational Time Increment | 0.017 hours |
| Unit Hydrograph Shape Factor | 483.432 |
| K Factor | 0.749 |
| Receding/Rising, Tr/Tp | 1.670 |
| Unit peak, qp | 2.86 ft³/s |
| Unit peak time, Tp | 0.086 hours |

| SCS Unit Hydrograph Parameters | |
|---|---|
| Unit receding limb, Tr | 0.345 hours |
| Total unit time, Tb | 0.431 hours |

| | |
|---|---|
| Storm Event | 10 yr |
| Return Event | 10 years |
| Duration | 24.000 hours |
| Depth | 5.8 in |
| Time of Concentration (Composite) | 0.180 hours |
| Scaled Area | 0.357 acres |

| | |
|---|---|
| Computational Time Increment | 0.024 hours |
| Time to Peak (Computed) | 11.998 hours |
| Flow (Peak, Computed) | 1.23 ft³/s |
| Output Increment | 0.005 hours |
| Time to Flow (Peak Interpolated Output) | 12.000 hours |
| Flow (Peak Interpolated Output) | 1.23 ft³/s |

| Drainage Area | |
|---|---|
| SCS CN (Composite) | 69.000 |
| Scaled Area | 0.357 acres |
| Maximum Retention (Pervious) | 4.5 in |
| Maximum Retention (Pervious, 20 percent) | 0.9 in |

| Cumulative Runoff | |
|---|---|
| Cumulative Runoff Depth (Pervious) | 2.6 in |
| Runoff Volume (Pervious) | 0.076 ac-ft |

| Hydrograph Volume (Area under Hydrograph curve) | |
|---|---|
| Volume | 0.076 ac-ft |

| SCS Unit Hydrograph Parameters | |
|---|---|
| Time of Concentration (Composite) | 0.180 hours |
| Computational Time Increment | 0.024 hours |
| Unit Hydrograph Shape Factor | 483.432 |
| K Factor | 0.749 |
| Receding/Rising, Tr/Tp | 1.670 |
| Unit peak, qp | 2.25 ft³/s |
| Unit peak time, Tp | 0.120 hours |

| SCS Unit Hydrograph Parameters | |
|---|---|
| Unit receding limb, Tr | 0.480 hours |
| Total unit time, Tb | 0.600 hours |

## Solution to Manning's Open Channel Flow Equation
## (Computed values are based on normal depth.)

**Q = (k/n) * A * (R**2/3) * (S**1/2)**

| where: | English Units | SI units |
|---|---|---|
| Q = Channel Flow | cfs | cms |
| k = Manning's Constant | 1.485919 | 1.0 |
| n = Manning's n | no units | no units |
| R = Hydraulic radius, A/WP | feet | meter |
| A = X-section flow area | ft^2 | m^2 |
| WP = Wetted perimeter | feet | meter |
| S = Slope | ft/ft | m/m |

**Additional Output Variables:**
**Vel= Q/A**
**Hd = A/TpW**
**F = Vel / (g * Hd)**1/2**

| where: | English Units | SI units |
|---|---|---|
| Q = Channel Flow | cfs | cms |
| k = Manning's Constant | 1.485919 | 1.0 |
| n = Manning's n | no units | no units |
| R = Hydraulic radius, A/WP | feet | meter |
| A = X-section flow area | ft^2 | m^2 |
| WP = Wetted perimeter | feet | meter |
| S = Slope | ft/ft | m/m |

## Solution to Manning's Open Channel Flow Equation
## (Computed values are based on normal depth.)

**Q = (k/n) * A * (R**2/3) * (S**1/2)**

| where: | English Units | SI units |
|---|---|---|
| Q = Channel Flow | cfs | cms |
| k = Manning's Constant | 1.485919 | 1.0 |
| n = Manning's n | no units | no units |
| R = Hydraulic radius, A/WP | feet | meter |
| A = X-section flow area | ft^2 | m^2 |
| WP = Wetted perimeter | feet | meter |
| S = Slope | ft/ft | m/m |

**Additional Output Variables:**
**Vel= Q/A**
**Hd = A/TpW**
**F = Vel / (g * Hd)**1/2**

| where: | English Units | SI units |
|---|---|---|
| Q = Channel Flow | cfs | cms |
| k = Manning's Constant | 1.485919 | 1.0 |
| n = Manning's n | no units | no units |
| R = Hydraulic radius, A/WP | feet | meter |
| A = X-section flow area | ft^2 | m^2 |
| WP = Wetted perimeter | feet | meter |
| S = Slope | ft/ft | m/m |

## Solution to Manning's Open Channel Flow Equation
## (Computed values are based on normal depth.)

**Q = (k/n) * A * (R**2/3) * (S**1/2)**

| where: | English Units | SI units |
|---|---|---|
| Q = Channel Flow | cfs | cms |
| k = Manning's Constant | 1.485919 | 1.0 |
| n = Manning's n | no units | no units |
| R = Hydraulic radius, A/WP | feet | meter |
| A = X-section flow area | ft^2 | m^2 |
| WP = Wetted perimeter | feet | meter |
| S = Slope | ft/ft | m/m |

**Additional Output Variables:**
**Vel= Q/A**
**Hd = A/TpW**
**F = Vel / (g * Hd)**1/2**

| where: | English Units | SI units |
|---|---|---|
| Q = Channel Flow | cfs | cms |
| k = Manning's Constant | 1.485919 | 1.0 |
| n = Manning's n | no units | no units |
| R = Hydraulic radius, A/WP | feet | meter |
| A = X-section flow area | ft^2 | m^2 |
| WP = Wetted perimeter | feet | meter |
| S = Slope | ft/ft | m/m |

## Solution to Manning's Open Channel Flow Equation
## (Computed values are based on normal depth.)

**Q = (k/n) * A * (R**2/3) * (S**1/2)**

| where: | English Units | SI units |
|---|---|---|
| Q = Channel Flow | cfs | cms |
| k = Manning's Constant | 1.485919 | 1.0 |
| n = Manning's n | no units | no units |
| R = Hydraulic radius, A/WP | feet | meter |
| A = X-section flow area | ft^2 | m^2 |
| WP = Wetted perimeter | feet | meter |
| S = Slope | ft/ft | m/m |

**Additional Output Variables:**
**Vel= Q/A**
**Hd = A/TpW**
**F = Vel / (g * Hd)**1/2**

| where: | English Units | SI units |
|---|---|---|
| Q = Channel Flow | cfs | cms |
| k = Manning's Constant | 1.485919 | 1.0 |
| n = Manning's n | no units | no units |
| R = Hydraulic radius, A/WP | feet | meter |
| A = X-section flow area | ft^2 | m^2 |
| WP = Wetted perimeter | feet | meter |
| S = Slope | ft/ft | m/m |

| Modified Puls Results Summary | |
|---|---|
| Length (Channel) | 524.75 ft |
| Travel Time (Channel) | 0.058 hours |
| Number of Sections | 12 |
| Length (Section) | 43.73 ft |
| Flow (Weighted) | 2.73 ft³/s |
| Overflow Channel | No Overflow Data |
| Elevation (Overflow) | 132.00 ft |

| Infiltration | |
|---|---|
| Infiltration Method (Computed) | No Infiltration |

| Initial Conditions | |
|---|---|
| Elevation (Starting Water Surface) | 130.00 ft |
| Volume (Starting, per section) | 0.000 ac-ft |
| Flow (Out Starting) | 0.00 ft³/s |
| Infiltration (Starting, per section) | 0.00 ft³/s |
| Flow (Total Out Starting) | 0.00 ft³/s |
| Time Increment | 0.005 hours |

**Number of sections = 12**
**Storage, Area, Infiltration (per 43.73 ft section)**

| Elevation (ft) | Outflow (ft³/s) | Storage (ac-ft) | Area (acres) | Infiltration (ft³/s) | Flow (Total) (ft³/s) | 2S/t + O (ft³/s) |
|---|---|---|---|---|---|---|
| 130.00 | 0.00 | 0.000 | 0.000 | 0.00 | 0.00 | 0.00 |
| 130.01 | 0.01 | 0.000 | 0.003 | 0.00 | 0.01 | 0.16 |
| 130.04 | 0.10 | 0.000 | 0.003 | 0.00 | 0.10 | 0.70 |
| 130.08 | 0.31 | 0.000 | 0.003 | 0.00 | 0.31 | 1.57 |
| 130.12 | 0.62 | 0.000 | 0.004 | 0.00 | 0.62 | 2.58 |
| 130.16 | 1.02 | 0.001 | 0.004 | 0.00 | 1.02 | 3.73 |
| 130.20 | 1.50 | 0.001 | 0.004 | 0.00 | 1.50 | 5.00 |
| 130.24 | 2.07 | 0.001 | 0.004 | 0.00 | 2.07 | 6.41 |
| 130.28 | 2.72 | 0.001 | 0.005 | 0.00 | 2.72 | 7.95 |
| 130.32 | 3.46 | 0.001 | 0.005 | 0.00 | 3.46 | 9.62 |
| 130.36 | 4.28 | 0.001 | 0.005 | 0.00 | 4.28 | 11.42 |
| 130.40 | 5.19 | 0.002 | 0.005 | 0.00 | 5.19 | 13.35 |
| 130.44 | 6.19 | 0.002 | 0.006 | 0.00 | 6.19 | 15.43 |
| 130.48 | 7.28 | 0.002 | 0.006 | 0.00 | 7.28 | 17.63 |
| 130.52 | 8.46 | 0.002 | 0.006 | 0.00 | 8.46 | 19.98 |
| 130.56 | 9.74 | 0.003 | 0.006 | 0.00 | 9.74 | 22.47 |
| 130.60 | 11.11 | 0.003 | 0.007 | 0.00 | 11.11 | 25.10 |
| 130.64 | 12.58 | 0.003 | 0.007 | 0.00 | 12.58 | 27.88 |

**Number of sections = 12**
**Storage, Area, Infiltration (per 43.73 ft section)**

| Elevation (ft) | Outflow ($ft^3/s$) | Storage (ac-ft) | Area (acres) | Infiltration ($ft^3/s$) | Flow (Total) ($ft^3/s$) | 2S/t + O ($ft^3/s$) |
|---|---|---|---|---|---|---|
| 130.68 | 14.15 | 0.003 | 0.007 | 0.00 | 14.15 | 30.81 |
| 130.72 | 15.83 | 0.004 | 0.007 | 0.00 | 15.83 | 33.88 |
| 130.76 | 17.61 | 0.004 | 0.008 | 0.00 | 17.61 | 37.10 |
| 130.80 | 19.49 | 0.004 | 0.008 | 0.00 | 19.49 | 40.48 |
| 130.84 | 21.48 | 0.005 | 0.008 | 0.00 | 21.48 | 44.01 |
| 130.88 | 23.59 | 0.005 | 0.008 | 0.00 | 23.59 | 47.70 |
| 130.92 | 25.80 | 0.005 | 0.009 | 0.00 | 25.80 | 51.55 |
| 130.96 | 28.13 | 0.006 | 0.009 | 0.00 | 28.13 | 55.56 |
| 131.00 | 30.58 | 0.006 | 0.009 | 0.00 | 30.58 | 59.73 |
| 131.04 | 33.14 | 0.006 | 0.009 | 0.00 | 33.14 | 64.07 |
| 131.08 | 35.83 | 0.007 | 0.010 | 0.00 | 35.83 | 68.57 |
| 131.12 | 38.63 | 0.007 | 0.010 | 0.00 | 38.63 | 73.24 |
| 131.16 | 41.56 | 0.008 | 0.010 | 0.00 | 41.56 | 78.09 |
| 131.20 | 44.62 | 0.008 | 0.010 | 0.00 | 44.62 | 83.10 |
| 131.24 | 47.80 | 0.008 | 0.010 | 0.00 | 47.80 | 88.29 |
| 131.28 | 51.12 | 0.009 | 0.011 | 0.00 | 51.12 | 93.66 |
| 131.32 | 54.56 | 0.009 | 0.011 | 0.00 | 54.56 | 99.20 |
| 131.36 | 58.14 | 0.010 | 0.011 | 0.00 | 58.14 | 104.93 |
| 131.40 | 61.86 | 0.010 | 0.011 | 0.00 | 61.86 | 110.84 |
| 131.44 | 65.71 | 0.011 | 0.012 | 0.00 | 65.71 | 116.93 |
| 131.48 | 69.71 | 0.011 | 0.012 | 0.00 | 69.71 | 123.21 |
| 131.52 | 73.84 | 0.012 | 0.012 | 0.00 | 73.84 | 129.67 |
| 131.56 | 78.12 | 0.012 | 0.012 | 0.00 | 78.12 | 136.33 |
| 131.60 | 82.54 | 0.013 | 0.013 | 0.00 | 82.54 | 143.17 |
| 131.64 | 87.10 | 0.013 | 0.013 | 0.00 | 87.10 | 150.21 |
| 131.68 | 91.82 | 0.014 | 0.013 | 0.00 | 91.82 | 157.45 |
| 131.72 | 96.69 | 0.014 | 0.013 | 0.00 | 96.69 | 164.88 |
| 131.76 | 101.71 | 0.015 | 0.014 | 0.00 | 101.71 | 172.51 |
| 131.80 | 106.88 | 0.015 | 0.014 | 0.00 | 106.88 | 180.34 |
| 131.84 | 112.21 | 0.016 | 0.014 | 0.00 | 112.21 | 188.38 |
| 131.88 | 117.69 | 0.016 | 0.014 | 0.00 | 117.69 | 196.62 |
| 131.92 | 123.34 | 0.017 | 0.015 | 0.00 | 123.34 | 205.06 |
| 131.96 | 129.14 | 0.017 | 0.015 | 0.00 | 129.14 | 213.71 |
| 132.00 | 135.11 | 0.018 | 0.015 | 0.00 | 135.11 | 222.57 |

| Modified Puls Results Summary | |
|---|---|
| Length (Channel) | 245.95 ft |
| Travel Time (Channel) | 0.020 hours |
| Number of Sections | 1 |
| Length (Section) | 245.95 ft |
| Flow (Weighted) | 2.59 ft³/s |
| Overflow Channel | No Overflow Data |
| Elevation (Overflow) | 131.00 ft |

| Infiltration | |
|---|---|
| Infiltration Method (Computed) | No Infiltration |

| Initial Conditions | |
|---|---|
| Elevation (Starting Water Surface) | 129.00 ft |
| Volume (Starting, per section) | 0.000 ac-ft |
| Flow (Out Starting) | 0.00 ft³/s |
| Infiltration (Starting, per section) | 0.00 ft³/s |
| Flow (Total Out Starting) | 0.00 ft³/s |
| Time Increment | 0.005 hours |

**Number of sections = 1**
**Storage, Area, Infiltration (per 245.95 ft section)**

| Elevation (ft) | Outflow (ft³/s) | Storage (ac-ft) | Area (acres) | Infiltration (ft³/s) | Flow (Total) (ft³/s) | 2S/t + O (ft³/s) |
|---|---|---|---|---|---|---|
| 129.00 | 0.00 | 0.000 | 0.000 | 0.00 | 0.00 | 0.00 |
| 129.01 | 0.01 | 0.000 | 0.017 | 0.00 | 0.01 | 0.84 |
| 129.04 | 0.15 | 0.001 | 0.018 | 0.00 | 0.15 | 3.56 |
| 129.08 | 0.48 | 0.001 | 0.020 | 0.00 | 0.48 | 7.56 |
| 129.12 | 0.95 | 0.002 | 0.021 | 0.00 | 0.95 | 11.97 |
| 129.16 | 1.56 | 0.003 | 0.022 | 0.00 | 1.56 | 16.78 |
| 129.20 | 2.30 | 0.004 | 0.024 | 0.00 | 2.30 | 21.98 |
| 129.24 | 3.17 | 0.005 | 0.025 | 0.00 | 3.17 | 27.57 |
| 129.28 | 4.17 | 0.006 | 0.026 | 0.00 | 4.17 | 33.55 |
| 129.32 | 5.30 | 0.007 | 0.028 | 0.00 | 5.30 | 39.93 |
| 129.36 | 6.56 | 0.008 | 0.029 | 0.00 | 6.56 | 46.70 |
| 129.40 | 7.95 | 0.009 | 0.030 | 0.00 | 7.95 | 53.86 |
| 129.44 | 9.48 | 0.011 | 0.032 | 0.00 | 9.48 | 61.43 |
| 129.48 | 11.15 | 0.012 | 0.033 | 0.00 | 11.15 | 69.39 |
| 129.52 | 12.96 | 0.013 | 0.035 | 0.00 | 12.96 | 77.76 |
| 129.56 | 14.92 | 0.015 | 0.036 | 0.00 | 14.92 | 86.54 |
| 129.60 | 17.02 | 0.016 | 0.037 | 0.00 | 17.02 | 95.73 |
| 129.64 | 19.28 | 0.018 | 0.039 | 0.00 | 19.28 | 105.33 |

**Number of sections = 1**
**Storage, Area, Infiltration (per 245.95 ft section)**

| Elevation (ft) | Outflow ($ft^3/s$) | Storage (ac-ft) | Area (acres) | Infiltration ($ft^3/s$) | Flow (Total) ($ft^3/s$) | 2S/t + O ($ft^3/s$) |
|---|---|---|---|---|---|---|
| 129.68 | 21.68 | 0.019 | 0.040 | 0.00 | 21.68 | 115.34 |
| 129.72 | 24.25 | 0.021 | 0.041 | 0.00 | 24.25 | 125.78 |
| 129.76 | 26.97 | 0.023 | 0.043 | 0.00 | 26.97 | 136.63 |
| 129.80 | 29.86 | 0.024 | 0.044 | 0.00 | 29.86 | 147.91 |
| 129.84 | 32.91 | 0.026 | 0.045 | 0.00 | 32.91 | 159.62 |
| 129.88 | 36.13 | 0.028 | 0.047 | 0.00 | 36.13 | 171.77 |
| 129.92 | 39.53 | 0.030 | 0.048 | 0.00 | 39.53 | 184.34 |
| 129.96 | 43.10 | 0.032 | 0.049 | 0.00 | 43.10 | 197.35 |
| 130.00 | 46.84 | 0.034 | 0.051 | 0.00 | 46.84 | 210.81 |
| 130.04 | 50.77 | 0.036 | 0.052 | 0.00 | 50.77 | 224.71 |
| 130.08 | 54.88 | 0.038 | 0.054 | 0.00 | 54.88 | 239.05 |
| 130.12 | 59.18 | 0.040 | 0.055 | 0.00 | 59.18 | 253.84 |
| 130.16 | 63.67 | 0.042 | 0.056 | 0.00 | 63.67 | 269.09 |
| 130.20 | 68.36 | 0.045 | 0.058 | 0.00 | 68.36 | 284.79 |
| 130.24 | 73.23 | 0.047 | 0.059 | 0.00 | 73.23 | 300.95 |
| 130.28 | 78.31 | 0.049 | 0.060 | 0.00 | 78.31 | 317.57 |
| 130.32 | 83.59 | 0.052 | 0.062 | 0.00 | 83.59 | 334.66 |
| 130.36 | 89.08 | 0.054 | 0.063 | 0.00 | 89.08 | 352.21 |
| 130.40 | 94.77 | 0.057 | 0.064 | 0.00 | 94.77 | 370.23 |
| 130.44 | 100.67 | 0.060 | 0.066 | 0.00 | 100.67 | 388.72 |
| 130.48 | 106.79 | 0.062 | 0.067 | 0.00 | 106.79 | 407.70 |
| 130.52 | 113.12 | 0.065 | 0.068 | 0.00 | 113.12 | 427.15 |
| 130.56 | 119.67 | 0.068 | 0.070 | 0.00 | 119.67 | 447.08 |
| 130.60 | 126.44 | 0.070 | 0.071 | 0.00 | 126.44 | 467.49 |
| 130.64 | 133.44 | 0.073 | 0.072 | 0.00 | 133.44 | 488.39 |
| 130.68 | 140.67 | 0.076 | 0.074 | 0.00 | 140.67 | 509.79 |
| 130.72 | 148.12 | 0.079 | 0.075 | 0.00 | 148.12 | 531.67 |
| 130.76 | 155.81 | 0.082 | 0.077 | 0.00 | 155.81 | 554.05 |
| 130.80 | 163.74 | 0.085 | 0.078 | 0.00 | 163.74 | 576.93 |
| 130.84 | 171.90 | 0.089 | 0.079 | 0.00 | 171.90 | 600.31 |
| 130.88 | 180.30 | 0.092 | 0.081 | 0.00 | 180.30 | 624.19 |
| 130.92 | 188.95 | 0.095 | 0.082 | 0.00 | 188.95 | 648.58 |
| 130.96 | 197.84 | 0.098 | 0.083 | 0.00 | 197.84 | 673.47 |
| 131.00 | 206.99 | 0.102 | 0.085 | 0.00 | 206.99 | 698.88 |

| Modified Puls Results Summary | |
|---|---|
| Length (Channel) | 156.30 ft |
| Travel Time (Channel) | 0.024 hours |
| Number of Sections | 1 |
| Length (Section) | 156.30 ft |
| Flow (Weighted) | 0.86 ft³/s |
| Overflow Channel | No Overflow Data |
| Elevation (Overflow) | 121.00 ft |

| Infiltration | |
|---|---|
| Infiltration Method (Computed) | No Infiltration |

| Initial Conditions | |
|---|---|
| Elevation (Starting Water Surface) | 120.00 ft |
| Volume (Starting, per section) | 0.000 ac-ft |
| Flow (Out Starting) | 0.00 ft³/s |
| Infiltration (Starting, per section) | 0.00 ft³/s |
| Flow (Total Out Starting) | 0.00 ft³/s |
| Time Increment | 0.005 hours |

**Number of sections = 1**
**Storage, Area, Infiltration (per 156.30 ft section)**

| Elevation (ft) | Outflow (ft³/s) | Storage (ac-ft) | Area (acres) | Infiltration (ft³/s) | Flow (Total) (ft³/s) | 2S/t + O (ft³/s) |
|---|---|---|---|---|---|---|
| 120.00 | 0.00 | 0.000 | 0.000 | 0.00 | 0.00 | 0.00 |
| 120.01 | 0.00 | 0.000 | 0.000 | 0.00 | 0.00 | 0.01 |
| 120.02 | 0.00 | 0.000 | 0.000 | 0.00 | 0.00 | 0.02 |
| 120.04 | 0.00 | 0.000 | 0.001 | 0.00 | 0.00 | 0.09 |
| 120.06 | 0.01 | 0.000 | 0.001 | 0.00 | 0.01 | 0.19 |
| 120.08 | 0.01 | 0.000 | 0.002 | 0.00 | 0.01 | 0.35 |
| 120.10 | 0.02 | 0.000 | 0.002 | 0.00 | 0.02 | 0.54 |
| 120.12 | 0.04 | 0.000 | 0.003 | 0.00 | 0.04 | 0.79 |
| 120.14 | 0.05 | 0.000 | 0.003 | 0.00 | 0.05 | 1.08 |
| 120.16 | 0.08 | 0.000 | 0.003 | 0.00 | 0.08 | 1.41 |
| 120.18 | 0.11 | 0.000 | 0.004 | 0.00 | 0.11 | 1.79 |
| 120.20 | 0.14 | 0.000 | 0.004 | 0.00 | 0.14 | 2.22 |
| 120.22 | 0.18 | 0.001 | 0.005 | 0.00 | 0.18 | 2.70 |
| 120.24 | 0.23 | 0.001 | 0.005 | 0.00 | 0.23 | 3.23 |
| 120.26 | 0.28 | 0.001 | 0.006 | 0.00 | 0.28 | 3.80 |
| 120.28 | 0.34 | 0.001 | 0.006 | 0.00 | 0.34 | 4.43 |
| 120.30 | 0.41 | 0.001 | 0.006 | 0.00 | 0.41 | 5.10 |
| 120.32 | 0.49 | 0.001 | 0.007 | 0.00 | 0.49 | 5.82 |

**Number of sections = 1**
**Storage, Area, Infiltration (per 156.30 ft section)**

| Elevation (ft) | Outflow ($ft^3/s$) | Storage (ac-ft) | Area (acres) | Infiltration ($ft^3/s$) | Flow (Total) ($ft^3/s$) | 2S/t + O ($ft^3/s$) |
|---|---|---|---|---|---|---|
| 120.34 | 0.58 | 0.001 | 0.007 | 0.00 | 0.58 | 6.60 |
| 120.36 | 0.67 | 0.001 | 0.008 | 0.00 | 0.67 | 7.42 |
| 120.38 | 0.77 | 0.002 | 0.008 | 0.00 | 0.77 | 8.30 |
| 120.40 | 0.89 | 0.002 | 0.009 | 0.00 | 0.89 | 9.22 |
| 120.42 | 1.01 | 0.002 | 0.009 | 0.00 | 1.01 | 10.20 |
| 120.44 | 1.14 | 0.002 | 0.009 | 0.00 | 1.14 | 11.23 |
| 120.46 | 1.29 | 0.002 | 0.010 | 0.00 | 1.29 | 12.31 |
| 120.48 | 1.44 | 0.002 | 0.010 | 0.00 | 1.44 | 13.45 |
| 120.50 | 1.61 | 0.003 | 0.011 | 0.00 | 1.61 | 14.64 |
| 120.52 | 1.79 | 0.003 | 0.011 | 0.00 | 1.79 | 15.88 |
| 120.54 | 1.98 | 0.003 | 0.012 | 0.00 | 1.98 | 17.17 |
| 120.56 | 2.18 | 0.003 | 0.012 | 0.00 | 2.18 | 18.52 |
| 120.58 | 2.39 | 0.004 | 0.012 | 0.00 | 2.39 | 19.92 |
| 120.60 | 2.62 | 0.004 | 0.013 | 0.00 | 2.62 | 21.37 |
| 120.62 | 2.86 | 0.004 | 0.013 | 0.00 | 2.86 | 22.88 |
| 120.64 | 3.11 | 0.004 | 0.014 | 0.00 | 3.11 | 24.45 |
| 120.66 | 3.38 | 0.005 | 0.014 | 0.00 | 3.38 | 26.07 |
| 120.68 | 3.66 | 0.005 | 0.015 | 0.00 | 3.66 | 27.75 |
| 120.70 | 3.95 | 0.005 | 0.015 | 0.00 | 3.95 | 29.48 |
| 120.72 | 4.26 | 0.006 | 0.016 | 0.00 | 4.26 | 31.27 |
| 120.74 | 4.58 | 0.006 | 0.016 | 0.00 | 4.58 | 33.11 |
| 120.76 | 4.92 | 0.006 | 0.016 | 0.00 | 4.92 | 35.01 |
| 120.78 | 5.27 | 0.007 | 0.017 | 0.00 | 5.27 | 36.97 |
| 120.80 | 5.64 | 0.007 | 0.017 | 0.00 | 5.64 | 38.98 |
| 120.82 | 6.02 | 0.007 | 0.018 | 0.00 | 6.02 | 41.05 |
| 120.84 | 6.42 | 0.008 | 0.018 | 0.00 | 6.42 | 43.18 |
| 120.86 | 6.84 | 0.008 | 0.019 | 0.00 | 6.84 | 45.37 |
| 120.88 | 7.27 | 0.008 | 0.019 | 0.00 | 7.27 | 47.62 |
| 120.90 | 7.72 | 0.009 | 0.019 | 0.00 | 7.72 | 49.92 |
| 120.92 | 8.19 | 0.009 | 0.020 | 0.00 | 8.19 | 52.28 |
| 120.94 | 8.67 | 0.010 | 0.020 | 0.00 | 8.67 | 54.70 |
| 120.96 | 9.17 | 0.010 | 0.021 | 0.00 | 9.17 | 57.18 |
| 120.98 | 9.69 | 0.010 | 0.021 | 0.00 | 9.69 | 59.72 |
| 121.00 | 10.22 | 0.011 | 0.022 | 0.00 | 10.22 | 62.32 |

Subsection: Elevation-Volume-Flow Table (Channel)
Label: CO-89

Return Event: 10 years
Storm Event: 10 yr

| Modified Puls Results Summary | |
|---|---|
| Length (Channel) | 312.17 ft |
| Travel Time (Channel) | 0.025 hours |
| Number of Sections | 1 |
| Length (Section) | 312.17 ft |
| Flow (Weighted) | 5.65 ft³/s |
| Overflow Channel | No Overflow Data |
| Elevation (Overflow) | 134.00 ft |

| Infiltration | |
|---|---|
| Infiltration Method (Computed) | No Infiltration |

| Initial Conditions | |
|---|---|
| Elevation (Starting Water Surface) | 132.00 ft |
| Volume (Starting, per section) | 0.000 ac-ft |
| Flow (Out Starting) | 0.00 ft³/s |
| Infiltration (Starting, per section) | 0.00 ft³/s |
| Flow (Total Out Starting) | 0.00 ft³/s |
| Time Increment | 0.005 hours |

**Number of sections = 1**
**Storage, Area, Infiltration (per 312.17 ft section)**

| Elevation (ft) | Outflow (ft³/s) | Storage (ac-ft) | Area (acres) | Infiltration (ft³/s) | Flow (Total) (ft³/s) | 2S/t + O (ft³/s) |
|---|---|---|---|---|---|---|
| 132.00 | 0.00 | 0.000 | 0.000 | 0.00 | 0.00 | 0.00 |
| 132.01 | 0.00 | 0.000 | 0.000 | 0.00 | 0.00 | 0.01 |
| 132.04 | 0.00 | 0.000 | 0.002 | 0.00 | 0.00 | 0.17 |
| 132.08 | 0.01 | 0.000 | 0.003 | 0.00 | 0.01 | 0.68 |
| 132.12 | 0.04 | 0.000 | 0.005 | 0.00 | 0.04 | 1.54 |
| 132.16 | 0.09 | 0.001 | 0.007 | 0.00 | 0.09 | 2.76 |
| 132.20 | 0.17 | 0.001 | 0.009 | 0.00 | 0.17 | 4.33 |
| 132.24 | 0.28 | 0.001 | 0.010 | 0.00 | 0.28 | 6.27 |
| 132.28 | 0.42 | 0.002 | 0.012 | 0.00 | 0.42 | 8.58 |
| 132.32 | 0.60 | 0.002 | 0.014 | 0.00 | 0.60 | 11.26 |
| 132.36 | 0.82 | 0.003 | 0.015 | 0.00 | 0.82 | 14.31 |
| 132.40 | 1.09 | 0.003 | 0.017 | 0.00 | 1.09 | 17.74 |
| 132.44 | 1.40 | 0.004 | 0.019 | 0.00 | 1.40 | 21.55 |
| 132.48 | 1.77 | 0.005 | 0.021 | 0.00 | 1.77 | 25.74 |
| 132.52 | 2.19 | 0.006 | 0.022 | 0.00 | 2.19 | 30.33 |
| 132.56 | 2.67 | 0.007 | 0.024 | 0.00 | 2.67 | 35.30 |
| 132.60 | 3.21 | 0.008 | 0.026 | 0.00 | 3.21 | 40.67 |
| 132.64 | 3.81 | 0.009 | 0.028 | 0.00 | 3.81 | 46.43 |

**Number of sections = 1**
**Storage, Area, Infiltration (per 312.17 ft section)**

| Elevation (ft) | Outflow ($ft^3/s$) | Storage (ac-ft) | Area (acres) | Infiltration ($ft^3/s$) | Flow (Total) ($ft^3/s$) | 2S/t + O ($ft^3/s$) |
|---|---|---|---|---|---|---|
| 132.68 | 4.48 | 0.010 | 0.029 | 0.00 | 4.48 | 52.60 |
| 132.72 | 5.22 | 0.011 | 0.031 | 0.00 | 5.22 | 59.16 |
| 132.76 | 6.03 | 0.012 | 0.033 | 0.00 | 6.03 | 66.13 |
| 132.80 | 6.91 | 0.014 | 0.034 | 0.00 | 6.91 | 73.51 |
| 132.84 | 7.87 | 0.015 | 0.036 | 0.00 | 7.87 | 81.29 |
| 132.88 | 8.91 | 0.017 | 0.038 | 0.00 | 8.91 | 89.49 |
| 132.92 | 10.03 | 0.018 | 0.040 | 0.00 | 10.03 | 98.11 |
| 132.96 | 11.24 | 0.020 | 0.041 | 0.00 | 11.24 | 107.14 |
| 133.00 | 12.53 | 0.022 | 0.043 | 0.00 | 12.53 | 116.59 |
| 133.04 | 13.91 | 0.023 | 0.045 | 0.00 | 13.91 | 126.46 |
| 133.08 | 15.38 | 0.025 | 0.046 | 0.00 | 15.38 | 136.76 |
| 133.12 | 16.95 | 0.027 | 0.048 | 0.00 | 16.95 | 147.48 |
| 133.16 | 18.61 | 0.029 | 0.050 | 0.00 | 18.61 | 158.63 |
| 133.20 | 20.37 | 0.031 | 0.052 | 0.00 | 20.37 | 170.22 |
| 133.24 | 22.24 | 0.033 | 0.053 | 0.00 | 22.24 | 182.23 |
| 133.28 | 24.20 | 0.035 | 0.055 | 0.00 | 24.20 | 194.69 |
| 133.32 | 26.27 | 0.037 | 0.057 | 0.00 | 26.27 | 207.58 |
| 133.36 | 28.45 | 0.040 | 0.058 | 0.00 | 28.45 | 220.91 |
| 133.40 | 30.73 | 0.042 | 0.060 | 0.00 | 30.73 | 234.69 |
| 133.44 | 33.13 | 0.045 | 0.062 | 0.00 | 33.13 | 248.90 |
| 133.48 | 35.64 | 0.047 | 0.064 | 0.00 | 35.64 | 263.57 |
| 133.52 | 38.27 | 0.050 | 0.065 | 0.00 | 38.27 | 278.68 |
| 133.56 | 41.01 | 0.052 | 0.067 | 0.00 | 41.01 | 294.25 |
| 133.60 | 43.88 | 0.055 | 0.069 | 0.00 | 43.88 | 310.27 |
| 133.64 | 46.87 | 0.058 | 0.071 | 0.00 | 46.87 | 326.74 |
| 133.68 | 49.98 | 0.061 | 0.072 | 0.00 | 49.98 | 343.67 |
| 133.72 | 53.21 | 0.064 | 0.074 | 0.00 | 53.21 | 361.05 |
| 133.76 | 56.58 | 0.067 | 0.076 | 0.00 | 56.58 | 378.90 |
| 133.80 | 60.07 | 0.070 | 0.077 | 0.00 | 60.07 | 397.22 |
| 133.84 | 63.70 | 0.073 | 0.079 | 0.00 | 63.70 | 415.99 |
| 133.88 | 67.46 | 0.076 | 0.081 | 0.00 | 67.46 | 435.24 |
| 133.92 | 71.35 | 0.079 | 0.083 | 0.00 | 71.35 | 454.95 |
| 133.96 | 75.38 | 0.083 | 0.084 | 0.00 | 75.38 | 475.13 |
| 134.00 | 79.56 | 0.086 | 0.086 | 0.00 | 79.56 | 495.79 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 0.000 | 130.00 | 130.03 | 130.03 | 130.03 | 130.03 |
| 0.025 | 130.03 | 130.03 | 130.03 | 130.03 | 130.03 |
| 0.050 | 130.03 | 130.03 | 130.03 | 130.03 | 130.03 |
| 0.075 | 130.03 | 130.03 | 130.03 | 130.03 | 130.03 |
| 0.100 | 130.02 | 130.02 | 130.02 | 130.02 | 130.02 |
| 0.125 | 130.02 | 130.02 | 130.02 | 130.02 | 130.02 |
| 0.150 | 130.02 | 130.02 | 130.01 | 130.01 | 130.01 |
| 0.175 | 130.01 | 130.01 | 130.01 | 130.01 | 130.01 |
| 0.200 | 130.01 | 130.01 | 130.01 | 130.01 | 130.01 |
| 0.225 | 130.01 | 130.01 | 130.01 | 130.01 | 130.01 |
| 0.250 | 130.01 | 130.01 | 130.01 | 130.01 | 130.01 |
| 0.275 | 130.01 | 130.01 | 130.01 | 130.01 | 130.01 |
| 0.300 | 130.01 | 130.01 | 130.01 | 130.01 | 130.01 |
| 0.325 | 130.01 | 130.01 | 130.01 | 130.01 | 130.01 |
| 0.350 | 130.01 | 130.01 | 130.01 | 130.01 | 130.01 |
| 0.375 | 130.01 | 130.01 | 130.01 | 130.01 | 130.01 |
| 0.400 | 130.01 | 130.01 | 130.01 | 130.01 | 130.01 |
| 0.425 | 130.01 | 130.01 | 130.01 | 130.01 | 130.01 |
| 0.450 | 130.01 | 130.00 | 130.00 | 130.00 | 130.00 |
| 0.475 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 0.500 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 0.525 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 0.550 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 0.575 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 0.600 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 0.625 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 0.650 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 0.675 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 0.700 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 0.725 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 0.750 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 0.775 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 0.800 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 0.825 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 0.850 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 0.875 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 0.900 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 0.925 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 0.950 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 0.975 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 1.000 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 1.025 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 1.050 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 1.075 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 1.100 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 1.125 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 1.150 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 1.175 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 1.200 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 1.225 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 1.250 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 1.275 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 1.300 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 1.325 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 1.350 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 1.375 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 1.400 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 1.425 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 1.450 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 1.475 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 1.500 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 1.525 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 1.550 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 1.575 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 1.600 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 1.625 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 1.650 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 1.675 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 1.700 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 1.725 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 1.750 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 1.775 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 1.800 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 1.825 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 1.850 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 1.875 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 1.900 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 1.925 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 1.950 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 1.975 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 2.000 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 2.025 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 2.050 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 2.075 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 2.100 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 2.125 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 2.150 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 2.175 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 2.200 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 2.225 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 2.250 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 2.275 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 2.300 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 2.325 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 2.350 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 2.375 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 2.400 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 2.425 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 2.450 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 2.475 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 2.500 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 2.525 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 2.550 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 2.575 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 2.600 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 2.625 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 2.650 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 2.675 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 2.700 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 2.725 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 2.750 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 2.775 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 2.800 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 2.825 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 2.850 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 2.875 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 2.900 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 2.925 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 2.950 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 2.975 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 3.000 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 3.025 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 3.050 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 3.075 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 3.100 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 3.125 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 3.150 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 3.175 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 3.200 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 3.225 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 3.250 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 3.275 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 3.300 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 3.325 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 3.350 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 3.375 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 3.400 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 3.425 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 3.450 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 3.475 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 3.500 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 3.525 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 3.550 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 3.575 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 3.600 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 3.625 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 3.650 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 3.675 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 3.700 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 3.725 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 3.750 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 3.775 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 3.800 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 3.825 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 3.850 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 3.875 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 3.900 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 3.925 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 3.950 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 3.975 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 4.000 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 4.025 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 4.050 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 4.075 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 4.100 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 4.125 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 4.150 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 4.175 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 4.200 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 4.225 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 4.250 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 4.275 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 4.300 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 4.325 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 4.350 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 4.375 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 4.400 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 4.425 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 4.450 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 4.475 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 4.500 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 4.525 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 4.550 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 4.575 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 4.600 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 4.625 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 4.650 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 4.675 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 4.700 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 4.725 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 4.750 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 4.775 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 4.800 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 4.825 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 4.850 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 4.875 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 4.900 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 4.925 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 4.950 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 4.975 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 5.000 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 5.025 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 5.050 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 5.075 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 5.100 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 5.125 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 5.150 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 5.175 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 5.200 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 5.225 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 5.250 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 5.275 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 5.300 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 5.325 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 5.350 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 5.375 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 5.400 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 5.425 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 5.450 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 5.475 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 5.500 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 5.525 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 5.550 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 5.575 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 5.600 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 5.625 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 5.650 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 5.675 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 5.700 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 5.725 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 5.750 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 5.775 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 5.800 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 5.825 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 5.850 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 5.875 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 5.900 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 5.925 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 5.950 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 5.975 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 6.000 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 6.025 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 6.050 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 6.075 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 6.100 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 6.125 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 6.150 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 6.175 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 6.200 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 6.225 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 6.250 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 6.275 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 6.300 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 6.325 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 6.350 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 6.375 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 6.400 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 6.425 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 6.450 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 6.475 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 6.500 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 6.525 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 6.550 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 6.575 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 6.600 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 6.625 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 6.650 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 6.675 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 6.700 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 6.725 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 6.750 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 6.775 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 6.800 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 6.825 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 6.850 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 6.875 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 6.900 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 6.925 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 6.950 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 6.975 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 7.000 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 7.025 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 7.050 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 7.075 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 7.100 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 7.125 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 7.150 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 7.175 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 7.200 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 7.225 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 7.250 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 7.275 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 7.300 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 7.325 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 7.350 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 7.375 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 7.400 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 7.425 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 7.450 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 7.475 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 7.500 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 7.525 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 7.550 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 7.575 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 7.600 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 7.625 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 7.650 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 7.675 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 7.700 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 7.725 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 7.750 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 7.775 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 7.800 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 7.825 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 7.850 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 7.875 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 7.900 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 7.925 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 7.950 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 7.975 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 8.000 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 8.025 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 8.050 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 8.075 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 8.100 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 8.125 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 8.150 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 8.175 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 8.200 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 8.225 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 8.250 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 8.275 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 8.300 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 8.325 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 8.350 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 8.375 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 8.400 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 8.425 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 8.450 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 8.475 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 8.500 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 8.525 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 8.550 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 8.575 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 8.600 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 8.625 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 8.650 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 8.675 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 8.700 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 8.725 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 8.750 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 8.775 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 8.800 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 8.825 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 8.850 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 8.875 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 8.900 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 8.925 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 8.950 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 8.975 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 9.000 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 9.025 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 9.050 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 9.075 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 9.100 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 9.125 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 9.150 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 9.175 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 9.200 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 9.225 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 9.250 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 9.275 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 9.300 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 9.325 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 9.350 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 9.375 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 9.400 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 9.425 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 9.450 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 9.475 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 9.500 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 9.525 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 9.550 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 9.575 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 9.600 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 9.625 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 9.650 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 9.675 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 9.700 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 9.725 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 9.750 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 9.775 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 9.800 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 9.825 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 9.850 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 9.875 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 9.900 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 9.925 | 130.00 | 130.00 | 130.01 | 130.01 | 130.01 |
| 9.950 | 130.01 | 130.01 | 130.01 | 130.01 | 130.01 |
| 9.975 | 130.01 | 130.01 | 130.01 | 130.01 | 130.01 |
| 10.000 | 130.01 | 130.01 | 130.01 | 130.01 | 130.01 |
| 10.025 | 130.01 | 130.01 | 130.01 | 130.01 | 130.01 |
| 10.050 | 130.01 | 130.01 | 130.01 | 130.01 | 130.01 |
| 10.075 | 130.01 | 130.01 | 130.01 | 130.01 | 130.01 |
| 10.100 | 130.01 | 130.01 | 130.02 | 130.02 | 130.02 |
| 10.125 | 130.02 | 130.02 | 130.02 | 130.02 | 130.02 |
| 10.150 | 130.02 | 130.02 | 130.02 | 130.02 | 130.02 |
| 10.175 | 130.02 | 130.02 | 130.02 | 130.02 | 130.02 |
| 10.200 | 130.02 | 130.02 | 130.02 | 130.02 | 130.02 |
| 10.225 | 130.02 | 130.02 | 130.02 | 130.02 | 130.02 |
| 10.250 | 130.02 | 130.02 | 130.02 | 130.02 | 130.02 |
| 10.275 | 130.02 | 130.02 | 130.02 | 130.02 | 130.02 |
| 10.300 | 130.02 | 130.02 | 130.02 | 130.02 | 130.02 |
| 10.325 | 130.02 | 130.02 | 130.02 | 130.02 | 130.02 |
| 10.350 | 130.02 | 130.02 | 130.02 | 130.02 | 130.02 |
| 10.375 | 130.02 | 130.02 | 130.02 | 130.02 | 130.02 |
| 10.400 | 130.02 | 130.02 | 130.02 | 130.02 | 130.02 |
| 10.425 | 130.02 | 130.02 | 130.02 | 130.02 | 130.02 |
| 10.450 | 130.02 | 130.02 | 130.02 | 130.02 | 130.02 |
| 10.475 | 130.02 | 130.02 | 130.02 | 130.02 | 130.02 |
| 10.500 | 130.02 | 130.03 | 130.03 | 130.03 | 130.03 |
| 10.525 | 130.03 | 130.03 | 130.03 | 130.03 | 130.03 |
| 10.550 | 130.03 | 130.03 | 130.03 | 130.03 | 130.03 |
| 10.575 | 130.03 | 130.03 | 130.03 | 130.03 | 130.03 |
| 10.600 | 130.03 | 130.03 | 130.03 | 130.03 | 130.03 |
| 10.625 | 130.03 | 130.03 | 130.03 | 130.03 | 130.03 |
| 10.650 | 130.03 | 130.03 | 130.03 | 130.03 | 130.03 |
| 10.675 | 130.03 | 130.03 | 130.03 | 130.03 | 130.03 |
| 10.700 | 130.03 | 130.03 | 130.03 | 130.03 | 130.03 |
| 10.725 | 130.03 | 130.03 | 130.03 | 130.03 | 130.03 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 10.750 | 130.03 | 130.03 | 130.03 | 130.03 | 130.03 |
| 10.775 | 130.04 | 130.04 | 130.04 | 130.04 | 130.04 |
| 10.800 | 130.04 | 130.04 | 130.04 | 130.04 | 130.04 |
| 10.825 | 130.04 | 130.04 | 130.04 | 130.04 | 130.04 |
| 10.850 | 130.04 | 130.04 | 130.04 | 130.04 | 130.04 |
| 10.875 | 130.04 | 130.04 | 130.04 | 130.04 | 130.04 |
| 10.900 | 130.04 | 130.04 | 130.04 | 130.04 | 130.04 |
| 10.925 | 130.04 | 130.04 | 130.04 | 130.04 | 130.04 |
| 10.950 | 130.04 | 130.04 | 130.04 | 130.05 | 130.05 |
| 10.975 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 11.000 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 11.025 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 11.050 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 11.075 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 11.100 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 11.125 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 11.150 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 11.175 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 11.200 | 130.05 | 130.06 | 130.06 | 130.06 | 130.06 |
| 11.225 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 11.250 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 11.275 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 11.300 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 11.325 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 11.350 | 130.06 | 130.07 | 130.07 | 130.07 | 130.07 |
| 11.375 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 11.400 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 11.425 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 11.450 | 130.07 | 130.07 | 130.07 | 130.08 | 130.08 |
| 11.475 | 130.08 | 130.08 | 130.08 | 130.08 | 130.08 |
| 11.500 | 130.08 | 130.08 | 130.08 | 130.08 | 130.08 |
| 11.525 | 130.08 | 130.08 | 130.08 | 130.08 | 130.08 |
| 11.550 | 130.08 | 130.08 | 130.09 | 130.09 | 130.09 |
| 11.575 | 130.09 | 130.09 | 130.09 | 130.09 | 130.09 |
| 11.600 | 130.09 | 130.09 | 130.09 | 130.09 | 130.10 |
| 11.625 | 130.10 | 130.10 | 130.10 | 130.10 | 130.10 |
| 11.650 | 130.11 | 130.11 | 130.11 | 130.11 | 130.11 |
| 11.675 | 130.12 | 130.12 | 130.13 | 130.13 | 130.13 |
| 11.700 | 130.13 | 130.14 | 130.14 | 130.15 | 130.15 |
| 11.725 | 130.15 | 130.16 | 130.16 | 130.17 | 130.17 |
| 11.750 | 130.18 | 130.18 | 130.18 | 130.19 | 130.19 |
| 11.775 | 130.20 | 130.20 | 130.21 | 130.21 | 130.22 |
| 11.800 | 130.22 | 130.23 | 130.24 | 130.24 | 130.25 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 11.825 | 130.25 | 130.26 | 130.26 | 130.27 | 130.28 |
| 11.850 | 130.28 | 130.29 | 130.29 | 130.30 | 130.31 |
| 11.875 | 130.32 | 130.32 | 130.33 | 130.34 | 130.35 |
| 11.900 | 130.36 | 130.36 | 130.37 | 130.38 | 130.39 |
| 11.925 | 130.40 | 130.41 | 130.41 | 130.42 | 130.43 |
| 11.950 | 130.44 | 130.44 | 130.45 | 130.46 | 130.46 |
| 11.975 | 130.47 | 130.47 | 130.48 | 130.48 | 130.48 |
| 12.000 | 130.49 | 130.49 | 130.49 | 130.50 | 130.50 |
| 12.025 | 130.50 | 130.50 | 130.50 | 130.50 | 130.50 |
| 12.050 | 130.50 | 130.50 | 130.50 | 130.50 | 130.50 |
| 12.075 | 130.50 | 130.49 | 130.49 | 130.49 | 130.48 |
| 12.100 | 130.48 | 130.47 | 130.47 | 130.46 | 130.46 |
| 12.125 | 130.45 | 130.45 | 130.44 | 130.44 | 130.43 |
| 12.150 | 130.42 | 130.42 | 130.41 | 130.40 | 130.40 |
| 12.175 | 130.39 | 130.38 | 130.38 | 130.37 | 130.37 |
| 12.200 | 130.36 | 130.35 | 130.35 | 130.34 | 130.34 |
| 12.225 | 130.33 | 130.33 | 130.32 | 130.32 | 130.31 |
| 12.250 | 130.31 | 130.30 | 130.30 | 130.29 | 130.29 |
| 12.275 | 130.28 | 130.28 | 130.28 | 130.27 | 130.27 |
| 12.300 | 130.27 | 130.26 | 130.26 | 130.26 | 130.25 |
| 12.325 | 130.25 | 130.25 | 130.25 | 130.24 | 130.24 |
| 12.350 | 130.24 | 130.24 | 130.23 | 130.23 | 130.23 |
| 12.375 | 130.23 | 130.23 | 130.22 | 130.22 | 130.22 |
| 12.400 | 130.22 | 130.22 | 130.21 | 130.21 | 130.21 |
| 12.425 | 130.21 | 130.21 | 130.21 | 130.20 | 130.20 |
| 12.450 | 130.20 | 130.20 | 130.20 | 130.20 | 130.20 |
| 12.475 | 130.20 | 130.19 | 130.19 | 130.19 | 130.19 |
| 12.500 | 130.19 | 130.19 | 130.19 | 130.19 | 130.18 |
| 12.525 | 130.18 | 130.18 | 130.18 | 130.18 | 130.18 |
| 12.550 | 130.18 | 130.18 | 130.17 | 130.17 | 130.17 |
| 12.575 | 130.17 | 130.17 | 130.17 | 130.17 | 130.17 |
| 12.600 | 130.17 | 130.17 | 130.17 | 130.16 | 130.16 |
| 12.625 | 130.16 | 130.16 | 130.16 | 130.16 | 130.16 |
| 12.650 | 130.16 | 130.16 | 130.16 | 130.16 | 130.16 |
| 12.675 | 130.15 | 130.15 | 130.15 | 130.15 | 130.15 |
| 12.700 | 130.15 | 130.15 | 130.15 | 130.15 | 130.15 |
| 12.725 | 130.15 | 130.15 | 130.15 | 130.15 | 130.15 |
| 12.750 | 130.15 | 130.14 | 130.14 | 130.14 | 130.14 |
| 12.775 | 130.14 | 130.14 | 130.14 | 130.14 | 130.14 |
| 12.800 | 130.14 | 130.14 | 130.14 | 130.14 | 130.14 |
| 12.825 | 130.14 | 130.14 | 130.14 | 130.14 | 130.14 |
| 12.850 | 130.14 | 130.14 | 130.14 | 130.14 | 130.14 |
| 12.875 | 130.14 | 130.14 | 130.14 | 130.13 | 130.13 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 12.900 | 130.13 | 130.13 | 130.13 | 130.13 | 130.13 |
| 12.925 | 130.13 | 130.13 | 130.13 | 130.13 | 130.13 |
| 12.950 | 130.13 | 130.13 | 130.13 | 130.13 | 130.13 |
| 12.975 | 130.13 | 130.13 | 130.13 | 130.13 | 130.13 |
| 13.000 | 130.13 | 130.13 | 130.13 | 130.13 | 130.13 |
| 13.025 | 130.13 | 130.13 | 130.13 | 130.13 | 130.13 |
| 13.050 | 130.13 | 130.13 | 130.13 | 130.13 | 130.13 |
| 13.075 | 130.13 | 130.12 | 130.12 | 130.12 | 130.12 |
| 13.100 | 130.12 | 130.12 | 130.12 | 130.12 | 130.12 |
| 13.125 | 130.12 | 130.12 | 130.12 | 130.12 | 130.12 |
| 13.150 | 130.12 | 130.12 | 130.12 | 130.12 | 130.12 |
| 13.175 | 130.12 | 130.12 | 130.12 | 130.12 | 130.12 |
| 13.200 | 130.12 | 130.12 | 130.12 | 130.12 | 130.12 |
| 13.225 | 130.12 | 130.12 | 130.12 | 130.12 | 130.12 |
| 13.250 | 130.12 | 130.12 | 130.12 | 130.12 | 130.12 |
| 13.275 | 130.12 | 130.12 | 130.12 | 130.12 | 130.12 |
| 13.300 | 130.12 | 130.12 | 130.12 | 130.12 | 130.12 |
| 13.325 | 130.11 | 130.11 | 130.11 | 130.11 | 130.11 |
| 13.350 | 130.11 | 130.11 | 130.11 | 130.11 | 130.11 |
| 13.375 | 130.11 | 130.11 | 130.11 | 130.11 | 130.11 |
| 13.400 | 130.11 | 130.11 | 130.11 | 130.11 | 130.11 |
| 13.425 | 130.11 | 130.11 | 130.11 | 130.11 | 130.11 |
| 13.450 | 130.11 | 130.11 | 130.11 | 130.11 | 130.11 |
| 13.475 | 130.11 | 130.11 | 130.11 | 130.11 | 130.11 |
| 13.500 | 130.11 | 130.11 | 130.11 | 130.11 | 130.11 |
| 13.525 | 130.11 | 130.11 | 130.11 | 130.11 | 130.11 |
| 13.550 | 130.11 | 130.11 | 130.11 | 130.11 | 130.11 |
| 13.575 | 130.11 | 130.11 | 130.11 | 130.11 | 130.11 |
| 13.600 | 130.11 | 130.11 | 130.10 | 130.10 | 130.10 |
| 13.625 | 130.10 | 130.10 | 130.10 | 130.10 | 130.10 |
| 13.650 | 130.10 | 130.10 | 130.10 | 130.10 | 130.10 |
| 13.675 | 130.10 | 130.10 | 130.10 | 130.10 | 130.10 |
| 13.700 | 130.10 | 130.10 | 130.10 | 130.10 | 130.10 |
| 13.725 | 130.10 | 130.10 | 130.10 | 130.10 | 130.10 |
| 13.750 | 130.10 | 130.10 | 130.10 | 130.10 | 130.10 |
| 13.775 | 130.10 | 130.10 | 130.10 | 130.10 | 130.10 |
| 13.800 | 130.10 | 130.10 | 130.10 | 130.10 | 130.10 |
| 13.825 | 130.10 | 130.10 | 130.10 | 130.10 | 130.10 |
| 13.850 | 130.10 | 130.10 | 130.10 | 130.10 | 130.10 |
| 13.875 | 130.10 | 130.10 | 130.10 | 130.10 | 130.10 |
| 13.900 | 130.10 | 130.10 | 130.10 | 130.10 | 130.10 |
| 13.925 | 130.10 | 130.10 | 130.10 | 130.10 | 130.10 |
| 13.950 | 130.10 | 130.10 | 130.10 | 130.10 | 130.09 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 13.975 | 130.09 | 130.09 | 130.09 | 130.09 | 130.09 |
| 14.000 | 130.09 | 130.09 | 130.09 | 130.09 | 130.09 |
| 14.025 | 130.09 | 130.09 | 130.09 | 130.09 | 130.09 |
| 14.050 | 130.09 | 130.09 | 130.09 | 130.09 | 130.09 |
| 14.075 | 130.09 | 130.09 | 130.09 | 130.09 | 130.09 |
| 14.100 | 130.09 | 130.09 | 130.09 | 130.09 | 130.09 |
| 14.125 | 130.09 | 130.09 | 130.09 | 130.09 | 130.09 |
| 14.150 | 130.09 | 130.09 | 130.09 | 130.09 | 130.09 |
| 14.175 | 130.09 | 130.09 | 130.09 | 130.09 | 130.09 |
| 14.200 | 130.09 | 130.09 | 130.09 | 130.09 | 130.09 |
| 14.225 | 130.09 | 130.09 | 130.09 | 130.09 | 130.09 |
| 14.250 | 130.09 | 130.09 | 130.09 | 130.09 | 130.09 |
| 14.275 | 130.09 | 130.09 | 130.09 | 130.09 | 130.09 |
| 14.300 | 130.09 | 130.09 | 130.09 | 130.09 | 130.09 |
| 14.325 | 130.09 | 130.09 | 130.09 | 130.09 | 130.09 |
| 14.350 | 130.09 | 130.09 | 130.09 | 130.09 | 130.09 |
| 14.375 | 130.09 | 130.09 | 130.09 | 130.09 | 130.09 |
| 14.400 | 130.09 | 130.09 | 130.09 | 130.09 | 130.09 |
| 14.425 | 130.09 | 130.09 | 130.09 | 130.09 | 130.09 |
| 14.450 | 130.09 | 130.09 | 130.09 | 130.09 | 130.09 |
| 14.475 | 130.09 | 130.09 | 130.09 | 130.09 | 130.09 |
| 14.500 | 130.09 | 130.09 | 130.09 | 130.09 | 130.09 |
| 14.525 | 130.09 | 130.09 | 130.09 | 130.09 | 130.09 |
| 14.550 | 130.09 | 130.09 | 130.09 | 130.09 | 130.09 |
| 14.575 | 130.09 | 130.09 | 130.09 | 130.09 | 130.09 |
| 14.600 | 130.09 | 130.09 | 130.09 | 130.09 | 130.09 |
| 14.625 | 130.09 | 130.09 | 130.09 | 130.09 | 130.08 |
| 14.650 | 130.08 | 130.08 | 130.08 | 130.08 | 130.08 |
| 14.675 | 130.08 | 130.08 | 130.08 | 130.08 | 130.08 |
| 14.700 | 130.08 | 130.08 | 130.08 | 130.08 | 130.08 |
| 14.725 | 130.08 | 130.08 | 130.08 | 130.08 | 130.08 |
| 14.750 | 130.08 | 130.08 | 130.08 | 130.08 | 130.08 |
| 14.775 | 130.08 | 130.08 | 130.08 | 130.08 | 130.08 |
| 14.800 | 130.08 | 130.08 | 130.08 | 130.08 | 130.08 |
| 14.825 | 130.08 | 130.08 | 130.08 | 130.08 | 130.08 |
| 14.850 | 130.08 | 130.08 | 130.08 | 130.08 | 130.08 |
| 14.875 | 130.08 | 130.08 | 130.08 | 130.08 | 130.08 |
| 14.900 | 130.08 | 130.08 | 130.08 | 130.08 | 130.08 |
| 14.925 | 130.08 | 130.08 | 130.08 | 130.08 | 130.08 |
| 14.950 | 130.08 | 130.08 | 130.08 | 130.08 | 130.08 |
| 14.975 | 130.08 | 130.08 | 130.08 | 130.08 | 130.08 |
| 15.000 | 130.08 | 130.08 | 130.08 | 130.08 | 130.08 |
| 15.025 | 130.08 | 130.08 | 130.08 | 130.08 | 130.08 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 15.050 | 130.08 | 130.08 | 130.08 | 130.08 | 130.08 |
| 15.075 | 130.08 | 130.08 | 130.08 | 130.08 | 130.08 |
| 15.100 | 130.08 | 130.08 | 130.08 | 130.08 | 130.08 |
| 15.125 | 130.08 | 130.08 | 130.08 | 130.08 | 130.08 |
| 15.150 | 130.08 | 130.08 | 130.08 | 130.08 | 130.08 |
| 15.175 | 130.08 | 130.08 | 130.08 | 130.08 | 130.08 |
| 15.200 | 130.08 | 130.08 | 130.08 | 130.08 | 130.08 |
| 15.225 | 130.08 | 130.08 | 130.08 | 130.08 | 130.08 |
| 15.250 | 130.08 | 130.08 | 130.08 | 130.08 | 130.08 |
| 15.275 | 130.08 | 130.08 | 130.08 | 130.08 | 130.08 |
| 15.300 | 130.08 | 130.08 | 130.08 | 130.08 | 130.08 |
| 15.325 | 130.08 | 130.08 | 130.08 | 130.08 | 130.08 |
| 15.350 | 130.08 | 130.08 | 130.08 | 130.08 | 130.08 |
| 15.375 | 130.08 | 130.08 | 130.08 | 130.08 | 130.08 |
| 15.400 | 130.08 | 130.08 | 130.08 | 130.08 | 130.08 |
| 15.425 | 130.08 | 130.08 | 130.08 | 130.08 | 130.08 |
| 15.450 | 130.08 | 130.08 | 130.08 | 130.08 | 130.08 |
| 15.475 | 130.08 | 130.08 | 130.08 | 130.08 | 130.08 |
| 15.500 | 130.08 | 130.08 | 130.08 | 130.08 | 130.08 |
| 15.525 | 130.08 | 130.08 | 130.08 | 130.08 | 130.08 |
| 15.550 | 130.08 | 130.08 | 130.08 | 130.08 | 130.08 |
| 15.575 | 130.08 | 130.08 | 130.08 | 130.08 | 130.08 |
| 15.600 | 130.08 | 130.08 | 130.08 | 130.08 | 130.08 |
| 15.625 | 130.08 | 130.08 | 130.08 | 130.07 | 130.07 |
| 15.650 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 15.675 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 15.700 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 15.725 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 15.750 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 15.775 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 15.800 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 15.825 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 15.850 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 15.875 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 15.900 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 15.925 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 15.950 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 15.975 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 16.000 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 16.025 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 16.050 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 16.075 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 16.100 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 16.125 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 16.150 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 16.175 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 16.200 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 16.225 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 16.250 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 16.275 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 16.300 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 16.325 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 16.350 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 16.375 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 16.400 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 16.425 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 16.450 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 16.475 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 16.500 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 16.525 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 16.550 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 16.575 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 16.600 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 16.625 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 16.650 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 16.675 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 16.700 | 130.07 | 130.06 | 130.06 | 130.06 | 130.06 |
| 16.725 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 16.750 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 16.775 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 16.800 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 16.825 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 16.850 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 16.875 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 16.900 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 16.925 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 16.950 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 16.975 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 17.000 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 17.025 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 17.050 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 17.075 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 17.100 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 17.125 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 17.150 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 17.175 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 17.200 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 17.225 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 17.250 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 17.275 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 17.300 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 17.325 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 17.350 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 17.375 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 17.400 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 17.425 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 17.450 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 17.475 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 17.500 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 17.525 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 17.550 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 17.575 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 17.600 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 17.625 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 17.650 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 17.675 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 17.700 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 17.725 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 17.750 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 17.775 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 17.800 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 17.825 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 17.850 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 17.875 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 17.900 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 17.925 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 17.950 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 17.975 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 18.000 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 18.025 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 18.050 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 18.075 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 18.100 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 18.125 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 18.150 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 18.175 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 18.200 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 18.225 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 18.250 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 18.275 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 18.300 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 18.325 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 18.350 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 18.375 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 18.400 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 18.425 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 18.450 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 18.475 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 18.500 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 18.525 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 18.550 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 18.575 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 18.600 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 18.625 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 18.650 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 18.675 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 18.700 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 18.725 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 18.750 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 18.775 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 18.800 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 18.825 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 18.850 | 130.06 | 130.06 | 130.05 | 130.05 | 130.05 |
| 18.875 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 18.900 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 18.925 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 18.950 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 18.975 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 19.000 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 19.025 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 19.050 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 19.075 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 19.100 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 19.125 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 19.150 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 19.175 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 19.200 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 19.225 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 19.250 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 19.275 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 19.300 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 19.325 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 19.350 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 19.375 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 19.400 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 19.425 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 19.450 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 19.475 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 19.500 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 19.525 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 19.550 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 19.575 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 19.600 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 19.625 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 19.650 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 19.675 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 19.700 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 19.725 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 19.750 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 19.775 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 19.800 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 19.825 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 19.850 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 19.875 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 19.900 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 19.925 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 19.950 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 19.975 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 20.000 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 20.025 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 20.050 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 20.075 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 20.100 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 20.125 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 20.150 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 20.175 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 20.200 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 20.225 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 20.250 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 20.275 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 20.300 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 20.325 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 20.350 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 20.375 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 20.400 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 20.425 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 20.450 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 20.475 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 20.500 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 20.525 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 20.550 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 20.575 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 20.600 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 20.625 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 20.650 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 20.675 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 20.700 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 20.725 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 20.750 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 20.775 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 20.800 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 20.825 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 20.850 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 20.875 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 20.900 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 20.925 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 20.950 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 20.975 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 21.000 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 21.025 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 21.050 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 21.075 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 21.100 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 21.125 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 21.150 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 21.175 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 21.200 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 21.225 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 21.250 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 21.275 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 21.300 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 21.325 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 21.350 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 21.375 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 21.400 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 21.425 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 21.450 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 21.475 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 21.500 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 21.525 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 21.550 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 21.575 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 21.600 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 21.625 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 21.650 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 21.675 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 21.700 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 21.725 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 21.750 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 21.775 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 21.800 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 21.825 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 21.850 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 21.875 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 21.900 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 21.925 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 21.950 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 21.975 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 22.000 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 22.025 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 22.050 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 22.075 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 22.100 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 22.125 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 22.150 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 22.175 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 22.200 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 22.225 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 22.250 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 22.275 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 22.300 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 22.325 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 22.350 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 22.375 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 22.400 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 22.425 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 22.450 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 22.475 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 22.500 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 22.525 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 22.550 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 22.575 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 22.600 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 22.625 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 22.650 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 22.675 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 22.700 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 22.725 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 22.750 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 22.775 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 22.800 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 22.825 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 22.850 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 22.875 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 22.900 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 22.925 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 22.950 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 22.975 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 23.000 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 23.025 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 23.050 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 23.075 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 23.100 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 23.125 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 23.150 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 23.175 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 23.200 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 23.225 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 23.250 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 23.275 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 23.300 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 23.325 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 23.350 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 23.375 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 23.400 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 23.425 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 23.450 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 23.475 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 23.500 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 23.525 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 23.550 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 23.575 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 23.600 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 23.625 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 23.650 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 23.675 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 23.700 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 23.725 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 23.750 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 23.775 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 23.800 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 23.825 | 130.05 | 130.05 | 130.05 | 130.04 | 130.04 |
| 23.850 | 130.04 | 130.04 | 130.04 | 130.04 | 130.04 |
| 23.875 | 130.04 | 130.04 | 130.04 | 130.04 | 130.04 |
| 23.900 | 130.04 | 130.04 | 130.04 | 130.04 | 130.04 |
| 23.925 | 130.04 | 130.04 | 130.04 | 130.04 | 130.04 |
| 23.950 | 130.04 | 130.04 | 130.04 | 130.04 | 130.04 |
| 23.975 | 130.04 | 130.04 | 130.04 | 130.04 | 130.04 |
| 24.000 | 130.04 | (N/A) | (N/A) | (N/A) | (N/A) |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 0.000 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 0.025 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 0.050 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 0.075 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 0.100 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 0.125 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 0.150 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 0.175 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 0.200 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 0.225 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 0.250 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 0.275 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 0.300 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 0.325 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 0.350 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 0.375 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 0.400 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 0.425 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 0.450 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 0.475 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 0.500 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 0.525 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 0.550 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 0.575 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 0.600 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 0.625 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 0.650 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 0.675 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 0.700 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 0.725 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 0.750 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 0.775 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 0.800 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 0.825 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 0.850 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 0.875 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 0.900 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 0.925 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 0.950 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 0.975 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 1.000 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 1.025 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 1.050 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 1.075 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 1.100 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 1.125 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 1.150 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 1.175 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 1.200 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 1.225 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 1.250 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 1.275 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 1.300 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 1.325 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 1.350 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 1.375 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 1.400 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 1.425 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 1.450 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 1.475 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 1.500 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 1.525 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 1.550 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 1.575 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 1.600 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 1.625 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 1.650 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 1.675 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 1.700 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 1.725 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 1.750 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 1.775 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 1.800 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 1.825 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 1.850 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 1.875 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 1.900 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 1.925 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 1.950 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 1.975 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 2.000 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 2.025 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 2.050 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 2.075 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 2.100 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 2.125 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 2.150 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 2.175 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 2.200 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 2.225 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 2.250 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 2.275 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 2.300 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 2.325 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 2.350 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 2.375 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 2.400 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 2.425 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 2.450 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 2.475 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 2.500 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 2.525 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 2.550 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 2.575 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 2.600 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 2.625 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 2.650 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 2.675 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 2.700 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 2.725 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 2.750 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 2.775 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 2.800 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 2.825 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 2.850 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 2.875 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 2.900 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 2.925 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 2.950 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 2.975 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 3.000 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 3.025 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 3.050 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 3.075 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 3.100 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 3.125 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 3.150 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 3.175 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 3.200 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 3.225 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 3.250 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 3.275 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 3.300 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 3.325 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 3.350 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 3.375 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 3.400 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 3.425 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 3.450 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 3.475 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 3.500 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 3.525 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 3.550 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 3.575 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 3.600 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 3.625 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 3.650 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 3.675 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 3.700 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 3.725 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 3.750 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 3.775 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 3.800 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 3.825 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 3.850 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 3.875 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 3.900 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 3.925 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 3.950 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 3.975 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 4.000 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 4.025 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 4.050 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 4.075 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 4.100 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 4.125 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 4.150 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 4.175 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 4.200 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 4.225 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 4.250 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 4.275 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 4.300 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 4.325 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 4.350 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 4.375 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 4.400 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 4.425 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 4.450 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 4.475 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 4.500 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 4.525 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 4.550 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 4.575 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 4.600 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 4.625 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 4.650 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 4.675 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 4.700 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 4.725 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 4.750 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 4.775 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 4.800 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 4.825 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 4.850 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 4.875 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 4.900 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 4.925 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 4.950 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 4.975 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 5.000 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 5.025 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 5.050 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 5.075 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 5.100 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 5.125 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 5.150 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 5.175 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 5.200 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 5.225 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 5.250 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 5.275 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 5.300 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 5.325 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 5.350 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 5.375 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 5.400 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 5.425 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 5.450 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 5.475 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 5.500 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 5.525 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 5.550 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 5.575 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 5.600 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 5.625 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 5.650 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 5.675 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 5.700 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 5.725 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 5.750 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 5.775 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 5.800 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 5.825 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 5.850 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 5.875 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 5.900 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 5.925 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 5.950 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 5.975 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 6.000 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 6.025 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 6.050 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 6.075 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 6.100 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 6.125 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 6.150 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 6.175 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 6.200 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 6.225 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 6.250 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 6.275 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 6.300 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 6.325 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 6.350 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 6.375 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 6.400 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 6.425 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 6.450 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 6.475 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 6.500 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 6.525 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 6.550 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 6.575 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 6.600 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 6.625 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 6.650 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 6.675 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 6.700 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 6.725 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 6.750 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 6.775 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 6.800 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 6.825 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 6.850 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 6.875 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 6.900 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 6.925 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 6.950 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 6.975 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 7.000 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 7.025 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 7.050 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 7.075 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 7.100 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 7.125 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 7.150 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 7.175 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 7.200 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 7.225 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 7.250 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 7.275 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 7.300 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 7.325 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 7.350 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 7.375 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 7.400 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 7.425 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 7.450 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 7.475 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 7.500 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 7.525 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 7.550 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 7.575 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 7.600 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 7.625 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 7.650 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 7.675 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 7.700 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 7.725 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 7.750 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 7.775 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 7.800 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 7.825 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 7.850 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 7.875 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 7.900 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 7.925 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 7.950 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 7.975 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 8.000 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 8.025 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 8.050 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 8.075 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 8.100 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 8.125 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 8.150 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 8.175 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 8.200 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 8.225 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 8.250 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 8.275 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 8.300 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 8.325 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 8.350 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 8.375 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 8.400 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 8.425 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 8.450 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 8.475 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 8.500 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 8.525 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 8.550 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 8.575 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 8.600 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 8.625 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 8.650 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 8.675 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 8.700 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 8.725 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 8.750 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 8.775 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 8.800 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 8.825 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 8.850 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 8.875 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 8.900 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 8.925 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 8.950 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 8.975 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 9.000 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 9.025 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 9.050 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 9.075 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 9.100 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 9.125 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 9.150 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 9.175 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 9.200 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 9.225 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 9.250 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 9.275 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 9.300 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 9.325 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 9.350 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 9.375 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 9.400 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 9.425 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 9.450 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 9.475 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 9.500 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 9.525 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 9.550 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 9.575 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 9.600 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 9.625 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 9.650 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 9.675 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 9.700 | 129.00 | 129.00 | 129.00 | 129.00 | 129.01 |
| 9.725 | 129.01 | 129.01 | 129.01 | 129.01 | 129.01 |
| 9.750 | 129.01 | 129.01 | 129.01 | 129.01 | 129.01 |
| 9.775 | 129.01 | 129.01 | 129.01 | 129.01 | 129.01 |
| 9.800 | 129.01 | 129.01 | 129.01 | 129.01 | 129.01 |
| 9.825 | 129.01 | 129.01 | 129.01 | 129.01 | 129.01 |
| 9.850 | 129.01 | 129.01 | 129.01 | 129.01 | 129.01 |
| 9.875 | 129.01 | 129.01 | 129.01 | 129.01 | 129.01 |
| 9.900 | 129.01 | 129.01 | 129.01 | 129.01 | 129.01 |
| 9.925 | 129.01 | 129.01 | 129.01 | 129.01 | 129.01 |
| 9.950 | 129.01 | 129.01 | 129.01 | 129.01 | 129.01 |
| 9.975 | 129.01 | 129.01 | 129.01 | 129.01 | 129.01 |
| 10.000 | 129.01 | 129.01 | 129.01 | 129.01 | 129.01 |
| 10.025 | 129.01 | 129.01 | 129.01 | 129.01 | 129.01 |
| 10.050 | 129.01 | 129.01 | 129.01 | 129.01 | 129.01 |
| 10.075 | 129.01 | 129.01 | 129.01 | 129.01 | 129.01 |
| 10.100 | 129.01 | 129.01 | 129.01 | 129.01 | 129.01 |
| 10.125 | 129.01 | 129.01 | 129.01 | 129.01 | 129.01 |
| 10.150 | 129.01 | 129.01 | 129.01 | 129.01 | 129.01 |
| 10.175 | 129.01 | 129.01 | 129.01 | 129.01 | 129.01 |
| 10.200 | 129.01 | 129.01 | 129.01 | 129.01 | 129.01 |
| 10.225 | 129.01 | 129.01 | 129.02 | 129.02 | 129.02 |
| 10.250 | 129.02 | 129.02 | 129.02 | 129.02 | 129.02 |
| 10.275 | 129.02 | 129.02 | 129.02 | 129.02 | 129.02 |
| 10.300 | 129.02 | 129.02 | 129.02 | 129.02 | 129.02 |
| 10.325 | 129.02 | 129.02 | 129.02 | 129.02 | 129.02 |
| 10.350 | 129.02 | 129.02 | 129.02 | 129.02 | 129.02 |
| 10.375 | 129.02 | 129.02 | 129.02 | 129.02 | 129.02 |
| 10.400 | 129.02 | 129.02 | 129.02 | 129.02 | 129.02 |
| 10.425 | 129.02 | 129.02 | 129.02 | 129.02 | 129.02 |
| 10.450 | 129.02 | 129.02 | 129.02 | 129.02 | 129.02 |
| 10.475 | 129.02 | 129.02 | 129.02 | 129.02 | 129.02 |
| 10.500 | 129.02 | 129.02 | 129.02 | 129.02 | 129.02 |
| 10.525 | 129.02 | 129.02 | 129.02 | 129.02 | 129.02 |
| 10.550 | 129.02 | 129.02 | 129.02 | 129.02 | 129.02 |
| 10.575 | 129.02 | 129.02 | 129.02 | 129.02 | 129.02 |
| 10.600 | 129.02 | 129.02 | 129.02 | 129.02 | 129.02 |
| 10.625 | 129.02 | 129.02 | 129.02 | 129.02 | 129.02 |
| 10.650 | 129.02 | 129.02 | 129.02 | 129.02 | 129.02 |
| 10.675 | 129.02 | 129.02 | 129.02 | 129.02 | 129.02 |
| 10.700 | 129.02 | 129.02 | 129.03 | 129.03 | 129.03 |
| 10.725 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 10.750 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 10.775 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 10.800 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 10.825 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 10.850 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 10.875 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 10.900 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 10.925 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 10.950 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 10.975 | 129.03 | 129.03 | 129.03 | 129.04 | 129.04 |
| 11.000 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 11.025 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 11.050 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 11.075 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 11.100 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 11.125 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 11.150 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 11.175 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 11.200 | 129.04 | 129.04 | 129.04 | 129.04 | 129.05 |
| 11.225 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 11.250 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 11.275 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 11.300 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 11.325 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 11.350 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 11.375 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 11.400 | 129.05 | 129.05 | 129.05 | 129.05 | 129.06 |
| 11.425 | 129.06 | 129.06 | 129.06 | 129.06 | 129.06 |
| 11.450 | 129.06 | 129.06 | 129.06 | 129.06 | 129.06 |
| 11.475 | 129.06 | 129.06 | 129.06 | 129.06 | 129.06 |
| 11.500 | 129.06 | 129.06 | 129.06 | 129.06 | 129.06 |
| 11.525 | 129.06 | 129.06 | 129.06 | 129.06 | 129.06 |
| 11.550 | 129.07 | 129.07 | 129.07 | 129.07 | 129.07 |
| 11.575 | 129.07 | 129.07 | 129.07 | 129.08 | 129.08 |
| 11.600 | 129.08 | 129.08 | 129.08 | 129.08 | 129.09 |
| 11.625 | 129.09 | 129.09 | 129.09 | 129.09 | 129.10 |
| 11.650 | 129.10 | 129.10 | 129.10 | 129.11 | 129.11 |
| 11.675 | 129.11 | 129.11 | 129.12 | 129.12 | 129.12 |
| 11.700 | 129.13 | 129.13 | 129.13 | 129.14 | 129.14 |
| 11.725 | 129.14 | 129.15 | 129.15 | 129.15 | 129.16 |
| 11.750 | 129.16 | 129.17 | 129.17 | 129.17 | 129.18 |
| 11.775 | 129.18 | 129.19 | 129.19 | 129.19 | 129.20 |
| 11.800 | 129.20 | 129.21 | 129.21 | 129.22 | 129.22 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 11.825 | 129.22 | 129.23 | 129.23 | 129.24 | 129.24 |
| 11.850 | 129.25 | 129.25 | 129.26 | 129.27 | 129.27 |
| 11.875 | 129.28 | 129.29 | 129.29 | 129.30 | 129.31 |
| 11.900 | 129.31 | 129.32 | 129.33 | 129.33 | 129.34 |
| 11.925 | 129.35 | 129.35 | 129.36 | 129.36 | 129.37 |
| 11.950 | 129.37 | 129.37 | 129.38 | 129.38 | 129.38 |
| 11.975 | 129.39 | 129.39 | 129.39 | 129.39 | 129.39 |
| 12.000 | 129.39 | 129.39 | 129.39 | 129.39 | 129.39 |
| 12.025 | 129.39 | 129.39 | 129.39 | 129.38 | 129.38 |
| 12.050 | 129.38 | 129.38 | 129.37 | 129.37 | 129.37 |
| 12.075 | 129.36 | 129.36 | 129.35 | 129.34 | 129.34 |
| 12.100 | 129.33 | 129.33 | 129.32 | 129.31 | 129.31 |
| 12.125 | 129.30 | 129.29 | 129.28 | 129.28 | 129.27 |
| 12.150 | 129.27 | 129.26 | 129.25 | 129.25 | 129.24 |
| 12.175 | 129.24 | 129.23 | 129.23 | 129.22 | 129.22 |
| 12.200 | 129.21 | 129.21 | 129.21 | 129.20 | 129.20 |
| 12.225 | 129.20 | 129.19 | 129.19 | 129.19 | 129.18 |
| 12.250 | 129.18 | 129.18 | 129.18 | 129.17 | 129.17 |
| 12.275 | 129.17 | 129.17 | 129.17 | 129.17 | 129.16 |
| 12.300 | 129.16 | 129.16 | 129.16 | 129.16 | 129.16 |
| 12.325 | 129.16 | 129.15 | 129.15 | 129.15 | 129.15 |
| 12.350 | 129.15 | 129.15 | 129.15 | 129.15 | 129.15 |
| 12.375 | 129.14 | 129.14 | 129.14 | 129.14 | 129.14 |
| 12.400 | 129.14 | 129.14 | 129.14 | 129.14 | 129.14 |
| 12.425 | 129.14 | 129.13 | 129.13 | 129.13 | 129.13 |
| 12.450 | 129.13 | 129.13 | 129.13 | 129.13 | 129.13 |
| 12.475 | 129.13 | 129.13 | 129.13 | 129.13 | 129.13 |
| 12.500 | 129.12 | 129.12 | 129.12 | 129.12 | 129.12 |
| 12.525 | 129.12 | 129.12 | 129.12 | 129.12 | 129.12 |
| 12.550 | 129.12 | 129.12 | 129.12 | 129.12 | 129.12 |
| 12.575 | 129.12 | 129.11 | 129.11 | 129.11 | 129.11 |
| 12.600 | 129.11 | 129.11 | 129.11 | 129.11 | 129.11 |
| 12.625 | 129.11 | 129.11 | 129.11 | 129.11 | 129.11 |
| 12.650 | 129.11 | 129.11 | 129.11 | 129.11 | 129.11 |
| 12.675 | 129.10 | 129.10 | 129.10 | 129.10 | 129.10 |
| 12.700 | 129.10 | 129.10 | 129.10 | 129.10 | 129.10 |
| 12.725 | 129.10 | 129.10 | 129.10 | 129.10 | 129.10 |
| 12.750 | 129.10 | 129.10 | 129.10 | 129.10 | 129.10 |
| 12.775 | 129.10 | 129.10 | 129.10 | 129.10 | 129.10 |
| 12.800 | 129.10 | 129.10 | 129.10 | 129.10 | 129.10 |
| 12.825 | 129.10 | 129.10 | 129.10 | 129.10 | 129.10 |
| 12.850 | 129.10 | 129.10 | 129.10 | 129.10 | 129.10 |
| 12.875 | 129.09 | 129.09 | 129.09 | 129.09 | 129.09 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 12.900 | 129.09 | 129.09 | 129.09 | 129.09 | 129.09 |
| 12.925 | 129.09 | 129.09 | 129.09 | 129.09 | 129.09 |
| 12.950 | 129.09 | 129.09 | 129.09 | 129.09 | 129.09 |
| 12.975 | 129.09 | 129.09 | 129.09 | 129.09 | 129.09 |
| 13.000 | 129.09 | 129.09 | 129.09 | 129.09 | 129.09 |
| 13.025 | 129.09 | 129.09 | 129.09 | 129.09 | 129.09 |
| 13.050 | 129.09 | 129.09 | 129.09 | 129.09 | 129.09 |
| 13.075 | 129.09 | 129.09 | 129.09 | 129.09 | 129.09 |
| 13.100 | 129.09 | 129.09 | 129.09 | 129.09 | 129.09 |
| 13.125 | 129.09 | 129.09 | 129.09 | 129.09 | 129.09 |
| 13.150 | 129.09 | 129.09 | 129.09 | 129.09 | 129.09 |
| 13.175 | 129.08 | 129.08 | 129.08 | 129.08 | 129.08 |
| 13.200 | 129.08 | 129.08 | 129.08 | 129.08 | 129.08 |
| 13.225 | 129.08 | 129.08 | 129.08 | 129.08 | 129.08 |
| 13.250 | 129.08 | 129.08 | 129.08 | 129.08 | 129.08 |
| 13.275 | 129.08 | 129.08 | 129.08 | 129.08 | 129.08 |
| 13.300 | 129.08 | 129.08 | 129.08 | 129.08 | 129.08 |
| 13.325 | 129.08 | 129.08 | 129.08 | 129.08 | 129.08 |
| 13.350 | 129.08 | 129.08 | 129.08 | 129.08 | 129.08 |
| 13.375 | 129.08 | 129.08 | 129.08 | 129.08 | 129.08 |
| 13.400 | 129.08 | 129.08 | 129.08 | 129.08 | 129.08 |
| 13.425 | 129.08 | 129.08 | 129.08 | 129.08 | 129.08 |
| 13.450 | 129.08 | 129.08 | 129.08 | 129.08 | 129.08 |
| 13.475 | 129.08 | 129.08 | 129.08 | 129.08 | 129.08 |
| 13.500 | 129.08 | 129.08 | 129.08 | 129.08 | 129.08 |
| 13.525 | 129.08 | 129.08 | 129.08 | 129.08 | 129.08 |
| 13.550 | 129.08 | 129.08 | 129.08 | 129.08 | 129.08 |
| 13.575 | 129.08 | 129.08 | 129.08 | 129.08 | 129.07 |
| 13.600 | 129.07 | 129.07 | 129.07 | 129.07 | 129.07 |
| 13.625 | 129.07 | 129.07 | 129.07 | 129.07 | 129.07 |
| 13.650 | 129.07 | 129.07 | 129.07 | 129.07 | 129.07 |
| 13.675 | 129.07 | 129.07 | 129.07 | 129.07 | 129.07 |
| 13.700 | 129.07 | 129.07 | 129.07 | 129.07 | 129.07 |
| 13.725 | 129.07 | 129.07 | 129.07 | 129.07 | 129.07 |
| 13.750 | 129.07 | 129.07 | 129.07 | 129.07 | 129.07 |
| 13.775 | 129.07 | 129.07 | 129.07 | 129.07 | 129.07 |
| 13.800 | 129.07 | 129.07 | 129.07 | 129.07 | 129.07 |
| 13.825 | 129.07 | 129.07 | 129.07 | 129.07 | 129.07 |
| 13.850 | 129.07 | 129.07 | 129.07 | 129.07 | 129.07 |
| 13.875 | 129.07 | 129.07 | 129.07 | 129.07 | 129.07 |
| 13.900 | 129.07 | 129.07 | 129.07 | 129.07 | 129.07 |
| 13.925 | 129.07 | 129.07 | 129.07 | 129.07 | 129.07 |
| 13.950 | 129.07 | 129.07 | 129.07 | 129.07 | 129.07 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 13.975 | 129.07 | 129.07 | 129.07 | 129.07 | 129.07 |
| 14.000 | 129.07 | 129.07 | 129.07 | 129.07 | 129.07 |
| 14.025 | 129.07 | 129.07 | 129.07 | 129.07 | 129.07 |
| 14.050 | 129.06 | 129.06 | 129.06 | 129.06 | 129.06 |
| 14.075 | 129.06 | 129.06 | 129.06 | 129.06 | 129.06 |
| 14.100 | 129.06 | 129.06 | 129.06 | 129.06 | 129.06 |
| 14.125 | 129.06 | 129.06 | 129.06 | 129.06 | 129.06 |
| 14.150 | 129.06 | 129.06 | 129.06 | 129.06 | 129.06 |
| 14.175 | 129.06 | 129.06 | 129.06 | 129.06 | 129.06 |
| 14.200 | 129.06 | 129.06 | 129.06 | 129.06 | 129.06 |
| 14.225 | 129.06 | 129.06 | 129.06 | 129.06 | 129.06 |
| 14.250 | 129.06 | 129.06 | 129.06 | 129.06 | 129.06 |
| 14.275 | 129.06 | 129.06 | 129.06 | 129.06 | 129.06 |
| 14.300 | 129.06 | 129.06 | 129.06 | 129.06 | 129.06 |
| 14.325 | 129.06 | 129.06 | 129.06 | 129.06 | 129.06 |
| 14.350 | 129.06 | 129.06 | 129.06 | 129.06 | 129.06 |
| 14.375 | 129.06 | 129.06 | 129.06 | 129.06 | 129.06 |
| 14.400 | 129.06 | 129.06 | 129.06 | 129.06 | 129.06 |
| 14.425 | 129.06 | 129.06 | 129.06 | 129.06 | 129.06 |
| 14.450 | 129.06 | 129.06 | 129.06 | 129.06 | 129.06 |
| 14.475 | 129.06 | 129.06 | 129.06 | 129.06 | 129.06 |
| 14.500 | 129.06 | 129.06 | 129.06 | 129.06 | 129.06 |
| 14.525 | 129.06 | 129.06 | 129.06 | 129.06 | 129.06 |
| 14.550 | 129.06 | 129.06 | 129.06 | 129.06 | 129.06 |
| 14.575 | 129.06 | 129.06 | 129.06 | 129.06 | 129.06 |
| 14.600 | 129.06 | 129.06 | 129.06 | 129.06 | 129.06 |
| 14.625 | 129.06 | 129.06 | 129.06 | 129.06 | 129.06 |
| 14.650 | 129.06 | 129.06 | 129.06 | 129.06 | 129.06 |
| 14.675 | 129.06 | 129.06 | 129.06 | 129.06 | 129.06 |
| 14.700 | 129.06 | 129.06 | 129.06 | 129.06 | 129.06 |
| 14.725 | 129.06 | 129.06 | 129.06 | 129.06 | 129.06 |
| 14.750 | 129.06 | 129.06 | 129.06 | 129.06 | 129.06 |
| 14.775 | 129.06 | 129.06 | 129.06 | 129.06 | 129.06 |
| 14.800 | 129.06 | 129.06 | 129.06 | 129.06 | 129.06 |
| 14.825 | 129.06 | 129.06 | 129.06 | 129.06 | 129.06 |
| 14.850 | 129.06 | 129.06 | 129.06 | 129.06 | 129.06 |
| 14.875 | 129.06 | 129.06 | 129.06 | 129.06 | 129.06 |
| 14.900 | 129.06 | 129.06 | 129.06 | 129.06 | 129.06 |
| 14.925 | 129.06 | 129.06 | 129.06 | 129.06 | 129.06 |
| 14.950 | 129.06 | 129.06 | 129.06 | 129.06 | 129.06 |
| 14.975 | 129.06 | 129.06 | 129.06 | 129.06 | 129.06 |
| 15.000 | 129.06 | 129.06 | 129.06 | 129.06 | 129.06 |
| 15.025 | 129.06 | 129.06 | 129.06 | 129.06 | 129.06 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 15.050 | 129.06 | 129.06 | 129.06 | 129.06 | 129.06 |
| 15.075 | 129.06 | 129.06 | 129.06 | 129.06 | 129.06 |
| 15.100 | 129.06 | 129.06 | 129.06 | 129.06 | 129.06 |
| 15.125 | 129.06 | 129.06 | 129.06 | 129.06 | 129.06 |
| 15.150 | 129.06 | 129.06 | 129.06 | 129.06 | 129.06 |
| 15.175 | 129.06 | 129.06 | 129.06 | 129.06 | 129.06 |
| 15.200 | 129.06 | 129.06 | 129.06 | 129.06 | 129.06 |
| 15.225 | 129.06 | 129.06 | 129.05 | 129.05 | 129.05 |
| 15.250 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 15.275 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 15.300 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 15.325 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 15.350 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 15.375 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 15.400 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 15.425 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 15.450 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 15.475 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 15.500 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 15.525 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 15.550 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 15.575 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 15.600 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 15.625 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 15.650 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 15.675 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 15.700 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 15.725 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 15.750 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 15.775 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 15.800 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 15.825 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 15.850 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 15.875 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 15.900 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 15.925 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 15.950 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 15.975 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 16.000 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 16.025 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 16.050 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 16.075 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 16.100 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 16.125 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 16.150 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 16.175 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 16.200 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 16.225 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 16.250 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 16.275 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 16.300 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 16.325 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 16.350 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 16.375 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 16.400 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 16.425 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 16.450 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 16.475 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 16.500 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 16.525 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 16.550 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 16.575 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 16.600 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 16.625 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 16.650 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 16.675 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 16.700 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 16.725 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 16.750 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 16.775 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 16.800 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 16.825 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 16.850 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 16.875 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 16.900 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 16.925 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 16.950 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 16.975 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 17.000 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 17.025 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 17.050 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 17.075 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 17.100 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 17.125 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 17.150 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 17.175 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 17.200 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 17.225 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 17.250 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 17.275 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 17.300 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 17.325 | 129.05 | 129.05 | 129.04 | 129.04 | 129.04 |
| 17.350 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 17.375 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 17.400 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 17.425 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 17.450 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 17.475 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 17.500 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 17.525 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 17.550 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 17.575 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 17.600 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 17.625 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 17.650 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 17.675 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 17.700 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 17.725 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 17.750 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 17.775 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 17.800 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 17.825 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 17.850 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 17.875 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 17.900 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 17.925 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 17.950 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 17.975 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 18.000 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 18.025 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 18.050 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 18.075 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 18.100 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 18.125 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 18.150 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 18.175 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 18.200 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 18.225 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 18.250 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 18.275 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 18.300 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 18.325 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 18.350 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 18.375 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 18.400 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 18.425 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 18.450 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 18.475 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 18.500 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 18.525 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 18.550 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 18.575 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 18.600 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 18.625 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 18.650 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 18.675 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 18.700 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 18.725 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 18.750 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 18.775 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 18.800 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 18.825 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 18.850 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 18.875 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 18.900 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 18.925 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 18.950 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 18.975 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 19.000 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 19.025 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 19.050 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 19.075 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 19.100 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 19.125 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 19.150 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 19.175 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 19.200 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 19.225 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 19.250 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 19.275 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 19.300 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 19.325 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 19.350 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 19.375 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 19.400 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 19.425 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 19.450 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 19.475 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 19.500 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 19.525 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 19.550 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 19.575 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 19.600 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 19.625 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 19.650 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 19.675 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 19.700 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 19.725 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 19.750 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 19.775 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 19.800 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 19.825 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 19.850 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 19.875 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 19.900 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 19.925 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 19.950 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 19.975 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 20.000 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 20.025 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 20.050 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 20.075 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 20.100 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 20.125 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 20.150 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 20.175 | 129.04 | 129.03 | 129.03 | 129.03 | 129.03 |
| 20.200 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 20.225 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 20.250 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 20.275 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 20.300 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 20.325 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 20.350 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 20.375 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 20.400 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 20.425 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 20.450 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 20.475 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 20.500 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 20.525 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 20.550 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 20.575 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 20.600 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 20.625 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 20.650 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 20.675 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 20.700 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 20.725 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 20.750 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 20.775 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 20.800 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 20.825 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 20.850 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 20.875 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 20.900 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 20.925 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 20.950 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 20.975 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 21.000 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 21.025 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 21.050 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 21.075 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 21.100 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 21.125 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 21.150 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 21.175 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 21.200 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 21.225 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 21.250 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 21.275 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 21.300 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 21.325 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 21.350 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 21.375 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 21.400 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 21.425 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 21.450 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 21.475 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 21.500 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 21.525 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 21.550 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 21.575 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 21.600 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 21.625 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 21.650 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 21.675 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 21.700 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 21.725 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 21.750 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 21.775 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 21.800 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 21.825 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 21.850 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 21.875 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 21.900 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 21.925 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 21.950 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 21.975 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 22.000 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 22.025 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 22.050 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 22.075 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 22.100 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 22.125 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 22.150 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 22.175 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 22.200 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 22.225 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 22.250 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 22.275 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 22.300 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 22.325 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 22.350 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 22.375 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 22.400 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 22.425 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 22.450 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 22.475 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 22.500 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 22.525 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 22.550 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 22.575 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 22.600 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 22.625 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 22.650 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 22.675 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 22.700 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 22.725 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 22.750 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 22.775 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 22.800 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 22.825 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 22.850 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 22.875 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 22.900 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 22.925 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 22.950 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 22.975 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 23.000 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 23.025 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 23.050 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 23.075 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 23.100 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 23.125 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 23.150 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 23.175 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 23.200 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 23.225 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 23.250 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 23.275 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 23.300 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 23.325 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 23.350 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 23.375 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 23.400 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 23.425 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 23.450 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 23.475 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 23.500 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 23.525 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 23.550 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 23.575 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 23.600 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 23.625 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 23.650 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 23.675 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 23.700 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 23.725 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 23.750 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 23.775 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 23.800 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 23.825 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 23.850 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 23.875 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 23.900 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 23.925 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 23.950 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 23.975 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 24.000 | 129.03 | (N/A) | (N/A) | (N/A) | (N/A) |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 0.000 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 0.025 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 0.050 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 0.075 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 0.100 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 0.125 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 0.150 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 0.175 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 0.200 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 0.225 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 0.250 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 0.275 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 0.300 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 0.325 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 0.350 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 0.375 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 0.400 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 0.425 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 0.450 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 0.475 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 0.500 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 0.525 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 0.550 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 0.575 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 0.600 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 0.625 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 0.650 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 0.675 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 0.700 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 0.725 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 0.750 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 0.775 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 0.800 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 0.825 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 0.850 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 0.875 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 0.900 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 0.925 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 0.950 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 0.975 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 1.000 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 1.025 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 1.050 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 1.075 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 1.100 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 1.125 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 1.150 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 1.175 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 1.200 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 1.225 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 1.250 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 1.275 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 1.300 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 1.325 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 1.350 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 1.375 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 1.400 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 1.425 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 1.450 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 1.475 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 1.500 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 1.525 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 1.550 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 1.575 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 1.600 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 1.625 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 1.650 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 1.675 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 1.700 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 1.725 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 1.750 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 1.775 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 1.800 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 1.825 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 1.850 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 1.875 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 1.900 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 1.925 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 1.950 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 1.975 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 2.000 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 2.025 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 2.050 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 2.075 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 2.100 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 2.125 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 2.150 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 2.175 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 2.200 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 2.225 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 2.250 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 2.275 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 2.300 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 2.325 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 2.350 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 2.375 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 2.400 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 2.425 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 2.450 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 2.475 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 2.500 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 2.525 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 2.550 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 2.575 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 2.600 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 2.625 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 2.650 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 2.675 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 2.700 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 2.725 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 2.750 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 2.775 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 2.800 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 2.825 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 2.850 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 2.875 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 2.900 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 2.925 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 2.950 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 2.975 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 3.000 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 3.025 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 3.050 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 3.075 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 3.100 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 3.125 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 3.150 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 3.175 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 3.200 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 3.225 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 3.250 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 3.275 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 3.300 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 3.325 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 3.350 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 3.375 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 3.400 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 3.425 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 3.450 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 3.475 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 3.500 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 3.525 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 3.550 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 3.575 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 3.600 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 3.625 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 3.650 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 3.675 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 3.700 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 3.725 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 3.750 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 3.775 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 3.800 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 3.825 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 3.850 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 3.875 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 3.900 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 3.925 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 3.950 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 3.975 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 4.000 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 4.025 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 4.050 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 4.075 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 4.100 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 4.125 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 4.150 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 4.175 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 4.200 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 4.225 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 4.250 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 4.275 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 4.300 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 4.325 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 4.350 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 4.375 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 4.400 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 4.425 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 4.450 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 4.475 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 4.500 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 4.525 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 4.550 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 4.575 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 4.600 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 4.625 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 4.650 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 4.675 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 4.700 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 4.725 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 4.750 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 4.775 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 4.800 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 4.825 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 4.850 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 4.875 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 4.900 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 4.925 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 4.950 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 4.975 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 5.000 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 5.025 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 5.050 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 5.075 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 5.100 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 5.125 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 5.150 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 5.175 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 5.200 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 5.225 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 5.250 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 5.275 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 5.300 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 5.325 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 5.350 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 5.375 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 5.400 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 5.425 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 5.450 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 5.475 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 5.500 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 5.525 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 5.550 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 5.575 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 5.600 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 5.625 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 5.650 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 5.675 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 5.700 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 5.725 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 5.750 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 5.775 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 5.800 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 5.825 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 5.850 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 5.875 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 5.900 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 5.925 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 5.950 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 5.975 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 6.000 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 6.025 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 6.050 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 6.075 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 6.100 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 6.125 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 6.150 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 6.175 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 6.200 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 6.225 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 6.250 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 6.275 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 6.300 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 6.325 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 6.350 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 6.375 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 6.400 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 6.425 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 6.450 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 6.475 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 6.500 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 6.525 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 6.550 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 6.575 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 6.600 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 6.625 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 6.650 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 6.675 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 6.700 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 6.725 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 6.750 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 6.775 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 6.800 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 6.825 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 6.850 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 6.875 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 6.900 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 6.925 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 6.950 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 6.975 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 7.000 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 7.025 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 7.050 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 7.075 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 7.100 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 7.125 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 7.150 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 7.175 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 7.200 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 7.225 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 7.250 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 7.275 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 7.300 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 7.325 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 7.350 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 7.375 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 7.400 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 7.425 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 7.450 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 7.475 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 7.500 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 7.525 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 7.550 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 7.575 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 7.600 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 7.625 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 7.650 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 7.675 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 7.700 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 7.725 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 7.750 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 7.775 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 7.800 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 7.825 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 7.850 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 7.875 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 7.900 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 7.925 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 7.950 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 7.975 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 8.000 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 8.025 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 8.050 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 8.075 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 8.100 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 8.125 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 8.150 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 8.175 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 8.200 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 8.225 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 8.250 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 8.275 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 8.300 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 8.325 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 8.350 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 8.375 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 8.400 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 8.425 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 8.450 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 8.475 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 8.500 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 8.525 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 8.550 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 8.575 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 8.600 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 8.625 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 8.650 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 8.675 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 8.700 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 8.725 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 8.750 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 8.775 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 8.800 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 8.825 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 8.850 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 8.875 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 8.900 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 8.925 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 8.950 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 8.975 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 9.000 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 9.025 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 9.050 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 9.075 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 9.100 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 9.125 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 9.150 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 9.175 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 9.200 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 9.225 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 9.250 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 9.275 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 9.300 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 9.325 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 9.350 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 9.375 | 120.01 | 120.01 | 120.01 | 120.01 | 120.01 |
| 9.400 | 120.01 | 120.01 | 120.01 | 120.01 | 120.01 |
| 9.425 | 120.01 | 120.01 | 120.01 | 120.01 | 120.02 |
| 9.450 | 120.02 | 120.02 | 120.02 | 120.02 | 120.02 |
| 9.475 | 120.02 | 120.02 | 120.02 | 120.02 | 120.02 |
| 9.500 | 120.02 | 120.02 | 120.02 | 120.02 | 120.02 |
| 9.525 | 120.03 | 120.03 | 120.03 | 120.03 | 120.03 |
| 9.550 | 120.03 | 120.03 | 120.03 | 120.03 | 120.03 |
| 9.575 | 120.03 | 120.03 | 120.03 | 120.03 | 120.03 |
| 9.600 | 120.03 | 120.03 | 120.04 | 120.04 | 120.04 |
| 9.625 | 120.04 | 120.04 | 120.04 | 120.04 | 120.04 |
| 9.650 | 120.04 | 120.04 | 120.04 | 120.04 | 120.04 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 9.675 | 120.04 | 120.04 | 120.04 | 120.04 | 120.04 |
| 9.700 | 120.04 | 120.04 | 120.04 | 120.05 | 120.05 |
| 9.725 | 120.05 | 120.05 | 120.05 | 120.05 | 120.05 |
| 9.750 | 120.05 | 120.05 | 120.05 | 120.05 | 120.05 |
| 9.775 | 120.05 | 120.05 | 120.05 | 120.05 | 120.05 |
| 9.800 | 120.05 | 120.05 | 120.05 | 120.05 | 120.05 |
| 9.825 | 120.05 | 120.05 | 120.05 | 120.05 | 120.06 |
| 9.850 | 120.06 | 120.06 | 120.06 | 120.06 | 120.06 |
| 9.875 | 120.06 | 120.06 | 120.06 | 120.06 | 120.06 |
| 9.900 | 120.06 | 120.06 | 120.06 | 120.06 | 120.06 |
| 9.925 | 120.06 | 120.06 | 120.06 | 120.06 | 120.06 |
| 9.950 | 120.06 | 120.06 | 120.06 | 120.06 | 120.06 |
| 9.975 | 120.06 | 120.06 | 120.06 | 120.06 | 120.07 |
| 10.000 | 120.07 | 120.07 | 120.07 | 120.07 | 120.07 |
| 10.025 | 120.07 | 120.07 | 120.07 | 120.07 | 120.07 |
| 10.050 | 120.07 | 120.07 | 120.07 | 120.07 | 120.07 |
| 10.075 | 120.07 | 120.07 | 120.07 | 120.07 | 120.07 |
| 10.100 | 120.07 | 120.07 | 120.07 | 120.07 | 120.07 |
| 10.125 | 120.07 | 120.07 | 120.07 | 120.07 | 120.07 |
| 10.150 | 120.07 | 120.07 | 120.07 | 120.08 | 120.08 |
| 10.175 | 120.08 | 120.08 | 120.08 | 120.08 | 120.08 |
| 10.200 | 120.08 | 120.08 | 120.08 | 120.08 | 120.08 |
| 10.225 | 120.08 | 120.08 | 120.08 | 120.08 | 120.08 |
| 10.250 | 120.08 | 120.08 | 120.08 | 120.08 | 120.08 |
| 10.275 | 120.08 | 120.08 | 120.08 | 120.08 | 120.08 |
| 10.300 | 120.08 | 120.08 | 120.08 | 120.08 | 120.08 |
| 10.325 | 120.08 | 120.09 | 120.09 | 120.09 | 120.09 |
| 10.350 | 120.09 | 120.09 | 120.09 | 120.09 | 120.09 |
| 10.375 | 120.09 | 120.09 | 120.09 | 120.09 | 120.09 |
| 10.400 | 120.09 | 120.09 | 120.09 | 120.09 | 120.09 |
| 10.425 | 120.09 | 120.09 | 120.09 | 120.09 | 120.09 |
| 10.450 | 120.09 | 120.09 | 120.09 | 120.09 | 120.09 |
| 10.475 | 120.09 | 120.09 | 120.09 | 120.09 | 120.09 |
| 10.500 | 120.10 | 120.10 | 120.10 | 120.10 | 120.10 |
| 10.525 | 120.10 | 120.10 | 120.10 | 120.10 | 120.10 |
| 10.550 | 120.10 | 120.10 | 120.10 | 120.10 | 120.10 |
| 10.575 | 120.10 | 120.10 | 120.10 | 120.10 | 120.10 |
| 10.600 | 120.10 | 120.10 | 120.10 | 120.10 | 120.10 |
| 10.625 | 120.10 | 120.10 | 120.10 | 120.10 | 120.10 |
| 10.650 | 120.10 | 120.10 | 120.11 | 120.11 | 120.11 |
| 10.675 | 120.11 | 120.11 | 120.11 | 120.11 | 120.11 |
| 10.700 | 120.11 | 120.11 | 120.11 | 120.11 | 120.11 |
| 10.725 | 120.11 | 120.11 | 120.11 | 120.11 | 120.11 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 10.750 | 120.11 | 120.11 | 120.11 | 120.11 | 120.11 |
| 10.775 | 120.11 | 120.11 | 120.11 | 120.11 | 120.11 |
| 10.800 | 120.11 | 120.11 | 120.12 | 120.12 | 120.12 |
| 10.825 | 120.12 | 120.12 | 120.12 | 120.12 | 120.12 |
| 10.850 | 120.12 | 120.12 | 120.12 | 120.12 | 120.12 |
| 10.875 | 120.12 | 120.12 | 120.12 | 120.12 | 120.12 |
| 10.900 | 120.12 | 120.12 | 120.12 | 120.12 | 120.12 |
| 10.925 | 120.12 | 120.12 | 120.12 | 120.12 | 120.12 |
| 10.950 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 10.975 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 11.000 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 11.025 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 11.050 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 11.075 | 120.13 | 120.13 | 120.14 | 120.14 | 120.14 |
| 11.100 | 120.14 | 120.14 | 120.14 | 120.14 | 120.14 |
| 11.125 | 120.14 | 120.14 | 120.14 | 120.14 | 120.14 |
| 11.150 | 120.14 | 120.14 | 120.14 | 120.14 | 120.14 |
| 11.175 | 120.14 | 120.14 | 120.14 | 120.14 | 120.14 |
| 11.200 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |
| 11.225 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |
| 11.250 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |
| 11.275 | 120.15 | 120.15 | 120.15 | 120.15 | 120.16 |
| 11.300 | 120.16 | 120.16 | 120.16 | 120.16 | 120.16 |
| 11.325 | 120.16 | 120.16 | 120.16 | 120.16 | 120.16 |
| 11.350 | 120.16 | 120.16 | 120.16 | 120.16 | 120.16 |
| 11.375 | 120.16 | 120.17 | 120.17 | 120.17 | 120.17 |
| 11.400 | 120.17 | 120.17 | 120.17 | 120.17 | 120.17 |
| 11.425 | 120.17 | 120.17 | 120.17 | 120.17 | 120.17 |
| 11.450 | 120.17 | 120.17 | 120.17 | 120.17 | 120.18 |
| 11.475 | 120.18 | 120.18 | 120.18 | 120.18 | 120.18 |
| 11.500 | 120.18 | 120.18 | 120.18 | 120.18 | 120.18 |
| 11.525 | 120.18 | 120.18 | 120.18 | 120.19 | 120.19 |
| 11.550 | 120.19 | 120.19 | 120.19 | 120.19 | 120.19 |
| 11.575 | 120.19 | 120.20 | 120.20 | 120.20 | 120.20 |
| 11.600 | 120.20 | 120.21 | 120.21 | 120.21 | 120.22 |
| 11.625 | 120.22 | 120.22 | 120.22 | 120.23 | 120.23 |
| 11.650 | 120.23 | 120.24 | 120.24 | 120.24 | 120.25 |
| 11.675 | 120.25 | 120.26 | 120.26 | 120.26 | 120.27 |
| 11.700 | 120.27 | 120.28 | 120.28 | 120.29 | 120.29 |
| 11.725 | 120.30 | 120.30 | 120.30 | 120.31 | 120.31 |
| 11.750 | 120.32 | 120.32 | 120.33 | 120.33 | 120.34 |
| 11.775 | 120.34 | 120.35 | 120.35 | 120.36 | 120.36 |
| 11.800 | 120.37 | 120.37 | 120.38 | 120.38 | 120.39 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 11.825 | 120.40 | 120.40 | 120.41 | 120.41 | 120.42 |
| 11.850 | 120.42 | 120.43 | 120.44 | 120.44 | 120.45 |
| 11.875 | 120.46 | 120.46 | 120.47 | 120.48 | 120.49 |
| 11.900 | 120.49 | 120.50 | 120.51 | 120.51 | 120.52 |
| 11.925 | 120.53 | 120.53 | 120.54 | 120.55 | 120.55 |
| 11.950 | 120.56 | 120.56 | 120.57 | 120.57 | 120.57 |
| 11.975 | 120.58 | 120.58 | 120.58 | 120.59 | 120.59 |
| 12.000 | 120.59 | 120.59 | 120.59 | 120.59 | 120.59 |
| 12.025 | 120.59 | 120.59 | 120.59 | 120.59 | 120.59 |
| 12.050 | 120.59 | 120.59 | 120.58 | 120.58 | 120.58 |
| 12.075 | 120.57 | 120.57 | 120.57 | 120.56 | 120.56 |
| 12.100 | 120.55 | 120.54 | 120.54 | 120.53 | 120.53 |
| 12.125 | 120.52 | 120.51 | 120.51 | 120.50 | 120.49 |
| 12.150 | 120.49 | 120.48 | 120.47 | 120.47 | 120.46 |
| 12.175 | 120.45 | 120.45 | 120.44 | 120.43 | 120.43 |
| 12.200 | 120.42 | 120.42 | 120.41 | 120.41 | 120.40 |
| 12.225 | 120.40 | 120.39 | 120.39 | 120.39 | 120.38 |
| 12.250 | 120.38 | 120.38 | 120.37 | 120.37 | 120.37 |
| 12.275 | 120.36 | 120.36 | 120.36 | 120.35 | 120.35 |
| 12.300 | 120.35 | 120.35 | 120.34 | 120.34 | 120.34 |
| 12.325 | 120.34 | 120.33 | 120.33 | 120.33 | 120.33 |
| 12.350 | 120.33 | 120.33 | 120.32 | 120.32 | 120.32 |
| 12.375 | 120.32 | 120.32 | 120.32 | 120.31 | 120.31 |
| 12.400 | 120.31 | 120.31 | 120.31 | 120.31 | 120.31 |
| 12.425 | 120.30 | 120.30 | 120.30 | 120.30 | 120.30 |
| 12.450 | 120.30 | 120.30 | 120.30 | 120.30 | 120.29 |
| 12.475 | 120.29 | 120.29 | 120.29 | 120.29 | 120.29 |
| 12.500 | 120.29 | 120.29 | 120.28 | 120.28 | 120.28 |
| 12.525 | 120.28 | 120.28 | 120.28 | 120.28 | 120.28 |
| 12.550 | 120.28 | 120.28 | 120.27 | 120.27 | 120.27 |
| 12.575 | 120.27 | 120.27 | 120.27 | 120.27 | 120.27 |
| 12.600 | 120.27 | 120.27 | 120.27 | 120.26 | 120.26 |
| 12.625 | 120.26 | 120.26 | 120.26 | 120.26 | 120.26 |
| 12.650 | 120.26 | 120.26 | 120.26 | 120.26 | 120.26 |
| 12.675 | 120.26 | 120.26 | 120.25 | 120.25 | 120.25 |
| 12.700 | 120.25 | 120.25 | 120.25 | 120.25 | 120.25 |
| 12.725 | 120.25 | 120.25 | 120.25 | 120.25 | 120.25 |
| 12.750 | 120.25 | 120.25 | 120.25 | 120.25 | 120.25 |
| 12.775 | 120.25 | 120.25 | 120.25 | 120.25 | 120.24 |
| 12.800 | 120.24 | 120.24 | 120.24 | 120.24 | 120.24 |
| 12.825 | 120.24 | 120.24 | 120.24 | 120.24 | 120.24 |
| 12.850 | 120.24 | 120.24 | 120.24 | 120.24 | 120.24 |
| 12.875 | 120.24 | 120.24 | 120.24 | 120.24 | 120.24 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 12.900 | 120.24 | 120.24 | 120.24 | 120.24 | 120.24 |
| 12.925 | 120.24 | 120.24 | 120.24 | 120.24 | 120.24 |
| 12.950 | 120.24 | 120.23 | 120.23 | 120.23 | 120.23 |
| 12.975 | 120.23 | 120.23 | 120.23 | 120.23 | 120.23 |
| 13.000 | 120.23 | 120.23 | 120.23 | 120.23 | 120.23 |
| 13.025 | 120.23 | 120.23 | 120.23 | 120.23 | 120.23 |
| 13.050 | 120.23 | 120.23 | 120.23 | 120.23 | 120.23 |
| 13.075 | 120.23 | 120.23 | 120.23 | 120.23 | 120.23 |
| 13.100 | 120.23 | 120.23 | 120.23 | 120.23 | 120.22 |
| 13.125 | 120.22 | 120.22 | 120.22 | 120.22 | 120.22 |
| 13.150 | 120.22 | 120.22 | 120.22 | 120.22 | 120.22 |
| 13.175 | 120.22 | 120.22 | 120.22 | 120.22 | 120.22 |
| 13.200 | 120.22 | 120.22 | 120.22 | 120.22 | 120.22 |
| 13.225 | 120.22 | 120.22 | 120.22 | 120.22 | 120.22 |
| 13.250 | 120.22 | 120.22 | 120.22 | 120.22 | 120.22 |
| 13.275 | 120.22 | 120.22 | 120.22 | 120.22 | 120.22 |
| 13.300 | 120.22 | 120.22 | 120.22 | 120.22 | 120.22 |
| 13.325 | 120.22 | 120.22 | 120.22 | 120.22 | 120.21 |
| 13.350 | 120.21 | 120.21 | 120.21 | 120.21 | 120.21 |
| 13.375 | 120.21 | 120.21 | 120.21 | 120.21 | 120.21 |
| 13.400 | 120.21 | 120.21 | 120.21 | 120.21 | 120.21 |
| 13.425 | 120.21 | 120.21 | 120.21 | 120.21 | 120.21 |
| 13.450 | 120.21 | 120.21 | 120.21 | 120.21 | 120.21 |
| 13.475 | 120.21 | 120.21 | 120.21 | 120.21 | 120.21 |
| 13.500 | 120.21 | 120.21 | 120.21 | 120.21 | 120.21 |
| 13.525 | 120.21 | 120.21 | 120.21 | 120.21 | 120.21 |
| 13.550 | 120.21 | 120.21 | 120.21 | 120.21 | 120.21 |
| 13.575 | 120.21 | 120.21 | 120.21 | 120.21 | 120.21 |
| 13.600 | 120.20 | 120.20 | 120.20 | 120.20 | 120.20 |
| 13.625 | 120.20 | 120.20 | 120.20 | 120.20 | 120.20 |
| 13.650 | 120.20 | 120.20 | 120.20 | 120.20 | 120.20 |
| 13.675 | 120.20 | 120.20 | 120.20 | 120.20 | 120.20 |
| 13.700 | 120.20 | 120.20 | 120.20 | 120.20 | 120.20 |
| 13.725 | 120.20 | 120.20 | 120.20 | 120.20 | 120.20 |
| 13.750 | 120.20 | 120.20 | 120.20 | 120.20 | 120.20 |
| 13.775 | 120.20 | 120.20 | 120.20 | 120.20 | 120.20 |
| 13.800 | 120.20 | 120.20 | 120.20 | 120.20 | 120.20 |
| 13.825 | 120.20 | 120.20 | 120.20 | 120.20 | 120.20 |
| 13.850 | 120.20 | 120.20 | 120.20 | 120.20 | 120.20 |
| 13.875 | 120.20 | 120.20 | 120.20 | 120.19 | 120.19 |
| 13.900 | 120.19 | 120.19 | 120.19 | 120.19 | 120.19 |
| 13.925 | 120.19 | 120.19 | 120.19 | 120.19 | 120.19 |
| 13.950 | 120.19 | 120.19 | 120.19 | 120.19 | 120.19 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 13.975 | 120.19 | 120.19 | 120.19 | 120.19 | 120.19 |
| 14.000 | 120.19 | 120.19 | 120.19 | 120.19 | 120.19 |
| 14.025 | 120.19 | 120.19 | 120.19 | 120.19 | 120.19 |
| 14.050 | 120.19 | 120.19 | 120.19 | 120.19 | 120.19 |
| 14.075 | 120.19 | 120.19 | 120.19 | 120.19 | 120.19 |
| 14.100 | 120.19 | 120.19 | 120.19 | 120.19 | 120.19 |
| 14.125 | 120.19 | 120.19 | 120.19 | 120.19 | 120.19 |
| 14.150 | 120.19 | 120.19 | 120.19 | 120.19 | 120.19 |
| 14.175 | 120.19 | 120.19 | 120.19 | 120.19 | 120.19 |
| 14.200 | 120.19 | 120.19 | 120.19 | 120.19 | 120.19 |
| 14.225 | 120.19 | 120.18 | 120.18 | 120.18 | 120.18 |
| 14.250 | 120.18 | 120.18 | 120.18 | 120.18 | 120.18 |
| 14.275 | 120.18 | 120.18 | 120.18 | 120.18 | 120.18 |
| 14.300 | 120.18 | 120.18 | 120.18 | 120.18 | 120.18 |
| 14.325 | 120.18 | 120.18 | 120.18 | 120.18 | 120.18 |
| 14.350 | 120.18 | 120.18 | 120.18 | 120.18 | 120.18 |
| 14.375 | 120.18 | 120.18 | 120.18 | 120.18 | 120.18 |
| 14.400 | 120.18 | 120.18 | 120.18 | 120.18 | 120.18 |
| 14.425 | 120.18 | 120.18 | 120.18 | 120.18 | 120.18 |
| 14.450 | 120.18 | 120.18 | 120.18 | 120.18 | 120.18 |
| 14.475 | 120.18 | 120.18 | 120.18 | 120.18 | 120.18 |
| 14.500 | 120.18 | 120.18 | 120.18 | 120.18 | 120.18 |
| 14.525 | 120.18 | 120.18 | 120.18 | 120.18 | 120.18 |
| 14.550 | 120.18 | 120.18 | 120.18 | 120.18 | 120.18 |
| 14.575 | 120.18 | 120.18 | 120.18 | 120.18 | 120.18 |
| 14.600 | 120.18 | 120.18 | 120.18 | 120.18 | 120.18 |
| 14.625 | 120.18 | 120.18 | 120.18 | 120.18 | 120.18 |
| 14.650 | 120.18 | 120.18 | 120.18 | 120.18 | 120.18 |
| 14.675 | 120.18 | 120.18 | 120.18 | 120.18 | 120.18 |
| 14.700 | 120.18 | 120.18 | 120.18 | 120.18 | 120.18 |
| 14.725 | 120.18 | 120.18 | 120.18 | 120.18 | 120.18 |
| 14.750 | 120.18 | 120.18 | 120.18 | 120.18 | 120.18 |
| 14.775 | 120.18 | 120.18 | 120.18 | 120.18 | 120.18 |
| 14.800 | 120.18 | 120.18 | 120.18 | 120.18 | 120.18 |
| 14.825 | 120.18 | 120.18 | 120.18 | 120.18 | 120.18 |
| 14.850 | 120.18 | 120.18 | 120.18 | 120.18 | 120.18 |
| 14.875 | 120.18 | 120.18 | 120.18 | 120.18 | 120.18 |
| 14.900 | 120.18 | 120.18 | 120.18 | 120.18 | 120.18 |
| 14.925 | 120.18 | 120.18 | 120.18 | 120.18 | 120.18 |
| 14.950 | 120.18 | 120.18 | 120.18 | 120.18 | 120.18 |
| 14.975 | 120.18 | 120.18 | 120.17 | 120.17 | 120.17 |
| 15.000 | 120.17 | 120.17 | 120.17 | 120.17 | 120.17 |
| 15.025 | 120.17 | 120.17 | 120.17 | 120.17 | 120.17 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 15.050 | 120.17 | 120.17 | 120.17 | 120.17 | 120.17 |
| 15.075 | 120.17 | 120.17 | 120.17 | 120.17 | 120.17 |
| 15.100 | 120.17 | 120.17 | 120.17 | 120.17 | 120.17 |
| 15.125 | 120.17 | 120.17 | 120.17 | 120.17 | 120.17 |
| 15.150 | 120.17 | 120.17 | 120.17 | 120.17 | 120.17 |
| 15.175 | 120.17 | 120.17 | 120.17 | 120.17 | 120.17 |
| 15.200 | 120.17 | 120.17 | 120.17 | 120.17 | 120.17 |
| 15.225 | 120.17 | 120.17 | 120.17 | 120.17 | 120.17 |
| 15.250 | 120.17 | 120.17 | 120.17 | 120.17 | 120.17 |
| 15.275 | 120.17 | 120.17 | 120.17 | 120.17 | 120.17 |
| 15.300 | 120.17 | 120.17 | 120.17 | 120.17 | 120.17 |
| 15.325 | 120.17 | 120.17 | 120.17 | 120.17 | 120.17 |
| 15.350 | 120.17 | 120.17 | 120.17 | 120.17 | 120.17 |
| 15.375 | 120.17 | 120.17 | 120.17 | 120.17 | 120.17 |
| 15.400 | 120.17 | 120.17 | 120.17 | 120.17 | 120.17 |
| 15.425 | 120.17 | 120.17 | 120.17 | 120.17 | 120.17 |
| 15.450 | 120.17 | 120.17 | 120.17 | 120.17 | 120.17 |
| 15.475 | 120.17 | 120.17 | 120.17 | 120.17 | 120.17 |
| 15.500 | 120.17 | 120.17 | 120.17 | 120.17 | 120.17 |
| 15.525 | 120.17 | 120.17 | 120.17 | 120.17 | 120.17 |
| 15.550 | 120.17 | 120.17 | 120.17 | 120.17 | 120.17 |
| 15.575 | 120.17 | 120.17 | 120.17 | 120.17 | 120.17 |
| 15.600 | 120.17 | 120.17 | 120.17 | 120.17 | 120.17 |
| 15.625 | 120.17 | 120.17 | 120.17 | 120.17 | 120.17 |
| 15.650 | 120.17 | 120.17 | 120.17 | 120.17 | 120.16 |
| 15.675 | 120.16 | 120.16 | 120.16 | 120.16 | 120.16 |
| 15.700 | 120.16 | 120.16 | 120.16 | 120.16 | 120.16 |
| 15.725 | 120.16 | 120.16 | 120.16 | 120.16 | 120.16 |
| 15.750 | 120.16 | 120.16 | 120.16 | 120.16 | 120.16 |
| 15.775 | 120.16 | 120.16 | 120.16 | 120.16 | 120.16 |
| 15.800 | 120.16 | 120.16 | 120.16 | 120.16 | 120.16 |
| 15.825 | 120.16 | 120.16 | 120.16 | 120.16 | 120.16 |
| 15.850 | 120.16 | 120.16 | 120.16 | 120.16 | 120.16 |
| 15.875 | 120.16 | 120.16 | 120.16 | 120.16 | 120.16 |
| 15.900 | 120.16 | 120.16 | 120.16 | 120.16 | 120.16 |
| 15.925 | 120.16 | 120.16 | 120.16 | 120.16 | 120.16 |
| 15.950 | 120.16 | 120.16 | 120.16 | 120.16 | 120.16 |
| 15.975 | 120.16 | 120.16 | 120.16 | 120.16 | 120.16 |
| 16.000 | 120.16 | 120.16 | 120.16 | 120.16 | 120.16 |
| 16.025 | 120.16 | 120.16 | 120.16 | 120.16 | 120.16 |
| 16.050 | 120.16 | 120.16 | 120.16 | 120.16 | 120.16 |
| 16.075 | 120.16 | 120.16 | 120.16 | 120.16 | 120.16 |
| 16.100 | 120.16 | 120.16 | 120.16 | 120.16 | 120.16 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 16.125 | 120.16 | 120.16 | 120.16 | 120.16 | 120.16 |
| 16.150 | 120.16 | 120.16 | 120.16 | 120.16 | 120.16 |
| 16.175 | 120.16 | 120.16 | 120.16 | 120.16 | 120.16 |
| 16.200 | 120.16 | 120.16 | 120.16 | 120.16 | 120.16 |
| 16.225 | 120.16 | 120.16 | 120.16 | 120.16 | 120.16 |
| 16.250 | 120.16 | 120.16 | 120.16 | 120.16 | 120.16 |
| 16.275 | 120.16 | 120.16 | 120.16 | 120.16 | 120.16 |
| 16.300 | 120.16 | 120.16 | 120.16 | 120.16 | 120.16 |
| 16.325 | 120.16 | 120.16 | 120.16 | 120.16 | 120.16 |
| 16.350 | 120.16 | 120.16 | 120.16 | 120.16 | 120.16 |
| 16.375 | 120.16 | 120.16 | 120.16 | 120.16 | 120.16 |
| 16.400 | 120.16 | 120.16 | 120.16 | 120.16 | 120.16 |
| 16.425 | 120.16 | 120.16 | 120.16 | 120.16 | 120.16 |
| 16.450 | 120.16 | 120.16 | 120.16 | 120.15 | 120.15 |
| 16.475 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |
| 16.500 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |
| 16.525 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |
| 16.550 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |
| 16.575 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |
| 16.600 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |
| 16.625 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |
| 16.650 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |
| 16.675 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |
| 16.700 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |
| 16.725 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |
| 16.750 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |
| 16.775 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |
| 16.800 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |
| 16.825 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |
| 16.850 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |
| 16.875 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |
| 16.900 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |
| 16.925 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |
| 16.950 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |
| 16.975 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |
| 17.000 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |
| 17.025 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |
| 17.050 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |
| 17.075 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |
| 17.100 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |
| 17.125 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |
| 17.150 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |
| 17.175 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 17.200 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |
| 17.225 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |
| 17.250 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |
| 17.275 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |
| 17.300 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |
| 17.325 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |
| 17.350 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |
| 17.375 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |
| 17.400 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |
| 17.425 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |
| 17.450 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |
| 17.475 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |
| 17.500 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |
| 17.525 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |
| 17.550 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |
| 17.575 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |
| 17.600 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |
| 17.625 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |
| 17.650 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |
| 17.675 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |
| 17.700 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |
| 17.725 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |
| 17.750 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |
| 17.775 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |
| 17.800 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |
| 17.825 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |
| 17.850 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |
| 17.875 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |
| 17.900 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |
| 17.925 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |
| 17.950 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |
| 17.975 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |
| 18.000 | 120.15 | 120.15 | 120.15 | 120.15 | 120.14 |
| 18.025 | 120.14 | 120.14 | 120.14 | 120.14 | 120.14 |
| 18.050 | 120.14 | 120.14 | 120.14 | 120.14 | 120.14 |
| 18.075 | 120.14 | 120.14 | 120.14 | 120.14 | 120.14 |
| 18.100 | 120.14 | 120.14 | 120.14 | 120.14 | 120.14 |
| 18.125 | 120.14 | 120.14 | 120.14 | 120.14 | 120.14 |
| 18.150 | 120.14 | 120.14 | 120.14 | 120.14 | 120.14 |
| 18.175 | 120.14 | 120.14 | 120.14 | 120.14 | 120.14 |
| 18.200 | 120.14 | 120.14 | 120.14 | 120.14 | 120.14 |
| 18.225 | 120.14 | 120.14 | 120.14 | 120.14 | 120.14 |
| 18.250 | 120.14 | 120.14 | 120.14 | 120.14 | 120.14 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 18.275 | 120.14 | 120.14 | 120.14 | 120.14 | 120.14 |
| 18.300 | 120.14 | 120.14 | 120.14 | 120.14 | 120.14 |
| 18.325 | 120.14 | 120.14 | 120.14 | 120.14 | 120.14 |
| 18.350 | 120.14 | 120.14 | 120.14 | 120.14 | 120.14 |
| 18.375 | 120.14 | 120.14 | 120.14 | 120.14 | 120.14 |
| 18.400 | 120.14 | 120.14 | 120.14 | 120.14 | 120.14 |
| 18.425 | 120.14 | 120.14 | 120.14 | 120.14 | 120.14 |
| 18.450 | 120.14 | 120.14 | 120.14 | 120.14 | 120.14 |
| 18.475 | 120.14 | 120.14 | 120.14 | 120.14 | 120.14 |
| 18.500 | 120.14 | 120.14 | 120.14 | 120.14 | 120.14 |
| 18.525 | 120.14 | 120.14 | 120.14 | 120.14 | 120.14 |
| 18.550 | 120.14 | 120.14 | 120.14 | 120.14 | 120.14 |
| 18.575 | 120.14 | 120.14 | 120.14 | 120.14 | 120.14 |
| 18.600 | 120.14 | 120.14 | 120.14 | 120.14 | 120.14 |
| 18.625 | 120.14 | 120.14 | 120.14 | 120.14 | 120.14 |
| 18.650 | 120.14 | 120.14 | 120.14 | 120.14 | 120.14 |
| 18.675 | 120.14 | 120.14 | 120.14 | 120.14 | 120.14 |
| 18.700 | 120.14 | 120.14 | 120.14 | 120.14 | 120.14 |
| 18.725 | 120.14 | 120.14 | 120.14 | 120.14 | 120.14 |
| 18.750 | 120.14 | 120.14 | 120.14 | 120.14 | 120.14 |
| 18.775 | 120.14 | 120.14 | 120.14 | 120.14 | 120.14 |
| 18.800 | 120.14 | 120.14 | 120.14 | 120.14 | 120.14 |
| 18.825 | 120.14 | 120.14 | 120.14 | 120.14 | 120.14 |
| 18.850 | 120.14 | 120.14 | 120.14 | 120.14 | 120.14 |
| 18.875 | 120.14 | 120.14 | 120.14 | 120.14 | 120.14 |
| 18.900 | 120.14 | 120.14 | 120.14 | 120.14 | 120.14 |
| 18.925 | 120.14 | 120.14 | 120.14 | 120.14 | 120.14 |
| 18.950 | 120.14 | 120.14 | 120.14 | 120.14 | 120.14 |
| 18.975 | 120.14 | 120.14 | 120.14 | 120.14 | 120.14 |
| 19.000 | 120.14 | 120.14 | 120.14 | 120.14 | 120.14 |
| 19.025 | 120.14 | 120.14 | 120.14 | 120.14 | 120.14 |
| 19.050 | 120.14 | 120.14 | 120.14 | 120.14 | 120.14 |
| 19.075 | 120.14 | 120.14 | 120.14 | 120.14 | 120.14 |
| 19.100 | 120.14 | 120.14 | 120.14 | 120.14 | 120.14 |
| 19.125 | 120.14 | 120.14 | 120.14 | 120.14 | 120.14 |
| 19.150 | 120.14 | 120.14 | 120.14 | 120.14 | 120.14 |
| 19.175 | 120.14 | 120.14 | 120.14 | 120.14 | 120.14 |
| 19.200 | 120.14 | 120.14 | 120.14 | 120.14 | 120.14 |
| 19.225 | 120.14 | 120.14 | 120.14 | 120.14 | 120.14 |
| 19.250 | 120.14 | 120.14 | 120.14 | 120.14 | 120.14 |
| 19.275 | 120.14 | 120.14 | 120.14 | 120.14 | 120.14 |
| 19.300 | 120.14 | 120.14 | 120.14 | 120.14 | 120.14 |
| 19.325 | 120.14 | 120.14 | 120.14 | 120.14 | 120.14 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 19.350 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 19.375 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 19.400 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 19.425 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 19.450 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 19.475 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 19.500 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 19.525 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 19.550 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 19.575 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 19.600 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 19.625 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 19.650 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 19.675 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 19.700 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 19.725 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 19.750 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 19.775 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 19.800 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 19.825 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 19.850 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 19.875 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 19.900 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 19.925 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 19.950 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 19.975 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 20.000 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 20.025 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 20.050 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 20.075 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 20.100 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 20.125 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 20.150 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 20.175 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 20.200 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 20.225 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 20.250 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 20.275 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 20.300 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 20.325 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 20.350 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 20.375 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 20.400 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 20.425 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 20.450 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 20.475 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 20.500 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 20.525 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 20.550 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 20.575 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 20.600 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 20.625 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 20.650 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 20.675 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 20.700 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 20.725 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 20.750 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 20.775 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 20.800 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 20.825 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 20.850 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 20.875 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 20.900 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 20.925 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 20.950 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 20.975 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 21.000 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 21.025 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 21.050 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 21.075 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 21.100 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 21.125 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 21.150 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 21.175 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 21.200 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 21.225 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 21.250 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 21.275 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 21.300 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 21.325 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 21.350 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 21.375 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 21.400 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 21.425 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 21.450 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 21.475 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 21.500 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 21.525 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 21.550 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 21.575 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 21.600 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 21.625 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 21.650 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 21.675 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 21.700 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 21.725 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 21.750 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 21.775 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 21.800 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 21.825 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 21.850 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 21.875 | 120.13 | 120.13 | 120.13 | 120.13 | 120.12 |
| 21.900 | 120.12 | 120.12 | 120.12 | 120.12 | 120.12 |
| 21.925 | 120.12 | 120.12 | 120.12 | 120.12 | 120.12 |
| 21.950 | 120.12 | 120.12 | 120.12 | 120.12 | 120.12 |
| 21.975 | 120.12 | 120.12 | 120.12 | 120.12 | 120.12 |
| 22.000 | 120.12 | 120.12 | 120.12 | 120.12 | 120.12 |
| 22.025 | 120.12 | 120.12 | 120.12 | 120.12 | 120.12 |
| 22.050 | 120.12 | 120.12 | 120.12 | 120.12 | 120.12 |
| 22.075 | 120.12 | 120.12 | 120.12 | 120.12 | 120.12 |
| 22.100 | 120.12 | 120.12 | 120.12 | 120.12 | 120.12 |
| 22.125 | 120.12 | 120.12 | 120.12 | 120.12 | 120.12 |
| 22.150 | 120.12 | 120.12 | 120.12 | 120.12 | 120.12 |
| 22.175 | 120.12 | 120.12 | 120.12 | 120.12 | 120.12 |
| 22.200 | 120.12 | 120.12 | 120.12 | 120.12 | 120.12 |
| 22.225 | 120.12 | 120.12 | 120.12 | 120.12 | 120.12 |
| 22.250 | 120.12 | 120.12 | 120.12 | 120.12 | 120.12 |
| 22.275 | 120.12 | 120.12 | 120.12 | 120.12 | 120.12 |
| 22.300 | 120.12 | 120.12 | 120.12 | 120.12 | 120.12 |
| 22.325 | 120.12 | 120.12 | 120.12 | 120.12 | 120.12 |
| 22.350 | 120.12 | 120.12 | 120.12 | 120.12 | 120.12 |
| 22.375 | 120.12 | 120.12 | 120.12 | 120.12 | 120.12 |
| 22.400 | 120.12 | 120.12 | 120.12 | 120.12 | 120.12 |
| 22.425 | 120.12 | 120.12 | 120.12 | 120.12 | 120.12 |
| 22.450 | 120.12 | 120.12 | 120.12 | 120.12 | 120.12 |
| 22.475 | 120.12 | 120.12 | 120.12 | 120.12 | 120.12 |
| 22.500 | 120.12 | 120.12 | 120.12 | 120.12 | 120.12 |
| 22.525 | 120.12 | 120.12 | 120.12 | 120.12 | 120.12 |
| 22.550 | 120.12 | 120.12 | 120.12 | 120.12 | 120.12 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 22.575 | 120.12 | 120.12 | 120.12 | 120.12 | 120.12 |
| 22.600 | 120.12 | 120.12 | 120.12 | 120.12 | 120.12 |
| 22.625 | 120.12 | 120.12 | 120.12 | 120.12 | 120.12 |
| 22.650 | 120.12 | 120.12 | 120.12 | 120.12 | 120.12 |
| 22.675 | 120.12 | 120.12 | 120.12 | 120.12 | 120.12 |
| 22.700 | 120.12 | 120.12 | 120.12 | 120.12 | 120.12 |
| 22.725 | 120.12 | 120.12 | 120.12 | 120.12 | 120.12 |
| 22.750 | 120.12 | 120.12 | 120.12 | 120.12 | 120.12 |
| 22.775 | 120.12 | 120.12 | 120.12 | 120.12 | 120.12 |
| 22.800 | 120.12 | 120.12 | 120.12 | 120.12 | 120.12 |
| 22.825 | 120.12 | 120.12 | 120.12 | 120.12 | 120.12 |
| 22.850 | 120.12 | 120.12 | 120.12 | 120.12 | 120.12 |
| 22.875 | 120.12 | 120.12 | 120.12 | 120.12 | 120.12 |
| 22.900 | 120.12 | 120.12 | 120.12 | 120.12 | 120.12 |
| 22.925 | 120.12 | 120.12 | 120.12 | 120.12 | 120.12 |
| 22.950 | 120.12 | 120.12 | 120.12 | 120.12 | 120.12 |
| 22.975 | 120.12 | 120.12 | 120.12 | 120.12 | 120.12 |
| 23.000 | 120.12 | 120.12 | 120.12 | 120.12 | 120.12 |
| 23.025 | 120.12 | 120.12 | 120.12 | 120.12 | 120.12 |
| 23.050 | 120.12 | 120.12 | 120.12 | 120.12 | 120.12 |
| 23.075 | 120.12 | 120.12 | 120.12 | 120.12 | 120.12 |
| 23.100 | 120.12 | 120.12 | 120.12 | 120.12 | 120.12 |
| 23.125 | 120.12 | 120.12 | 120.12 | 120.12 | 120.12 |
| 23.150 | 120.12 | 120.12 | 120.12 | 120.12 | 120.12 |
| 23.175 | 120.12 | 120.12 | 120.12 | 120.12 | 120.12 |
| 23.200 | 120.12 | 120.12 | 120.12 | 120.12 | 120.12 |
| 23.225 | 120.12 | 120.12 | 120.12 | 120.12 | 120.12 |
| 23.250 | 120.12 | 120.12 | 120.12 | 120.12 | 120.12 |
| 23.275 | 120.12 | 120.12 | 120.12 | 120.12 | 120.12 |
| 23.300 | 120.12 | 120.12 | 120.12 | 120.12 | 120.12 |
| 23.325 | 120.12 | 120.12 | 120.12 | 120.12 | 120.12 |
| 23.350 | 120.12 | 120.12 | 120.12 | 120.12 | 120.12 |
| 23.375 | 120.12 | 120.12 | 120.12 | 120.12 | 120.12 |
| 23.400 | 120.12 | 120.12 | 120.12 | 120.12 | 120.12 |
| 23.425 | 120.12 | 120.12 | 120.12 | 120.12 | 120.12 |
| 23.450 | 120.12 | 120.12 | 120.12 | 120.12 | 120.12 |
| 23.475 | 120.12 | 120.12 | 120.12 | 120.12 | 120.12 |
| 23.500 | 120.12 | 120.12 | 120.12 | 120.12 | 120.12 |
| 23.525 | 120.12 | 120.12 | 120.12 | 120.12 | 120.12 |
| 23.550 | 120.12 | 120.12 | 120.12 | 120.12 | 120.12 |
| 23.575 | 120.12 | 120.12 | 120.12 | 120.12 | 120.12 |
| 23.600 | 120.12 | 120.12 | 120.12 | 120.12 | 120.12 |
| 23.625 | 120.12 | 120.12 | 120.12 | 120.12 | 120.12 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 23.650 | 120.12 | 120.12 | 120.12 | 120.12 | 120.12 |
| 23.675 | 120.12 | 120.12 | 120.12 | 120.12 | 120.12 |
| 23.700 | 120.12 | 120.12 | 120.12 | 120.12 | 120.12 |
| 23.725 | 120.12 | 120.12 | 120.12 | 120.12 | 120.12 |
| 23.750 | 120.12 | 120.12 | 120.12 | 120.12 | 120.12 |
| 23.775 | 120.12 | 120.12 | 120.12 | 120.12 | 120.12 |
| 23.800 | 120.12 | 120.12 | 120.12 | 120.12 | 120.12 |
| 23.825 | 120.12 | 120.12 | 120.12 | 120.12 | 120.12 |
| 23.850 | 120.12 | 120.12 | 120.12 | 120.12 | 120.12 |
| 23.875 | 120.12 | 120.12 | 120.12 | 120.12 | 120.12 |
| 23.900 | 120.12 | 120.12 | 120.12 | 120.12 | 120.12 |
| 23.925 | 120.12 | 120.12 | 120.12 | 120.12 | 120.12 |
| 23.950 | 120.12 | 120.12 | 120.12 | 120.12 | 120.12 |
| 23.975 | 120.12 | 120.12 | 120.12 | 120.12 | 120.12 |
| 24.000 | 120.12 | (N/A) | (N/A) | (N/A) | (N/A) |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 0.000 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 0.025 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 0.050 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 0.075 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 0.100 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 0.125 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 0.150 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 0.175 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 0.200 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 0.225 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 0.250 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 0.275 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 0.300 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 0.325 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 0.350 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 0.375 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 0.400 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 0.425 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 0.450 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 0.475 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 0.500 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 0.525 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 0.550 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 0.575 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 0.600 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 0.625 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 0.650 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 0.675 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 0.700 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 0.725 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 0.750 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 0.775 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 0.800 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 0.825 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 0.850 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 0.875 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 0.900 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 0.925 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 0.950 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 0.975 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 1.000 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 1.025 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 1.050 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 1.075 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 1.100 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 1.125 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 1.150 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 1.175 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 1.200 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 1.225 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 1.250 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 1.275 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 1.300 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 1.325 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 1.350 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 1.375 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 1.400 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 1.425 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 1.450 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 1.475 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 1.500 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 1.525 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 1.550 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 1.575 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 1.600 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 1.625 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 1.650 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 1.675 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 1.700 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 1.725 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 1.750 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 1.775 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 1.800 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 1.825 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 1.850 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 1.875 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 1.900 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 1.925 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 1.950 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 1.975 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 2.000 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 2.025 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 2.050 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 2.075 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 2.100 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 2.125 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 2.150 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 2.175 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 2.200 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 2.225 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 2.250 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 2.275 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 2.300 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 2.325 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 2.350 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 2.375 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 2.400 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 2.425 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 2.450 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 2.475 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 2.500 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 2.525 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 2.550 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 2.575 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 2.600 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 2.625 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 2.650 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 2.675 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 2.700 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 2.725 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 2.750 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 2.775 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 2.800 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 2.825 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 2.850 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 2.875 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 2.900 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 2.925 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 2.950 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 2.975 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 3.000 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 3.025 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 3.050 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 3.075 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 3.100 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 3.125 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 3.150 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 3.175 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 3.200 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 3.225 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 3.250 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 3.275 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 3.300 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 3.325 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 3.350 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 3.375 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 3.400 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 3.425 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 3.450 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 3.475 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 3.500 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 3.525 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 3.550 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 3.575 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 3.600 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 3.625 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 3.650 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 3.675 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 3.700 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 3.725 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 3.750 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 3.775 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 3.800 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 3.825 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 3.850 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 3.875 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 3.900 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 3.925 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 3.950 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 3.975 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 4.000 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 4.025 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 4.050 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 4.075 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 4.100 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 4.125 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 4.150 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 4.175 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 4.200 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 4.225 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 4.250 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 4.275 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 4.300 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 4.325 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 4.350 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 4.375 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 4.400 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 4.425 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 4.450 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 4.475 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 4.500 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 4.525 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 4.550 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 4.575 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 4.600 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 4.625 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 4.650 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 4.675 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 4.700 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 4.725 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 4.750 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 4.775 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 4.800 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 4.825 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 4.850 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 4.875 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 4.900 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 4.925 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 4.950 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 4.975 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 5.000 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 5.025 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 5.050 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 5.075 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 5.100 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 5.125 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 5.150 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 5.175 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 5.200 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 5.225 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 5.250 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 5.275 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 5.300 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 5.325 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 5.350 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 5.375 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 5.400 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 5.425 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 5.450 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 5.475 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 5.500 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 5.525 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 5.550 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 5.575 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 5.600 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 5.625 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 5.650 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 5.675 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 5.700 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 5.725 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 5.750 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 5.775 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 5.800 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 5.825 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 5.850 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 5.875 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 5.900 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 5.925 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 5.950 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 5.975 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 6.000 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 6.025 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 6.050 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 6.075 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 6.100 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 6.125 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 6.150 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 6.175 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 6.200 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 6.225 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 6.250 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 6.275 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 6.300 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 6.325 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 6.350 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 6.375 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 6.400 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 6.425 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 6.450 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 6.475 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 6.500 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 6.525 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 6.550 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 6.575 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 6.600 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 6.625 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 6.650 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 6.675 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 6.700 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 6.725 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 6.750 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 6.775 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 6.800 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 6.825 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 6.850 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 6.875 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 6.900 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 6.925 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 6.950 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 6.975 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 7.000 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 7.025 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 7.050 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 7.075 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 7.100 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 7.125 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 7.150 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 7.175 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 7.200 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 7.225 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 7.250 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 7.275 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 7.300 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 7.325 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 7.350 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 7.375 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 7.400 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 7.425 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 7.450 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 7.475 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 7.500 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 7.525 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 7.550 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 7.575 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 7.600 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 7.625 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 7.650 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 7.675 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 7.700 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 7.725 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 7.750 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 7.775 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 7.800 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 7.825 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 7.850 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 7.875 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 7.900 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 7.925 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 7.950 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 7.975 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 8.000 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 8.025 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 8.050 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 8.075 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 8.100 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 8.125 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 8.150 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 8.175 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 8.200 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 8.225 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 8.250 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 8.275 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 8.300 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 8.325 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 8.350 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 8.375 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 8.400 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 8.425 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 8.450 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 8.475 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 8.500 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 8.525 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 8.550 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 8.575 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 8.600 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 8.625 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 8.650 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 8.675 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 8.700 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 8.725 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 8.750 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 8.775 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 8.800 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 8.825 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 8.850 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 8.875 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 8.900 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 8.925 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 8.950 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 8.975 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 9.000 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 9.025 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 9.050 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 9.075 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 9.100 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 9.125 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 9.150 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 9.175 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 9.200 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 9.225 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 9.250 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 9.275 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 9.300 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 9.325 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 9.350 | 132.00 | 132.01 | 132.01 | 132.01 | 132.01 |
| 9.375 | 132.01 | 132.01 | 132.01 | 132.01 | 132.01 |
| 9.400 | 132.01 | 132.01 | 132.01 | 132.01 | 132.02 |
| 9.425 | 132.02 | 132.02 | 132.02 | 132.02 | 132.02 |
| 9.450 | 132.02 | 132.02 | 132.02 | 132.02 | 132.03 |
| 9.475 | 132.03 | 132.03 | 132.03 | 132.03 | 132.03 |
| 9.500 | 132.04 | 132.04 | 132.04 | 132.04 | 132.04 |
| 9.525 | 132.04 | 132.04 | 132.04 | 132.04 | 132.05 |
| 9.550 | 132.05 | 132.05 | 132.05 | 132.05 | 132.05 |
| 9.575 | 132.05 | 132.05 | 132.05 | 132.05 | 132.05 |
| 9.600 | 132.06 | 132.06 | 132.06 | 132.06 | 132.06 |
| 9.625 | 132.06 | 132.06 | 132.06 | 132.06 | 132.07 |
| 9.650 | 132.07 | 132.07 | 132.07 | 132.07 | 132.07 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 9.675 | 132.07 | 132.07 | 132.07 | 132.08 | 132.08 |
| 9.700 | 132.08 | 132.08 | 132.08 | 132.08 | 132.08 |
| 9.725 | 132.08 | 132.08 | 132.08 | 132.08 | 132.09 |
| 9.750 | 132.09 | 132.09 | 132.09 | 132.09 | 132.09 |
| 9.775 | 132.09 | 132.09 | 132.09 | 132.09 | 132.09 |
| 9.800 | 132.09 | 132.09 | 132.09 | 132.09 | 132.10 |
| 9.825 | 132.10 | 132.10 | 132.10 | 132.10 | 132.10 |
| 9.850 | 132.10 | 132.10 | 132.10 | 132.10 | 132.10 |
| 9.875 | 132.10 | 132.10 | 132.10 | 132.11 | 132.11 |
| 9.900 | 132.11 | 132.11 | 132.11 | 132.11 | 132.11 |
| 9.925 | 132.11 | 132.11 | 132.11 | 132.11 | 132.11 |
| 9.950 | 132.11 | 132.11 | 132.12 | 132.12 | 132.12 |
| 9.975 | 132.12 | 132.12 | 132.12 | 132.12 | 132.12 |
| 10.000 | 132.12 | 132.12 | 132.12 | 132.12 | 132.12 |
| 10.025 | 132.12 | 132.12 | 132.12 | 132.13 | 132.13 |
| 10.050 | 132.13 | 132.13 | 132.13 | 132.13 | 132.13 |
| 10.075 | 132.13 | 132.13 | 132.13 | 132.13 | 132.13 |
| 10.100 | 132.13 | 132.13 | 132.13 | 132.13 | 132.13 |
| 10.125 | 132.13 | 132.14 | 132.14 | 132.14 | 132.14 |
| 10.150 | 132.14 | 132.14 | 132.14 | 132.14 | 132.14 |
| 10.175 | 132.14 | 132.14 | 132.14 | 132.14 | 132.14 |
| 10.200 | 132.14 | 132.14 | 132.14 | 132.14 | 132.15 |
| 10.225 | 132.15 | 132.15 | 132.15 | 132.15 | 132.15 |
| 10.250 | 132.15 | 132.15 | 132.15 | 132.15 | 132.15 |
| 10.275 | 132.15 | 132.15 | 132.15 | 132.15 | 132.15 |
| 10.300 | 132.16 | 132.16 | 132.16 | 132.16 | 132.16 |
| 10.325 | 132.16 | 132.16 | 132.16 | 132.16 | 132.16 |
| 10.350 | 132.16 | 132.16 | 132.16 | 132.16 | 132.16 |
| 10.375 | 132.16 | 132.16 | 132.17 | 132.17 | 132.17 |
| 10.400 | 132.17 | 132.17 | 132.17 | 132.17 | 132.17 |
| 10.425 | 132.17 | 132.17 | 132.17 | 132.17 | 132.17 |
| 10.450 | 132.17 | 132.17 | 132.17 | 132.17 | 132.17 |
| 10.475 | 132.18 | 132.18 | 132.18 | 132.18 | 132.18 |
| 10.500 | 132.18 | 132.18 | 132.18 | 132.18 | 132.18 |
| 10.525 | 132.18 | 132.18 | 132.18 | 132.18 | 132.18 |
| 10.550 | 132.18 | 132.18 | 132.18 | 132.19 | 132.19 |
| 10.575 | 132.19 | 132.19 | 132.19 | 132.19 | 132.19 |
| 10.600 | 132.19 | 132.19 | 132.19 | 132.19 | 132.19 |
| 10.625 | 132.19 | 132.19 | 132.19 | 132.19 | 132.20 |
| 10.650 | 132.20 | 132.20 | 132.20 | 132.20 | 132.20 |
| 10.675 | 132.20 | 132.20 | 132.20 | 132.20 | 132.20 |
| 10.700 | 132.20 | 132.20 | 132.20 | 132.20 | 132.20 |
| 10.725 | 132.21 | 132.21 | 132.21 | 132.21 | 132.21 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 10.750 | 132.21 | 132.21 | 132.21 | 132.21 | 132.21 |
| 10.775 | 132.21 | 132.21 | 132.21 | 132.21 | 132.21 |
| 10.800 | 132.21 | 132.22 | 132.22 | 132.22 | 132.22 |
| 10.825 | 132.22 | 132.22 | 132.22 | 132.22 | 132.22 |
| 10.850 | 132.22 | 132.22 | 132.22 | 132.22 | 132.22 |
| 10.875 | 132.22 | 132.23 | 132.23 | 132.23 | 132.23 |
| 10.900 | 132.23 | 132.23 | 132.23 | 132.23 | 132.23 |
| 10.925 | 132.23 | 132.23 | 132.23 | 132.23 | 132.23 |
| 10.950 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 10.975 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 11.000 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 11.025 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 11.050 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 11.075 | 132.25 | 132.25 | 132.25 | 132.25 | 132.26 |
| 11.100 | 132.26 | 132.26 | 132.26 | 132.26 | 132.26 |
| 11.125 | 132.26 | 132.26 | 132.26 | 132.26 | 132.26 |
| 11.150 | 132.26 | 132.26 | 132.27 | 132.27 | 132.27 |
| 11.175 | 132.27 | 132.27 | 132.27 | 132.27 | 132.27 |
| 11.200 | 132.27 | 132.27 | 132.27 | 132.28 | 132.28 |
| 11.225 | 132.28 | 132.28 | 132.28 | 132.28 | 132.28 |
| 11.250 | 132.28 | 132.28 | 132.28 | 132.28 | 132.29 |
| 11.275 | 132.29 | 132.29 | 132.29 | 132.29 | 132.29 |
| 11.300 | 132.29 | 132.29 | 132.29 | 132.29 | 132.30 |
| 11.325 | 132.30 | 132.30 | 132.30 | 132.30 | 132.30 |
| 11.350 | 132.30 | 132.30 | 132.30 | 132.30 | 132.31 |
| 11.375 | 132.31 | 132.31 | 132.31 | 132.31 | 132.31 |
| 11.400 | 132.31 | 132.31 | 132.31 | 132.32 | 132.32 |
| 11.425 | 132.32 | 132.32 | 132.32 | 132.32 | 132.32 |
| 11.450 | 132.32 | 132.32 | 132.33 | 132.33 | 132.33 |
| 11.475 | 132.33 | 132.33 | 132.33 | 132.33 | 132.33 |
| 11.500 | 132.33 | 132.34 | 132.34 | 132.34 | 132.34 |
| 11.525 | 132.34 | 132.34 | 132.34 | 132.34 | 132.35 |
| 11.550 | 132.35 | 132.35 | 132.35 | 132.35 | 132.36 |
| 11.575 | 132.36 | 132.36 | 132.36 | 132.37 | 132.37 |
| 11.600 | 132.37 | 132.38 | 132.38 | 132.38 | 132.39 |
| 11.625 | 132.39 | 132.39 | 132.40 | 132.40 | 132.41 |
| 11.650 | 132.41 | 132.42 | 132.42 | 132.43 | 132.44 |
| 11.675 | 132.44 | 132.45 | 132.45 | 132.46 | 132.47 |
| 11.700 | 132.47 | 132.48 | 132.49 | 132.50 | 132.50 |
| 11.725 | 132.51 | 132.52 | 132.53 | 132.53 | 132.54 |
| 11.750 | 132.55 | 132.56 | 132.57 | 132.58 | 132.59 |
| 11.775 | 132.59 | 132.60 | 132.61 | 132.62 | 132.63 |
| 11.800 | 132.64 | 132.65 | 132.66 | 132.67 | 132.68 |

Subsection: Time vs. Elevation
Label: CO-89

Return Event: 10 years
Storm Event: 10 yr

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 11.825 | 132.69 | 132.70 | 132.71 | 132.72 | 132.73 |
| 11.850 | 132.74 | 132.75 | 132.76 | 132.77 | 132.78 |
| 11.875 | 132.80 | 132.81 | 132.82 | 132.83 | 132.84 |
| 11.900 | 132.86 | 132.87 | 132.88 | 132.89 | 132.90 |
| 11.925 | 132.92 | 132.93 | 132.94 | 132.95 | 132.96 |
| 11.950 | 132.97 | 132.99 | 133.00 | 133.01 | 133.01 |
| 11.975 | 133.02 | 133.03 | 133.04 | 133.05 | 133.06 |
| 12.000 | 133.06 | 133.07 | 133.07 | 133.08 | 133.08 |
| 12.025 | 133.09 | 133.09 | 133.10 | 133.10 | 133.10 |
| 12.050 | 133.10 | 133.10 | 133.10 | 133.10 | 133.10 |
| 12.075 | 133.10 | 133.10 | 133.09 | 133.09 | 133.09 |
| 12.100 | 133.08 | 133.08 | 133.07 | 133.07 | 133.06 |
| 12.125 | 133.05 | 133.05 | 133.04 | 133.03 | 133.02 |
| 12.150 | 133.01 | 133.00 | 133.00 | 132.99 | 132.98 |
| 12.175 | 132.97 | 132.96 | 132.95 | 132.94 | 132.93 |
| 12.200 | 132.92 | 132.91 | 132.90 | 132.89 | 132.88 |
| 12.225 | 132.87 | 132.86 | 132.86 | 132.85 | 132.84 |
| 12.250 | 132.83 | 132.82 | 132.81 | 132.80 | 132.80 |
| 12.275 | 132.79 | 132.78 | 132.77 | 132.77 | 132.76 |
| 12.300 | 132.75 | 132.75 | 132.74 | 132.74 | 132.73 |
| 12.325 | 132.72 | 132.72 | 132.71 | 132.71 | 132.70 |
| 12.350 | 132.70 | 132.69 | 132.69 | 132.68 | 132.68 |
| 12.375 | 132.68 | 132.67 | 132.67 | 132.66 | 132.66 |
| 12.400 | 132.65 | 132.65 | 132.65 | 132.64 | 132.64 |
| 12.425 | 132.64 | 132.63 | 132.63 | 132.63 | 132.62 |
| 12.450 | 132.62 | 132.62 | 132.61 | 132.61 | 132.61 |
| 12.475 | 132.61 | 132.60 | 132.60 | 132.60 | 132.59 |
| 12.500 | 132.59 | 132.59 | 132.59 | 132.58 | 132.58 |
| 12.525 | 132.58 | 132.58 | 132.57 | 132.57 | 132.57 |
| 12.550 | 132.57 | 132.56 | 132.56 | 132.56 | 132.56 |
| 12.575 | 132.55 | 132.55 | 132.55 | 132.55 | 132.54 |
| 12.600 | 132.54 | 132.54 | 132.54 | 132.54 | 132.53 |
| 12.625 | 132.53 | 132.53 | 132.53 | 132.53 | 132.52 |
| 12.650 | 132.52 | 132.52 | 132.52 | 132.52 | 132.52 |
| 12.675 | 132.51 | 132.51 | 132.51 | 132.51 | 132.51 |
| 12.700 | 132.51 | 132.50 | 132.50 | 132.50 | 132.50 |
| 12.725 | 132.50 | 132.50 | 132.50 | 132.49 | 132.49 |
| 12.750 | 132.49 | 132.49 | 132.49 | 132.49 | 132.49 |
| 12.775 | 132.49 | 132.49 | 132.49 | 132.48 | 132.48 |
| 12.800 | 132.48 | 132.48 | 132.48 | 132.48 | 132.48 |
| 12.825 | 132.48 | 132.48 | 132.48 | 132.48 | 132.47 |
| 12.850 | 132.47 | 132.47 | 132.47 | 132.47 | 132.47 |
| 12.875 | 132.47 | 132.47 | 132.47 | 132.47 | 132.47 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 12.900 | 132.47 | 132.47 | 132.47 | 132.46 | 132.46 |
| 12.925 | 132.46 | 132.46 | 132.46 | 132.46 | 132.46 |
| 12.950 | 132.46 | 132.46 | 132.46 | 132.46 | 132.46 |
| 12.975 | 132.46 | 132.46 | 132.46 | 132.46 | 132.45 |
| 13.000 | 132.45 | 132.45 | 132.45 | 132.45 | 132.45 |
| 13.025 | 132.45 | 132.45 | 132.45 | 132.45 | 132.45 |
| 13.050 | 132.45 | 132.45 | 132.45 | 132.45 | 132.45 |
| 13.075 | 132.45 | 132.44 | 132.44 | 132.44 | 132.44 |
| 13.100 | 132.44 | 132.44 | 132.44 | 132.44 | 132.44 |
| 13.125 | 132.44 | 132.44 | 132.44 | 132.44 | 132.44 |
| 13.150 | 132.44 | 132.44 | 132.44 | 132.44 | 132.43 |
| 13.175 | 132.43 | 132.43 | 132.43 | 132.43 | 132.43 |
| 13.200 | 132.43 | 132.43 | 132.43 | 132.43 | 132.43 |
| 13.225 | 132.43 | 132.43 | 132.43 | 132.43 | 132.43 |
| 13.250 | 132.43 | 132.43 | 132.43 | 132.43 | 132.42 |
| 13.275 | 132.42 | 132.42 | 132.42 | 132.42 | 132.42 |
| 13.300 | 132.42 | 132.42 | 132.42 | 132.42 | 132.42 |
| 13.325 | 132.42 | 132.42 | 132.42 | 132.42 | 132.42 |
| 13.350 | 132.42 | 132.42 | 132.42 | 132.42 | 132.42 |
| 13.375 | 132.42 | 132.42 | 132.42 | 132.41 | 132.41 |
| 13.400 | 132.41 | 132.41 | 132.41 | 132.41 | 132.41 |
| 13.425 | 132.41 | 132.41 | 132.41 | 132.41 | 132.41 |
| 13.450 | 132.41 | 132.41 | 132.41 | 132.41 | 132.41 |
| 13.475 | 132.41 | 132.41 | 132.41 | 132.41 | 132.41 |
| 13.500 | 132.41 | 132.41 | 132.41 | 132.41 | 132.41 |
| 13.525 | 132.40 | 132.40 | 132.40 | 132.40 | 132.40 |
| 13.550 | 132.40 | 132.40 | 132.40 | 132.40 | 132.40 |
| 13.575 | 132.40 | 132.40 | 132.40 | 132.40 | 132.40 |
| 13.600 | 132.40 | 132.40 | 132.40 | 132.40 | 132.40 |
| 13.625 | 132.40 | 132.40 | 132.40 | 132.40 | 132.40 |
| 13.650 | 132.40 | 132.40 | 132.39 | 132.39 | 132.39 |
| 13.675 | 132.39 | 132.39 | 132.39 | 132.39 | 132.39 |
| 13.700 | 132.39 | 132.39 | 132.39 | 132.39 | 132.39 |
| 13.725 | 132.39 | 132.39 | 132.39 | 132.39 | 132.39 |
| 13.750 | 132.39 | 132.39 | 132.39 | 132.39 | 132.39 |
| 13.775 | 132.39 | 132.39 | 132.39 | 132.39 | 132.39 |
| 13.800 | 132.38 | 132.38 | 132.38 | 132.38 | 132.38 |
| 13.825 | 132.38 | 132.38 | 132.38 | 132.38 | 132.38 |
| 13.850 | 132.38 | 132.38 | 132.38 | 132.38 | 132.38 |
| 13.875 | 132.38 | 132.38 | 132.38 | 132.38 | 132.38 |
| 13.900 | 132.38 | 132.38 | 132.38 | 132.38 | 132.38 |
| 13.925 | 132.38 | 132.38 | 132.38 | 132.38 | 132.38 |
| 13.950 | 132.38 | 132.37 | 132.37 | 132.37 | 132.37 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 13.975 | 132.37 | 132.37 | 132.37 | 132.37 | 132.37 |
| 14.000 | 132.37 | 132.37 | 132.37 | 132.37 | 132.37 |
| 14.025 | 132.37 | 132.37 | 132.37 | 132.37 | 132.37 |
| 14.050 | 132.37 | 132.37 | 132.37 | 132.37 | 132.37 |
| 14.075 | 132.37 | 132.37 | 132.37 | 132.37 | 132.37 |
| 14.100 | 132.37 | 132.37 | 132.37 | 132.37 | 132.36 |
| 14.125 | 132.36 | 132.36 | 132.36 | 132.36 | 132.36 |
| 14.150 | 132.36 | 132.36 | 132.36 | 132.36 | 132.36 |
| 14.175 | 132.36 | 132.36 | 132.36 | 132.36 | 132.36 |
| 14.200 | 132.36 | 132.36 | 132.36 | 132.36 | 132.36 |
| 14.225 | 132.36 | 132.36 | 132.36 | 132.36 | 132.36 |
| 14.250 | 132.36 | 132.36 | 132.36 | 132.36 | 132.36 |
| 14.275 | 132.36 | 132.36 | 132.36 | 132.36 | 132.36 |
| 14.300 | 132.36 | 132.36 | 132.36 | 132.36 | 132.36 |
| 14.325 | 132.36 | 132.36 | 132.36 | 132.36 | 132.36 |
| 14.350 | 132.36 | 132.36 | 132.35 | 132.35 | 132.35 |
| 14.375 | 132.35 | 132.35 | 132.35 | 132.35 | 132.35 |
| 14.400 | 132.35 | 132.35 | 132.35 | 132.35 | 132.35 |
| 14.425 | 132.35 | 132.35 | 132.35 | 132.35 | 132.35 |
| 14.450 | 132.35 | 132.35 | 132.35 | 132.35 | 132.35 |
| 14.475 | 132.35 | 132.35 | 132.35 | 132.35 | 132.35 |
| 14.500 | 132.35 | 132.35 | 132.35 | 132.35 | 132.35 |
| 14.525 | 132.35 | 132.35 | 132.35 | 132.35 | 132.35 |
| 14.550 | 132.35 | 132.35 | 132.35 | 132.35 | 132.35 |
| 14.575 | 132.35 | 132.35 | 132.35 | 132.35 | 132.35 |
| 14.600 | 132.35 | 132.35 | 132.35 | 132.35 | 132.35 |
| 14.625 | 132.35 | 132.35 | 132.35 | 132.35 | 132.35 |
| 14.650 | 132.35 | 132.35 | 132.35 | 132.35 | 132.35 |
| 14.675 | 132.35 | 132.35 | 132.35 | 132.35 | 132.35 |
| 14.700 | 132.35 | 132.35 | 132.35 | 132.35 | 132.35 |
| 14.725 | 132.35 | 132.35 | 132.34 | 132.34 | 132.34 |
| 14.750 | 132.34 | 132.34 | 132.34 | 132.34 | 132.34 |
| 14.775 | 132.34 | 132.34 | 132.34 | 132.34 | 132.34 |
| 14.800 | 132.34 | 132.34 | 132.34 | 132.34 | 132.34 |
| 14.825 | 132.34 | 132.34 | 132.34 | 132.34 | 132.34 |
| 14.850 | 132.34 | 132.34 | 132.34 | 132.34 | 132.34 |
| 14.875 | 132.34 | 132.34 | 132.34 | 132.34 | 132.34 |
| 14.900 | 132.34 | 132.34 | 132.34 | 132.34 | 132.34 |
| 14.925 | 132.34 | 132.34 | 132.34 | 132.34 | 132.34 |
| 14.950 | 132.34 | 132.34 | 132.34 | 132.34 | 132.34 |
| 14.975 | 132.34 | 132.34 | 132.34 | 132.34 | 132.34 |
| 15.000 | 132.34 | 132.34 | 132.34 | 132.34 | 132.34 |
| 15.025 | 132.34 | 132.34 | 132.34 | 132.34 | 132.34 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 15.050 | 132.34 | 132.34 | 132.34 | 132.34 | 132.34 |
| 15.075 | 132.34 | 132.34 | 132.34 | 132.34 | 132.34 |
| 15.100 | 132.34 | 132.34 | 132.34 | 132.34 | 132.33 |
| 15.125 | 132.33 | 132.33 | 132.33 | 132.33 | 132.33 |
| 15.150 | 132.33 | 132.33 | 132.33 | 132.33 | 132.33 |
| 15.175 | 132.33 | 132.33 | 132.33 | 132.33 | 132.33 |
| 15.200 | 132.33 | 132.33 | 132.33 | 132.33 | 132.33 |
| 15.225 | 132.33 | 132.33 | 132.33 | 132.33 | 132.33 |
| 15.250 | 132.33 | 132.33 | 132.33 | 132.33 | 132.33 |
| 15.275 | 132.33 | 132.33 | 132.33 | 132.33 | 132.33 |
| 15.300 | 132.33 | 132.33 | 132.33 | 132.33 | 132.33 |
| 15.325 | 132.33 | 132.33 | 132.33 | 132.33 | 132.33 |
| 15.350 | 132.33 | 132.33 | 132.33 | 132.33 | 132.33 |
| 15.375 | 132.33 | 132.33 | 132.33 | 132.33 | 132.33 |
| 15.400 | 132.33 | 132.33 | 132.33 | 132.33 | 132.33 |
| 15.425 | 132.33 | 132.33 | 132.33 | 132.33 | 132.33 |
| 15.450 | 132.33 | 132.33 | 132.33 | 132.33 | 132.33 |
| 15.475 | 132.33 | 132.33 | 132.33 | 132.33 | 132.33 |
| 15.500 | 132.32 | 132.32 | 132.32 | 132.32 | 132.32 |
| 15.525 | 132.32 | 132.32 | 132.32 | 132.32 | 132.32 |
| 15.550 | 132.32 | 132.32 | 132.32 | 132.32 | 132.32 |
| 15.575 | 132.32 | 132.32 | 132.32 | 132.32 | 132.32 |
| 15.600 | 132.32 | 132.32 | 132.32 | 132.32 | 132.32 |
| 15.625 | 132.32 | 132.32 | 132.32 | 132.32 | 132.32 |
| 15.650 | 132.32 | 132.32 | 132.32 | 132.32 | 132.32 |
| 15.675 | 132.32 | 132.32 | 132.32 | 132.32 | 132.32 |
| 15.700 | 132.32 | 132.32 | 132.32 | 132.32 | 132.32 |
| 15.725 | 132.32 | 132.32 | 132.32 | 132.32 | 132.32 |
| 15.750 | 132.32 | 132.32 | 132.32 | 132.32 | 132.32 |
| 15.775 | 132.32 | 132.32 | 132.32 | 132.32 | 132.32 |
| 15.800 | 132.32 | 132.32 | 132.32 | 132.32 | 132.32 |
| 15.825 | 132.32 | 132.32 | 132.32 | 132.31 | 132.31 |
| 15.850 | 132.31 | 132.31 | 132.31 | 132.31 | 132.31 |
| 15.875 | 132.31 | 132.31 | 132.31 | 132.31 | 132.31 |
| 15.900 | 132.31 | 132.31 | 132.31 | 132.31 | 132.31 |
| 15.925 | 132.31 | 132.31 | 132.31 | 132.31 | 132.31 |
| 15.950 | 132.31 | 132.31 | 132.31 | 132.31 | 132.31 |
| 15.975 | 132.31 | 132.31 | 132.31 | 132.31 | 132.31 |
| 16.000 | 132.31 | 132.31 | 132.31 | 132.31 | 132.31 |
| 16.025 | 132.31 | 132.31 | 132.31 | 132.31 | 132.31 |
| 16.050 | 132.31 | 132.31 | 132.31 | 132.31 | 132.31 |
| 16.075 | 132.31 | 132.31 | 132.31 | 132.31 | 132.31 |
| 16.100 | 132.31 | 132.31 | 132.31 | 132.31 | 132.31 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 16.125 | 132.31 | 132.31 | 132.31 | 132.31 | 132.30 |
| 16.150 | 132.30 | 132.30 | 132.30 | 132.30 | 132.30 |
| 16.175 | 132.30 | 132.30 | 132.30 | 132.30 | 132.30 |
| 16.200 | 132.30 | 132.30 | 132.30 | 132.30 | 132.30 |
| 16.225 | 132.30 | 132.30 | 132.30 | 132.30 | 132.30 |
| 16.250 | 132.30 | 132.30 | 132.30 | 132.30 | 132.30 |
| 16.275 | 132.30 | 132.30 | 132.30 | 132.30 | 132.30 |
| 16.300 | 132.30 | 132.30 | 132.30 | 132.30 | 132.30 |
| 16.325 | 132.30 | 132.30 | 132.30 | 132.30 | 132.30 |
| 16.350 | 132.30 | 132.30 | 132.30 | 132.30 | 132.30 |
| 16.375 | 132.30 | 132.30 | 132.30 | 132.30 | 132.30 |
| 16.400 | 132.30 | 132.30 | 132.30 | 132.30 | 132.30 |
| 16.425 | 132.30 | 132.30 | 132.30 | 132.30 | 132.30 |
| 16.450 | 132.30 | 132.30 | 132.30 | 132.30 | 132.30 |
| 16.475 | 132.30 | 132.30 | 132.30 | 132.30 | 132.30 |
| 16.500 | 132.30 | 132.30 | 132.30 | 132.30 | 132.30 |
| 16.525 | 132.30 | 132.30 | 132.30 | 132.30 | 132.30 |
| 16.550 | 132.30 | 132.30 | 132.30 | 132.30 | 132.30 |
| 16.575 | 132.30 | 132.30 | 132.30 | 132.30 | 132.30 |
| 16.600 | 132.30 | 132.30 | 132.30 | 132.30 | 132.30 |
| 16.625 | 132.30 | 132.30 | 132.30 | 132.30 | 132.30 |
| 16.650 | 132.30 | 132.30 | 132.30 | 132.30 | 132.30 |
| 16.675 | 132.30 | 132.30 | 132.30 | 132.30 | 132.30 |
| 16.700 | 132.30 | 132.30 | 132.30 | 132.30 | 132.30 |
| 16.725 | 132.30 | 132.30 | 132.30 | 132.30 | 132.30 |
| 16.750 | 132.30 | 132.30 | 132.30 | 132.30 | 132.30 |
| 16.775 | 132.30 | 132.30 | 132.30 | 132.30 | 132.30 |
| 16.800 | 132.30 | 132.30 | 132.30 | 132.30 | 132.30 |
| 16.825 | 132.30 | 132.30 | 132.29 | 132.29 | 132.29 |
| 16.850 | 132.29 | 132.29 | 132.29 | 132.29 | 132.29 |
| 16.875 | 132.29 | 132.29 | 132.29 | 132.29 | 132.29 |
| 16.900 | 132.29 | 132.29 | 132.29 | 132.29 | 132.29 |
| 16.925 | 132.29 | 132.29 | 132.29 | 132.29 | 132.29 |
| 16.950 | 132.29 | 132.29 | 132.29 | 132.29 | 132.29 |
| 16.975 | 132.29 | 132.29 | 132.29 | 132.29 | 132.29 |
| 17.000 | 132.29 | 132.29 | 132.29 | 132.29 | 132.29 |
| 17.025 | 132.29 | 132.29 | 132.29 | 132.29 | 132.29 |
| 17.050 | 132.29 | 132.29 | 132.29 | 132.29 | 132.29 |
| 17.075 | 132.29 | 132.29 | 132.29 | 132.29 | 132.29 |
| 17.100 | 132.29 | 132.29 | 132.29 | 132.29 | 132.29 |
| 17.125 | 132.29 | 132.29 | 132.29 | 132.29 | 132.29 |
| 17.150 | 132.29 | 132.29 | 132.29 | 132.29 | 132.29 |
| 17.175 | 132.29 | 132.29 | 132.29 | 132.29 | 132.29 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 17.200 | 132.29 | 132.29 | 132.29 | 132.29 | 132.29 |
| 17.225 | 132.29 | 132.29 | 132.29 | 132.29 | 132.29 |
| 17.250 | 132.29 | 132.29 | 132.29 | 132.29 | 132.29 |
| 17.275 | 132.29 | 132.29 | 132.29 | 132.29 | 132.29 |
| 17.300 | 132.29 | 132.29 | 132.29 | 132.29 | 132.29 |
| 17.325 | 132.29 | 132.29 | 132.29 | 132.29 | 132.29 |
| 17.350 | 132.29 | 132.29 | 132.29 | 132.29 | 132.29 |
| 17.375 | 132.29 | 132.29 | 132.29 | 132.29 | 132.29 |
| 17.400 | 132.29 | 132.29 | 132.29 | 132.29 | 132.29 |
| 17.425 | 132.29 | 132.29 | 132.29 | 132.29 | 132.29 |
| 17.450 | 132.29 | 132.29 | 132.29 | 132.29 | 132.29 |
| 17.475 | 132.29 | 132.29 | 132.29 | 132.29 | 132.29 |
| 17.500 | 132.29 | 132.29 | 132.29 | 132.29 | 132.29 |
| 17.525 | 132.29 | 132.29 | 132.29 | 132.29 | 132.29 |
| 17.550 | 132.29 | 132.29 | 132.29 | 132.29 | 132.29 |
| 17.575 | 132.29 | 132.29 | 132.29 | 132.29 | 132.29 |
| 17.600 | 132.29 | 132.29 | 132.29 | 132.29 | 132.29 |
| 17.625 | 132.29 | 132.29 | 132.29 | 132.29 | 132.29 |
| 17.650 | 132.29 | 132.29 | 132.29 | 132.29 | 132.29 |
| 17.675 | 132.29 | 132.29 | 132.29 | 132.28 | 132.28 |
| 17.700 | 132.28 | 132.28 | 132.28 | 132.28 | 132.28 |
| 17.725 | 132.28 | 132.28 | 132.28 | 132.28 | 132.28 |
| 17.750 | 132.28 | 132.28 | 132.28 | 132.28 | 132.28 |
| 17.775 | 132.28 | 132.28 | 132.28 | 132.28 | 132.28 |
| 17.800 | 132.28 | 132.28 | 132.28 | 132.28 | 132.28 |
| 17.825 | 132.28 | 132.28 | 132.28 | 132.28 | 132.28 |
| 17.850 | 132.28 | 132.28 | 132.28 | 132.28 | 132.28 |
| 17.875 | 132.28 | 132.28 | 132.28 | 132.28 | 132.28 |
| 17.900 | 132.28 | 132.28 | 132.28 | 132.28 | 132.28 |
| 17.925 | 132.28 | 132.28 | 132.28 | 132.28 | 132.28 |
| 17.950 | 132.28 | 132.28 | 132.28 | 132.28 | 132.28 |
| 17.975 | 132.28 | 132.28 | 132.28 | 132.28 | 132.28 |
| 18.000 | 132.28 | 132.28 | 132.28 | 132.28 | 132.28 |
| 18.025 | 132.28 | 132.28 | 132.28 | 132.28 | 132.28 |
| 18.050 | 132.28 | 132.28 | 132.28 | 132.28 | 132.28 |
| 18.075 | 132.28 | 132.28 | 132.28 | 132.28 | 132.28 |
| 18.100 | 132.28 | 132.28 | 132.28 | 132.28 | 132.28 |
| 18.125 | 132.28 | 132.28 | 132.28 | 132.28 | 132.28 |
| 18.150 | 132.28 | 132.28 | 132.28 | 132.28 | 132.28 |
| 18.175 | 132.28 | 132.28 | 132.28 | 132.28 | 132.28 |
| 18.200 | 132.28 | 132.28 | 132.28 | 132.28 | 132.28 |
| 18.225 | 132.28 | 132.28 | 132.28 | 132.28 | 132.28 |
| 18.250 | 132.28 | 132.28 | 132.28 | 132.28 | 132.28 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 18.275 | 132.28 | 132.28 | 132.28 | 132.28 | 132.28 |
| 18.300 | 132.28 | 132.28 | 132.28 | 132.28 | 132.28 |
| 18.325 | 132.28 | 132.28 | 132.28 | 132.28 | 132.28 |
| 18.350 | 132.28 | 132.28 | 132.28 | 132.28 | 132.28 |
| 18.375 | 132.28 | 132.28 | 132.28 | 132.28 | 132.28 |
| 18.400 | 132.28 | 132.28 | 132.28 | 132.28 | 132.28 |
| 18.425 | 132.28 | 132.28 | 132.28 | 132.27 | 132.27 |
| 18.450 | 132.27 | 132.27 | 132.27 | 132.27 | 132.27 |
| 18.475 | 132.27 | 132.27 | 132.27 | 132.27 | 132.27 |
| 18.500 | 132.27 | 132.27 | 132.27 | 132.27 | 132.27 |
| 18.525 | 132.27 | 132.27 | 132.27 | 132.27 | 132.27 |
| 18.550 | 132.27 | 132.27 | 132.27 | 132.27 | 132.27 |
| 18.575 | 132.27 | 132.27 | 132.27 | 132.27 | 132.27 |
| 18.600 | 132.27 | 132.27 | 132.27 | 132.27 | 132.27 |
| 18.625 | 132.27 | 132.27 | 132.27 | 132.27 | 132.27 |
| 18.650 | 132.27 | 132.27 | 132.27 | 132.27 | 132.27 |
| 18.675 | 132.27 | 132.27 | 132.27 | 132.27 | 132.27 |
| 18.700 | 132.27 | 132.27 | 132.27 | 132.27 | 132.27 |
| 18.725 | 132.27 | 132.27 | 132.27 | 132.27 | 132.27 |
| 18.750 | 132.27 | 132.27 | 132.27 | 132.27 | 132.27 |
| 18.775 | 132.27 | 132.27 | 132.27 | 132.27 | 132.27 |
| 18.800 | 132.27 | 132.27 | 132.27 | 132.27 | 132.27 |
| 18.825 | 132.27 | 132.27 | 132.27 | 132.27 | 132.27 |
| 18.850 | 132.27 | 132.27 | 132.27 | 132.27 | 132.27 |
| 18.875 | 132.27 | 132.27 | 132.27 | 132.27 | 132.27 |
| 18.900 | 132.27 | 132.27 | 132.27 | 132.27 | 132.27 |
| 18.925 | 132.27 | 132.27 | 132.27 | 132.27 | 132.27 |
| 18.950 | 132.27 | 132.27 | 132.27 | 132.27 | 132.27 |
| 18.975 | 132.27 | 132.27 | 132.27 | 132.27 | 132.27 |
| 19.000 | 132.27 | 132.27 | 132.27 | 132.27 | 132.27 |
| 19.025 | 132.27 | 132.27 | 132.27 | 132.27 | 132.27 |
| 19.050 | 132.27 | 132.27 | 132.27 | 132.27 | 132.27 |
| 19.075 | 132.27 | 132.26 | 132.26 | 132.26 | 132.26 |
| 19.100 | 132.26 | 132.26 | 132.26 | 132.26 | 132.26 |
| 19.125 | 132.26 | 132.26 | 132.26 | 132.26 | 132.26 |
| 19.150 | 132.26 | 132.26 | 132.26 | 132.26 | 132.26 |
| 19.175 | 132.26 | 132.26 | 132.26 | 132.26 | 132.26 |
| 19.200 | 132.26 | 132.26 | 132.26 | 132.26 | 132.26 |
| 19.225 | 132.26 | 132.26 | 132.26 | 132.26 | 132.26 |
| 19.250 | 132.26 | 132.26 | 132.26 | 132.26 | 132.26 |
| 19.275 | 132.26 | 132.26 | 132.26 | 132.26 | 132.26 |
| 19.300 | 132.26 | 132.26 | 132.26 | 132.26 | 132.26 |
| 19.325 | 132.26 | 132.26 | 132.26 | 132.26 | 132.26 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 19.350 | 132.26 | 132.26 | 132.26 | 132.26 | 132.26 |
| 19.375 | 132.26 | 132.26 | 132.26 | 132.26 | 132.26 |
| 19.400 | 132.26 | 132.26 | 132.26 | 132.26 | 132.26 |
| 19.425 | 132.26 | 132.26 | 132.26 | 132.26 | 132.26 |
| 19.450 | 132.26 | 132.26 | 132.26 | 132.26 | 132.26 |
| 19.475 | 132.26 | 132.26 | 132.26 | 132.26 | 132.26 |
| 19.500 | 132.26 | 132.26 | 132.26 | 132.26 | 132.26 |
| 19.525 | 132.26 | 132.26 | 132.26 | 132.26 | 132.26 |
| 19.550 | 132.26 | 132.26 | 132.26 | 132.26 | 132.26 |
| 19.575 | 132.26 | 132.26 | 132.26 | 132.26 | 132.26 |
| 19.600 | 132.26 | 132.26 | 132.26 | 132.26 | 132.26 |
| 19.625 | 132.26 | 132.26 | 132.26 | 132.26 | 132.26 |
| 19.650 | 132.26 | 132.26 | 132.26 | 132.26 | 132.26 |
| 19.675 | 132.26 | 132.26 | 132.26 | 132.26 | 132.26 |
| 19.700 | 132.26 | 132.26 | 132.26 | 132.26 | 132.25 |
| 19.725 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 19.750 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 19.775 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 19.800 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 19.825 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 19.850 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 19.875 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 19.900 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 19.925 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 19.950 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 19.975 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 20.000 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 20.025 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 20.050 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 20.075 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 20.100 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 20.125 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 20.150 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 20.175 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 20.200 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 20.225 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 20.250 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 20.275 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 20.300 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 20.325 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 20.350 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 20.375 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 20.400 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 20.425 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 20.450 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 20.475 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 20.500 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 20.525 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 20.550 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 20.575 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 20.600 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 20.625 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 20.650 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 20.675 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 20.700 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 20.725 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 20.750 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 20.775 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 20.800 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 20.825 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 20.850 | 132.25 | 132.25 | 132.25 | 132.24 | 132.24 |
| 20.875 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 20.900 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 20.925 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 20.950 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 20.975 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 21.000 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 21.025 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 21.050 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 21.075 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 21.100 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 21.125 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 21.150 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 21.175 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 21.200 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 21.225 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 21.250 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 21.275 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 21.300 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 21.325 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 21.350 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 21.375 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 21.400 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 21.425 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 21.450 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 21.475 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 21.500 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 21.525 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 21.550 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 21.575 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 21.600 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 21.625 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 21.650 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 21.675 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 21.700 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 21.725 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 21.750 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 21.775 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 21.800 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 21.825 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 21.850 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 21.875 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 21.900 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 21.925 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 21.950 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 21.975 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 22.000 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 22.025 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 22.050 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 22.075 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 22.100 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 22.125 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 22.150 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 22.175 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 22.200 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 22.225 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 22.250 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 22.275 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 22.300 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 22.325 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 22.350 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 22.375 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 22.400 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 22.425 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 22.450 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 22.475 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 22.500 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 22.525 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 22.550 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 22.575 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 22.600 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 22.625 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 22.650 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 22.675 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 22.700 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 22.725 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 22.750 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 22.775 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 22.800 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 22.825 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 22.850 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 22.875 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 22.900 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 22.925 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 22.950 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 22.975 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 23.000 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 23.025 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 23.050 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 23.075 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 23.100 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 23.125 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 23.150 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 23.175 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 23.200 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 23.225 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 23.250 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 23.275 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 23.300 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 23.325 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 23.350 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 23.375 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 23.400 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 23.425 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 23.450 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 23.475 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 23.500 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 23.525 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 23.550 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 23.575 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 23.600 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 23.625 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 23.650 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 23.675 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 23.700 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 23.725 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 23.750 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 23.775 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 23.800 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 23.825 | 132.24 | 132.24 | 132.24 | 132.24 | 132.23 |
| 23.850 | 132.23 | 132.23 | 132.23 | 132.23 | 132.23 |
| 23.875 | 132.23 | 132.23 | 132.23 | 132.23 | 132.23 |
| 23.900 | 132.23 | 132.23 | 132.23 | 132.23 | 132.23 |
| 23.925 | 132.23 | 132.23 | 132.23 | 132.23 | 132.23 |
| 23.950 | 132.23 | 132.23 | 132.23 | 132.23 | 132.23 |
| 23.975 | 132.23 | 132.23 | 132.23 | 132.23 | 132.23 |
| 24.000 | 132.23 | (N/A) | (N/A) | (N/A) | (N/A) |

# Index

# Pond Pack – 25 Year Event

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# Table of Contents

Subsection: Master Network Summary

## Catchments Summary

| Label | Scenario | Return Event (years) | Hydrograph Volume (ac-ft) | Time to Peak (hours) | Peak Flow ($ft^3/s$) |
|---|---|---|---|---|---|
| CM-10 | Base | 25 | 0.297 | 11.940 | 5.42 |
| CM-11 | Base | 25 | 0.115 | 11.925 | 2.17 |
| CM-12 | Base | 25 | 0.108 | 11.935 | 1.98 |
| CM-13 | Base | 25 | 0.247 | 12.010 | 3.98 |
| CM-14 | Base | 25 | 1.421 | 12.010 | 23.07 |
| CM-16 | Base | 25 | 0.066 | 11.935 | 1.22 |
| CM-17 | Base | 25 | 0.160 | 12.120 | 1.81 |
| CM-18 | Base | 25 | 0.507 | 11.995 | 8.40 |
| CM-19 | Base | 25 | 0.116 | 11.995 | 1.92 |
| CM-2 | Base | 25 | 0.059 | 11.925 | 1.11 |
| CM-21 | Base | 25 | 0.192 | 12.005 | 3.11 |
| CM-29 | Base | 25 | 1.358 | 12.050 | 19.96 |
| CM-3 | Base | 25 | 0.143 | 11.930 | 2.68 |
| CM-5 | Base | 25 | 0.044 | 11.930 | 0.83 |
| CM-6 | Base | 25 | 0.103 | 11.970 | 1.76 |
| CM-7 | Base | 25 | 0.487 | 12.030 | 7.45 |
| CM-8 | Base | 25 | 0.085 | 11.960 | 1.47 |
| CM-9 | Base | 25 | 0.092 | 12.000 | 1.49 |

## Node Summary

| Label | Scenario | Return Event (years) | Hydrograph Volume (ac-ft) | Time to Peak (hours) | Peak Flow ($ft^3/s$) |
|---|---|---|---|---|---|
| J-10 | Base | 25 | 0.059 | 11.925 | 1.11 |
| J-129 | Base | 25 | 1.358 | 12.050 | 19.96 |
| J-13 | Base | 25 | 0.202 | 11.925 | 3.79 |
| J-17 | Base | 25 | 0.044 | 11.930 | 0.83 |
| J-18 | Base | 25 | 0.044 | 11.930 | 0.83 |
| J-19 | Base | 25 | 0.103 | 11.970 | 1.76 |
| J-20 | Base | 25 | 0.103 | 11.970 | 1.76 |
| J-21 | Base | 25 | 1.058 | 12.010 | 16.22 |
| J-27 | Base | 25 | 0.085 | 11.960 | 1.47 |
| J-28 | Base | 25 | 0.085 | 11.960 | 1.47 |
| J-31 | Base | 25 | 0.092 | 12.000 | 1.49 |
| J-32 | Base | 25 | 0.092 | 12.000 | 1.49 |
| J-33 | Base | 25 | 0.474 | 11.950 | 8.19 |
| J-35 | Base | 25 | 0.202 | 11.925 | 3.79 |
| J-36 | Base | 25 | 0.317 | 11.925 | 5.97 |
| J-39 | Base | 25 | 0.634 | 12.025 | 9.75 |
| J-4 | Base | 25 | 0.059 | 11.925 | 1.11 |
| J-41 | Base | 25 | 0.247 | 12.010 | 3.98 |
| J-42 | Base | 25 | 0.247 | 12.010 | 3.98 |
| J-43 | Base | 25 | 1.668 | 12.010 | 27.05 |
| J-52 | Base | 25 | 0.066 | 11.935 | 1.22 |

Subsection: Master Network Summary

## Node Summary

| Label | Scenario | Return Event (years) | Hydrograph Volume (ac-ft) | Time to Peak (hours) | Peak Flow ($ft^3/s$) |
|---|---|---|---|---|---|
| J-53 | Base | 25 | 0.066 | 11.935 | 1.22 |
| J-59 | Base | 25 | 0.507 | 11.995 | 8.40 |
| J-60 | Base | 25 | 0.506 | 12.000 | 8.36 |
| J-62 | Base | 25 | 0.622 | 12.000 | 10.28 |
| J-64 | Base | 25 | 0.192 | 12.020 | 3.08 |
| J-66 | Base | 25 | 0.192 | 12.005 | 3.11 |
| O-10 | Base | 25 | 0.192 | 12.020 | 3.08 |
| O-12 | Base | 25 | 0.474 | 11.950 | 8.19 |
| O-13 | Base | 25 | 1.668 | 12.010 | 27.05 |
| O-14 | Base | 25 | 1.356 | 12.055 | 19.84 |
| O-5 | Base | 25 | 1.058 | 12.010 | 16.22 |
| O-8 | Base | 25 | 0.226 | 12.025 | 2.48 |
| O-9 | Base | 25 | 0.622 | 12.000 | 10.28 |

Subsection: Unit Hydrograph Equations

## Unit Hydrograph Method (Computational Notes)
## Definition of Terms

| | |
|---|---|
| At | Total area (acres): At = Ai+Ap |
| Ai | Impervious area (acres) |
| Ap | Pervious area (acres) |
| CNi | Runoff curve number for impervious area |
| CNp | Runoff curve number for pervious area |
| fLoss | f loss constant infiltration (depth/time) |
| gKs | Saturated Hydraulic Conductivity (depth/time) |
| Md | Volumetric Moisture Deficit |
| Psi | Capillary Suction (length) |
| hK | Horton Infiltration Decay Rate (time^-1) |
| fo | Initial Infiltration Rate (depth/time) |
| fc | Ultimate(capacity)Infiltration Rate (depth/time) |
| Ia | Initial Abstraction (length) |
| dt | Computational increment (duration of unit excess rainfall)<br>Default dt is smallest value of 0.1333Tc, rtm, and th<br>(Smallest dt is then adjusted to match up with Tp) |
| UDdt | User specified override computational main time increment<br>(only used if UDdt is => .1333Tc) |
| D(t) | Point on distribution curve (fraction of P) for time step t |
| K | 2 / (1 + (Tr/Tp)): default K = 0.75: (for Tr/Tp = 1.67) |
| Ks | Hydrograph shape factor = Unit Conversions * K: = ((1hr/3600sec) * (1ft/12in) * ((5280ft)**2/sq.mi)) * K<br>Default Ks = 645.333 * 0.75 = 484 |
| Lag | Lag time from center of excess runoff (dt) to Tp: Lag = 0.6Tc |
| P | Total precipitation depth, inches |
| Pa(t) | Accumulated rainfall at time step t |
| Pi(t) | Incremental rainfall at time step t |
| qp | Peak discharge (cfs) for 1in. runoff, for 1hr, for 1 sq.mi. = (Ks * A * Q) / Tp (where Q = 1in. runoff, A=sq.mi.) |
| Qu(t) | Unit hydrograph ordinate (cfs) at time step t |
| Q(t) | Final hydrograph ordinate (cfs) at time step t |
| Rai(t) | Accumulated runoff (inches) at time step t for impervious area |
| Rap(t) | Accumulated runoff (inches) at time step t for pervious area |
| Rii(t) | Incremental runoff (inches) at time step t for impervious area |
| Rip(t) | Incremental runoff (inches) at time step t for pervious area |
| R(t) | Incremental weighted total runoff (inches) |
| Rtm | Time increment for rainfall table |
| Si | S for impervious area: Si = (1000/CNi) - 10 |
| Sp | S for pervious area: Sp = (1000/CNp) - 10 |
| t | Time step (row) number |
| Tc | Time of concentration |
| Tb | Time (hrs) of entire unit hydrograph: Tb = Tp + Tr |
| Tp | Time (hrs) to peak of a unit hydrograph: Tp = (dt/2) + Lag |
| Tr | Time (hrs) of receding limb of unit hydrograph: Tr = ratio of Tp |

Subsection: Unit Hydrograph Equations

## Unit Hydrograph Method
## Computational Notes
## Precipitation

| | |
|---|---|
| Column (1) | Time for time step t |
| Column (2) | D(t) = Point on distribution curve for time step t |
| Column (3) | Pi(t) = Pa(t) - Pa(t-1): Col.(4) - Preceding Col.(4) |
| Column (4) | Pa(t) = D(t) x P: Col.(2) x P |

## Pervious Area Runoff (using SCS Runoff CN Method)

| | |
|---|---|
| Column (5) | Rap(t) = Accumulated pervious runoff for time step t<br>If (Pa(t) is <= 0.2Sp) then use: Rap(t) = 0.0<br>If (Pa(t) is > 0.2Sp) then use:<br><br>Rap(t) = (Col.(4)-0.2Sp)**2 / (Col.(4)+0.8Sp) |
| Column (6) | Rip(t) = Incremental pervious runoff for time step t<br>Rip(t) = Rap(t) - Rap(t-1)<br>Rip(t) = Col.(5) for current row - Col.(5) for preceding row. |

## Impervious Area Runoff

| | |
|---|---|
| Column (7 & 8)... | Did not specify to use impervious areas. |

## Incremental Weighted Runoff

| | |
|---|---|
| Column (9) | R(t) = (Ap/At) x Rip(t) + (Ai/At) x Rii(t)<br>R(t) = (Ap/At) x Col.(6) + (Ai/At) x Col.(8) |

## SCS Unit Hydrograph Method

| | |
|---|---|
| Column (10) | Q(t) is computed with the SCS unit hydrograph method using R(t) and Qu(t). |

| | |
|---|---|
| Storm Event | 25 yr |
| Return Event | 25 years |
| Duration | 24.000 hours |
| Depth | 6.5 in |
| Time of Concentration (Composite) | 0.101 hours |
| Scaled Area | 1.148 acres |

| | |
|---|---|
| Computational Time Increment | 0.013 hours |
| Time to Peak (Computed) | 11.940 hours |
| Flow (Peak, Computed) | 5.42 ft³/s |
| Output Increment | 0.005 hours |
| Time to Flow (Peak Interpolated Output) | 11.940 hours |
| Flow (Peak Interpolated Output) | 5.42 ft³/s |

| Drainage Area | |
|---|---|
| SCS CN (Composite) | 69.000 |
| Scaled Area | 1.148 acres |
| Maximum Retention (Pervious) | 4.5 in |
| Maximum Retention (Pervious, 20 percent) | 0.9 in |

| Cumulative Runoff | |
|---|---|
| Cumulative Runoff Depth (Pervious) | 3.1 in |
| Runoff Volume (Pervious) | 0.297 ac-ft |

| Hydrograph Volume (Area under Hydrograph curve) | |
|---|---|
| Volume | 0.297 ac-ft |

| SCS Unit Hydrograph Parameters | |
|---|---|
| Time of Concentration (Composite) | 0.101 hours |
| Computational Time Increment | 0.013 hours |
| Unit Hydrograph Shape Factor | 483.432 |
| K Factor | 0.749 |
| Receding/Rising, Tr/Tp | 1.670 |
| Unit peak, qp | 12.90 ft³/s |
| Unit peak time, Tp | 0.067 hours |

| SCS Unit Hydrograph Parameters | |
|---|---|
| Unit receding limb, Tr | 0.269 hours |
| Total unit time, Tb | 0.336 hours |

| | |
|---|---|
| Storm Event | 25 yr |
| Return Event | 25 years |
| Duration | 24.000 hours |
| Depth | 6.5 in |
| Time of Concentration (Composite) | 0.083 hours |
| Scaled Area | 0.445 acres |

| | |
|---|---|
| Computational Time Increment | 0.011 hours |
| Time to Peak (Computed) | 11.922 hours |
| Flow (Peak, Computed) | 2.18 ft³/s |
| Output Increment | 0.005 hours |
| Time to Flow (Peak Interpolated Output) | 11.925 hours |
| Flow (Peak Interpolated Output) | 2.17 ft³/s |

| Drainage Area | |
|---|---|
| SCS CN (Composite) | 69.000 |
| Scaled Area | 0.445 acres |
| Maximum Retention (Pervious) | 4.5 in |
| Maximum Retention (Pervious, 20 percent) | 0.9 in |

| Cumulative Runoff | |
|---|---|
| Cumulative Runoff Depth (Pervious) | 3.1 in |
| Runoff Volume (Pervious) | 0.115 ac-ft |

| Hydrograph Volume (Area under Hydrograph curve) | |
|---|---|
| Volume | 0.115 ac-ft |

| SCS Unit Hydrograph Parameters | |
|---|---|
| Time of Concentration (Composite) | 0.083 hours |
| Computational Time Increment | 0.011 hours |
| Unit Hydrograph Shape Factor | 483.432 |
| K Factor | 0.749 |
| Receding/Rising, Tr/Tp | 1.670 |
| Unit peak, qp | 6.05 ft³/s |
| Unit peak time, Tp | 0.056 hours |

| SCS Unit Hydrograph Parameters | |
|---|---|
| Unit receding limb, Tr | 0.222 hours |
| Total unit time, Tb | 0.278 hours |

| | |
|---|---|
| Storm Event | 25 yr |
| Return Event | 25 years |
| Duration | 24.000 hours |
| Depth | 6.5 in |
| Time of Concentration (Composite) | 0.096 hours |
| Scaled Area | 0.416 acres |

| | |
|---|---|
| Computational Time Increment | 0.013 hours |
| Time to Peak (Computed) | 11.936 hours |
| Flow (Peak, Computed) | 1.99 ft³/s |
| Output Increment | 0.005 hours |
| Time to Flow (Peak Interpolated Output) | 11.935 hours |
| Flow (Peak Interpolated Output) | 1.98 ft³/s |

| Drainage Area | |
|---|---|
| SCS CN (Composite) | 69.000 |
| Scaled Area | 0.416 acres |
| Maximum Retention (Pervious) | 4.5 in |
| Maximum Retention (Pervious, 20 percent) | 0.9 in |

| Cumulative Runoff | |
|---|---|
| Cumulative Runoff Depth (Pervious) | 3.1 in |
| Runoff Volume (Pervious) | 0.108 ac-ft |

| Hydrograph Volume (Area under Hydrograph curve) | |
|---|---|
| Volume | 0.108 ac-ft |

| SCS Unit Hydrograph Parameters | |
|---|---|
| Time of Concentration (Composite) | 0.096 hours |
| Computational Time Increment | 0.013 hours |
| Unit Hydrograph Shape Factor | 483.432 |
| K Factor | 0.749 |
| Receding/Rising, Tr/Tp | 1.670 |
| Unit peak, qp | 4.93 ft³/s |
| Unit peak time, Tp | 0.064 hours |

| SCS Unit Hydrograph Parameters | |
|---|---|
| Unit receding limb, Tr | 0.255 hours |
| Total unit time, Tb | 0.319 hours |

| | |
|---|---|
| Storm Event | 25 yr |
| Return Event | 25 years |
| Duration | 24.000 hours |
| Depth | 6.5 in |
| Time of Concentration (Composite) | 0.182 hours |
| Scaled Area | 0.955 acres |

| | |
|---|---|
| Computational Time Increment | 0.024 hours |
| Time to Peak (Computed) | 12.012 hours |
| Flow (Peak, Computed) | 3.98 ft³/s |
| Output Increment | 0.005 hours |
| Time to Flow (Peak Interpolated Output) | 12.010 hours |
| Flow (Peak Interpolated Output) | 3.98 ft³/s |

| Drainage Area | |
|---|---|
| SCS CN (Composite) | 69.000 |
| Scaled Area | 0.955 acres |
| Maximum Retention (Pervious) | 4.5 in |
| Maximum Retention (Pervious, 20 percent) | 0.9 in |

| Cumulative Runoff | |
|---|---|
| Cumulative Runoff Depth (Pervious) | 3.1 in |
| Runoff Volume (Pervious) | 0.247 ac-ft |

| Hydrograph Volume (Area under Hydrograph curve) | |
|---|---|
| Volume | 0.247 ac-ft |

| SCS Unit Hydrograph Parameters | |
|---|---|
| Time of Concentration (Composite) | 0.182 hours |
| Computational Time Increment | 0.024 hours |
| Unit Hydrograph Shape Factor | 483.432 |
| K Factor | 0.749 |
| Receding/Rising, Tr/Tp | 1.670 |
| Unit peak, qp | 5.94 ft³/s |
| Unit peak time, Tp | 0.121 hours |

| SCS Unit Hydrograph Parameters | |
|---|---|
| Unit receding limb, Tr | 0.485 hours |
| Total unit time, Tb | 0.607 hours |

| | |
|---|---|
| Storm Event | 25 yr |
| Return Event | 25 years |
| Duration | 24.000 hours |
| Depth | 6.5 in |
| Time of Concentration (Composite) | 0.177 hours |
| Scaled Area | 5.502 acres |

| | |
|---|---|
| Computational Time Increment | 0.024 hours |
| Time to Peak (Computed) | 12.009 hours |
| Flow (Peak, Computed) | 23.09 ft³/s |
| Output Increment | 0.005 hours |
| Time to Flow (Peak Interpolated Output) | 12.010 hours |
| Flow (Peak Interpolated Output) | 23.07 ft³/s |

| Drainage Area | |
|---|---|
| SCS CN (Composite) | 69.000 |
| Scaled Area | 5.502 acres |
| Maximum Retention (Pervious) | 4.5 in |
| Maximum Retention (Pervious, 20 percent) | 0.9 in |

| Cumulative Runoff | |
|---|---|
| Cumulative Runoff Depth (Pervious) | 3.1 in |
| Runoff Volume (Pervious) | 1.425 ac-ft |

| Hydrograph Volume (Area under Hydrograph curve) | |
|---|---|
| Volume | 1.421 ac-ft |

| SCS Unit Hydrograph Parameters | |
|---|---|
| Time of Concentration (Composite) | 0.177 hours |
| Computational Time Increment | 0.024 hours |
| Unit Hydrograph Shape Factor | 483.432 |
| K Factor | 0.749 |
| Receding/Rising, Tr/Tp | 1.670 |
| Unit peak, qp | 35.23 ft³/s |
| Unit peak time, Tp | 0.118 hours |

| SCS Unit Hydrograph Parameters | |
|---|---|
| Unit receding limb, Tr | 0.472 hours |
| Total unit time, Tb | 0.590 hours |

| | |
|---|---|
| Storm Event | 25 yr |
| Return Event | 25 years |
| Duration | 24.000 hours |
| Depth | 6.5 in |
| Time of Concentration (Composite) | 0.093 hours |
| Scaled Area | 0.255 acres |

| | |
|---|---|
| Computational Time Increment | 0.012 hours |
| Time to Peak (Computed) | 11.936 hours |
| Flow (Peak, Computed) | 1.22 ft³/s |
| Output Increment | 0.005 hours |
| Time to Flow (Peak Interpolated Output) | 11.935 hours |
| Flow (Peak Interpolated Output) | 1.22 ft³/s |

| Drainage Area | |
|---|---|
| SCS CN (Composite) | 69.000 |
| Scaled Area | 0.255 acres |
| Maximum Retention (Pervious) | 4.5 in |
| Maximum Retention (Pervious, 20 percent) | 0.9 in |

| Cumulative Runoff | |
|---|---|
| Cumulative Runoff Depth (Pervious) | 3.1 in |
| Runoff Volume (Pervious) | 0.066 ac-ft |

| Hydrograph Volume (Area under Hydrograph curve) | |
|---|---|
| Volume | 0.066 ac-ft |

| SCS Unit Hydrograph Parameters | |
|---|---|
| Time of Concentration (Composite) | 0.093 hours |
| Computational Time Increment | 0.012 hours |
| Unit Hydrograph Shape Factor | 483.432 |
| K Factor | 0.749 |
| Receding/Rising, Tr/Tp | 1.670 |
| Unit peak, qp | 3.09 ft³/s |
| Unit peak time, Tp | 0.062 hours |

| SCS Unit Hydrograph Parameters | |
|---|---|
| Unit receding limb, Tr | 0.249 hours |
| Total unit time, Tb | 0.311 hours |

| | |
|---|---|
| Storm Event | 25 yr |
| Return Event | 25 years |
| Duration | 24.000 hours |
| Depth | 6.5 in |
| Time of Concentration (Composite) | 0.417 hours |
| Scaled Area | 0.622 acres |

| | |
|---|---|
| Computational Time Increment | 0.056 hours |
| Time to Peak (Computed) | 12.116 hours |
| Flow (Peak, Computed) | 1.81 ft³/s |
| Output Increment | 0.005 hours |
| Time to Flow (Peak Interpolated Output) | 12.120 hours |
| Flow (Peak Interpolated Output) | 1.81 ft³/s |

| Drainage Area | |
|---|---|
| SCS CN (Composite) | 69.000 |
| Scaled Area | 0.622 acres |
| Maximum Retention (Pervious) | 4.5 in |
| Maximum Retention (Pervious, 20 percent) | 0.9 in |

| Cumulative Runoff | |
|---|---|
| Cumulative Runoff Depth (Pervious) | 3.1 in |
| Runoff Volume (Pervious) | 0.161 ac-ft |

| Hydrograph Volume (Area under Hydrograph curve) | |
|---|---|
| Volume | 0.160 ac-ft |

| SCS Unit Hydrograph Parameters | |
|---|---|
| Time of Concentration (Composite) | 0.417 hours |
| Computational Time Increment | 0.056 hours |
| Unit Hydrograph Shape Factor | 483.432 |
| K Factor | 0.749 |
| Receding/Rising, Tr/Tp | 1.670 |
| Unit peak, qp | 1.69 ft³/s |
| Unit peak time, Tp | 0.278 hours |

| SCS Unit Hydrograph Parameters | |
|---|---|
| Unit receding limb, Tr | 1.112 hours |
| Total unit time, Tb | 1.389 hours |

| | |
|---|---|
| Storm Event | 25 yr |
| Return Event | 25 years |
| Duration | 24.000 hours |
| Depth | 6.5 in |
| Time of Concentration (Composite) | 0.163 hours |
| Scaled Area | 1.960 acres |

| | |
|---|---|
| Computational Time Increment | 0.022 hours |
| Time to Peak (Computed) | 11.996 hours |
| Flow (Peak, Computed) | 8.40 ft³/s |
| Output Increment | 0.005 hours |
| Time to Flow (Peak Interpolated Output) | 11.995 hours |
| Flow (Peak Interpolated Output) | 8.40 ft³/s |

| Drainage Area | |
|---|---|
| SCS CN (Composite) | 69.000 |
| Scaled Area | 1.960 acres |
| Maximum Retention (Pervious) | 4.5 in |
| Maximum Retention (Pervious, 20 percent) | 0.9 in |

| Cumulative Runoff | |
|---|---|
| Cumulative Runoff Depth (Pervious) | 3.1 in |
| Runoff Volume (Pervious) | 0.508 ac-ft |

| Hydrograph Volume (Area under Hydrograph curve) | |
|---|---|
| Volume | 0.507 ac-ft |

| SCS Unit Hydrograph Parameters | |
|---|---|
| Time of Concentration (Composite) | 0.163 hours |
| Computational Time Increment | 0.022 hours |
| Unit Hydrograph Shape Factor | 483.432 |
| K Factor | 0.749 |
| Receding/Rising, Tr/Tp | 1.670 |
| Unit peak, qp | 13.65 ft³/s |
| Unit peak time, Tp | 0.108 hours |

| SCS Unit Hydrograph Parameters | |
|---|---|
| Unit receding limb, Tr | 0.434 hours |
| Total unit time, Tb | 0.542 hours |

| | |
|---|---|
| Storm Event | 25 yr |
| Return Event | 25 years |
| Duration | 24.000 hours |
| Depth | 6.5 in |
| Time of Concentration (Composite) | 0.163 hours |
| Scaled Area | 0.449 acres |

| | |
|---|---|
| Computational Time Increment | 0.022 hours |
| Time to Peak (Computed) | 11.996 hours |
| Flow (Peak, Computed) | 1.92 ft³/s |
| Output Increment | 0.005 hours |
| Time to Flow (Peak Interpolated Output) | 11.995 hours |
| Flow (Peak Interpolated Output) | 1.92 ft³/s |

| Drainage Area | |
|---|---|
| SCS CN (Composite) | 69.000 |
| Scaled Area | 0.449 acres |
| Maximum Retention (Pervious) | 4.5 in |
| Maximum Retention (Pervious, 20 percent) | 0.9 in |

| Cumulative Runoff | |
|---|---|
| Cumulative Runoff Depth (Pervious) | 3.1 in |
| Runoff Volume (Pervious) | 0.116 ac-ft |

| Hydrograph Volume (Area under Hydrograph curve) | |
|---|---|
| Volume | 0.116 ac-ft |

| SCS Unit Hydrograph Parameters | |
|---|---|
| Time of Concentration (Composite) | 0.163 hours |
| Computational Time Increment | 0.022 hours |
| Unit Hydrograph Shape Factor | 483.432 |
| K Factor | 0.749 |
| Receding/Rising, Tr/Tp | 1.670 |
| Unit peak, qp | 3.13 ft³/s |
| Unit peak time, Tp | 0.108 hours |

| SCS Unit Hydrograph Parameters | |
|---|---|
| Unit receding limb, Tr | 0.434 hours |
| Total unit time, Tb | 0.542 hours |

| | |
|---|---|
| Storm Event | 25 yr |
| Return Event | 25 years |
| Duration | 24.000 hours |
| Depth | 6.5 in |
| Time of Concentration (Composite) | 0.083 hours |
| Scaled Area | 0.227 acres |

| | |
|---|---|
| Computational Time Increment | 0.011 hours |
| Time to Peak (Computed) | 11.922 hours |
| Flow (Peak, Computed) | 1.11 ft³/s |
| Output Increment | 0.005 hours |
| Time to Flow (Peak Interpolated Output) | 11.925 hours |
| Flow (Peak Interpolated Output) | 1.11 ft³/s |

| Drainage Area | |
|---|---|
| SCS CN (Composite) | 69.000 |
| Scaled Area | 0.227 acres |
| Maximum Retention (Pervious) | 4.5 in |
| Maximum Retention (Pervious, 20 percent) | 0.9 in |

| Cumulative Runoff | |
|---|---|
| Cumulative Runoff Depth (Pervious) | 3.1 in |
| Runoff Volume (Pervious) | 0.059 ac-ft |

| Hydrograph Volume (Area under Hydrograph curve) | |
|---|---|
| Volume | 0.059 ac-ft |

| SCS Unit Hydrograph Parameters | |
|---|---|
| Time of Concentration (Composite) | 0.083 hours |
| Computational Time Increment | 0.011 hours |
| Unit Hydrograph Shape Factor | 483.432 |
| K Factor | 0.749 |
| Receding/Rising, Tr/Tp | 1.670 |
| Unit peak, qp | 3.09 ft³/s |
| Unit peak time, Tp | 0.056 hours |

| SCS Unit Hydrograph Parameters | |
|---|---|
| Unit receding limb, Tr | 0.222 hours |
| Total unit time, Tb | 0.278 hours |

| | |
|---|---|
| Storm Event | 25 yr |
| Return Event | 25 years |
| Duration | 24.000 hours |
| Depth | 6.5 in |
| Time of Concentration (Composite) | 0.182 hours |
| Scaled Area | 0.744 acres |

| | |
|---|---|
| Computational Time Increment | 0.024 hours |
| Time to Peak (Computed) | 12.005 hours |
| Flow (Peak, Computed) | 3.11 ft³/s |
| Output Increment | 0.005 hours |
| Time to Flow (Peak Interpolated Output) | 12.005 hours |
| Flow (Peak Interpolated Output) | 3.11 ft³/s |

| Drainage Area | |
|---|---|
| SCS CN (Composite) | 69.000 |
| Scaled Area | 0.744 acres |
| Maximum Retention (Pervious) | 4.5 in |
| Maximum Retention (Pervious, 20 percent) | 0.9 in |

| Cumulative Runoff | |
|---|---|
| Cumulative Runoff Depth (Pervious) | 3.1 in |
| Runoff Volume (Pervious) | 0.193 ac-ft |

| Hydrograph Volume (Area under Hydrograph curve) | |
|---|---|
| Volume | 0.192 ac-ft |

| SCS Unit Hydrograph Parameters | |
|---|---|
| Time of Concentration (Composite) | 0.182 hours |
| Computational Time Increment | 0.024 hours |
| Unit Hydrograph Shape Factor | 483.432 |
| K Factor | 0.749 |
| Receding/Rising, Tr/Tp | 1.670 |
| Unit peak, qp | 4.64 ft³/s |
| Unit peak time, Tp | 0.121 hours |

| SCS Unit Hydrograph Parameters | |
|---|---|
| Unit receding limb, Tr | 0.485 hours |
| Total unit time, Tb | 0.606 hours |

| | |
|---|---|
| Storm Event | 25 yr |
| Return Event | 25 years |
| Duration | 24.000 hours |
| Depth | 6.5 in |
| Time of Concentration (Composite) | 0.244 hours |
| Scaled Area | 5.261 acres |

| | |
|---|---|
| Computational Time Increment | 0.032 hours |
| Time to Peak (Computed) | 12.052 hours |
| Flow (Peak, Computed) | 19.98 ft³/s |
| Output Increment | 0.005 hours |
| Time to Flow (Peak Interpolated Output) | 12.050 hours |
| Flow (Peak Interpolated Output) | 19.96 ft³/s |

| Drainage Area | |
|---|---|
| SCS CN (Composite) | 69.000 |
| Scaled Area | 5.261 acres |
| Maximum Retention (Pervious) | 4.5 in |
| Maximum Retention (Pervious, 20 percent) | 0.9 in |

| Cumulative Runoff | |
|---|---|
| Cumulative Runoff Depth (Pervious) | 3.1 in |
| Runoff Volume (Pervious) | 1.363 ac-ft |

| Hydrograph Volume (Area under Hydrograph curve) | |
|---|---|
| Volume | 1.358 ac-ft |

| SCS Unit Hydrograph Parameters | |
|---|---|
| Time of Concentration (Composite) | 0.244 hours |
| Computational Time Increment | 0.032 hours |
| Unit Hydrograph Shape Factor | 483.432 |
| K Factor | 0.749 |
| Receding/Rising, Tr/Tp | 1.670 |
| Unit peak, qp | 24.46 ft³/s |
| Unit peak time, Tp | 0.162 hours |

| SCS Unit Hydrograph Parameters | |
|---|---|
| Unit receding limb, Tr | 0.650 hours |
| Total unit time, Tb | 0.812 hours |

| | |
|---|---|
| Storm Event | 25 yr |
| Return Event | 25 years |
| Duration | 24.000 hours |
| Depth | 6.5 in |
| Time of Concentration (Composite) | 0.086 hours |
| Scaled Area | 0.553 acres |

| | |
|---|---|
| Computational Time Increment | 0.012 hours |
| Time to Peak (Computed) | 11.928 hours |
| Flow (Peak, Computed) | 2.69 ft³/s |
| Output Increment | 0.005 hours |
| Time to Flow (Peak Interpolated Output) | 11.930 hours |
| Flow (Peak Interpolated Output) | 2.68 ft³/s |

| Drainage Area | |
|---|---|
| SCS CN (Composite) | 69.000 |
| Scaled Area | 0.553 acres |
| Maximum Retention (Pervious) | 4.5 in |
| Maximum Retention (Pervious, 20 percent) | 0.9 in |

| Cumulative Runoff | |
|---|---|
| Cumulative Runoff Depth (Pervious) | 3.1 in |
| Runoff Volume (Pervious) | 0.143 ac-ft |

| Hydrograph Volume (Area under Hydrograph curve) | |
|---|---|
| Volume | 0.143 ac-ft |

| SCS Unit Hydrograph Parameters | |
|---|---|
| Time of Concentration (Composite) | 0.086 hours |
| Computational Time Increment | 0.012 hours |
| Unit Hydrograph Shape Factor | 483.432 |
| K Factor | 0.749 |
| Receding/Rising, Tr/Tp | 1.670 |
| Unit peak, qp | 7.26 ft³/s |
| Unit peak time, Tp | 0.058 hours |

| SCS Unit Hydrograph Parameters | |
|---|---|
| Unit receding limb, Tr | 0.230 hours |
| Total unit time, Tb | 0.288 hours |

| | |
|---|---|
| Storm Event | 25 yr |
| Return Event | 25 years |
| Duration | 24.000 hours |
| Depth | 6.5 in |
| Time of Concentration (Composite) | 0.089 hours |
| Scaled Area | 0.171 acres |

| | |
|---|---|
| Computational Time Increment | 0.012 hours |
| Time to Peak (Computed) | 11.929 hours |
| Flow (Peak, Computed) | 0.83 ft³/s |
| Output Increment | 0.005 hours |
| Time to Flow (Peak Interpolated Output) | 11.930 hours |
| Flow (Peak Interpolated Output) | 0.83 ft³/s |

| Drainage Area | |
|---|---|
| SCS CN (Composite) | 69.000 |
| Scaled Area | 0.171 acres |
| Maximum Retention (Pervious) | 4.5 in |
| Maximum Retention (Pervious, 20 percent) | 0.9 in |

| Cumulative Runoff | |
|---|---|
| Cumulative Runoff Depth (Pervious) | 3.1 in |
| Runoff Volume (Pervious) | 0.044 ac-ft |

| Hydrograph Volume (Area under Hydrograph curve) | |
|---|---|
| Volume | 0.044 ac-ft |

| SCS Unit Hydrograph Parameters | |
|---|---|
| Time of Concentration (Composite) | 0.089 hours |
| Computational Time Increment | 0.012 hours |
| Unit Hydrograph Shape Factor | 483.432 |
| K Factor | 0.749 |
| Receding/Rising, Tr/Tp | 1.670 |
| Unit peak, qp | 2.18 ft³/s |
| Unit peak time, Tp | 0.059 hours |

| SCS Unit Hydrograph Parameters | |
|---|---|
| Unit receding limb, Tr | 0.237 hours |
| Total unit time, Tb | 0.296 hours |

| | |
|---|---|
| Storm Event | 25 yr |
| Return Event | 25 years |
| Duration | 24.000 hours |
| Depth | 6.5 in |
| Time of Concentration (Composite) | 0.142 hours |
| Scaled Area | 0.399 acres |

| | |
|---|---|
| Computational Time Increment | 0.019 hours |
| Time to Peak (Computed) | 11.967 hours |
| Flow (Peak, Computed) | 1.76 ft³/s |
| Output Increment | 0.005 hours |
| Time to Flow (Peak Interpolated Output) | 11.970 hours |
| Flow (Peak Interpolated Output) | 1.76 ft³/s |

| Drainage Area | |
|---|---|
| SCS CN (Composite) | 69.000 |
| Scaled Area | 0.399 acres |
| Maximum Retention (Pervious) | 4.5 in |
| Maximum Retention (Pervious, 20 percent) | 0.9 in |

| Cumulative Runoff | |
|---|---|
| Cumulative Runoff Depth (Pervious) | 3.1 in |
| Runoff Volume (Pervious) | 0.103 ac-ft |

| Hydrograph Volume (Area under Hydrograph curve) | |
|---|---|
| Volume | 0.103 ac-ft |

| SCS Unit Hydrograph Parameters | |
|---|---|
| Time of Concentration (Composite) | 0.142 hours |
| Computational Time Increment | 0.019 hours |
| Unit Hydrograph Shape Factor | 483.432 |
| K Factor | 0.749 |
| Receding/Rising, Tr/Tp | 1.670 |
| Unit peak, qp | 3.19 ft³/s |
| Unit peak time, Tp | 0.095 hours |

| SCS Unit Hydrograph Parameters | |
|---|---|
| Unit receding limb, Tr | 0.378 hours |
| Total unit time, Tb | 0.473 hours |

| | |
|---|---|
| Storm Event | 25 yr |
| Return Event | 25 years |
| Duration | 24.000 hours |
| Depth | 6.5 in |
| Time of Concentration (Composite) | 0.222 hours |
| Scaled Area | 1.886 acres |

| | |
|---|---|
| Computational Time Increment | 0.030 hours |
| Time to Peak (Computed) | 12.030 hours |
| Flow (Peak, Computed) | 7.45 ft³/s |
| Output Increment | 0.005 hours |
| Time to Flow (Peak Interpolated Output) | 12.030 hours |
| Flow (Peak Interpolated Output) | 7.45 ft³/s |

| Drainage Area | |
|---|---|
| SCS CN (Composite) | 69.000 |
| Scaled Area | 1.886 acres |
| Maximum Retention (Pervious) | 4.5 in |
| Maximum Retention (Pervious, 20 percent) | 0.9 in |

| Cumulative Runoff | |
|---|---|
| Cumulative Runoff Depth (Pervious) | 3.1 in |
| Runoff Volume (Pervious) | 0.489 ac-ft |

| Hydrograph Volume (Area under Hydrograph curve) | |
|---|---|
| Volume | 0.487 ac-ft |

| SCS Unit Hydrograph Parameters | |
|---|---|
| Time of Concentration (Composite) | 0.222 hours |
| Computational Time Increment | 0.030 hours |
| Unit Hydrograph Shape Factor | 483.432 |
| K Factor | 0.749 |
| Receding/Rising, Tr/Tp | 1.670 |
| Unit peak, qp | 9.64 ft³/s |
| Unit peak time, Tp | 0.148 hours |

| SCS Unit Hydrograph Parameters | |
|---|---|
| Unit receding limb, Tr | 0.591 hours |
| Total unit time, Tb | 0.739 hours |

| | |
|---|---|
| Storm Event | 25 yr |
| Return Event | 25 years |
| Duration | 24.000 hours |
| Depth | 6.5 in |
| Time of Concentration (Composite) | 0.129 hours |
| Scaled Area | 0.327 acres |

| | |
|---|---|
| Computational Time Increment | 0.017 hours |
| Time to Peak (Computed) | 11.960 hours |
| Flow (Peak, Computed) | 1.47 ft³/s |
| Output Increment | 0.005 hours |
| Time to Flow (Peak Interpolated Output) | 11.960 hours |
| Flow (Peak Interpolated Output) | 1.47 ft³/s |

| Drainage Area | |
|---|---|
| SCS CN (Composite) | 69.000 |
| Scaled Area | 0.327 acres |
| Maximum Retention (Pervious) | 4.5 in |
| Maximum Retention (Pervious, 20 percent) | 0.9 in |

| Cumulative Runoff | |
|---|---|
| Cumulative Runoff Depth (Pervious) | 3.1 in |
| Runoff Volume (Pervious) | 0.085 ac-ft |

| Hydrograph Volume (Area under Hydrograph curve) | |
|---|---|
| Volume | 0.085 ac-ft |

| SCS Unit Hydrograph Parameters | |
|---|---|
| Time of Concentration (Composite) | 0.129 hours |
| Computational Time Increment | 0.017 hours |
| Unit Hydrograph Shape Factor | 483.432 |
| K Factor | 0.749 |
| Receding/Rising, Tr/Tp | 1.670 |
| Unit peak, qp | 2.86 ft³/s |
| Unit peak time, Tp | 0.086 hours |

| SCS Unit Hydrograph Parameters | |
|---|---|
| Unit receding limb, Tr | 0.345 hours |
| Total unit time, Tb | 0.431 hours |

| | |
|---|---|
| Storm Event | 25 yr |
| Return Event | 25 years |
| Duration | 24.000 hours |
| Depth | 6.5 in |
| Time of Concentration (Composite) | 0.180 hours |
| Scaled Area | 0.357 acres |

| | |
|---|---|
| Computational Time Increment | 0.024 hours |
| Time to Peak (Computed) | 11.998 hours |
| Flow (Peak, Computed) | 1.50 ft³/s |
| Output Increment | 0.005 hours |
| Time to Flow (Peak Interpolated Output) | 12.000 hours |
| Flow (Peak Interpolated Output) | 1.49 ft³/s |

| Drainage Area | |
|---|---|
| SCS CN (Composite) | 69.000 |
| Scaled Area | 0.357 acres |
| Maximum Retention (Pervious) | 4.5 in |
| Maximum Retention (Pervious, 20 percent) | 0.9 in |

| Cumulative Runoff | |
|---|---|
| Cumulative Runoff Depth (Pervious) | 3.1 in |
| Runoff Volume (Pervious) | 0.093 ac-ft |

| Hydrograph Volume (Area under Hydrograph curve) | |
|---|---|
| Volume | 0.092 ac-ft |

| SCS Unit Hydrograph Parameters | |
|---|---|
| Time of Concentration (Composite) | 0.180 hours |
| Computational Time Increment | 0.024 hours |
| Unit Hydrograph Shape Factor | 483.432 |
| K Factor | 0.749 |
| Receding/Rising, Tr/Tp | 1.670 |
| Unit peak, qp | 2.25 ft³/s |
| Unit peak time, Tp | 0.120 hours |

| SCS Unit Hydrograph Parameters | |
|---|---|
| Unit receding limb, Tr | 0.480 hours |
| Total unit time, Tb | 0.600 hours |

## Solution to Manning's Open Channel Flow Equation
## (Computed values are based on normal depth.)

**Q = (k/n) * A * (R**2/3) * (S**1/2)**

| where: | English Units | SI units |
|---|---|---|
| Q = Channel Flow | cfs | cms |
| k = Manning's Constant | 1.485919 | 1.0 |
| n = Manning's n | no units | no units |
| R = Hydraulic radius, A/WP | feet | meter |
| A = X-section flow area | ft^2 | m^2 |
| WP = Wetted perimeter | feet | meter |
| S = Slope | ft/ft | m/m |

**Additional Output Variables:**
**Vel= Q/A**
**Hd = A/TpW**
**F = Vel / (g * Hd)**1/2**

| where: | English Units | SI units |
|---|---|---|
| Q = Channel Flow | cfs | cms |
| k = Manning's Constant | 1.485919 | 1.0 |
| n = Manning's n | no units | no units |
| R = Hydraulic radius, A/WP | feet | meter |
| A = X-section flow area | ft^2 | m^2 |
| WP = Wetted perimeter | feet | meter |
| S = Slope | ft/ft | m/m |

## Solution to Manning's Open Channel Flow Equation
## (Computed values are based on normal depth.)

**Q = (k/n) * A * (R**2/3) * (S**1/2)**

| where: | English Units | SI units |
|---|---|---|
| Q = Channel Flow | cfs | cms |
| k = Manning's Constant | 1.485919 | 1.0 |
| n = Manning's n | no units | no units |
| R = Hydraulic radius, A/WP | feet | meter |
| A = X-section flow area | ft^2 | m^2 |
| WP = Wetted perimeter | feet | meter |
| S = Slope | ft/ft | m/m |

**Additional Output Variables:**
**Vel= Q/A**
**Hd = A/TpW**
**F = Vel / (g * Hd)**1/2**

| where: | English Units | SI units |
|---|---|---|
| Q = Channel Flow | cfs | cms |
| k = Manning's Constant | 1.485919 | 1.0 |
| n = Manning's n | no units | no units |
| R = Hydraulic radius, A/WP | feet | meter |
| A = X-section flow area | ft^2 | m^2 |
| WP = Wetted perimeter | feet | meter |
| S = Slope | ft/ft | m/m |

## Solution to Manning's Open Channel Flow Equation
## (Computed values are based on normal depth.)

**Q = (k/n) * A * (R**2/3) * (S**1/2)**

| where: | English Units | SI units |
|---|---|---|
| Q = Channel Flow | cfs | cms |
| k = Manning's Constant | 1.485919 | 1.0 |
| n = Manning's n | no units | no units |
| R = Hydraulic radius, A/WP | feet | meter |
| A = X-section flow area | ft^2 | m^2 |
| WP = Wetted perimeter | feet | meter |
| S = Slope | ft/ft | m/m |

**Additional Output Variables:**
**Vel= Q/A**
**Hd = A/TpW**
**F = Vel / (g * Hd)**1/2**

| where: | English Units | SI units |
|---|---|---|
| Q = Channel Flow | cfs | cms |
| k = Manning's Constant | 1.485919 | 1.0 |
| n = Manning's n | no units | no units |
| R = Hydraulic radius, A/WP | feet | meter |
| A = X-section flow area | ft^2 | m^2 |
| WP = Wetted perimeter | feet | meter |
| S = Slope | ft/ft | m/m |

## Solution to Manning's Open Channel Flow Equation
## (Computed values are based on normal depth.)

**Q = (k/n) * A * (R**2/3) * (S**1/2)**

| where: | English Units | SI units |
|---|---|---|
| Q = Channel Flow | cfs | cms |
| k = Manning's Constant | 1.485919 | 1.0 |
| n = Manning's n | no units | no units |
| R = Hydraulic radius, A/WP | feet | meter |
| A = X-section flow area | ft^2 | m^2 |
| WP = Wetted perimeter | feet | meter |
| S = Slope | ft/ft | m/m |

**Additional Output Variables:**
**Vel= Q/A**
**Hd = A/TpW**
**F = Vel / (g * Hd)**1/2**

| where: | English Units | SI units |
|---|---|---|
| Q = Channel Flow | cfs | cms |
| k = Manning's Constant | 1.485919 | 1.0 |
| n = Manning's n | no units | no units |
| R = Hydraulic radius, A/WP | feet | meter |
| A = X-section flow area | ft^2 | m^2 |
| WP = Wetted perimeter | feet | meter |
| S = Slope | ft/ft | m/m |

Subsection: Elevation-Volume-Flow Table (Channel)
Label: CO-28

Return Event: 25 years
Storm Event: 25 yr

| Modified Puls Results Summary | |
|---|---|
| Length (Channel) | 524.51 ft |
| Travel Time (Channel) | 0.054 hours |
| Number of Sections | 11 |
| Length (Section) | 47.68 ft |
| Flow (Weighted) | 3.35 ft³/s |
| Overflow Channel | No Overflow Data |
| Elevation (Overflow) | 132.00 ft |

| Infiltration | |
|---|---|
| Infiltration Method (Computed) | No Infiltration |

| Initial Conditions | |
|---|---|
| Elevation (Starting Water Surface) | 130.00 ft |
| Volume (Starting, per section) | 0.000 ac-ft |
| Flow (Out Starting) | 0.00 ft³/s |
| Infiltration (Starting, per section) | 0.00 ft³/s |
| Flow (Total Out Starting) | 0.00 ft³/s |
| Time Increment | 0.005 hours |

**Number of sections = 11**
**Storage, Area, Infiltration (per 47.68 ft section)**

| Elevation (ft) | Outflow (ft³/s) | Storage (ac-ft) | Area (acres) | Infiltration (ft³/s) | Flow (Total) (ft³/s) | 2S/t + O (ft³/s) |
|---|---|---|---|---|---|---|
| 130.00 | 0.00 | 0.000 | 0.000 | 0.00 | 0.00 | 0.00 |
| 130.01 | 0.01 | 0.000 | 0.003 | 0.00 | 0.01 | 0.17 |
| 130.04 | 0.10 | 0.000 | 0.004 | 0.00 | 0.10 | 0.76 |
| 130.08 | 0.31 | 0.000 | 0.004 | 0.00 | 0.31 | 1.69 |
| 130.12 | 0.62 | 0.000 | 0.004 | 0.00 | 0.62 | 2.76 |
| 130.16 | 1.02 | 0.001 | 0.004 | 0.00 | 1.02 | 3.97 |
| 130.20 | 1.50 | 0.001 | 0.005 | 0.00 | 1.50 | 5.32 |
| 130.24 | 2.07 | 0.001 | 0.005 | 0.00 | 2.07 | 6.80 |
| 130.28 | 2.72 | 0.001 | 0.005 | 0.00 | 2.72 | 8.42 |
| 130.32 | 3.46 | 0.001 | 0.005 | 0.00 | 3.46 | 10.17 |
| 130.36 | 4.28 | 0.002 | 0.006 | 0.00 | 4.28 | 12.06 |
| 130.40 | 5.19 | 0.002 | 0.006 | 0.00 | 5.19 | 14.09 |
| 130.44 | 6.19 | 0.002 | 0.006 | 0.00 | 6.19 | 16.26 |
| 130.48 | 7.28 | 0.002 | 0.006 | 0.00 | 7.28 | 18.57 |
| 130.52 | 8.46 | 0.003 | 0.007 | 0.00 | 8.46 | 21.03 |
| 130.56 | 9.74 | 0.003 | 0.007 | 0.00 | 9.74 | 23.63 |
| 130.60 | 11.11 | 0.003 | 0.007 | 0.00 | 11.11 | 26.37 |
| 130.64 | 12.59 | 0.003 | 0.007 | 0.00 | 12.59 | 29.27 |

**Number of sections = 11**
**Storage, Area, Infiltration (per 47.68 ft section)**

| Elevation (ft) | Outflow ($ft^3/s$) | Storage (ac-ft) | Area (acres) | Infiltration ($ft^3/s$) | Flow (Total) ($ft^3/s$) | 2S/t + O ($ft^3/s$) |
|---|---|---|---|---|---|---|
| 130.68 | 14.16 | 0.004 | 0.008 | 0.00 | 14.16 | 32.32 |
| 130.72 | 15.83 | 0.004 | 0.008 | 0.00 | 15.83 | 35.52 |
| 130.76 | 17.61 | 0.004 | 0.008 | 0.00 | 17.61 | 38.87 |
| 130.80 | 19.50 | 0.005 | 0.009 | 0.00 | 19.50 | 42.38 |
| 130.84 | 21.49 | 0.005 | 0.009 | 0.00 | 21.49 | 46.05 |
| 130.88 | 23.59 | 0.005 | 0.009 | 0.00 | 23.59 | 49.89 |
| 130.92 | 25.81 | 0.006 | 0.009 | 0.00 | 25.81 | 53.88 |
| 130.96 | 28.14 | 0.006 | 0.010 | 0.00 | 28.14 | 58.04 |
| 131.00 | 30.58 | 0.007 | 0.010 | 0.00 | 30.58 | 62.37 |
| 131.04 | 33.15 | 0.007 | 0.010 | 0.00 | 33.15 | 66.87 |
| 131.08 | 35.83 | 0.007 | 0.010 | 0.00 | 35.83 | 71.54 |
| 131.12 | 38.64 | 0.008 | 0.011 | 0.00 | 38.64 | 76.38 |
| 131.16 | 41.57 | 0.008 | 0.011 | 0.00 | 41.57 | 81.40 |
| 131.20 | 44.63 | 0.009 | 0.011 | 0.00 | 44.63 | 86.59 |
| 131.24 | 47.81 | 0.009 | 0.011 | 0.00 | 47.81 | 91.96 |
| 131.28 | 51.13 | 0.010 | 0.012 | 0.00 | 51.13 | 97.52 |
| 131.32 | 54.58 | 0.010 | 0.012 | 0.00 | 54.58 | 103.25 |
| 131.36 | 58.16 | 0.011 | 0.012 | 0.00 | 58.16 | 109.17 |
| 131.40 | 61.87 | 0.011 | 0.012 | 0.00 | 61.87 | 115.28 |
| 131.44 | 65.73 | 0.012 | 0.013 | 0.00 | 65.73 | 121.57 |
| 131.48 | 69.72 | 0.012 | 0.013 | 0.00 | 69.72 | 128.06 |
| 131.52 | 73.86 | 0.013 | 0.013 | 0.00 | 73.86 | 134.74 |
| 131.56 | 78.13 | 0.013 | 0.014 | 0.00 | 78.13 | 141.61 |
| 131.60 | 82.56 | 0.014 | 0.014 | 0.00 | 82.56 | 148.68 |
| 131.64 | 87.12 | 0.014 | 0.014 | 0.00 | 87.12 | 155.94 |
| 131.68 | 91.84 | 0.015 | 0.014 | 0.00 | 91.84 | 163.40 |
| 131.72 | 96.71 | 0.015 | 0.015 | 0.00 | 96.71 | 171.07 |
| 131.76 | 101.73 | 0.016 | 0.015 | 0.00 | 101.73 | 178.94 |
| 131.80 | 106.90 | 0.017 | 0.015 | 0.00 | 106.90 | 187.01 |
| 131.84 | 112.23 | 0.017 | 0.015 | 0.00 | 112.23 | 195.29 |
| 131.88 | 117.72 | 0.018 | 0.016 | 0.00 | 117.72 | 203.78 |
| 131.92 | 123.37 | 0.018 | 0.016 | 0.00 | 123.37 | 212.48 |
| 131.96 | 129.17 | 0.019 | 0.016 | 0.00 | 129.17 | 221.38 |
| 132.00 | 135.14 | 0.020 | 0.016 | 0.00 | 135.14 | 230.51 |

Subsection: Channel Routing Summary
Label: CO-28

Return Event: 25 years
Storm Event: 25 yr

| Modified Puls Results Summary | |
|---|---|
| Length (Channel) | 524.51 ft |
| Travel Time (Channel) | 0.054 hours |
| Number of Sections | 11 |
| Length (Section) | 47.68 ft |
| Flow (Weighted) | 3.35 ft³/s |
| Overflow Channel | No Overflow Data |
| Elevation (Overflow) | 132.00 ft |

| Infiltration | |
|---|---|
| Infiltration Method (Computed) | No Infiltration |

| Initial Conditions | |
|---|---|
| Elevation (Starting Water Surface) | 130.00 ft |
| Volume (Starting, per section) | 0.000 ac-ft |
| Flow (Out Starting) | 0.00 ft³/s |
| Infiltration (Starting, per section) | 0.00 ft³/s |
| Flow (Total Out Starting) | 0.00 ft³/s |
| Time Increment | 0.005 hours |

| Inflow/Outflow Hydrograph Summary | | | |
|---|---|---|---|
| Flow (Peak In) | 9.75 ft³/s | Time to Peak (In) | 12.025 hours |
| Flow (Peak Out) | 9.74 ft³/s | Time to Peak (Out) | 12.045 hours |

| Mass Balance (ac-ft) | |
|---|---|
| Volume (Initial) | 0.000 ac-ft |
| Volume (Total Inflow) | 0.634 ac-ft |
| Volume (Total Infiltration) | 0.000 ac-ft |
| Volume (Total Outlet Outflow) | 0.634 ac-ft |
| Volume (Retained) | 0.001 ac-ft |
| Volume (Unrouted) | 0.001 ac-ft |
| Error (Mass Balance) | 0.1 % |

| Modified Puls Results Summary | |
|---|---|
| Length (Channel) | 245.95 ft |
| Travel Time (Channel) | 0.020 hours |
| Number of Sections | 1 |
| Length (Section) | 245.95 ft |
| Flow (Weighted) | 2.85 ft³/s |
| Overflow Channel | No Overflow Data |
| Elevation (Overflow) | 131.00 ft |

| Infiltration | |
|---|---|
| Infiltration Method (Computed) | No Infiltration |

| Initial Conditions | |
|---|---|
| Elevation (Starting Water Surface) | 129.00 ft |
| Volume (Starting, per section) | 0.000 ac-ft |
| Flow (Out Starting) | 0.00 ft³/s |
| Infiltration (Starting, per section) | 0.00 ft³/s |
| Flow (Total Out Starting) | 0.00 ft³/s |
| Time Increment | 0.005 hours |

**Number of sections = 1**
**Storage, Area, Infiltration (per 245.95 ft section)**

| Elevation (ft) | Outflow (ft³/s) | Storage (ac-ft) | Area (acres) | Infiltration (ft³/s) | Flow (Total) (ft³/s) | 2S/t + O (ft³/s) |
|---|---|---|---|---|---|---|
| 129.00 | 0.00 | 0.000 | 0.000 | 0.00 | 0.00 | 0.00 |
| 129.01 | 0.01 | 0.000 | 0.017 | 0.00 | 0.01 | 0.84 |
| 129.04 | 0.15 | 0.001 | 0.018 | 0.00 | 0.15 | 3.56 |
| 129.08 | 0.48 | 0.001 | 0.020 | 0.00 | 0.48 | 7.56 |
| 129.12 | 0.95 | 0.002 | 0.021 | 0.00 | 0.95 | 11.97 |
| 129.16 | 1.56 | 0.003 | 0.022 | 0.00 | 1.56 | 16.78 |
| 129.20 | 2.30 | 0.004 | 0.024 | 0.00 | 2.30 | 21.98 |
| 129.24 | 3.17 | 0.005 | 0.025 | 0.00 | 3.17 | 27.57 |
| 129.28 | 4.17 | 0.006 | 0.026 | 0.00 | 4.17 | 33.55 |
| 129.32 | 5.30 | 0.007 | 0.028 | 0.00 | 5.30 | 39.93 |
| 129.36 | 6.56 | 0.008 | 0.029 | 0.00 | 6.56 | 46.70 |
| 129.40 | 7.95 | 0.009 | 0.030 | 0.00 | 7.95 | 53.86 |
| 129.44 | 9.48 | 0.011 | 0.032 | 0.00 | 9.48 | 61.43 |
| 129.48 | 11.15 | 0.012 | 0.033 | 0.00 | 11.15 | 69.39 |
| 129.52 | 12.96 | 0.013 | 0.035 | 0.00 | 12.96 | 77.76 |
| 129.56 | 14.92 | 0.015 | 0.036 | 0.00 | 14.92 | 86.54 |
| 129.60 | 17.02 | 0.016 | 0.037 | 0.00 | 17.02 | 95.73 |
| 129.64 | 19.28 | 0.018 | 0.039 | 0.00 | 19.28 | 105.33 |

**Number of sections = 1**
**Storage, Area, Infiltration (per 245.95 ft section)**

| Elevation (ft) | Outflow ($ft^3/s$) | Storage (ac-ft) | Area (acres) | Infiltration ($ft^3/s$) | Flow (Total) ($ft^3/s$) | 2S/t + O ($ft^3/s$) |
|---|---|---|---|---|---|---|
| 129.68 | 21.68 | 0.019 | 0.040 | 0.00 | 21.68 | 115.34 |
| 129.72 | 24.25 | 0.021 | 0.041 | 0.00 | 24.25 | 125.78 |
| 129.76 | 26.97 | 0.023 | 0.043 | 0.00 | 26.97 | 136.63 |
| 129.80 | 29.86 | 0.024 | 0.044 | 0.00 | 29.86 | 147.91 |
| 129.84 | 32.91 | 0.026 | 0.045 | 0.00 | 32.91 | 159.62 |
| 129.88 | 36.13 | 0.028 | 0.047 | 0.00 | 36.13 | 171.77 |
| 129.92 | 39.53 | 0.030 | 0.048 | 0.00 | 39.53 | 184.34 |
| 129.96 | 43.10 | 0.032 | 0.049 | 0.00 | 43.10 | 197.35 |
| 130.00 | 46.84 | 0.034 | 0.051 | 0.00 | 46.84 | 210.81 |
| 130.04 | 50.77 | 0.036 | 0.052 | 0.00 | 50.77 | 224.71 |
| 130.08 | 54.88 | 0.038 | 0.054 | 0.00 | 54.88 | 239.05 |
| 130.12 | 59.18 | 0.040 | 0.055 | 0.00 | 59.18 | 253.84 |
| 130.16 | 63.67 | 0.042 | 0.056 | 0.00 | 63.67 | 269.09 |
| 130.20 | 68.36 | 0.045 | 0.058 | 0.00 | 68.36 | 284.79 |
| 130.24 | 73.23 | 0.047 | 0.059 | 0.00 | 73.23 | 300.95 |
| 130.28 | 78.31 | 0.049 | 0.060 | 0.00 | 78.31 | 317.57 |
| 130.32 | 83.59 | 0.052 | 0.062 | 0.00 | 83.59 | 334.66 |
| 130.36 | 89.08 | 0.054 | 0.063 | 0.00 | 89.08 | 352.21 |
| 130.40 | 94.77 | 0.057 | 0.064 | 0.00 | 94.77 | 370.23 |
| 130.44 | 100.67 | 0.060 | 0.066 | 0.00 | 100.67 | 388.72 |
| 130.48 | 106.79 | 0.062 | 0.067 | 0.00 | 106.79 | 407.70 |
| 130.52 | 113.12 | 0.065 | 0.068 | 0.00 | 113.12 | 427.15 |
| 130.56 | 119.67 | 0.068 | 0.070 | 0.00 | 119.67 | 447.08 |
| 130.60 | 126.44 | 0.070 | 0.071 | 0.00 | 126.44 | 467.49 |
| 130.64 | 133.44 | 0.073 | 0.072 | 0.00 | 133.44 | 488.39 |
| 130.68 | 140.67 | 0.076 | 0.074 | 0.00 | 140.67 | 509.79 |
| 130.72 | 148.12 | 0.079 | 0.075 | 0.00 | 148.12 | 531.67 |
| 130.76 | 155.81 | 0.082 | 0.077 | 0.00 | 155.81 | 554.05 |
| 130.80 | 163.74 | 0.085 | 0.078 | 0.00 | 163.74 | 576.93 |
| 130.84 | 171.90 | 0.089 | 0.079 | 0.00 | 171.90 | 600.31 |
| 130.88 | 180.30 | 0.092 | 0.081 | 0.00 | 180.30 | 624.19 |
| 130.92 | 188.95 | 0.095 | 0.082 | 0.00 | 188.95 | 648.58 |
| 130.96 | 197.84 | 0.098 | 0.083 | 0.00 | 197.84 | 673.47 |
| 131.00 | 206.99 | 0.102 | 0.085 | 0.00 | 206.99 | 698.88 |

Subsection: Channel Routing Summary
Label: CO-45

Return Event: 25 years
Storm Event: 25 yr

| Modified Puls Results Summary | |
|---|---|
| Length (Channel) | 245.95 ft |
| Travel Time (Channel) | 0.020 hours |
| Number of Sections | 1 |
| Length (Section) | 245.95 ft |
| Flow (Weighted) | 2.85 ft³/s |
| Overflow Channel | No Overflow Data |
| Elevation (Overflow) | 131.00 ft |

| Infiltration | |
|---|---|
| Infiltration Method (Computed) | No Infiltration |

| Initial Conditions | |
|---|---|
| Elevation (Starting Water Surface) | 129.00 ft |
| Volume (Starting, per section) | 0.000 ac-ft |
| Flow (Out Starting) | 0.00 ft³/s |
| Infiltration (Starting, per section) | 0.00 ft³/s |
| Flow (Total Out Starting) | 0.00 ft³/s |
| Time Increment | 0.005 hours |

| Inflow/Outflow Hydrograph Summary | | | |
|---|---|---|---|
| Flow (Peak In) | 8.40 ft³/s | Time to Peak (In) | 11.995 hours |
| Flow (Peak Out) | 8.36 ft³/s | Time to Peak (Out) | 12.000 hours |

| Mass Balance (ac-ft) | |
|---|---|
| Volume (Initial) | 0.000 ac-ft |
| Volume (Total Inflow) | 0.507 ac-ft |
| Volume (Total Infiltration) | 0.000 ac-ft |
| Volume (Total Outlet Outflow) | 0.506 ac-ft |
| Volume (Retained) | 0.001 ac-ft |
| Volume (Unrouted) | 0.000 ac-ft |
| Error (Mass Balance) | 0.0 % |

Subsection: Elevation-Volume-Flow Table (Channel)
Label: CO-49

Return Event: 25 years
Storm Event: 25 yr

| Modified Puls Results Summary | |
|---|---|
| Length (Channel) | 156.31 ft |
| Travel Time (Channel) | 0.022 hours |
| Number of Sections | 1 |
| Length (Section) | 156.31 ft |
| Flow (Weighted) | 1.06 ft³/s |
| Overflow Channel | No Overflow Data |
| Elevation (Overflow) | 121.00 ft |

| Infiltration | |
|---|---|
| Infiltration Method (Computed) | No Infiltration |

| Initial Conditions | |
|---|---|
| Elevation (Starting Water Surface) | 120.00 ft |
| Volume (Starting, per section) | 0.000 ac-ft |
| Flow (Out Starting) | 0.00 ft³/s |
| Infiltration (Starting, per section) | 0.00 ft³/s |
| Flow (Total Out Starting) | 0.00 ft³/s |
| Time Increment | 0.005 hours |

**Number of sections = 1**
**Storage, Area, Infiltration (per 156.31 ft section)**

| Elevation (ft) | Outflow (ft³/s) | Storage (ac-ft) | Area (acres) | Infiltration (ft³/s) | Flow (Total) (ft³/s) | 2S/t + O (ft³/s) |
|---|---|---|---|---|---|---|
| 120.00 | 0.00 | 0.000 | 0.000 | 0.00 | 0.00 | 0.00 |
| 120.01 | 0.00 | 0.000 | 0.000 | 0.00 | 0.00 | 0.01 |
| 120.02 | 0.00 | 0.000 | 0.000 | 0.00 | 0.00 | 0.02 |
| 120.04 | 0.00 | 0.000 | 0.001 | 0.00 | 0.00 | 0.09 |
| 120.06 | 0.01 | 0.000 | 0.001 | 0.00 | 0.01 | 0.19 |
| 120.08 | 0.01 | 0.000 | 0.002 | 0.00 | 0.01 | 0.35 |
| 120.10 | 0.02 | 0.000 | 0.002 | 0.00 | 0.02 | 0.54 |
| 120.12 | 0.04 | 0.000 | 0.003 | 0.00 | 0.04 | 0.79 |
| 120.14 | 0.05 | 0.000 | 0.003 | 0.00 | 0.05 | 1.08 |
| 120.16 | 0.08 | 0.000 | 0.003 | 0.00 | 0.08 | 1.41 |
| 120.18 | 0.11 | 0.000 | 0.004 | 0.00 | 0.11 | 1.79 |
| 120.20 | 0.14 | 0.000 | 0.004 | 0.00 | 0.14 | 2.22 |
| 120.22 | 0.18 | 0.001 | 0.005 | 0.00 | 0.18 | 2.70 |
| 120.24 | 0.23 | 0.001 | 0.005 | 0.00 | 0.23 | 3.23 |
| 120.26 | 0.28 | 0.001 | 0.006 | 0.00 | 0.28 | 3.80 |
| 120.28 | 0.34 | 0.001 | 0.006 | 0.00 | 0.34 | 4.43 |
| 120.30 | 0.41 | 0.001 | 0.006 | 0.00 | 0.41 | 5.10 |
| 120.32 | 0.49 | 0.001 | 0.007 | 0.00 | 0.49 | 5.83 |

**Number of sections = 1**
**Storage, Area, Infiltration (per 156.31 ft section)**

| Elevation (ft) | Outflow ($ft^3/s$) | Storage (ac-ft) | Area (acres) | Infiltration ($ft^3/s$) | Flow (Total) ($ft^3/s$) | 2S/t + O ($ft^3/s$) |
|---|---|---|---|---|---|---|
| 120.34 | 0.58 | 0.001 | 0.007 | 0.00 | 0.58 | 6.60 |
| 120.36 | 0.67 | 0.001 | 0.008 | 0.00 | 0.67 | 7.42 |
| 120.38 | 0.77 | 0.002 | 0.008 | 0.00 | 0.77 | 8.30 |
| 120.40 | 0.89 | 0.002 | 0.009 | 0.00 | 0.89 | 9.22 |
| 120.42 | 1.01 | 0.002 | 0.009 | 0.00 | 1.01 | 10.20 |
| 120.44 | 1.14 | 0.002 | 0.009 | 0.00 | 1.14 | 11.23 |
| 120.46 | 1.29 | 0.002 | 0.010 | 0.00 | 1.29 | 12.31 |
| 120.48 | 1.44 | 0.002 | 0.010 | 0.00 | 1.44 | 13.45 |
| 120.50 | 1.61 | 0.003 | 0.011 | 0.00 | 1.61 | 14.64 |
| 120.52 | 1.79 | 0.003 | 0.011 | 0.00 | 1.79 | 15.88 |
| 120.54 | 1.98 | 0.003 | 0.012 | 0.00 | 1.98 | 17.17 |
| 120.56 | 2.18 | 0.003 | 0.012 | 0.00 | 2.18 | 18.52 |
| 120.58 | 2.39 | 0.004 | 0.012 | 0.00 | 2.39 | 19.92 |
| 120.60 | 2.62 | 0.004 | 0.013 | 0.00 | 2.62 | 21.37 |
| 120.62 | 2.86 | 0.004 | 0.013 | 0.00 | 2.86 | 22.89 |
| 120.64 | 3.11 | 0.004 | 0.014 | 0.00 | 3.11 | 24.45 |
| 120.66 | 3.38 | 0.005 | 0.014 | 0.00 | 3.38 | 26.07 |
| 120.68 | 3.66 | 0.005 | 0.015 | 0.00 | 3.66 | 27.75 |
| 120.70 | 3.95 | 0.005 | 0.015 | 0.00 | 3.95 | 29.48 |
| 120.72 | 4.26 | 0.006 | 0.016 | 0.00 | 4.26 | 31.27 |
| 120.74 | 4.58 | 0.006 | 0.016 | 0.00 | 4.58 | 33.11 |
| 120.76 | 4.92 | 0.006 | 0.016 | 0.00 | 4.92 | 35.01 |
| 120.78 | 5.27 | 0.007 | 0.017 | 0.00 | 5.27 | 36.97 |
| 120.80 | 5.64 | 0.007 | 0.017 | 0.00 | 5.64 | 38.98 |
| 120.82 | 6.02 | 0.007 | 0.018 | 0.00 | 6.02 | 41.06 |
| 120.84 | 6.42 | 0.008 | 0.018 | 0.00 | 6.42 | 43.19 |
| 120.86 | 6.84 | 0.008 | 0.019 | 0.00 | 6.84 | 45.37 |
| 120.88 | 7.27 | 0.008 | 0.019 | 0.00 | 7.27 | 47.62 |
| 120.90 | 7.72 | 0.009 | 0.019 | 0.00 | 7.72 | 49.92 |
| 120.92 | 8.18 | 0.009 | 0.020 | 0.00 | 8.18 | 52.28 |
| 120.94 | 8.67 | 0.010 | 0.020 | 0.00 | 8.67 | 54.71 |
| 120.96 | 9.17 | 0.010 | 0.021 | 0.00 | 9.17 | 57.19 |
| 120.98 | 9.69 | 0.010 | 0.021 | 0.00 | 9.69 | 59.73 |
| 121.00 | 10.22 | 0.011 | 0.022 | 0.00 | 10.22 | 62.33 |

Subsection: Channel Routing Summary
Label: CO-49

Return Event: 25 years
Storm Event: 25 yr

| Modified Puls Results Summary | |
|---|---|
| Length (Channel) | 156.31 ft |
| Travel Time (Channel) | 0.022 hours |
| Number of Sections | 1 |
| Length (Section) | 156.31 ft |
| Flow (Weighted) | 1.06 ft³/s |
| Overflow Channel | No Overflow Data |
| Elevation (Overflow) | 121.00 ft |

| Infiltration | |
|---|---|
| Infiltration Method (Computed) | No Infiltration |

| Initial Conditions | |
|---|---|
| Elevation (Starting Water Surface) | 120.00 ft |
| Volume (Starting, per section) | 0.000 ac-ft |
| Flow (Out Starting) | 0.00 ft³/s |
| Infiltration (Starting, per section) | 0.00 ft³/s |
| Flow (Total Out Starting) | 0.00 ft³/s |
| Time Increment | 0.005 hours |

| Inflow/Outflow Hydrograph Summary | | | |
|---|---|---|---|
| Flow (Peak In) | 3.11 ft³/s | Time to Peak (In) | 12.005 hours |
| Flow (Peak Out) | 3.08 ft³/s | Time to Peak (Out) | 12.020 hours |

| Mass Balance (ac-ft) | |
|---|---|
| Volume (Initial) | 0.000 ac-ft |
| Volume (Total Inflow) | 0.192 ac-ft |
| Volume (Total Infiltration) | 0.000 ac-ft |
| Volume (Total Outlet Outflow) | 0.192 ac-ft |
| Volume (Retained) | 0.000 ac-ft |
| Volume (Unrouted) | 0.000 ac-ft |
| Error (Mass Balance) | 0.0 % |

| Modified Puls Results Summary | |
|---|---|
| Length (Channel) | 312.17 ft |
| Travel Time (Channel) | 0.024 hours |
| Number of Sections | 1 |
| Length (Section) | 312.17 ft |
| Flow (Weighted) | 6.93 ft³/s |
| Overflow Channel | No Overflow Data |
| Elevation (Overflow) | 134.00 ft |

| Infiltration | |
|---|---|
| Infiltration Method (Computed) | No Infiltration |

| Initial Conditions | |
|---|---|
| Elevation (Starting Water Surface) | 132.00 ft |
| Volume (Starting, per section) | 0.000 ac-ft |
| Flow (Out Starting) | 0.00 ft³/s |
| Infiltration (Starting, per section) | 0.00 ft³/s |
| Flow (Total Out Starting) | 0.00 ft³/s |
| Time Increment | 0.005 hours |

**Number of sections = 1**
**Storage, Area, Infiltration (per 312.17 ft section)**

| Elevation (ft) | Outflow (ft³/s) | Storage (ac-ft) | Area (acres) | Infiltration (ft³/s) | Flow (Total) (ft³/s) | 2S/t + O (ft³/s) |
|---|---|---|---|---|---|---|
| 132.00 | 0.00 | 0.000 | 0.000 | 0.00 | 0.00 | 0.00 |
| 132.01 | 0.00 | 0.000 | 0.000 | 0.00 | 0.00 | 0.01 |
| 132.04 | 0.00 | 0.000 | 0.002 | 0.00 | 0.00 | 0.17 |
| 132.08 | 0.01 | 0.000 | 0.003 | 0.00 | 0.01 | 0.68 |
| 132.12 | 0.04 | 0.000 | 0.005 | 0.00 | 0.04 | 1.54 |
| 132.16 | 0.09 | 0.001 | 0.007 | 0.00 | 0.09 | 2.76 |
| 132.20 | 0.17 | 0.001 | 0.009 | 0.00 | 0.17 | 4.33 |
| 132.24 | 0.28 | 0.001 | 0.010 | 0.00 | 0.28 | 6.27 |
| 132.28 | 0.42 | 0.002 | 0.012 | 0.00 | 0.42 | 8.58 |
| 132.32 | 0.60 | 0.002 | 0.014 | 0.00 | 0.60 | 11.26 |
| 132.36 | 0.82 | 0.003 | 0.015 | 0.00 | 0.82 | 14.31 |
| 132.40 | 1.09 | 0.003 | 0.017 | 0.00 | 1.09 | 17.74 |
| 132.44 | 1.40 | 0.004 | 0.019 | 0.00 | 1.40 | 21.55 |
| 132.48 | 1.77 | 0.005 | 0.021 | 0.00 | 1.77 | 25.74 |
| 132.52 | 2.19 | 0.006 | 0.022 | 0.00 | 2.19 | 30.33 |
| 132.56 | 2.67 | 0.007 | 0.024 | 0.00 | 2.67 | 35.30 |
| 132.60 | 3.21 | 0.008 | 0.026 | 0.00 | 3.21 | 40.67 |
| 132.64 | 3.81 | 0.009 | 0.028 | 0.00 | 3.81 | 46.43 |

**Number of sections = 1**
**Storage, Area, Infiltration (per 312.17 ft section)**

| Elevation (ft) | Outflow ($ft^3/s$) | Storage (ac-ft) | Area (acres) | Infiltration ($ft^3/s$) | Flow (Total) ($ft^3/s$) | 2S/t + O ($ft^3/s$) |
|---|---|---|---|---|---|---|
| 132.68 | 4.48 | 0.010 | 0.029 | 0.00 | 4.48 | 52.60 |
| 132.72 | 5.22 | 0.011 | 0.031 | 0.00 | 5.22 | 59.16 |
| 132.76 | 6.03 | 0.012 | 0.033 | 0.00 | 6.03 | 66.13 |
| 132.80 | 6.91 | 0.014 | 0.034 | 0.00 | 6.91 | 73.51 |
| 132.84 | 7.87 | 0.015 | 0.036 | 0.00 | 7.87 | 81.29 |
| 132.88 | 8.91 | 0.017 | 0.038 | 0.00 | 8.91 | 89.49 |
| 132.92 | 10.03 | 0.018 | 0.040 | 0.00 | 10.03 | 98.11 |
| 132.96 | 11.24 | 0.020 | 0.041 | 0.00 | 11.24 | 107.14 |
| 133.00 | 12.53 | 0.022 | 0.043 | 0.00 | 12.53 | 116.59 |
| 133.04 | 13.91 | 0.023 | 0.045 | 0.00 | 13.91 | 126.46 |
| 133.08 | 15.38 | 0.025 | 0.046 | 0.00 | 15.38 | 136.76 |
| 133.12 | 16.95 | 0.027 | 0.048 | 0.00 | 16.95 | 147.48 |
| 133.16 | 18.61 | 0.029 | 0.050 | 0.00 | 18.61 | 158.63 |
| 133.20 | 20.37 | 0.031 | 0.052 | 0.00 | 20.37 | 170.22 |
| 133.24 | 22.24 | 0.033 | 0.053 | 0.00 | 22.24 | 182.23 |
| 133.28 | 24.20 | 0.035 | 0.055 | 0.00 | 24.20 | 194.69 |
| 133.32 | 26.27 | 0.037 | 0.057 | 0.00 | 26.27 | 207.58 |
| 133.36 | 28.45 | 0.040 | 0.058 | 0.00 | 28.45 | 220.91 |
| 133.40 | 30.73 | 0.042 | 0.060 | 0.00 | 30.73 | 234.69 |
| 133.44 | 33.13 | 0.045 | 0.062 | 0.00 | 33.13 | 248.90 |
| 133.48 | 35.64 | 0.047 | 0.064 | 0.00 | 35.64 | 263.57 |
| 133.52 | 38.27 | 0.050 | 0.065 | 0.00 | 38.27 | 278.68 |
| 133.56 | 41.01 | 0.052 | 0.067 | 0.00 | 41.01 | 294.25 |
| 133.60 | 43.88 | 0.055 | 0.069 | 0.00 | 43.88 | 310.27 |
| 133.64 | 46.87 | 0.058 | 0.071 | 0.00 | 46.87 | 326.74 |
| 133.68 | 49.98 | 0.061 | 0.072 | 0.00 | 49.98 | 343.67 |
| 133.72 | 53.21 | 0.064 | 0.074 | 0.00 | 53.21 | 361.05 |
| 133.76 | 56.58 | 0.067 | 0.076 | 0.00 | 56.58 | 378.90 |
| 133.80 | 60.07 | 0.070 | 0.077 | 0.00 | 60.07 | 397.22 |
| 133.84 | 63.70 | 0.073 | 0.079 | 0.00 | 63.70 | 415.99 |
| 133.88 | 67.46 | 0.076 | 0.081 | 0.00 | 67.46 | 435.24 |
| 133.92 | 71.35 | 0.079 | 0.083 | 0.00 | 71.35 | 454.95 |
| 133.96 | 75.38 | 0.083 | 0.084 | 0.00 | 75.38 | 475.13 |
| 134.00 | 79.56 | 0.086 | 0.086 | 0.00 | 79.56 | 495.79 |

Subsection: Channel Routing Summary
Label: CO-89

Return Event: 25 years
Storm Event: 25 yr

| Modified Puls Results Summary | |
|---|---|
| Length (Channel) | 312.17 ft |
| Travel Time (Channel) | 0.024 hours |
| Number of Sections | 1 |
| Length (Section) | 312.17 ft |
| Flow (Weighted) | 6.93 ft³/s |
| Overflow Channel | No Overflow Data |
| Elevation (Overflow) | 134.00 ft |

| Infiltration | |
|---|---|
| Infiltration Method (Computed) | No Infiltration |

| Initial Conditions | |
|---|---|
| Elevation (Starting Water Surface) | 132.00 ft |
| Volume (Starting, per section) | 0.000 ac-ft |
| Flow (Out Starting) | 0.00 ft³/s |
| Infiltration (Starting, per section) | 0.00 ft³/s |
| Flow (Total Out Starting) | 0.00 ft³/s |
| Time Increment | 0.005 hours |

| Inflow/Outflow Hydrograph Summary | | | |
|---|---|---|---|
| Flow (Peak In) | 19.96 ft³/s | Time to Peak (In) | 12.050 hours |
| Flow (Peak Out) | 19.84 ft³/s | Time to Peak (Out) | 12.055 hours |

| Mass Balance (ac-ft) | |
|---|---|
| Volume (Initial) | 0.000 ac-ft |
| Volume (Total Inflow) | 1.358 ac-ft |
| Volume (Total Infiltration) | 0.000 ac-ft |
| Volume (Total Outlet Outflow) | 1.356 ac-ft |
| Volume (Retained) | 0.001 ac-ft |
| Volume (Unrouted) | 0.000 ac-ft |
| Error (Mass Balance) | 0.0 % |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 0.000 | 130.00 | 130.03 | 130.03 | 130.03 | 130.03 |
| 0.025 | 130.03 | 130.03 | 130.03 | 130.03 | 130.03 |
| 0.050 | 130.03 | 130.03 | 130.03 | 130.03 | 130.03 |
| 0.075 | 130.03 | 130.03 | 130.03 | 130.03 | 130.03 |
| 0.100 | 130.03 | 130.03 | 130.03 | 130.02 | 130.02 |
| 0.125 | 130.02 | 130.02 | 130.02 | 130.02 | 130.02 |
| 0.150 | 130.02 | 130.02 | 130.02 | 130.01 | 130.01 |
| 0.175 | 130.01 | 130.01 | 130.01 | 130.01 | 130.01 |
| 0.200 | 130.01 | 130.01 | 130.01 | 130.01 | 130.01 |
| 0.225 | 130.01 | 130.01 | 130.01 | 130.01 | 130.01 |
| 0.250 | 130.01 | 130.01 | 130.01 | 130.01 | 130.01 |
| 0.275 | 130.01 | 130.01 | 130.01 | 130.01 | 130.01 |
| 0.300 | 130.01 | 130.01 | 130.01 | 130.01 | 130.01 |
| 0.325 | 130.01 | 130.01 | 130.01 | 130.01 | 130.01 |
| 0.350 | 130.01 | 130.01 | 130.01 | 130.01 | 130.01 |
| 0.375 | 130.01 | 130.01 | 130.01 | 130.01 | 130.01 |
| 0.400 | 130.01 | 130.01 | 130.01 | 130.01 | 130.01 |
| 0.425 | 130.01 | 130.01 | 130.01 | 130.01 | 130.01 |
| 0.450 | 130.01 | 130.00 | 130.00 | 130.00 | 130.00 |
| 0.475 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 0.500 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 0.525 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 0.550 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 0.575 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 0.600 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 0.625 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 0.650 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 0.675 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 0.700 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 0.725 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 0.750 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 0.775 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 0.800 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 0.825 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 0.850 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 0.875 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 0.900 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 0.925 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 0.950 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 0.975 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 1.000 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 1.025 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 1.050 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 1.075 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 1.100 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 1.125 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 1.150 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 1.175 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 1.200 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 1.225 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 1.250 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 1.275 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 1.300 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 1.325 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 1.350 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 1.375 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 1.400 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 1.425 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 1.450 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 1.475 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 1.500 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 1.525 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 1.550 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 1.575 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 1.600 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 1.625 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 1.650 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 1.675 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 1.700 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 1.725 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 1.750 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 1.775 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 1.800 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 1.825 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 1.850 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 1.875 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 1.900 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 1.925 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 1.950 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 1.975 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 2.000 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 2.025 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 2.050 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 2.075 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 2.100 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 2.125 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 2.150 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 2.175 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 2.200 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 2.225 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 2.250 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 2.275 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 2.300 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 2.325 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 2.350 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 2.375 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 2.400 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 2.425 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 2.450 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 2.475 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 2.500 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 2.525 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 2.550 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 2.575 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 2.600 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 2.625 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 2.650 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 2.675 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 2.700 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 2.725 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 2.750 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 2.775 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 2.800 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 2.825 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 2.850 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 2.875 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 2.900 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 2.925 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 2.950 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 2.975 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 3.000 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 3.025 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 3.050 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 3.075 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 3.100 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 3.125 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 3.150 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 3.175 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 3.200 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 3.225 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 3.250 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 3.275 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 3.300 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 3.325 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 3.350 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 3.375 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 3.400 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 3.425 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 3.450 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 3.475 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 3.500 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 3.525 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 3.550 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 3.575 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 3.600 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 3.625 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 3.650 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 3.675 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 3.700 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 3.725 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 3.750 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 3.775 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 3.800 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 3.825 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 3.850 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 3.875 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 3.900 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 3.925 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 3.950 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 3.975 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 4.000 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 4.025 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 4.050 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 4.075 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 4.100 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 4.125 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 4.150 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 4.175 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 4.200 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 4.225 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 4.250 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 4.275 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 4.300 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 4.325 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 4.350 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 4.375 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 4.400 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 4.425 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 4.450 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 4.475 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 4.500 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 4.525 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 4.550 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 4.575 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 4.600 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 4.625 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 4.650 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 4.675 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 4.700 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 4.725 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 4.750 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 4.775 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 4.800 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 4.825 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 4.850 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 4.875 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 4.900 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 4.925 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 4.950 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 4.975 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 5.000 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 5.025 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 5.050 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 5.075 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 5.100 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 5.125 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 5.150 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 5.175 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 5.200 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 5.225 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 5.250 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 5.275 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 5.300 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 5.325 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 5.350 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 5.375 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 5.400 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 5.425 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 5.450 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 5.475 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 5.500 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 5.525 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 5.550 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 5.575 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 5.600 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 5.625 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 5.650 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 5.675 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 5.700 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 5.725 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 5.750 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 5.775 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 5.800 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 5.825 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 5.850 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 5.875 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 5.900 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 5.925 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 5.950 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 5.975 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 6.000 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 6.025 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 6.050 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 6.075 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 6.100 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 6.125 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 6.150 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 6.175 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 6.200 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 6.225 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 6.250 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 6.275 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 6.300 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 6.325 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 6.350 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 6.375 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 6.400 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 6.425 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 6.450 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 6.475 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 6.500 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 6.525 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 6.550 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 6.575 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 6.600 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 6.625 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 6.650 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 6.675 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 6.700 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 6.725 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 6.750 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 6.775 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 6.800 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 6.825 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 6.850 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 6.875 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 6.900 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 6.925 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 6.950 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 6.975 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 7.000 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 7.025 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 7.050 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 7.075 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 7.100 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 7.125 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 7.150 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 7.175 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 7.200 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 7.225 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 7.250 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 7.275 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 7.300 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 7.325 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 7.350 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 7.375 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 7.400 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 7.425 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 7.450 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 7.475 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 7.500 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 7.525 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 7.550 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 7.575 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 7.600 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 7.625 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 7.650 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 7.675 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 7.700 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 7.725 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 7.750 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 7.775 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 7.800 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 7.825 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 7.850 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 7.875 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 7.900 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 7.925 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 7.950 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 7.975 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 8.000 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 8.025 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 8.050 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 8.075 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 8.100 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 8.125 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 8.150 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 8.175 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 8.200 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 8.225 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 8.250 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 8.275 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 8.300 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 8.325 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 8.350 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 8.375 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 8.400 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 8.425 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 8.450 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 8.475 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 8.500 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 8.525 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 8.550 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 8.575 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 8.600 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 8.625 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 8.650 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 8.675 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 8.700 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 8.725 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 8.750 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 8.775 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 8.800 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 8.825 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 8.850 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 8.875 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 8.900 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 8.925 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 8.950 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 8.975 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 9.000 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 9.025 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 9.050 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 9.075 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 9.100 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 9.125 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 9.150 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 9.175 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 9.200 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 9.225 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 9.250 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 9.275 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 9.300 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 9.325 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 9.350 | 130.00 | 130.00 | 130.00 | 130.00 | 130.00 |
| 9.375 | 130.01 | 130.01 | 130.01 | 130.01 | 130.01 |
| 9.400 | 130.01 | 130.01 | 130.01 | 130.01 | 130.01 |
| 9.425 | 130.01 | 130.01 | 130.01 | 130.01 | 130.01 |
| 9.450 | 130.01 | 130.01 | 130.01 | 130.01 | 130.01 |
| 9.475 | 130.01 | 130.01 | 130.01 | 130.01 | 130.01 |
| 9.500 | 130.01 | 130.01 | 130.01 | 130.01 | 130.01 |
| 9.525 | 130.01 | 130.01 | 130.01 | 130.01 | 130.01 |
| 9.550 | 130.01 | 130.01 | 130.01 | 130.01 | 130.02 |
| 9.575 | 130.02 | 130.02 | 130.02 | 130.02 | 130.02 |
| 9.600 | 130.02 | 130.02 | 130.02 | 130.02 | 130.02 |
| 9.625 | 130.02 | 130.02 | 130.02 | 130.02 | 130.02 |
| 9.650 | 130.02 | 130.02 | 130.02 | 130.02 | 130.02 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 9.675 | 130.02 | 130.02 | 130.02 | 130.02 | 130.02 |
| 9.700 | 130.02 | 130.02 | 130.02 | 130.02 | 130.02 |
| 9.725 | 130.02 | 130.02 | 130.02 | 130.02 | 130.02 |
| 9.750 | 130.02 | 130.02 | 130.02 | 130.02 | 130.02 |
| 9.775 | 130.02 | 130.02 | 130.02 | 130.02 | 130.02 |
| 9.800 | 130.02 | 130.02 | 130.02 | 130.02 | 130.02 |
| 9.825 | 130.02 | 130.02 | 130.02 | 130.02 | 130.02 |
| 9.850 | 130.02 | 130.02 | 130.02 | 130.02 | 130.02 |
| 9.875 | 130.02 | 130.02 | 130.02 | 130.02 | 130.02 |
| 9.900 | 130.02 | 130.02 | 130.02 | 130.02 | 130.02 |
| 9.925 | 130.02 | 130.02 | 130.02 | 130.02 | 130.02 |
| 9.950 | 130.02 | 130.02 | 130.02 | 130.02 | 130.02 |
| 9.975 | 130.02 | 130.02 | 130.02 | 130.02 | 130.02 |
| 10.000 | 130.02 | 130.02 | 130.02 | 130.02 | 130.02 |
| 10.025 | 130.02 | 130.02 | 130.02 | 130.02 | 130.02 |
| 10.050 | 130.02 | 130.02 | 130.02 | 130.02 | 130.02 |
| 10.075 | 130.02 | 130.03 | 130.03 | 130.03 | 130.03 |
| 10.100 | 130.03 | 130.03 | 130.03 | 130.03 | 130.03 |
| 10.125 | 130.03 | 130.03 | 130.03 | 130.03 | 130.03 |
| 10.150 | 130.03 | 130.03 | 130.03 | 130.03 | 130.03 |
| 10.175 | 130.03 | 130.03 | 130.03 | 130.03 | 130.03 |
| 10.200 | 130.03 | 130.03 | 130.03 | 130.03 | 130.03 |
| 10.225 | 130.03 | 130.03 | 130.03 | 130.03 | 130.03 |
| 10.250 | 130.03 | 130.03 | 130.03 | 130.03 | 130.03 |
| 10.275 | 130.03 | 130.03 | 130.03 | 130.03 | 130.03 |
| 10.300 | 130.03 | 130.03 | 130.03 | 130.03 | 130.03 |
| 10.325 | 130.03 | 130.03 | 130.03 | 130.03 | 130.03 |
| 10.350 | 130.03 | 130.03 | 130.03 | 130.03 | 130.03 |
| 10.375 | 130.03 | 130.03 | 130.03 | 130.03 | 130.03 |
| 10.400 | 130.04 | 130.04 | 130.04 | 130.04 | 130.04 |
| 10.425 | 130.04 | 130.04 | 130.04 | 130.04 | 130.04 |
| 10.450 | 130.04 | 130.04 | 130.04 | 130.04 | 130.04 |
| 10.475 | 130.04 | 130.04 | 130.04 | 130.04 | 130.04 |
| 10.500 | 130.04 | 130.04 | 130.04 | 130.04 | 130.04 |
| 10.525 | 130.04 | 130.04 | 130.04 | 130.04 | 130.04 |
| 10.550 | 130.04 | 130.04 | 130.04 | 130.04 | 130.04 |
| 10.575 | 130.04 | 130.04 | 130.04 | 130.04 | 130.04 |
| 10.600 | 130.04 | 130.04 | 130.04 | 130.04 | 130.04 |
| 10.625 | 130.04 | 130.04 | 130.04 | 130.04 | 130.04 |
| 10.650 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 10.675 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 10.700 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 10.725 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 10.750 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 10.775 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 10.800 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 10.825 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 10.850 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 10.875 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 10.900 | 130.05 | 130.05 | 130.05 | 130.05 | 130.06 |
| 10.925 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 10.950 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 10.975 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 11.000 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 11.025 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 11.050 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 11.075 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 11.100 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 11.125 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 11.150 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 11.175 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 11.200 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 11.225 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 11.250 | 130.07 | 130.07 | 130.07 | 130.07 | 130.08 |
| 11.275 | 130.08 | 130.08 | 130.08 | 130.08 | 130.08 |
| 11.300 | 130.08 | 130.08 | 130.08 | 130.08 | 130.08 |
| 11.325 | 130.08 | 130.08 | 130.08 | 130.08 | 130.08 |
| 11.350 | 130.08 | 130.08 | 130.08 | 130.08 | 130.09 |
| 11.375 | 130.09 | 130.09 | 130.09 | 130.09 | 130.09 |
| 11.400 | 130.09 | 130.09 | 130.09 | 130.09 | 130.09 |
| 11.425 | 130.09 | 130.09 | 130.09 | 130.09 | 130.09 |
| 11.450 | 130.09 | 130.09 | 130.09 | 130.09 | 130.09 |
| 11.475 | 130.09 | 130.09 | 130.09 | 130.10 | 130.10 |
| 11.500 | 130.10 | 130.10 | 130.10 | 130.10 | 130.10 |
| 11.525 | 130.10 | 130.10 | 130.10 | 130.10 | 130.10 |
| 11.550 | 130.10 | 130.10 | 130.10 | 130.10 | 130.10 |
| 11.575 | 130.10 | 130.11 | 130.11 | 130.11 | 130.11 |
| 11.600 | 130.11 | 130.11 | 130.11 | 130.11 | 130.12 |
| 11.625 | 130.12 | 130.12 | 130.12 | 130.13 | 130.13 |
| 11.650 | 130.13 | 130.13 | 130.14 | 130.14 | 130.14 |
| 11.675 | 130.14 | 130.15 | 130.15 | 130.15 | 130.16 |
| 11.700 | 130.16 | 130.17 | 130.17 | 130.18 | 130.18 |
| 11.725 | 130.19 | 130.19 | 130.19 | 130.20 | 130.21 |
| 11.750 | 130.21 | 130.21 | 130.22 | 130.22 | 130.23 |
| 11.775 | 130.23 | 130.24 | 130.25 | 130.25 | 130.26 |
| 11.800 | 130.26 | 130.27 | 130.28 | 130.28 | 130.29 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 11.825 | 130.29 | 130.30 | 130.31 | 130.31 | 130.32 |
| 11.850 | 130.33 | 130.33 | 130.34 | 130.35 | 130.36 |
| 11.875 | 130.36 | 130.37 | 130.38 | 130.39 | 130.40 |
| 11.900 | 130.41 | 130.42 | 130.42 | 130.43 | 130.44 |
| 11.925 | 130.45 | 130.46 | 130.47 | 130.48 | 130.48 |
| 11.950 | 130.49 | 130.50 | 130.51 | 130.51 | 130.52 |
| 11.975 | 130.52 | 130.53 | 130.53 | 130.54 | 130.54 |
| 12.000 | 130.54 | 130.55 | 130.55 | 130.55 | 130.55 |
| 12.025 | 130.56 | 130.56 | 130.56 | 130.56 | 130.56 |
| 12.050 | 130.56 | 130.56 | 130.56 | 130.56 | 130.55 |
| 12.075 | 130.55 | 130.55 | 130.54 | 130.54 | 130.53 |
| 12.100 | 130.53 | 130.52 | 130.52 | 130.51 | 130.51 |
| 12.125 | 130.50 | 130.49 | 130.49 | 130.48 | 130.47 |
| 12.150 | 130.47 | 130.46 | 130.45 | 130.44 | 130.44 |
| 12.175 | 130.43 | 130.42 | 130.42 | 130.41 | 130.40 |
| 12.200 | 130.40 | 130.39 | 130.38 | 130.38 | 130.37 |
| 12.225 | 130.36 | 130.36 | 130.35 | 130.35 | 130.34 |
| 12.250 | 130.34 | 130.33 | 130.33 | 130.32 | 130.32 |
| 12.275 | 130.31 | 130.31 | 130.30 | 130.30 | 130.30 |
| 12.300 | 130.29 | 130.29 | 130.29 | 130.28 | 130.28 |
| 12.325 | 130.28 | 130.27 | 130.27 | 130.27 | 130.27 |
| 12.350 | 130.26 | 130.26 | 130.26 | 130.25 | 130.25 |
| 12.375 | 130.25 | 130.25 | 130.25 | 130.24 | 130.24 |
| 12.400 | 130.24 | 130.24 | 130.24 | 130.23 | 130.23 |
| 12.425 | 130.23 | 130.23 | 130.23 | 130.23 | 130.22 |
| 12.450 | 130.22 | 130.22 | 130.22 | 130.22 | 130.22 |
| 12.475 | 130.21 | 130.21 | 130.21 | 130.21 | 130.21 |
| 12.500 | 130.21 | 130.21 | 130.21 | 130.20 | 130.20 |
| 12.525 | 130.20 | 130.20 | 130.20 | 130.20 | 130.20 |
| 12.550 | 130.20 | 130.19 | 130.19 | 130.19 | 130.19 |
| 12.575 | 130.19 | 130.19 | 130.19 | 130.19 | 130.19 |
| 12.600 | 130.18 | 130.18 | 130.18 | 130.18 | 130.18 |
| 12.625 | 130.18 | 130.18 | 130.18 | 130.18 | 130.17 |
| 12.650 | 130.17 | 130.17 | 130.17 | 130.17 | 130.17 |
| 12.675 | 130.17 | 130.17 | 130.17 | 130.17 | 130.17 |
| 12.700 | 130.17 | 130.17 | 130.16 | 130.16 | 130.16 |
| 12.725 | 130.16 | 130.16 | 130.16 | 130.16 | 130.16 |
| 12.750 | 130.16 | 130.16 | 130.16 | 130.16 | 130.16 |
| 12.775 | 130.16 | 130.16 | 130.16 | 130.16 | 130.16 |
| 12.800 | 130.16 | 130.16 | 130.16 | 130.15 | 130.15 |
| 12.825 | 130.15 | 130.15 | 130.15 | 130.15 | 130.15 |
| 12.850 | 130.15 | 130.15 | 130.15 | 130.15 | 130.15 |
| 12.875 | 130.15 | 130.15 | 130.15 | 130.15 | 130.15 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 12.900 | 130.15 | 130.15 | 130.15 | 130.15 | 130.15 |
| 12.925 | 130.15 | 130.15 | 130.15 | 130.15 | 130.15 |
| 12.950 | 130.15 | 130.14 | 130.14 | 130.14 | 130.14 |
| 12.975 | 130.14 | 130.14 | 130.14 | 130.14 | 130.14 |
| 13.000 | 130.14 | 130.14 | 130.14 | 130.14 | 130.14 |
| 13.025 | 130.14 | 130.14 | 130.14 | 130.14 | 130.14 |
| 13.050 | 130.14 | 130.14 | 130.14 | 130.14 | 130.14 |
| 13.075 | 130.14 | 130.14 | 130.14 | 130.14 | 130.14 |
| 13.100 | 130.14 | 130.14 | 130.14 | 130.14 | 130.13 |
| 13.125 | 130.13 | 130.13 | 130.13 | 130.13 | 130.13 |
| 13.150 | 130.13 | 130.13 | 130.13 | 130.13 | 130.13 |
| 13.175 | 130.13 | 130.13 | 130.13 | 130.13 | 130.13 |
| 13.200 | 130.13 | 130.13 | 130.13 | 130.13 | 130.13 |
| 13.225 | 130.13 | 130.13 | 130.13 | 130.13 | 130.13 |
| 13.250 | 130.13 | 130.13 | 130.13 | 130.13 | 130.13 |
| 13.275 | 130.13 | 130.13 | 130.13 | 130.13 | 130.13 |
| 13.300 | 130.13 | 130.13 | 130.13 | 130.13 | 130.13 |
| 13.325 | 130.13 | 130.13 | 130.13 | 130.13 | 130.13 |
| 13.350 | 130.13 | 130.13 | 130.13 | 130.12 | 130.12 |
| 13.375 | 130.12 | 130.12 | 130.12 | 130.12 | 130.12 |
| 13.400 | 130.12 | 130.12 | 130.12 | 130.12 | 130.12 |
| 13.425 | 130.12 | 130.12 | 130.12 | 130.12 | 130.12 |
| 13.450 | 130.12 | 130.12 | 130.12 | 130.12 | 130.12 |
| 13.475 | 130.12 | 130.12 | 130.12 | 130.12 | 130.12 |
| 13.500 | 130.12 | 130.12 | 130.12 | 130.12 | 130.12 |
| 13.525 | 130.12 | 130.12 | 130.12 | 130.12 | 130.12 |
| 13.550 | 130.12 | 130.12 | 130.12 | 130.12 | 130.12 |
| 13.575 | 130.12 | 130.12 | 130.12 | 130.12 | 130.12 |
| 13.600 | 130.12 | 130.12 | 130.12 | 130.12 | 130.12 |
| 13.625 | 130.12 | 130.12 | 130.12 | 130.12 | 130.12 |
| 13.650 | 130.12 | 130.11 | 130.11 | 130.11 | 130.11 |
| 13.675 | 130.11 | 130.11 | 130.11 | 130.11 | 130.11 |
| 13.700 | 130.11 | 130.11 | 130.11 | 130.11 | 130.11 |
| 13.725 | 130.11 | 130.11 | 130.11 | 130.11 | 130.11 |
| 13.750 | 130.11 | 130.11 | 130.11 | 130.11 | 130.11 |
| 13.775 | 130.11 | 130.11 | 130.11 | 130.11 | 130.11 |
| 13.800 | 130.11 | 130.11 | 130.11 | 130.11 | 130.11 |
| 13.825 | 130.11 | 130.11 | 130.11 | 130.11 | 130.11 |
| 13.850 | 130.11 | 130.11 | 130.11 | 130.11 | 130.11 |
| 13.875 | 130.11 | 130.11 | 130.11 | 130.11 | 130.11 |
| 13.900 | 130.11 | 130.11 | 130.11 | 130.11 | 130.11 |
| 13.925 | 130.11 | 130.11 | 130.11 | 130.11 | 130.11 |
| 13.950 | 130.11 | 130.11 | 130.10 | 130.10 | 130.10 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 13.975 | 130.10 | 130.10 | 130.10 | 130.10 | 130.10 |
| 14.000 | 130.10 | 130.10 | 130.10 | 130.10 | 130.10 |
| 14.025 | 130.10 | 130.10 | 130.10 | 130.10 | 130.10 |
| 14.050 | 130.10 | 130.10 | 130.10 | 130.10 | 130.10 |
| 14.075 | 130.10 | 130.10 | 130.10 | 130.10 | 130.10 |
| 14.100 | 130.10 | 130.10 | 130.10 | 130.10 | 130.10 |
| 14.125 | 130.10 | 130.10 | 130.10 | 130.10 | 130.10 |
| 14.150 | 130.10 | 130.10 | 130.10 | 130.10 | 130.10 |
| 14.175 | 130.10 | 130.10 | 130.10 | 130.10 | 130.10 |
| 14.200 | 130.10 | 130.10 | 130.10 | 130.10 | 130.10 |
| 14.225 | 130.10 | 130.10 | 130.10 | 130.10 | 130.10 |
| 14.250 | 130.10 | 130.10 | 130.10 | 130.10 | 130.10 |
| 14.275 | 130.10 | 130.10 | 130.10 | 130.10 | 130.10 |
| 14.300 | 130.10 | 130.10 | 130.10 | 130.10 | 130.10 |
| 14.325 | 130.10 | 130.10 | 130.10 | 130.10 | 130.10 |
| 14.350 | 130.10 | 130.10 | 130.10 | 130.10 | 130.10 |
| 14.375 | 130.10 | 130.10 | 130.10 | 130.10 | 130.10 |
| 14.400 | 130.10 | 130.10 | 130.10 | 130.10 | 130.10 |
| 14.425 | 130.10 | 130.10 | 130.10 | 130.10 | 130.09 |
| 14.450 | 130.09 | 130.09 | 130.09 | 130.09 | 130.09 |
| 14.475 | 130.09 | 130.09 | 130.09 | 130.09 | 130.09 |
| 14.500 | 130.09 | 130.09 | 130.09 | 130.09 | 130.09 |
| 14.525 | 130.09 | 130.09 | 130.09 | 130.09 | 130.09 |
| 14.550 | 130.09 | 130.09 | 130.09 | 130.09 | 130.09 |
| 14.575 | 130.09 | 130.09 | 130.09 | 130.09 | 130.09 |
| 14.600 | 130.09 | 130.09 | 130.09 | 130.09 | 130.09 |
| 14.625 | 130.09 | 130.09 | 130.09 | 130.09 | 130.09 |
| 14.650 | 130.09 | 130.09 | 130.09 | 130.09 | 130.09 |
| 14.675 | 130.09 | 130.09 | 130.09 | 130.09 | 130.09 |
| 14.700 | 130.09 | 130.09 | 130.09 | 130.09 | 130.09 |
| 14.725 | 130.09 | 130.09 | 130.09 | 130.09 | 130.09 |
| 14.750 | 130.09 | 130.09 | 130.09 | 130.09 | 130.09 |
| 14.775 | 130.09 | 130.09 | 130.09 | 130.09 | 130.09 |
| 14.800 | 130.09 | 130.09 | 130.09 | 130.09 | 130.09 |
| 14.825 | 130.09 | 130.09 | 130.09 | 130.09 | 130.09 |
| 14.850 | 130.09 | 130.09 | 130.09 | 130.09 | 130.09 |
| 14.875 | 130.09 | 130.09 | 130.09 | 130.09 | 130.09 |
| 14.900 | 130.09 | 130.09 | 130.09 | 130.09 | 130.09 |
| 14.925 | 130.09 | 130.09 | 130.09 | 130.09 | 130.09 |
| 14.950 | 130.09 | 130.09 | 130.09 | 130.09 | 130.09 |
| 14.975 | 130.09 | 130.09 | 130.09 | 130.09 | 130.09 |
| 15.000 | 130.09 | 130.09 | 130.09 | 130.09 | 130.09 |
| 15.025 | 130.09 | 130.09 | 130.09 | 130.09 | 130.09 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 15.050 | 130.09 | 130.09 | 130.09 | 130.09 | 130.09 |
| 15.075 | 130.09 | 130.09 | 130.09 | 130.09 | 130.09 |
| 15.100 | 130.09 | 130.09 | 130.09 | 130.09 | 130.09 |
| 15.125 | 130.09 | 130.09 | 130.09 | 130.09 | 130.09 |
| 15.150 | 130.09 | 130.09 | 130.09 | 130.09 | 130.09 |
| 15.175 | 130.09 | 130.09 | 130.09 | 130.09 | 130.09 |
| 15.200 | 130.09 | 130.09 | 130.09 | 130.09 | 130.09 |
| 15.225 | 130.09 | 130.09 | 130.09 | 130.09 | 130.09 |
| 15.250 | 130.09 | 130.09 | 130.09 | 130.09 | 130.09 |
| 15.275 | 130.09 | 130.09 | 130.09 | 130.09 | 130.09 |
| 15.300 | 130.09 | 130.09 | 130.09 | 130.09 | 130.09 |
| 15.325 | 130.09 | 130.09 | 130.09 | 130.09 | 130.09 |
| 15.350 | 130.09 | 130.09 | 130.09 | 130.09 | 130.09 |
| 15.375 | 130.09 | 130.09 | 130.09 | 130.09 | 130.09 |
| 15.400 | 130.09 | 130.09 | 130.09 | 130.09 | 130.08 |
| 15.425 | 130.08 | 130.08 | 130.08 | 130.08 | 130.08 |
| 15.450 | 130.08 | 130.08 | 130.08 | 130.08 | 130.08 |
| 15.475 | 130.08 | 130.08 | 130.08 | 130.08 | 130.08 |
| 15.500 | 130.08 | 130.08 | 130.08 | 130.08 | 130.08 |
| 15.525 | 130.08 | 130.08 | 130.08 | 130.08 | 130.08 |
| 15.550 | 130.08 | 130.08 | 130.08 | 130.08 | 130.08 |
| 15.575 | 130.08 | 130.08 | 130.08 | 130.08 | 130.08 |
| 15.600 | 130.08 | 130.08 | 130.08 | 130.08 | 130.08 |
| 15.625 | 130.08 | 130.08 | 130.08 | 130.08 | 130.08 |
| 15.650 | 130.08 | 130.08 | 130.08 | 130.08 | 130.08 |
| 15.675 | 130.08 | 130.08 | 130.08 | 130.08 | 130.08 |
| 15.700 | 130.08 | 130.08 | 130.08 | 130.08 | 130.08 |
| 15.725 | 130.08 | 130.08 | 130.08 | 130.08 | 130.08 |
| 15.750 | 130.08 | 130.08 | 130.08 | 130.08 | 130.08 |
| 15.775 | 130.08 | 130.08 | 130.08 | 130.08 | 130.08 |
| 15.800 | 130.08 | 130.08 | 130.08 | 130.08 | 130.08 |
| 15.825 | 130.08 | 130.08 | 130.08 | 130.08 | 130.08 |
| 15.850 | 130.08 | 130.08 | 130.08 | 130.08 | 130.08 |
| 15.875 | 130.08 | 130.08 | 130.08 | 130.08 | 130.08 |
| 15.900 | 130.08 | 130.08 | 130.08 | 130.08 | 130.08 |
| 15.925 | 130.08 | 130.08 | 130.08 | 130.08 | 130.08 |
| 15.950 | 130.08 | 130.08 | 130.08 | 130.08 | 130.08 |
| 15.975 | 130.08 | 130.08 | 130.08 | 130.08 | 130.08 |
| 16.000 | 130.08 | 130.08 | 130.08 | 130.08 | 130.08 |
| 16.025 | 130.08 | 130.08 | 130.08 | 130.08 | 130.08 |
| 16.050 | 130.08 | 130.08 | 130.08 | 130.08 | 130.08 |
| 16.075 | 130.08 | 130.08 | 130.08 | 130.08 | 130.08 |
| 16.100 | 130.08 | 130.08 | 130.08 | 130.08 | 130.08 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 16.125 | 130.08 | 130.08 | 130.08 | 130.08 | 130.08 |
| 16.150 | 130.08 | 130.08 | 130.08 | 130.08 | 130.08 |
| 16.175 | 130.08 | 130.08 | 130.08 | 130.08 | 130.08 |
| 16.200 | 130.08 | 130.08 | 130.08 | 130.08 | 130.08 |
| 16.225 | 130.08 | 130.08 | 130.08 | 130.08 | 130.08 |
| 16.250 | 130.08 | 130.08 | 130.08 | 130.08 | 130.07 |
| 16.275 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 16.300 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 16.325 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 16.350 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 16.375 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 16.400 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 16.425 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 16.450 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 16.475 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 16.500 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 16.525 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 16.550 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 16.575 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 16.600 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 16.625 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 16.650 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 16.675 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 16.700 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 16.725 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 16.750 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 16.775 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 16.800 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 16.825 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 16.850 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 16.875 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 16.900 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 16.925 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 16.950 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 16.975 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 17.000 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 17.025 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 17.050 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 17.075 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 17.100 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 17.125 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 17.150 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 17.175 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 17.200 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 17.225 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 17.250 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 17.275 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 17.300 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 17.325 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 17.350 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 17.375 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 17.400 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 17.425 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 17.450 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 17.475 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 17.500 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 17.525 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 17.550 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 17.575 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 17.600 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 17.625 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 17.650 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 17.675 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 17.700 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 17.725 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 17.750 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 17.775 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 17.800 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 17.825 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 17.850 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 17.875 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 17.900 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 17.925 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 17.950 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 17.975 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 18.000 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 18.025 | 130.07 | 130.07 | 130.07 | 130.07 | 130.07 |
| 18.050 | 130.07 | 130.07 | 130.07 | 130.07 | 130.06 |
| 18.075 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 18.100 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 18.125 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 18.150 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 18.175 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 18.200 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 18.225 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 18.250 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 18.275 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 18.300 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 18.325 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 18.350 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 18.375 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 18.400 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 18.425 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 18.450 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 18.475 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 18.500 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 18.525 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 18.550 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 18.575 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 18.600 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 18.625 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 18.650 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 18.675 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 18.700 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 18.725 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 18.750 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 18.775 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 18.800 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 18.825 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 18.850 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 18.875 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 18.900 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 18.925 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 18.950 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 18.975 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 19.000 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 19.025 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 19.050 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 19.075 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 19.100 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 19.125 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 19.150 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 19.175 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 19.200 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 19.225 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 19.250 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 19.275 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 19.300 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 19.325 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 19.350 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 19.375 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 19.400 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 19.425 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 19.450 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 19.475 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 19.500 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 19.525 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 19.550 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 19.575 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 19.600 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 19.625 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 19.650 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 19.675 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 19.700 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 19.725 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 19.750 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 19.775 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 19.800 | 130.06 | 130.06 | 130.06 | 130.06 | 130.06 |
| 19.825 | 130.06 | 130.06 | 130.06 | 130.06 | 130.05 |
| 19.850 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 19.875 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 19.900 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 19.925 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 19.950 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 19.975 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 20.000 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 20.025 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 20.050 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 20.075 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 20.100 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 20.125 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 20.150 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 20.175 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 20.200 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 20.225 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 20.250 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 20.275 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 20.300 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 20.325 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 20.350 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 20.375 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 20.400 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 20.425 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 20.450 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 20.475 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 20.500 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 20.525 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 20.550 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 20.575 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 20.600 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 20.625 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 20.650 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 20.675 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 20.700 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 20.725 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 20.750 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 20.775 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 20.800 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 20.825 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 20.850 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 20.875 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 20.900 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 20.925 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 20.950 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 20.975 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 21.000 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 21.025 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 21.050 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 21.075 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 21.100 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 21.125 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 21.150 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 21.175 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 21.200 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 21.225 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 21.250 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 21.275 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 21.300 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 21.325 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 21.350 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 21.375 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 21.400 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 21.425 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 21.450 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 21.475 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 21.500 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 21.525 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 21.550 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 21.575 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 21.600 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 21.625 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 21.650 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 21.675 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 21.700 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 21.725 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 21.750 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 21.775 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 21.800 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 21.825 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 21.850 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 21.875 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 21.900 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 21.925 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 21.950 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 21.975 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 22.000 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 22.025 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 22.050 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 22.075 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 22.100 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 22.125 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 22.150 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 22.175 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 22.200 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 22.225 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 22.250 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 22.275 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 22.300 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 22.325 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 22.350 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 22.375 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 22.400 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 22.425 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 22.450 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 22.475 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 22.500 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 22.525 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 22.550 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 22.575 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 22.600 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 22.625 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 22.650 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 22.675 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 22.700 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 22.725 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 22.750 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 22.775 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 22.800 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 22.825 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 22.850 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 22.875 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 22.900 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 22.925 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 22.950 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 22.975 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 23.000 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 23.025 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 23.050 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 23.075 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 23.100 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 23.125 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 23.150 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 23.175 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 23.200 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 23.225 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 23.250 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 23.275 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 23.300 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 23.325 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 23.350 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 23.375 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 23.400 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 23.425 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 23.450 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 23.475 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 23.500 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 23.525 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 23.550 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 23.575 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 23.600 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 23.625 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 23.650 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 23.675 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 23.700 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 23.725 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 23.750 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 23.775 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 23.800 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 23.825 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 23.850 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 23.875 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 23.900 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 23.925 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 23.950 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 23.975 | 130.05 | 130.05 | 130.05 | 130.05 | 130.05 |
| 24.000 | 130.05 | (N/A) | (N/A) | (N/A) | (N/A) |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 0.000 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 0.025 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 0.050 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 0.075 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 0.100 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 0.125 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 0.150 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 0.175 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 0.200 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 0.225 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 0.250 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 0.275 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 0.300 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 0.325 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 0.350 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 0.375 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 0.400 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 0.425 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 0.450 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 0.475 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 0.500 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 0.525 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 0.550 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 0.575 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 0.600 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 0.625 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 0.650 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 0.675 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 0.700 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 0.725 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 0.750 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 0.775 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 0.800 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 0.825 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 0.850 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 0.875 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 0.900 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 0.925 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 0.950 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 0.975 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 1.000 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 1.025 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 1.050 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 1.075 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 1.100 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 1.125 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 1.150 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 1.175 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 1.200 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 1.225 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 1.250 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 1.275 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 1.300 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 1.325 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 1.350 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 1.375 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 1.400 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 1.425 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 1.450 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 1.475 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 1.500 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 1.525 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 1.550 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 1.575 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 1.600 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 1.625 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 1.650 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 1.675 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 1.700 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 1.725 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 1.750 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 1.775 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 1.800 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 1.825 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 1.850 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 1.875 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 1.900 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 1.925 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 1.950 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 1.975 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 2.000 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 2.025 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 2.050 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 2.075 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 2.100 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 2.125 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 2.150 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 2.175 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 2.200 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 2.225 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 2.250 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 2.275 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 2.300 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 2.325 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 2.350 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 2.375 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 2.400 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 2.425 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 2.450 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 2.475 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 2.500 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 2.525 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 2.550 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 2.575 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 2.600 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 2.625 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 2.650 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 2.675 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 2.700 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 2.725 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 2.750 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 2.775 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 2.800 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 2.825 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 2.850 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 2.875 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 2.900 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 2.925 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 2.950 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 2.975 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 3.000 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 3.025 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 3.050 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 3.075 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 3.100 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 3.125 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 3.150 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 3.175 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 3.200 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 3.225 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 3.250 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 3.275 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 3.300 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 3.325 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 3.350 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 3.375 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 3.400 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 3.425 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 3.450 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 3.475 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 3.500 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 3.525 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 3.550 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 3.575 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 3.600 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 3.625 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 3.650 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 3.675 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 3.700 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 3.725 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 3.750 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 3.775 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 3.800 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 3.825 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 3.850 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 3.875 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 3.900 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 3.925 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 3.950 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 3.975 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 4.000 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 4.025 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 4.050 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 4.075 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 4.100 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 4.125 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 4.150 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 4.175 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 4.200 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 4.225 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 4.250 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 4.275 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 4.300 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 4.325 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 4.350 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 4.375 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 4.400 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 4.425 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 4.450 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 4.475 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 4.500 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 4.525 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 4.550 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 4.575 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 4.600 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 4.625 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 4.650 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 4.675 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 4.700 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 4.725 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 4.750 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 4.775 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 4.800 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 4.825 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 4.850 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 4.875 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 4.900 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 4.925 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 4.950 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 4.975 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 5.000 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 5.025 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 5.050 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 5.075 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 5.100 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 5.125 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 5.150 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 5.175 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 5.200 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 5.225 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 5.250 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 5.275 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 5.300 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 5.325 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 5.350 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 5.375 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 5.400 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 5.425 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 5.450 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 5.475 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 5.500 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 5.525 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 5.550 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 5.575 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 5.600 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 5.625 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 5.650 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 5.675 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 5.700 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 5.725 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 5.750 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 5.775 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 5.800 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 5.825 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 5.850 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 5.875 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 5.900 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 5.925 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 5.950 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 5.975 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 6.000 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 6.025 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 6.050 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 6.075 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 6.100 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 6.125 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 6.150 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 6.175 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 6.200 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 6.225 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 6.250 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 6.275 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 6.300 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 6.325 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 6.350 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 6.375 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 6.400 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 6.425 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 6.450 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 6.475 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 6.500 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 6.525 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 6.550 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 6.575 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 6.600 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 6.625 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 6.650 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 6.675 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 6.700 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 6.725 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 6.750 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 6.775 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 6.800 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 6.825 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 6.850 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 6.875 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 6.900 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 6.925 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 6.950 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 6.975 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 7.000 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 7.025 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 7.050 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 7.075 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 7.100 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 7.125 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 7.150 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 7.175 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 7.200 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 7.225 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 7.250 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 7.275 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 7.300 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 7.325 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 7.350 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 7.375 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 7.400 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 7.425 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 7.450 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 7.475 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 7.500 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 7.525 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 7.550 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 7.575 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 7.600 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 7.625 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 7.650 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 7.675 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 7.700 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 7.725 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 7.750 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 7.775 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 7.800 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 7.825 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 7.850 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 7.875 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 7.900 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 7.925 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 7.950 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 7.975 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 8.000 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 8.025 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 8.050 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 8.075 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 8.100 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 8.125 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 8.150 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 8.175 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 8.200 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 8.225 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 8.250 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 8.275 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 8.300 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 8.325 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 8.350 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 8.375 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 8.400 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 8.425 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 8.450 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 8.475 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 8.500 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 8.525 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 8.550 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 8.575 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 8.600 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 8.625 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 8.650 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 8.675 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 8.700 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 8.725 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 8.750 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 8.775 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 8.800 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 8.825 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 8.850 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 8.875 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 8.900 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 8.925 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 8.950 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 8.975 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 9.000 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 9.025 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 9.050 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 9.075 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 9.100 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 9.125 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 9.150 | 129.00 | 129.00 | 129.00 | 129.00 | 129.00 |
| 9.175 | 129.00 | 129.01 | 129.01 | 129.01 | 129.01 |
| 9.200 | 129.01 | 129.01 | 129.01 | 129.01 | 129.01 |
| 9.225 | 129.01 | 129.01 | 129.01 | 129.01 | 129.01 |
| 9.250 | 129.01 | 129.01 | 129.01 | 129.01 | 129.01 |
| 9.275 | 129.01 | 129.01 | 129.01 | 129.01 | 129.01 |
| 9.300 | 129.01 | 129.01 | 129.01 | 129.01 | 129.01 |
| 9.325 | 129.01 | 129.01 | 129.01 | 129.01 | 129.01 |
| 9.350 | 129.01 | 129.01 | 129.01 | 129.01 | 129.01 |
| 9.375 | 129.01 | 129.01 | 129.01 | 129.01 | 129.01 |
| 9.400 | 129.01 | 129.01 | 129.01 | 129.01 | 129.01 |
| 9.425 | 129.01 | 129.01 | 129.01 | 129.01 | 129.01 |
| 9.450 | 129.01 | 129.01 | 129.01 | 129.01 | 129.01 |
| 9.475 | 129.01 | 129.01 | 129.01 | 129.01 | 129.01 |
| 9.500 | 129.01 | 129.01 | 129.01 | 129.01 | 129.01 |
| 9.525 | 129.01 | 129.01 | 129.01 | 129.01 | 129.01 |
| 9.550 | 129.01 | 129.01 | 129.01 | 129.01 | 129.01 |
| 9.575 | 129.01 | 129.01 | 129.01 | 129.01 | 129.01 |
| 9.600 | 129.01 | 129.01 | 129.01 | 129.01 | 129.01 |
| 9.625 | 129.01 | 129.01 | 129.01 | 129.01 | 129.01 |
| 9.650 | 129.01 | 129.01 | 129.01 | 129.01 | 129.01 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 9.675 | 129.01 | 129.01 | 129.01 | 129.01 | 129.01 |
| 9.700 | 129.01 | 129.01 | 129.01 | 129.01 | 129.01 |
| 9.725 | 129.01 | 129.01 | 129.01 | 129.01 | 129.01 |
| 9.750 | 129.01 | 129.01 | 129.01 | 129.01 | 129.01 |
| 9.775 | 129.01 | 129.01 | 129.01 | 129.01 | 129.01 |
| 9.800 | 129.01 | 129.01 | 129.01 | 129.01 | 129.01 |
| 9.825 | 129.01 | 129.01 | 129.01 | 129.01 | 129.01 |
| 9.850 | 129.02 | 129.02 | 129.02 | 129.02 | 129.02 |
| 9.875 | 129.02 | 129.02 | 129.02 | 129.02 | 129.02 |
| 9.900 | 129.02 | 129.02 | 129.02 | 129.02 | 129.02 |
| 9.925 | 129.02 | 129.02 | 129.02 | 129.02 | 129.02 |
| 9.950 | 129.02 | 129.02 | 129.02 | 129.02 | 129.02 |
| 9.975 | 129.02 | 129.02 | 129.02 | 129.02 | 129.02 |
| 10.000 | 129.02 | 129.02 | 129.02 | 129.02 | 129.02 |
| 10.025 | 129.02 | 129.02 | 129.02 | 129.02 | 129.02 |
| 10.050 | 129.02 | 129.02 | 129.02 | 129.02 | 129.02 |
| 10.075 | 129.02 | 129.02 | 129.02 | 129.02 | 129.02 |
| 10.100 | 129.02 | 129.02 | 129.02 | 129.02 | 129.02 |
| 10.125 | 129.02 | 129.02 | 129.02 | 129.02 | 129.02 |
| 10.150 | 129.02 | 129.02 | 129.02 | 129.02 | 129.02 |
| 10.175 | 129.02 | 129.02 | 129.02 | 129.02 | 129.02 |
| 10.200 | 129.02 | 129.02 | 129.02 | 129.02 | 129.02 |
| 10.225 | 129.02 | 129.02 | 129.02 | 129.02 | 129.02 |
| 10.250 | 129.02 | 129.02 | 129.02 | 129.02 | 129.02 |
| 10.275 | 129.02 | 129.02 | 129.02 | 129.02 | 129.02 |
| 10.300 | 129.02 | 129.02 | 129.02 | 129.02 | 129.02 |
| 10.325 | 129.02 | 129.02 | 129.02 | 129.02 | 129.02 |
| 10.350 | 129.02 | 129.02 | 129.02 | 129.02 | 129.02 |
| 10.375 | 129.02 | 129.02 | 129.02 | 129.02 | 129.02 |
| 10.400 | 129.02 | 129.02 | 129.02 | 129.02 | 129.02 |
| 10.425 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 10.450 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 10.475 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 10.500 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 10.525 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 10.550 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 10.575 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 10.600 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 10.625 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 10.650 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 10.675 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 10.700 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 10.725 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 10.750 | 129.03 | 129.03 | 129.03 | 129.04 | 129.04 |
| 10.775 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 10.800 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 10.825 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 10.850 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 10.875 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 10.900 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 10.925 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 10.950 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 10.975 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 11.000 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 11.025 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 11.050 | 129.04 | 129.04 | 129.05 | 129.05 | 129.05 |
| 11.075 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 11.100 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 11.125 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 11.150 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 11.175 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 11.200 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 11.225 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 11.250 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 11.275 | 129.05 | 129.05 | 129.06 | 129.06 | 129.06 |
| 11.300 | 129.06 | 129.06 | 129.06 | 129.06 | 129.06 |
| 11.325 | 129.06 | 129.06 | 129.06 | 129.06 | 129.06 |
| 11.350 | 129.06 | 129.06 | 129.06 | 129.06 | 129.06 |
| 11.375 | 129.06 | 129.06 | 129.06 | 129.06 | 129.06 |
| 11.400 | 129.06 | 129.06 | 129.06 | 129.06 | 129.06 |
| 11.425 | 129.06 | 129.06 | 129.06 | 129.06 | 129.07 |
| 11.450 | 129.07 | 129.07 | 129.07 | 129.07 | 129.07 |
| 11.475 | 129.07 | 129.07 | 129.07 | 129.07 | 129.07 |
| 11.500 | 129.07 | 129.07 | 129.07 | 129.07 | 129.07 |
| 11.525 | 129.07 | 129.07 | 129.07 | 129.07 | 129.07 |
| 11.550 | 129.07 | 129.08 | 129.08 | 129.08 | 129.08 |
| 11.575 | 129.08 | 129.08 | 129.08 | 129.09 | 129.09 |
| 11.600 | 129.09 | 129.09 | 129.09 | 129.09 | 129.10 |
| 11.625 | 129.10 | 129.10 | 129.10 | 129.10 | 129.11 |
| 11.650 | 129.11 | 129.11 | 129.12 | 129.12 | 129.12 |
| 11.675 | 129.12 | 129.13 | 129.13 | 129.13 | 129.14 |
| 11.700 | 129.14 | 129.14 | 129.15 | 129.15 | 129.16 |
| 11.725 | 129.16 | 129.16 | 129.17 | 129.17 | 129.17 |
| 11.750 | 129.18 | 129.18 | 129.19 | 129.19 | 129.19 |
| 11.775 | 129.20 | 129.20 | 129.21 | 129.21 | 129.22 |
| 11.800 | 129.22 | 129.22 | 129.23 | 129.23 | 129.24 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 11.825 | 129.24 | 129.25 | 129.25 | 129.26 | 129.26 |
| 11.850 | 129.27 | 129.27 | 129.28 | 129.29 | 129.29 |
| 11.875 | 129.30 | 129.31 | 129.31 | 129.32 | 129.33 |
| 11.900 | 129.33 | 129.34 | 129.35 | 129.35 | 129.36 |
| 11.925 | 129.37 | 129.37 | 129.38 | 129.38 | 129.39 |
| 11.950 | 129.39 | 129.40 | 129.40 | 129.40 | 129.40 |
| 11.975 | 129.41 | 129.41 | 129.41 | 129.41 | 129.41 |
| 12.000 | 129.41 | 129.41 | 129.41 | 129.41 | 129.41 |
| 12.025 | 129.41 | 129.41 | 129.41 | 129.40 | 129.40 |
| 12.050 | 129.40 | 129.39 | 129.39 | 129.39 | 129.38 |
| 12.075 | 129.38 | 129.37 | 129.37 | 129.36 | 129.35 |
| 12.100 | 129.35 | 129.34 | 129.33 | 129.33 | 129.32 |
| 12.125 | 129.31 | 129.30 | 129.30 | 129.29 | 129.28 |
| 12.150 | 129.28 | 129.27 | 129.26 | 129.26 | 129.25 |
| 12.175 | 129.25 | 129.24 | 129.24 | 129.23 | 129.23 |
| 12.200 | 129.22 | 129.22 | 129.21 | 129.21 | 129.21 |
| 12.225 | 129.20 | 129.20 | 129.20 | 129.20 | 129.19 |
| 12.250 | 129.19 | 129.19 | 129.18 | 129.18 | 129.18 |
| 12.275 | 129.18 | 129.18 | 129.17 | 129.17 | 129.17 |
| 12.300 | 129.17 | 129.17 | 129.17 | 129.16 | 129.16 |
| 12.325 | 129.16 | 129.16 | 129.16 | 129.16 | 129.16 |
| 12.350 | 129.16 | 129.15 | 129.15 | 129.15 | 129.15 |
| 12.375 | 129.15 | 129.15 | 129.15 | 129.15 | 129.15 |
| 12.400 | 129.15 | 129.14 | 129.14 | 129.14 | 129.14 |
| 12.425 | 129.14 | 129.14 | 129.14 | 129.14 | 129.14 |
| 12.450 | 129.14 | 129.14 | 129.14 | 129.13 | 129.13 |
| 12.475 | 129.13 | 129.13 | 129.13 | 129.13 | 129.13 |
| 12.500 | 129.13 | 129.13 | 129.13 | 129.13 | 129.13 |
| 12.525 | 129.13 | 129.13 | 129.12 | 129.12 | 129.12 |
| 12.550 | 129.12 | 129.12 | 129.12 | 129.12 | 129.12 |
| 12.575 | 129.12 | 129.12 | 129.12 | 129.12 | 129.12 |
| 12.600 | 129.12 | 129.12 | 129.12 | 129.11 | 129.11 |
| 12.625 | 129.11 | 129.11 | 129.11 | 129.11 | 129.11 |
| 12.650 | 129.11 | 129.11 | 129.11 | 129.11 | 129.11 |
| 12.675 | 129.11 | 129.11 | 129.11 | 129.11 | 129.11 |
| 12.700 | 129.11 | 129.11 | 129.11 | 129.11 | 129.11 |
| 12.725 | 129.11 | 129.11 | 129.10 | 129.10 | 129.10 |
| 12.750 | 129.10 | 129.10 | 129.10 | 129.10 | 129.10 |
| 12.775 | 129.10 | 129.10 | 129.10 | 129.10 | 129.10 |
| 12.800 | 129.10 | 129.10 | 129.10 | 129.10 | 129.10 |
| 12.825 | 129.10 | 129.10 | 129.10 | 129.10 | 129.10 |
| 12.850 | 129.10 | 129.10 | 129.10 | 129.10 | 129.10 |
| 12.875 | 129.10 | 129.10 | 129.10 | 129.10 | 129.10 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 12.900 | 129.10 | 129.10 | 129.10 | 129.10 | 129.10 |
| 12.925 | 129.10 | 129.10 | 129.10 | 129.10 | 129.10 |
| 12.950 | 129.10 | 129.10 | 129.10 | 129.09 | 129.09 |
| 12.975 | 129.09 | 129.09 | 129.09 | 129.09 | 129.09 |
| 13.000 | 129.09 | 129.09 | 129.09 | 129.09 | 129.09 |
| 13.025 | 129.09 | 129.09 | 129.09 | 129.09 | 129.09 |
| 13.050 | 129.09 | 129.09 | 129.09 | 129.09 | 129.09 |
| 13.075 | 129.09 | 129.09 | 129.09 | 129.09 | 129.09 |
| 13.100 | 129.09 | 129.09 | 129.09 | 129.09 | 129.09 |
| 13.125 | 129.09 | 129.09 | 129.09 | 129.09 | 129.09 |
| 13.150 | 129.09 | 129.09 | 129.09 | 129.09 | 129.09 |
| 13.175 | 129.09 | 129.09 | 129.09 | 129.09 | 129.09 |
| 13.200 | 129.09 | 129.09 | 129.09 | 129.09 | 129.09 |
| 13.225 | 129.09 | 129.09 | 129.09 | 129.09 | 129.09 |
| 13.250 | 129.09 | 129.09 | 129.09 | 129.09 | 129.09 |
| 13.275 | 129.09 | 129.09 | 129.09 | 129.08 | 129.08 |
| 13.300 | 129.08 | 129.08 | 129.08 | 129.08 | 129.08 |
| 13.325 | 129.08 | 129.08 | 129.08 | 129.08 | 129.08 |
| 13.350 | 129.08 | 129.08 | 129.08 | 129.08 | 129.08 |
| 13.375 | 129.08 | 129.08 | 129.08 | 129.08 | 129.08 |
| 13.400 | 129.08 | 129.08 | 129.08 | 129.08 | 129.08 |
| 13.425 | 129.08 | 129.08 | 129.08 | 129.08 | 129.08 |
| 13.450 | 129.08 | 129.08 | 129.08 | 129.08 | 129.08 |
| 13.475 | 129.08 | 129.08 | 129.08 | 129.08 | 129.08 |
| 13.500 | 129.08 | 129.08 | 129.08 | 129.08 | 129.08 |
| 13.525 | 129.08 | 129.08 | 129.08 | 129.08 | 129.08 |
| 13.550 | 129.08 | 129.08 | 129.08 | 129.08 | 129.08 |
| 13.575 | 129.08 | 129.08 | 129.08 | 129.08 | 129.08 |
| 13.600 | 129.08 | 129.08 | 129.08 | 129.08 | 129.08 |
| 13.625 | 129.08 | 129.08 | 129.08 | 129.08 | 129.08 |
| 13.650 | 129.08 | 129.08 | 129.08 | 129.08 | 129.08 |
| 13.675 | 129.08 | 129.08 | 129.08 | 129.08 | 129.08 |
| 13.700 | 129.08 | 129.08 | 129.08 | 129.07 | 129.07 |
| 13.725 | 129.07 | 129.07 | 129.07 | 129.07 | 129.07 |
| 13.750 | 129.07 | 129.07 | 129.07 | 129.07 | 129.07 |
| 13.775 | 129.07 | 129.07 | 129.07 | 129.07 | 129.07 |
| 13.800 | 129.07 | 129.07 | 129.07 | 129.07 | 129.07 |
| 13.825 | 129.07 | 129.07 | 129.07 | 129.07 | 129.07 |
| 13.850 | 129.07 | 129.07 | 129.07 | 129.07 | 129.07 |
| 13.875 | 129.07 | 129.07 | 129.07 | 129.07 | 129.07 |
| 13.900 | 129.07 | 129.07 | 129.07 | 129.07 | 129.07 |
| 13.925 | 129.07 | 129.07 | 129.07 | 129.07 | 129.07 |
| 13.950 | 129.07 | 129.07 | 129.07 | 129.07 | 129.07 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 13.975 | 129.07 | 129.07 | 129.07 | 129.07 | 129.07 |
| 14.000 | 129.07 | 129.07 | 129.07 | 129.07 | 129.07 |
| 14.025 | 129.07 | 129.07 | 129.07 | 129.07 | 129.07 |
| 14.050 | 129.07 | 129.07 | 129.07 | 129.07 | 129.07 |
| 14.075 | 129.07 | 129.07 | 129.07 | 129.07 | 129.07 |
| 14.100 | 129.07 | 129.07 | 129.07 | 129.07 | 129.07 |
| 14.125 | 129.07 | 129.07 | 129.07 | 129.07 | 129.07 |
| 14.150 | 129.07 | 129.07 | 129.07 | 129.07 | 129.07 |
| 14.175 | 129.07 | 129.07 | 129.07 | 129.07 | 129.07 |
| 14.200 | 129.07 | 129.06 | 129.06 | 129.06 | 129.06 |
| 14.225 | 129.06 | 129.06 | 129.06 | 129.06 | 129.06 |
| 14.250 | 129.06 | 129.06 | 129.06 | 129.06 | 129.06 |
| 14.275 | 129.06 | 129.06 | 129.06 | 129.06 | 129.06 |
| 14.300 | 129.06 | 129.06 | 129.06 | 129.06 | 129.06 |
| 14.325 | 129.06 | 129.06 | 129.06 | 129.06 | 129.06 |
| 14.350 | 129.06 | 129.06 | 129.06 | 129.06 | 129.06 |
| 14.375 | 129.06 | 129.06 | 129.06 | 129.06 | 129.06 |
| 14.400 | 129.06 | 129.06 | 129.06 | 129.06 | 129.06 |
| 14.425 | 129.06 | 129.06 | 129.06 | 129.06 | 129.06 |
| 14.450 | 129.06 | 129.06 | 129.06 | 129.06 | 129.06 |
| 14.475 | 129.06 | 129.06 | 129.06 | 129.06 | 129.06 |
| 14.500 | 129.06 | 129.06 | 129.06 | 129.06 | 129.06 |
| 14.525 | 129.06 | 129.06 | 129.06 | 129.06 | 129.06 |
| 14.550 | 129.06 | 129.06 | 129.06 | 129.06 | 129.06 |
| 14.575 | 129.06 | 129.06 | 129.06 | 129.06 | 129.06 |
| 14.600 | 129.06 | 129.06 | 129.06 | 129.06 | 129.06 |
| 14.625 | 129.06 | 129.06 | 129.06 | 129.06 | 129.06 |
| 14.650 | 129.06 | 129.06 | 129.06 | 129.06 | 129.06 |
| 14.675 | 129.06 | 129.06 | 129.06 | 129.06 | 129.06 |
| 14.700 | 129.06 | 129.06 | 129.06 | 129.06 | 129.06 |
| 14.725 | 129.06 | 129.06 | 129.06 | 129.06 | 129.06 |
| 14.750 | 129.06 | 129.06 | 129.06 | 129.06 | 129.06 |
| 14.775 | 129.06 | 129.06 | 129.06 | 129.06 | 129.06 |
| 14.800 | 129.06 | 129.06 | 129.06 | 129.06 | 129.06 |
| 14.825 | 129.06 | 129.06 | 129.06 | 129.06 | 129.06 |
| 14.850 | 129.06 | 129.06 | 129.06 | 129.06 | 129.06 |
| 14.875 | 129.06 | 129.06 | 129.06 | 129.06 | 129.06 |
| 14.900 | 129.06 | 129.06 | 129.06 | 129.06 | 129.06 |
| 14.925 | 129.06 | 129.06 | 129.06 | 129.06 | 129.06 |
| 14.950 | 129.06 | 129.06 | 129.06 | 129.06 | 129.06 |
| 14.975 | 129.06 | 129.06 | 129.06 | 129.06 | 129.06 |
| 15.000 | 129.06 | 129.06 | 129.06 | 129.06 | 129.06 |
| 15.025 | 129.06 | 129.06 | 129.06 | 129.06 | 129.06 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 15.050 | 129.06 | 129.06 | 129.06 | 129.06 | 129.06 |
| 15.075 | 129.06 | 129.06 | 129.06 | 129.06 | 129.06 |
| 15.100 | 129.06 | 129.06 | 129.06 | 129.06 | 129.06 |
| 15.125 | 129.06 | 129.06 | 129.06 | 129.06 | 129.06 |
| 15.150 | 129.06 | 129.06 | 129.06 | 129.06 | 129.06 |
| 15.175 | 129.06 | 129.06 | 129.06 | 129.06 | 129.06 |
| 15.200 | 129.06 | 129.06 | 129.06 | 129.06 | 129.06 |
| 15.225 | 129.06 | 129.06 | 129.06 | 129.06 | 129.06 |
| 15.250 | 129.06 | 129.06 | 129.06 | 129.06 | 129.06 |
| 15.275 | 129.06 | 129.06 | 129.06 | 129.06 | 129.06 |
| 15.300 | 129.06 | 129.06 | 129.06 | 129.06 | 129.06 |
| 15.325 | 129.06 | 129.06 | 129.06 | 129.06 | 129.06 |
| 15.350 | 129.06 | 129.06 | 129.06 | 129.06 | 129.06 |
| 15.375 | 129.06 | 129.06 | 129.06 | 129.06 | 129.06 |
| 15.400 | 129.06 | 129.06 | 129.06 | 129.06 | 129.06 |
| 15.425 | 129.06 | 129.06 | 129.06 | 129.06 | 129.06 |
| 15.450 | 129.06 | 129.06 | 129.06 | 129.06 | 129.05 |
| 15.475 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 15.500 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 15.525 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 15.550 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 15.575 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 15.600 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 15.625 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 15.650 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 15.675 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 15.700 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 15.725 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 15.750 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 15.775 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 15.800 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 15.825 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 15.850 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 15.875 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 15.900 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 15.925 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 15.950 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 15.975 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 16.000 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 16.025 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 16.050 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 16.075 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 16.100 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 16.125 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 16.150 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 16.175 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 16.200 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 16.225 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 16.250 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 16.275 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 16.300 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 16.325 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 16.350 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 16.375 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 16.400 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 16.425 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 16.450 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 16.475 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 16.500 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 16.525 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 16.550 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 16.575 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 16.600 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 16.625 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 16.650 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 16.675 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 16.700 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 16.725 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 16.750 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 16.775 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 16.800 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 16.825 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 16.850 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 16.875 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 16.900 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 16.925 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 16.950 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 16.975 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 17.000 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 17.025 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 17.050 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 17.075 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 17.100 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 17.125 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 17.150 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 17.175 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 17.200 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 17.225 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 17.250 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 17.275 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 17.300 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 17.325 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 17.350 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 17.375 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 17.400 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 17.425 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 17.450 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 17.475 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 17.500 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 17.525 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 17.550 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 17.575 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 17.600 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 17.625 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 17.650 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 17.675 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 17.700 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 17.725 | 129.05 | 129.05 | 129.05 | 129.05 | 129.05 |
| 17.750 | 129.05 | 129.05 | 129.04 | 129.04 | 129.04 |
| 17.775 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 17.800 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 17.825 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 17.850 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 17.875 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 17.900 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 17.925 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 17.950 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 17.975 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 18.000 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 18.025 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 18.050 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 18.075 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 18.100 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 18.125 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 18.150 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 18.175 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 18.200 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 18.225 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 18.250 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 18.275 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 18.300 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 18.325 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 18.350 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 18.375 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 18.400 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 18.425 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 18.450 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 18.475 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 18.500 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 18.525 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 18.550 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 18.575 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 18.600 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 18.625 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 18.650 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 18.675 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 18.700 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 18.725 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 18.750 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 18.775 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 18.800 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 18.825 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 18.850 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 18.875 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 18.900 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 18.925 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 18.950 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 18.975 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 19.000 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 19.025 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 19.050 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 19.075 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 19.100 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 19.125 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 19.150 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 19.175 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 19.200 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 19.225 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 19.250 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 19.275 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 19.300 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 19.325 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 19.350 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 19.375 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 19.400 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 19.425 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 19.450 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 19.475 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 19.500 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 19.525 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 19.550 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 19.575 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 19.600 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 19.625 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 19.650 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 19.675 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 19.700 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 19.725 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 19.750 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 19.775 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 19.800 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 19.825 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 19.850 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 19.875 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 19.900 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 19.925 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 19.950 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 19.975 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 20.000 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 20.025 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 20.050 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 20.075 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 20.100 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 20.125 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 20.150 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 20.175 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 20.200 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 20.225 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 20.250 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 20.275 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 20.300 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 20.325 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 20.350 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 20.375 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 20.400 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 20.425 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 20.450 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 20.475 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 20.500 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 20.525 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 20.550 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 20.575 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 20.600 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 20.625 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 20.650 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 20.675 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 20.700 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 20.725 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 20.750 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 20.775 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 20.800 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 20.825 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 20.850 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 20.875 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 20.900 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 20.925 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 20.950 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 20.975 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 21.000 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 21.025 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 21.050 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 21.075 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 21.100 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 21.125 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 21.150 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 21.175 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 21.200 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 21.225 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 21.250 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 21.275 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 21.300 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 21.325 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 21.350 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 21.375 | 129.04 | 129.04 | 129.04 | 129.04 | 129.04 |
| 21.400 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 21.425 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 21.450 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 21.475 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 21.500 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 21.525 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 21.550 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 21.575 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 21.600 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 21.625 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 21.650 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 21.675 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 21.700 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 21.725 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 21.750 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 21.775 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 21.800 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 21.825 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 21.850 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 21.875 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 21.900 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 21.925 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 21.950 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 21.975 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 22.000 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 22.025 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 22.050 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 22.075 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 22.100 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 22.125 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 22.150 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 22.175 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 22.200 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 22.225 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 22.250 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 22.275 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 22.300 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 22.325 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 22.350 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 22.375 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 22.400 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 22.425 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 22.450 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 22.475 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 22.500 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 22.525 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 22.550 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 22.575 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 22.600 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 22.625 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 22.650 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 22.675 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 22.700 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 22.725 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 22.750 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 22.775 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 22.800 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 22.825 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 22.850 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 22.875 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 22.900 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 22.925 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 22.950 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 22.975 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 23.000 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 23.025 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 23.050 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 23.075 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 23.100 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 23.125 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 23.150 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 23.175 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 23.200 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 23.225 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 23.250 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 23.275 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 23.300 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 23.325 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 23.350 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 23.375 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 23.400 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 23.425 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 23.450 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 23.475 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 23.500 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 23.525 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 23.550 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 23.575 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 23.600 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 23.625 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 23.650 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 23.675 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 23.700 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 23.725 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 23.750 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 23.775 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 23.800 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 23.825 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 23.850 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 23.875 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 23.900 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 23.925 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 23.950 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 23.975 | 129.03 | 129.03 | 129.03 | 129.03 | 129.03 |
| 24.000 | 129.03 | (N/A) | (N/A) | (N/A) | (N/A) |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 0.000 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 0.025 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 0.050 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 0.075 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 0.100 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 0.125 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 0.150 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 0.175 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 0.200 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 0.225 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 0.250 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 0.275 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 0.300 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 0.325 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 0.350 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 0.375 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 0.400 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 0.425 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 0.450 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 0.475 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 0.500 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 0.525 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 0.550 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 0.575 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 0.600 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 0.625 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 0.650 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 0.675 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 0.700 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 0.725 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 0.750 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 0.775 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 0.800 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 0.825 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 0.850 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 0.875 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 0.900 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 0.925 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 0.950 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 0.975 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 1.000 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 1.025 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 1.050 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 1.075 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 1.100 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 1.125 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 1.150 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 1.175 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 1.200 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 1.225 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 1.250 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 1.275 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 1.300 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 1.325 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 1.350 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 1.375 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 1.400 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 1.425 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 1.450 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 1.475 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 1.500 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 1.525 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 1.550 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 1.575 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 1.600 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 1.625 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 1.650 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 1.675 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 1.700 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 1.725 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 1.750 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 1.775 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 1.800 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 1.825 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 1.850 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 1.875 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 1.900 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 1.925 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 1.950 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 1.975 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 2.000 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 2.025 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 2.050 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 2.075 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 2.100 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 2.125 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 2.150 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 2.175 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 2.200 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 2.225 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 2.250 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 2.275 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 2.300 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 2.325 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 2.350 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 2.375 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 2.400 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 2.425 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 2.450 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 2.475 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 2.500 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 2.525 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 2.550 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 2.575 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 2.600 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 2.625 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 2.650 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 2.675 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 2.700 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 2.725 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 2.750 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 2.775 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 2.800 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 2.825 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 2.850 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 2.875 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 2.900 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 2.925 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 2.950 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 2.975 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 3.000 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 3.025 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 3.050 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 3.075 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 3.100 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 3.125 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 3.150 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 3.175 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 3.200 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 3.225 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 3.250 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 3.275 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 3.300 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 3.325 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 3.350 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 3.375 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 3.400 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 3.425 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 3.450 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 3.475 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 3.500 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 3.525 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 3.550 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 3.575 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 3.600 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 3.625 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 3.650 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 3.675 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 3.700 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 3.725 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 3.750 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 3.775 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 3.800 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 3.825 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 3.850 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 3.875 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 3.900 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 3.925 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 3.950 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 3.975 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 4.000 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 4.025 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 4.050 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 4.075 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 4.100 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 4.125 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 4.150 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 4.175 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 4.200 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 4.225 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 4.250 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 4.275 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 4.300 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 4.325 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 4.350 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 4.375 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 4.400 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 4.425 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 4.450 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 4.475 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 4.500 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 4.525 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 4.550 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 4.575 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 4.600 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 4.625 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 4.650 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 4.675 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 4.700 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 4.725 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 4.750 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 4.775 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 4.800 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 4.825 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 4.850 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 4.875 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 4.900 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 4.925 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 4.950 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 4.975 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 5.000 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 5.025 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 5.050 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 5.075 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 5.100 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 5.125 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 5.150 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 5.175 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 5.200 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 5.225 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 5.250 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 5.275 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 5.300 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 5.325 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 5.350 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 5.375 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 5.400 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 5.425 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 5.450 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 5.475 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 5.500 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 5.525 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 5.550 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 5.575 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 5.600 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 5.625 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 5.650 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 5.675 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 5.700 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 5.725 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 5.750 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 5.775 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 5.800 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 5.825 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 5.850 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 5.875 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 5.900 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 5.925 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 5.950 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 5.975 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 6.000 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 6.025 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 6.050 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 6.075 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 6.100 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 6.125 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 6.150 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 6.175 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 6.200 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 6.225 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 6.250 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 6.275 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 6.300 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 6.325 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 6.350 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 6.375 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 6.400 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 6.425 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 6.450 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 6.475 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 6.500 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 6.525 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 6.550 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 6.575 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 6.600 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 6.625 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 6.650 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 6.675 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 6.700 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 6.725 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 6.750 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 6.775 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 6.800 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 6.825 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 6.850 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 6.875 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 6.900 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 6.925 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 6.950 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 6.975 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 7.000 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 7.025 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 7.050 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 7.075 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 7.100 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 7.125 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 7.150 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 7.175 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 7.200 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 7.225 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 7.250 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 7.275 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 7.300 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 7.325 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 7.350 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 7.375 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 7.400 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 7.425 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 7.450 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 7.475 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 7.500 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 7.525 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 7.550 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 7.575 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 7.600 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 7.625 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 7.650 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 7.675 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 7.700 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 7.725 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 7.750 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 7.775 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 7.800 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 7.825 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 7.850 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 7.875 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 7.900 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 7.925 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 7.950 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 7.975 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 8.000 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 8.025 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 8.050 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 8.075 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 8.100 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 8.125 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 8.150 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 8.175 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 8.200 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 8.225 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 8.250 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 8.275 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 8.300 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 8.325 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 8.350 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 8.375 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 8.400 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 8.425 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 8.450 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 8.475 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 8.500 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 8.525 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 8.550 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 8.575 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 8.600 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 8.625 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 8.650 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 8.675 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 8.700 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 8.725 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 8.750 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 8.775 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 8.800 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 8.825 | 120.00 | 120.00 | 120.01 | 120.01 | 120.01 |
| 8.850 | 120.01 | 120.01 | 120.01 | 120.01 | 120.01 |
| 8.875 | 120.01 | 120.01 | 120.01 | 120.01 | 120.01 |
| 8.900 | 120.01 | 120.02 | 120.02 | 120.02 | 120.02 |
| 8.925 | 120.02 | 120.02 | 120.02 | 120.02 | 120.02 |
| 8.950 | 120.02 | 120.02 | 120.02 | 120.02 | 120.02 |
| 8.975 | 120.02 | 120.03 | 120.03 | 120.03 | 120.03 |
| 9.000 | 120.03 | 120.03 | 120.03 | 120.03 | 120.03 |
| 9.025 | 120.03 | 120.03 | 120.03 | 120.03 | 120.03 |
| 9.050 | 120.03 | 120.04 | 120.04 | 120.04 | 120.04 |
| 9.075 | 120.04 | 120.04 | 120.04 | 120.04 | 120.04 |
| 9.100 | 120.04 | 120.04 | 120.04 | 120.04 | 120.04 |
| 9.125 | 120.04 | 120.04 | 120.04 | 120.04 | 120.04 |
| 9.150 | 120.05 | 120.05 | 120.05 | 120.05 | 120.05 |
| 9.175 | 120.05 | 120.05 | 120.05 | 120.05 | 120.05 |
| 9.200 | 120.05 | 120.05 | 120.05 | 120.05 | 120.05 |
| 9.225 | 120.05 | 120.05 | 120.05 | 120.05 | 120.05 |
| 9.250 | 120.05 | 120.05 | 120.05 | 120.05 | 120.05 |
| 9.275 | 120.05 | 120.06 | 120.06 | 120.06 | 120.06 |
| 9.300 | 120.06 | 120.06 | 120.06 | 120.06 | 120.06 |
| 9.325 | 120.06 | 120.06 | 120.06 | 120.06 | 120.06 |
| 9.350 | 120.06 | 120.06 | 120.06 | 120.06 | 120.06 |
| 9.375 | 120.06 | 120.06 | 120.06 | 120.06 | 120.06 |
| 9.400 | 120.06 | 120.06 | 120.06 | 120.06 | 120.06 |
| 9.425 | 120.06 | 120.06 | 120.06 | 120.06 | 120.06 |
| 9.450 | 120.06 | 120.07 | 120.07 | 120.07 | 120.07 |
| 9.475 | 120.07 | 120.07 | 120.07 | 120.07 | 120.07 |
| 9.500 | 120.07 | 120.07 | 120.07 | 120.07 | 120.07 |
| 9.525 | 120.07 | 120.07 | 120.07 | 120.07 | 120.07 |
| 9.550 | 120.07 | 120.07 | 120.07 | 120.07 | 120.07 |
| 9.575 | 120.07 | 120.07 | 120.07 | 120.07 | 120.07 |
| 9.600 | 120.07 | 120.07 | 120.07 | 120.07 | 120.07 |
| 9.625 | 120.07 | 120.07 | 120.07 | 120.07 | 120.07 |
| 9.650 | 120.07 | 120.07 | 120.07 | 120.07 | 120.07 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 9.675 | 120.07 | 120.08 | 120.08 | 120.08 | 120.08 |
| 9.700 | 120.08 | 120.08 | 120.08 | 120.08 | 120.08 |
| 9.725 | 120.08 | 120.08 | 120.08 | 120.08 | 120.08 |
| 9.750 | 120.08 | 120.08 | 120.08 | 120.08 | 120.08 |
| 9.775 | 120.08 | 120.08 | 120.08 | 120.08 | 120.08 |
| 9.800 | 120.08 | 120.08 | 120.08 | 120.08 | 120.08 |
| 9.825 | 120.08 | 120.08 | 120.08 | 120.08 | 120.08 |
| 9.850 | 120.08 | 120.08 | 120.08 | 120.08 | 120.08 |
| 9.875 | 120.08 | 120.08 | 120.08 | 120.09 | 120.09 |
| 9.900 | 120.09 | 120.09 | 120.09 | 120.09 | 120.09 |
| 9.925 | 120.09 | 120.09 | 120.09 | 120.09 | 120.09 |
| 9.950 | 120.09 | 120.09 | 120.09 | 120.09 | 120.09 |
| 9.975 | 120.09 | 120.09 | 120.09 | 120.09 | 120.09 |
| 10.000 | 120.09 | 120.09 | 120.09 | 120.09 | 120.09 |
| 10.025 | 120.09 | 120.09 | 120.09 | 120.09 | 120.09 |
| 10.050 | 120.09 | 120.09 | 120.09 | 120.09 | 120.09 |
| 10.075 | 120.09 | 120.09 | 120.09 | 120.09 | 120.10 |
| 10.100 | 120.10 | 120.10 | 120.10 | 120.10 | 120.10 |
| 10.125 | 120.10 | 120.10 | 120.10 | 120.10 | 120.10 |
| 10.150 | 120.10 | 120.10 | 120.10 | 120.10 | 120.10 |
| 10.175 | 120.10 | 120.10 | 120.10 | 120.10 | 120.10 |
| 10.200 | 120.10 | 120.10 | 120.10 | 120.10 | 120.10 |
| 10.225 | 120.10 | 120.10 | 120.10 | 120.10 | 120.10 |
| 10.250 | 120.10 | 120.10 | 120.10 | 120.10 | 120.10 |
| 10.275 | 120.10 | 120.10 | 120.11 | 120.11 | 120.11 |
| 10.300 | 120.11 | 120.11 | 120.11 | 120.11 | 120.11 |
| 10.325 | 120.11 | 120.11 | 120.11 | 120.11 | 120.11 |
| 10.350 | 120.11 | 120.11 | 120.11 | 120.11 | 120.11 |
| 10.375 | 120.11 | 120.11 | 120.11 | 120.11 | 120.11 |
| 10.400 | 120.11 | 120.11 | 120.11 | 120.11 | 120.11 |
| 10.425 | 120.11 | 120.11 | 120.11 | 120.11 | 120.11 |
| 10.450 | 120.11 | 120.11 | 120.11 | 120.12 | 120.12 |
| 10.475 | 120.12 | 120.12 | 120.12 | 120.12 | 120.12 |
| 10.500 | 120.12 | 120.12 | 120.12 | 120.12 | 120.12 |
| 10.525 | 120.12 | 120.12 | 120.12 | 120.12 | 120.12 |
| 10.550 | 120.12 | 120.12 | 120.12 | 120.12 | 120.12 |
| 10.575 | 120.12 | 120.12 | 120.12 | 120.12 | 120.12 |
| 10.600 | 120.12 | 120.12 | 120.12 | 120.12 | 120.12 |
| 10.625 | 120.12 | 120.12 | 120.12 | 120.13 | 120.13 |
| 10.650 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 10.675 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 10.700 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 10.725 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 10.750 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 10.775 | 120.13 | 120.13 | 120.13 | 120.14 | 120.14 |
| 10.800 | 120.14 | 120.14 | 120.14 | 120.14 | 120.14 |
| 10.825 | 120.14 | 120.14 | 120.14 | 120.14 | 120.14 |
| 10.850 | 120.14 | 120.14 | 120.14 | 120.14 | 120.14 |
| 10.875 | 120.14 | 120.14 | 120.14 | 120.14 | 120.14 |
| 10.900 | 120.14 | 120.14 | 120.14 | 120.14 | 120.14 |
| 10.925 | 120.14 | 120.15 | 120.15 | 120.15 | 120.15 |
| 10.950 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |
| 10.975 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |
| 11.000 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |
| 11.025 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |
| 11.050 | 120.15 | 120.15 | 120.15 | 120.15 | 120.16 |
| 11.075 | 120.16 | 120.16 | 120.16 | 120.16 | 120.16 |
| 11.100 | 120.16 | 120.16 | 120.16 | 120.16 | 120.16 |
| 11.125 | 120.16 | 120.16 | 120.16 | 120.16 | 120.16 |
| 11.150 | 120.16 | 120.16 | 120.16 | 120.16 | 120.16 |
| 11.175 | 120.16 | 120.17 | 120.17 | 120.17 | 120.17 |
| 11.200 | 120.17 | 120.17 | 120.17 | 120.17 | 120.17 |
| 11.225 | 120.17 | 120.17 | 120.17 | 120.17 | 120.17 |
| 11.250 | 120.17 | 120.17 | 120.17 | 120.17 | 120.17 |
| 11.275 | 120.18 | 120.18 | 120.18 | 120.18 | 120.18 |
| 11.300 | 120.18 | 120.18 | 120.18 | 120.18 | 120.18 |
| 11.325 | 120.18 | 120.18 | 120.18 | 120.18 | 120.18 |
| 11.350 | 120.18 | 120.18 | 120.19 | 120.19 | 120.19 |
| 11.375 | 120.19 | 120.19 | 120.19 | 120.19 | 120.19 |
| 11.400 | 120.19 | 120.19 | 120.19 | 120.19 | 120.19 |
| 11.425 | 120.19 | 120.19 | 120.19 | 120.19 | 120.20 |
| 11.450 | 120.20 | 120.20 | 120.20 | 120.20 | 120.20 |
| 11.475 | 120.20 | 120.20 | 120.20 | 120.20 | 120.20 |
| 11.500 | 120.20 | 120.20 | 120.20 | 120.20 | 120.20 |
| 11.525 | 120.21 | 120.21 | 120.21 | 120.21 | 120.21 |
| 11.550 | 120.21 | 120.21 | 120.21 | 120.22 | 120.22 |
| 11.575 | 120.22 | 120.22 | 120.22 | 120.23 | 120.23 |
| 11.600 | 120.23 | 120.23 | 120.24 | 120.24 | 120.24 |
| 11.625 | 120.24 | 120.25 | 120.25 | 120.25 | 120.26 |
| 11.650 | 120.26 | 120.27 | 120.27 | 120.27 | 120.28 |
| 11.675 | 120.28 | 120.29 | 120.29 | 120.29 | 120.30 |
| 11.700 | 120.30 | 120.31 | 120.31 | 120.32 | 120.32 |
| 11.725 | 120.33 | 120.33 | 120.34 | 120.34 | 120.35 |
| 11.750 | 120.35 | 120.36 | 120.36 | 120.37 | 120.37 |
| 11.775 | 120.38 | 120.38 | 120.39 | 120.40 | 120.40 |
| 11.800 | 120.41 | 120.41 | 120.42 | 120.42 | 120.43 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 11.825 | 120.44 | 120.44 | 120.45 | 120.45 | 120.46 |
| 11.850 | 120.47 | 120.47 | 120.48 | 120.49 | 120.49 |
| 11.875 | 120.50 | 120.51 | 120.51 | 120.52 | 120.53 |
| 11.900 | 120.54 | 120.55 | 120.55 | 120.56 | 120.57 |
| 11.925 | 120.57 | 120.58 | 120.59 | 120.59 | 120.60 |
| 11.950 | 120.60 | 120.61 | 120.61 | 120.62 | 120.62 |
| 11.975 | 120.62 | 120.63 | 120.63 | 120.63 | 120.63 |
| 12.000 | 120.64 | 120.64 | 120.64 | 120.64 | 120.64 |
| 12.025 | 120.64 | 120.64 | 120.64 | 120.64 | 120.63 |
| 12.050 | 120.63 | 120.63 | 120.63 | 120.62 | 120.62 |
| 12.075 | 120.62 | 120.61 | 120.61 | 120.60 | 120.60 |
| 12.100 | 120.59 | 120.58 | 120.58 | 120.57 | 120.56 |
| 12.125 | 120.56 | 120.55 | 120.54 | 120.54 | 120.53 |
| 12.150 | 120.52 | 120.51 | 120.51 | 120.50 | 120.49 |
| 12.175 | 120.48 | 120.48 | 120.47 | 120.46 | 120.46 |
| 12.200 | 120.45 | 120.45 | 120.44 | 120.44 | 120.43 |
| 12.225 | 120.43 | 120.42 | 120.42 | 120.41 | 120.41 |
| 12.250 | 120.40 | 120.40 | 120.40 | 120.39 | 120.39 |
| 12.275 | 120.39 | 120.38 | 120.38 | 120.38 | 120.37 |
| 12.300 | 120.37 | 120.37 | 120.37 | 120.36 | 120.36 |
| 12.325 | 120.36 | 120.36 | 120.36 | 120.35 | 120.35 |
| 12.350 | 120.35 | 120.35 | 120.35 | 120.34 | 120.34 |
| 12.375 | 120.34 | 120.34 | 120.34 | 120.34 | 120.33 |
| 12.400 | 120.33 | 120.33 | 120.33 | 120.33 | 120.33 |
| 12.425 | 120.33 | 120.32 | 120.32 | 120.32 | 120.32 |
| 12.450 | 120.32 | 120.32 | 120.32 | 120.31 | 120.31 |
| 12.475 | 120.31 | 120.31 | 120.31 | 120.31 | 120.31 |
| 12.500 | 120.31 | 120.30 | 120.30 | 120.30 | 120.30 |
| 12.525 | 120.30 | 120.30 | 120.30 | 120.30 | 120.30 |
| 12.550 | 120.29 | 120.29 | 120.29 | 120.29 | 120.29 |
| 12.575 | 120.29 | 120.29 | 120.29 | 120.29 | 120.29 |
| 12.600 | 120.28 | 120.28 | 120.28 | 120.28 | 120.28 |
| 12.625 | 120.28 | 120.28 | 120.28 | 120.28 | 120.28 |
| 12.650 | 120.28 | 120.28 | 120.27 | 120.27 | 120.27 |
| 12.675 | 120.27 | 120.27 | 120.27 | 120.27 | 120.27 |
| 12.700 | 120.27 | 120.27 | 120.27 | 120.27 | 120.27 |
| 12.725 | 120.27 | 120.27 | 120.27 | 120.27 | 120.27 |
| 12.750 | 120.26 | 120.26 | 120.26 | 120.26 | 120.26 |
| 12.775 | 120.26 | 120.26 | 120.26 | 120.26 | 120.26 |
| 12.800 | 120.26 | 120.26 | 120.26 | 120.26 | 120.26 |
| 12.825 | 120.26 | 120.26 | 120.26 | 120.26 | 120.26 |
| 12.850 | 120.26 | 120.26 | 120.26 | 120.26 | 120.26 |
| 12.875 | 120.26 | 120.25 | 120.25 | 120.25 | 120.25 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 12.900 | 120.25 | 120.25 | 120.25 | 120.25 | 120.25 |
| 12.925 | 120.25 | 120.25 | 120.25 | 120.25 | 120.25 |
| 12.950 | 120.25 | 120.25 | 120.25 | 120.25 | 120.25 |
| 12.975 | 120.25 | 120.25 | 120.25 | 120.25 | 120.25 |
| 13.000 | 120.25 | 120.25 | 120.25 | 120.25 | 120.25 |
| 13.025 | 120.25 | 120.25 | 120.24 | 120.24 | 120.24 |
| 13.050 | 120.24 | 120.24 | 120.24 | 120.24 | 120.24 |
| 13.075 | 120.24 | 120.24 | 120.24 | 120.24 | 120.24 |
| 13.100 | 120.24 | 120.24 | 120.24 | 120.24 | 120.24 |
| 13.125 | 120.24 | 120.24 | 120.24 | 120.24 | 120.24 |
| 13.150 | 120.24 | 120.24 | 120.24 | 120.24 | 120.24 |
| 13.175 | 120.24 | 120.24 | 120.24 | 120.24 | 120.24 |
| 13.200 | 120.24 | 120.23 | 120.23 | 120.23 | 120.23 |
| 13.225 | 120.23 | 120.23 | 120.23 | 120.23 | 120.23 |
| 13.250 | 120.23 | 120.23 | 120.23 | 120.23 | 120.23 |
| 13.275 | 120.23 | 120.23 | 120.23 | 120.23 | 120.23 |
| 13.300 | 120.23 | 120.23 | 120.23 | 120.23 | 120.23 |
| 13.325 | 120.23 | 120.23 | 120.23 | 120.23 | 120.23 |
| 13.350 | 120.23 | 120.23 | 120.23 | 120.23 | 120.23 |
| 13.375 | 120.23 | 120.23 | 120.23 | 120.23 | 120.23 |
| 13.400 | 120.23 | 120.23 | 120.23 | 120.23 | 120.23 |
| 13.425 | 120.23 | 120.23 | 120.22 | 120.22 | 120.22 |
| 13.450 | 120.22 | 120.22 | 120.22 | 120.22 | 120.22 |
| 13.475 | 120.22 | 120.22 | 120.22 | 120.22 | 120.22 |
| 13.500 | 120.22 | 120.22 | 120.22 | 120.22 | 120.22 |
| 13.525 | 120.22 | 120.22 | 120.22 | 120.22 | 120.22 |
| 13.550 | 120.22 | 120.22 | 120.22 | 120.22 | 120.22 |
| 13.575 | 120.22 | 120.22 | 120.22 | 120.22 | 120.22 |
| 13.600 | 120.22 | 120.22 | 120.22 | 120.22 | 120.22 |
| 13.625 | 120.22 | 120.22 | 120.22 | 120.22 | 120.22 |
| 13.650 | 120.22 | 120.22 | 120.22 | 120.22 | 120.22 |
| 13.675 | 120.21 | 120.21 | 120.21 | 120.21 | 120.21 |
| 13.700 | 120.21 | 120.21 | 120.21 | 120.21 | 120.21 |
| 13.725 | 120.21 | 120.21 | 120.21 | 120.21 | 120.21 |
| 13.750 | 120.21 | 120.21 | 120.21 | 120.21 | 120.21 |
| 13.775 | 120.21 | 120.21 | 120.21 | 120.21 | 120.21 |
| 13.800 | 120.21 | 120.21 | 120.21 | 120.21 | 120.21 |
| 13.825 | 120.21 | 120.21 | 120.21 | 120.21 | 120.21 |
| 13.850 | 120.21 | 120.21 | 120.21 | 120.21 | 120.21 |
| 13.875 | 120.21 | 120.21 | 120.21 | 120.21 | 120.21 |
| 13.900 | 120.21 | 120.21 | 120.21 | 120.21 | 120.21 |
| 13.925 | 120.21 | 120.21 | 120.21 | 120.21 | 120.21 |
| 13.950 | 120.21 | 120.20 | 120.20 | 120.20 | 120.20 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 13.975 | 120.20 | 120.20 | 120.20 | 120.20 | 120.20 |
| 14.000 | 120.20 | 120.20 | 120.20 | 120.20 | 120.20 |
| 14.025 | 120.20 | 120.20 | 120.20 | 120.20 | 120.20 |
| 14.050 | 120.20 | 120.20 | 120.20 | 120.20 | 120.20 |
| 14.075 | 120.20 | 120.20 | 120.20 | 120.20 | 120.20 |
| 14.100 | 120.20 | 120.20 | 120.20 | 120.20 | 120.20 |
| 14.125 | 120.20 | 120.20 | 120.20 | 120.20 | 120.20 |
| 14.150 | 120.20 | 120.20 | 120.20 | 120.20 | 120.20 |
| 14.175 | 120.20 | 120.20 | 120.20 | 120.20 | 120.20 |
| 14.200 | 120.20 | 120.20 | 120.20 | 120.20 | 120.20 |
| 14.225 | 120.20 | 120.20 | 120.20 | 120.20 | 120.20 |
| 14.250 | 120.20 | 120.20 | 120.20 | 120.20 | 120.20 |
| 14.275 | 120.20 | 120.20 | 120.20 | 120.20 | 120.20 |
| 14.300 | 120.20 | 120.20 | 120.20 | 120.20 | 120.20 |
| 14.325 | 120.20 | 120.20 | 120.19 | 120.19 | 120.19 |
| 14.350 | 120.19 | 120.19 | 120.19 | 120.19 | 120.19 |
| 14.375 | 120.19 | 120.19 | 120.19 | 120.19 | 120.19 |
| 14.400 | 120.19 | 120.19 | 120.19 | 120.19 | 120.19 |
| 14.425 | 120.19 | 120.19 | 120.19 | 120.19 | 120.19 |
| 14.450 | 120.19 | 120.19 | 120.19 | 120.19 | 120.19 |
| 14.475 | 120.19 | 120.19 | 120.19 | 120.19 | 120.19 |
| 14.500 | 120.19 | 120.19 | 120.19 | 120.19 | 120.19 |
| 14.525 | 120.19 | 120.19 | 120.19 | 120.19 | 120.19 |
| 14.550 | 120.19 | 120.19 | 120.19 | 120.19 | 120.19 |
| 14.575 | 120.19 | 120.19 | 120.19 | 120.19 | 120.19 |
| 14.600 | 120.19 | 120.19 | 120.19 | 120.19 | 120.19 |
| 14.625 | 120.19 | 120.19 | 120.19 | 120.19 | 120.19 |
| 14.650 | 120.19 | 120.19 | 120.19 | 120.19 | 120.19 |
| 14.675 | 120.19 | 120.19 | 120.19 | 120.19 | 120.19 |
| 14.700 | 120.19 | 120.19 | 120.19 | 120.19 | 120.19 |
| 14.725 | 120.19 | 120.19 | 120.19 | 120.19 | 120.19 |
| 14.750 | 120.19 | 120.19 | 120.19 | 120.19 | 120.19 |
| 14.775 | 120.19 | 120.19 | 120.19 | 120.19 | 120.19 |
| 14.800 | 120.19 | 120.19 | 120.19 | 120.19 | 120.19 |
| 14.825 | 120.19 | 120.19 | 120.19 | 120.19 | 120.19 |
| 14.850 | 120.19 | 120.19 | 120.19 | 120.19 | 120.19 |
| 14.875 | 120.19 | 120.19 | 120.19 | 120.19 | 120.19 |
| 14.900 | 120.19 | 120.19 | 120.19 | 120.19 | 120.19 |
| 14.925 | 120.19 | 120.19 | 120.19 | 120.19 | 120.19 |
| 14.950 | 120.19 | 120.19 | 120.19 | 120.19 | 120.19 |
| 14.975 | 120.19 | 120.19 | 120.19 | 120.19 | 120.19 |
| 15.000 | 120.19 | 120.19 | 120.19 | 120.19 | 120.19 |
| 15.025 | 120.19 | 120.19 | 120.19 | 120.19 | 120.18 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 15.050 | 120.18 | 120.18 | 120.18 | 120.18 | 120.18 |
| 15.075 | 120.18 | 120.18 | 120.18 | 120.18 | 120.18 |
| 15.100 | 120.18 | 120.18 | 120.18 | 120.18 | 120.18 |
| 15.125 | 120.18 | 120.18 | 120.18 | 120.18 | 120.18 |
| 15.150 | 120.18 | 120.18 | 120.18 | 120.18 | 120.18 |
| 15.175 | 120.18 | 120.18 | 120.18 | 120.18 | 120.18 |
| 15.200 | 120.18 | 120.18 | 120.18 | 120.18 | 120.18 |
| 15.225 | 120.18 | 120.18 | 120.18 | 120.18 | 120.18 |
| 15.250 | 120.18 | 120.18 | 120.18 | 120.18 | 120.18 |
| 15.275 | 120.18 | 120.18 | 120.18 | 120.18 | 120.18 |
| 15.300 | 120.18 | 120.18 | 120.18 | 120.18 | 120.18 |
| 15.325 | 120.18 | 120.18 | 120.18 | 120.18 | 120.18 |
| 15.350 | 120.18 | 120.18 | 120.18 | 120.18 | 120.18 |
| 15.375 | 120.18 | 120.18 | 120.18 | 120.18 | 120.18 |
| 15.400 | 120.18 | 120.18 | 120.18 | 120.18 | 120.18 |
| 15.425 | 120.18 | 120.18 | 120.18 | 120.18 | 120.18 |
| 15.450 | 120.18 | 120.18 | 120.18 | 120.18 | 120.18 |
| 15.475 | 120.18 | 120.18 | 120.18 | 120.18 | 120.18 |
| 15.500 | 120.18 | 120.18 | 120.18 | 120.18 | 120.18 |
| 15.525 | 120.18 | 120.18 | 120.18 | 120.18 | 120.18 |
| 15.550 | 120.18 | 120.18 | 120.18 | 120.18 | 120.18 |
| 15.575 | 120.18 | 120.18 | 120.18 | 120.18 | 120.18 |
| 15.600 | 120.18 | 120.18 | 120.18 | 120.18 | 120.18 |
| 15.625 | 120.18 | 120.18 | 120.18 | 120.18 | 120.18 |
| 15.650 | 120.18 | 120.18 | 120.18 | 120.18 | 120.18 |
| 15.675 | 120.18 | 120.18 | 120.17 | 120.17 | 120.17 |
| 15.700 | 120.17 | 120.17 | 120.17 | 120.17 | 120.17 |
| 15.725 | 120.17 | 120.17 | 120.17 | 120.17 | 120.17 |
| 15.750 | 120.17 | 120.17 | 120.17 | 120.17 | 120.17 |
| 15.775 | 120.17 | 120.17 | 120.17 | 120.17 | 120.17 |
| 15.800 | 120.17 | 120.17 | 120.17 | 120.17 | 120.17 |
| 15.825 | 120.17 | 120.17 | 120.17 | 120.17 | 120.17 |
| 15.850 | 120.17 | 120.17 | 120.17 | 120.17 | 120.17 |
| 15.875 | 120.17 | 120.17 | 120.17 | 120.17 | 120.17 |
| 15.900 | 120.17 | 120.17 | 120.17 | 120.17 | 120.17 |
| 15.925 | 120.17 | 120.17 | 120.17 | 120.17 | 120.17 |
| 15.950 | 120.17 | 120.17 | 120.17 | 120.17 | 120.17 |
| 15.975 | 120.17 | 120.17 | 120.17 | 120.17 | 120.17 |
| 16.000 | 120.17 | 120.17 | 120.17 | 120.17 | 120.17 |
| 16.025 | 120.17 | 120.17 | 120.17 | 120.17 | 120.17 |
| 16.050 | 120.17 | 120.17 | 120.17 | 120.17 | 120.17 |
| 16.075 | 120.17 | 120.17 | 120.17 | 120.17 | 120.17 |
| 16.100 | 120.17 | 120.17 | 120.17 | 120.17 | 120.17 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 16.125 | 120.17 | 120.17 | 120.17 | 120.17 | 120.17 |
| 16.150 | 120.17 | 120.17 | 120.17 | 120.17 | 120.17 |
| 16.175 | 120.17 | 120.17 | 120.17 | 120.17 | 120.17 |
| 16.200 | 120.17 | 120.17 | 120.17 | 120.17 | 120.17 |
| 16.225 | 120.17 | 120.17 | 120.17 | 120.17 | 120.17 |
| 16.250 | 120.17 | 120.17 | 120.17 | 120.17 | 120.17 |
| 16.275 | 120.17 | 120.17 | 120.17 | 120.17 | 120.17 |
| 16.300 | 120.17 | 120.17 | 120.17 | 120.17 | 120.17 |
| 16.325 | 120.17 | 120.17 | 120.17 | 120.17 | 120.17 |
| 16.350 | 120.17 | 120.17 | 120.17 | 120.17 | 120.17 |
| 16.375 | 120.17 | 120.17 | 120.17 | 120.17 | 120.17 |
| 16.400 | 120.16 | 120.16 | 120.16 | 120.16 | 120.16 |
| 16.425 | 120.16 | 120.16 | 120.16 | 120.16 | 120.16 |
| 16.450 | 120.16 | 120.16 | 120.16 | 120.16 | 120.16 |
| 16.475 | 120.16 | 120.16 | 120.16 | 120.16 | 120.16 |
| 16.500 | 120.16 | 120.16 | 120.16 | 120.16 | 120.16 |
| 16.525 | 120.16 | 120.16 | 120.16 | 120.16 | 120.16 |
| 16.550 | 120.16 | 120.16 | 120.16 | 120.16 | 120.16 |
| 16.575 | 120.16 | 120.16 | 120.16 | 120.16 | 120.16 |
| 16.600 | 120.16 | 120.16 | 120.16 | 120.16 | 120.16 |
| 16.625 | 120.16 | 120.16 | 120.16 | 120.16 | 120.16 |
| 16.650 | 120.16 | 120.16 | 120.16 | 120.16 | 120.16 |
| 16.675 | 120.16 | 120.16 | 120.16 | 120.16 | 120.16 |
| 16.700 | 120.16 | 120.16 | 120.16 | 120.16 | 120.16 |
| 16.725 | 120.16 | 120.16 | 120.16 | 120.16 | 120.16 |
| 16.750 | 120.16 | 120.16 | 120.16 | 120.16 | 120.16 |
| 16.775 | 120.16 | 120.16 | 120.16 | 120.16 | 120.16 |
| 16.800 | 120.16 | 120.16 | 120.16 | 120.16 | 120.16 |
| 16.825 | 120.16 | 120.16 | 120.16 | 120.16 | 120.16 |
| 16.850 | 120.16 | 120.16 | 120.16 | 120.16 | 120.16 |
| 16.875 | 120.16 | 120.16 | 120.16 | 120.16 | 120.16 |
| 16.900 | 120.16 | 120.16 | 120.16 | 120.16 | 120.16 |
| 16.925 | 120.16 | 120.16 | 120.16 | 120.16 | 120.16 |
| 16.950 | 120.16 | 120.16 | 120.16 | 120.16 | 120.16 |
| 16.975 | 120.16 | 120.16 | 120.16 | 120.16 | 120.16 |
| 17.000 | 120.16 | 120.16 | 120.16 | 120.16 | 120.16 |
| 17.025 | 120.16 | 120.16 | 120.16 | 120.16 | 120.16 |
| 17.050 | 120.16 | 120.16 | 120.16 | 120.16 | 120.16 |
| 17.075 | 120.16 | 120.16 | 120.16 | 120.16 | 120.16 |
| 17.100 | 120.16 | 120.16 | 120.16 | 120.16 | 120.16 |
| 17.125 | 120.16 | 120.16 | 120.16 | 120.16 | 120.16 |
| 17.150 | 120.16 | 120.16 | 120.16 | 120.16 | 120.16 |
| 17.175 | 120.16 | 120.16 | 120.16 | 120.16 | 120.16 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 17.200 | 120.16 | 120.16 | 120.16 | 120.16 | 120.16 |
| 17.225 | 120.16 | 120.16 | 120.16 | 120.16 | 120.16 |
| 17.250 | 120.16 | 120.16 | 120.16 | 120.16 | 120.16 |
| 17.275 | 120.16 | 120.16 | 120.16 | 120.16 | 120.16 |
| 17.300 | 120.16 | 120.16 | 120.16 | 120.16 | 120.16 |
| 17.325 | 120.16 | 120.16 | 120.16 | 120.16 | 120.16 |
| 17.350 | 120.16 | 120.16 | 120.16 | 120.16 | 120.16 |
| 17.375 | 120.16 | 120.16 | 120.16 | 120.16 | 120.16 |
| 17.400 | 120.16 | 120.16 | 120.16 | 120.16 | 120.16 |
| 17.425 | 120.16 | 120.16 | 120.16 | 120.16 | 120.16 |
| 17.450 | 120.16 | 120.16 | 120.16 | 120.16 | 120.16 |
| 17.475 | 120.16 | 120.16 | 120.16 | 120.16 | 120.16 |
| 17.500 | 120.16 | 120.16 | 120.16 | 120.16 | 120.16 |
| 17.525 | 120.16 | 120.16 | 120.16 | 120.16 | 120.16 |
| 17.550 | 120.16 | 120.16 | 120.16 | 120.16 | 120.16 |
| 17.575 | 120.16 | 120.16 | 120.16 | 120.16 | 120.16 |
| 17.600 | 120.16 | 120.16 | 120.16 | 120.16 | 120.16 |
| 17.625 | 120.16 | 120.16 | 120.16 | 120.16 | 120.16 |
| 17.650 | 120.16 | 120.16 | 120.16 | 120.16 | 120.16 |
| 17.675 | 120.16 | 120.16 | 120.16 | 120.16 | 120.16 |
| 17.700 | 120.16 | 120.16 | 120.16 | 120.16 | 120.16 |
| 17.725 | 120.16 | 120.16 | 120.16 | 120.16 | 120.16 |
| 17.750 | 120.16 | 120.16 | 120.16 | 120.16 | 120.16 |
| 17.775 | 120.16 | 120.16 | 120.16 | 120.16 | 120.16 |
| 17.800 | 120.16 | 120.16 | 120.16 | 120.16 | 120.16 |
| 17.825 | 120.16 | 120.16 | 120.16 | 120.16 | 120.16 |
| 17.850 | 120.16 | 120.16 | 120.16 | 120.15 | 120.15 |
| 17.875 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |
| 17.900 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |
| 17.925 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |
| 17.950 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |
| 17.975 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |
| 18.000 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |
| 18.025 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |
| 18.050 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |
| 18.075 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |
| 18.100 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |
| 18.125 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |
| 18.150 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |
| 18.175 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |
| 18.200 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |
| 18.225 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |
| 18.250 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 18.275 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |
| 18.300 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |
| 18.325 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |
| 18.350 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |
| 18.375 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |
| 18.400 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |
| 18.425 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |
| 18.450 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |
| 18.475 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |
| 18.500 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |
| 18.525 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |
| 18.550 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |
| 18.575 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |
| 18.600 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |
| 18.625 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |
| 18.650 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |
| 18.675 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |
| 18.700 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |
| 18.725 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |
| 18.750 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |
| 18.775 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |
| 18.800 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |
| 18.825 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |
| 18.850 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |
| 18.875 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |
| 18.900 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |
| 18.925 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |
| 18.950 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |
| 18.975 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |
| 19.000 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |
| 19.025 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |
| 19.050 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |
| 19.075 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |
| 19.100 | 120.15 | 120.15 | 120.15 | 120.15 | 120.15 |
| 19.125 | 120.15 | 120.15 | 120.14 | 120.14 | 120.14 |
| 19.150 | 120.14 | 120.14 | 120.14 | 120.14 | 120.14 |
| 19.175 | 120.14 | 120.14 | 120.14 | 120.14 | 120.14 |
| 19.200 | 120.14 | 120.14 | 120.14 | 120.14 | 120.14 |
| 19.225 | 120.14 | 120.14 | 120.14 | 120.14 | 120.14 |
| 19.250 | 120.14 | 120.14 | 120.14 | 120.14 | 120.14 |
| 19.275 | 120.14 | 120.14 | 120.14 | 120.14 | 120.14 |
| 19.300 | 120.14 | 120.14 | 120.14 | 120.14 | 120.14 |
| 19.325 | 120.14 | 120.14 | 120.14 | 120.14 | 120.14 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 19.350 | 120.14 | 120.14 | 120.14 | 120.14 | 120.14 |
| 19.375 | 120.14 | 120.14 | 120.14 | 120.14 | 120.14 |
| 19.400 | 120.14 | 120.14 | 120.14 | 120.14 | 120.14 |
| 19.425 | 120.14 | 120.14 | 120.14 | 120.14 | 120.14 |
| 19.450 | 120.14 | 120.14 | 120.14 | 120.14 | 120.14 |
| 19.475 | 120.14 | 120.14 | 120.14 | 120.14 | 120.14 |
| 19.500 | 120.14 | 120.14 | 120.14 | 120.14 | 120.14 |
| 19.525 | 120.14 | 120.14 | 120.14 | 120.14 | 120.14 |
| 19.550 | 120.14 | 120.14 | 120.14 | 120.14 | 120.14 |
| 19.575 | 120.14 | 120.14 | 120.14 | 120.14 | 120.14 |
| 19.600 | 120.14 | 120.14 | 120.14 | 120.14 | 120.14 |
| 19.625 | 120.14 | 120.14 | 120.14 | 120.14 | 120.14 |
| 19.650 | 120.14 | 120.14 | 120.14 | 120.14 | 120.14 |
| 19.675 | 120.14 | 120.14 | 120.14 | 120.14 | 120.14 |
| 19.700 | 120.14 | 120.14 | 120.14 | 120.14 | 120.14 |
| 19.725 | 120.14 | 120.14 | 120.14 | 120.14 | 120.14 |
| 19.750 | 120.14 | 120.14 | 120.14 | 120.14 | 120.14 |
| 19.775 | 120.14 | 120.14 | 120.14 | 120.14 | 120.14 |
| 19.800 | 120.14 | 120.14 | 120.14 | 120.14 | 120.14 |
| 19.825 | 120.14 | 120.14 | 120.14 | 120.14 | 120.14 |
| 19.850 | 120.14 | 120.14 | 120.14 | 120.14 | 120.14 |
| 19.875 | 120.14 | 120.14 | 120.14 | 120.14 | 120.14 |
| 19.900 | 120.14 | 120.14 | 120.14 | 120.14 | 120.14 |
| 19.925 | 120.14 | 120.14 | 120.14 | 120.14 | 120.14 |
| 19.950 | 120.14 | 120.14 | 120.14 | 120.14 | 120.14 |
| 19.975 | 120.14 | 120.14 | 120.14 | 120.14 | 120.14 |
| 20.000 | 120.14 | 120.14 | 120.14 | 120.14 | 120.14 |
| 20.025 | 120.14 | 120.14 | 120.14 | 120.14 | 120.14 |
| 20.050 | 120.14 | 120.14 | 120.14 | 120.14 | 120.14 |
| 20.075 | 120.14 | 120.14 | 120.14 | 120.14 | 120.14 |
| 20.100 | 120.14 | 120.14 | 120.14 | 120.14 | 120.14 |
| 20.125 | 120.14 | 120.14 | 120.14 | 120.14 | 120.14 |
| 20.150 | 120.14 | 120.14 | 120.14 | 120.14 | 120.14 |
| 20.175 | 120.14 | 120.14 | 120.14 | 120.14 | 120.14 |
| 20.200 | 120.14 | 120.14 | 120.14 | 120.14 | 120.14 |
| 20.225 | 120.14 | 120.14 | 120.14 | 120.14 | 120.14 |
| 20.250 | 120.14 | 120.14 | 120.14 | 120.14 | 120.14 |
| 20.275 | 120.14 | 120.14 | 120.14 | 120.14 | 120.14 |
| 20.300 | 120.14 | 120.14 | 120.14 | 120.14 | 120.14 |
| 20.325 | 120.14 | 120.14 | 120.14 | 120.14 | 120.14 |
| 20.350 | 120.14 | 120.14 | 120.14 | 120.14 | 120.14 |
| 20.375 | 120.14 | 120.14 | 120.14 | 120.14 | 120.14 |
| 20.400 | 120.14 | 120.14 | 120.14 | 120.14 | 120.14 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 20.425 | 120.14 | 120.14 | 120.14 | 120.14 | 120.14 |
| 20.450 | 120.14 | 120.14 | 120.14 | 120.14 | 120.14 |
| 20.475 | 120.14 | 120.14 | 120.14 | 120.14 | 120.14 |
| 20.500 | 120.14 | 120.14 | 120.14 | 120.14 | 120.13 |
| 20.525 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 20.550 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 20.575 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 20.600 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 20.625 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 20.650 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 20.675 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 20.700 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 20.725 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 20.750 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 20.775 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 20.800 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 20.825 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 20.850 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 20.875 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 20.900 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 20.925 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 20.950 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 20.975 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 21.000 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 21.025 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 21.050 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 21.075 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 21.100 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 21.125 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 21.150 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 21.175 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 21.200 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 21.225 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 21.250 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 21.275 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 21.300 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 21.325 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 21.350 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 21.375 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 21.400 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 21.425 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 21.450 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 21.475 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 21.500 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 21.525 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 21.550 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 21.575 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 21.600 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 21.625 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 21.650 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 21.675 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 21.700 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 21.725 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 21.750 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 21.775 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 21.800 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 21.825 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 21.850 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 21.875 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 21.900 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 21.925 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 21.950 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 21.975 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 22.000 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 22.025 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 22.050 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 22.075 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 22.100 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 22.125 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 22.150 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 22.175 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 22.200 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 22.225 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 22.250 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 22.275 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 22.300 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 22.325 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 22.350 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 22.375 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 22.400 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 22.425 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 22.450 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 22.475 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 22.500 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 22.525 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 22.550 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 22.575 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 22.600 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 22.625 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 22.650 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 22.675 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 22.700 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 22.725 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 22.750 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 22.775 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 22.800 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 22.825 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 22.850 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 22.875 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 22.900 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 22.925 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 22.950 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 22.975 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 23.000 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 23.025 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 23.050 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 23.075 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 23.100 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 23.125 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 23.150 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 23.175 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 23.200 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 23.225 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 23.250 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 23.275 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 23.300 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 23.325 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 23.350 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 23.375 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 23.400 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 23.425 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 23.450 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 23.475 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 23.500 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 23.525 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 23.550 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 23.575 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 23.600 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 23.625 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 23.650 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 23.675 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 23.700 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 23.725 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 23.750 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 23.775 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 23.800 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 23.825 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 23.850 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 23.875 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 23.900 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 23.925 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 23.950 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 23.975 | 120.13 | 120.13 | 120.13 | 120.13 | 120.13 |
| 24.000 | 120.13 | (N/A) | (N/A) | (N/A) | (N/A) |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 0.000 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 0.025 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 0.050 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 0.075 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 0.100 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 0.125 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 0.150 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 0.175 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 0.200 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 0.225 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 0.250 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 0.275 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 0.300 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 0.325 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 0.350 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 0.375 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 0.400 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 0.425 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 0.450 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 0.475 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 0.500 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 0.525 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 0.550 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 0.575 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 0.600 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 0.625 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 0.650 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 0.675 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 0.700 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 0.725 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 0.750 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 0.775 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 0.800 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 0.825 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 0.850 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 0.875 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 0.900 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 0.925 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 0.950 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 0.975 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 1.000 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 1.025 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 1.050 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 1.075 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 1.100 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 1.125 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 1.150 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 1.175 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 1.200 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 1.225 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 1.250 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 1.275 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 1.300 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 1.325 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 1.350 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 1.375 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 1.400 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 1.425 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 1.450 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 1.475 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 1.500 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 1.525 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 1.550 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 1.575 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 1.600 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 1.625 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 1.650 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 1.675 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 1.700 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 1.725 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 1.750 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 1.775 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 1.800 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 1.825 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 1.850 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 1.875 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 1.900 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 1.925 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 1.950 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 1.975 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 2.000 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 2.025 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 2.050 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 2.075 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 2.100 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 2.125 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 2.150 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 2.175 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 2.200 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 2.225 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 2.250 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 2.275 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 2.300 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 2.325 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 2.350 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 2.375 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 2.400 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 2.425 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 2.450 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 2.475 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 2.500 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 2.525 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 2.550 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 2.575 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 2.600 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 2.625 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 2.650 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 2.675 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 2.700 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 2.725 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 2.750 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 2.775 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 2.800 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 2.825 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 2.850 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 2.875 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 2.900 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 2.925 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 2.950 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 2.975 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 3.000 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 3.025 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 3.050 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 3.075 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 3.100 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 3.125 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 3.150 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 3.175 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 3.200 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 3.225 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 3.250 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 3.275 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 3.300 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 3.325 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 3.350 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 3.375 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 3.400 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 3.425 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 3.450 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 3.475 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 3.500 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 3.525 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 3.550 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 3.575 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 3.600 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 3.625 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 3.650 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 3.675 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 3.700 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 3.725 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 3.750 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 3.775 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 3.800 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 3.825 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 3.850 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 3.875 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 3.900 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 3.925 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 3.950 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 3.975 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 4.000 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 4.025 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 4.050 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 4.075 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 4.100 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 4.125 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 4.150 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 4.175 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 4.200 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 4.225 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 4.250 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 4.275 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 4.300 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 4.325 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 4.350 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 4.375 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 4.400 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 4.425 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 4.450 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 4.475 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 4.500 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 4.525 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 4.550 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 4.575 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 4.600 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 4.625 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 4.650 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 4.675 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 4.700 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 4.725 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 4.750 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 4.775 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 4.800 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 4.825 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 4.850 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 4.875 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 4.900 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 4.925 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 4.950 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 4.975 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 5.000 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 5.025 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 5.050 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 5.075 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 5.100 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 5.125 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 5.150 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 5.175 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 5.200 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 5.225 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 5.250 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 5.275 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 5.300 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 5.325 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 5.350 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 5.375 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 5.400 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 5.425 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 5.450 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 5.475 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 5.500 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 5.525 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 5.550 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 5.575 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 5.600 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 5.625 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 5.650 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 5.675 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 5.700 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 5.725 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 5.750 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 5.775 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 5.800 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 5.825 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 5.850 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 5.875 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 5.900 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 5.925 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 5.950 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 5.975 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 6.000 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 6.025 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 6.050 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 6.075 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 6.100 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 6.125 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 6.150 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 6.175 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 6.200 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 6.225 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 6.250 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 6.275 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 6.300 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 6.325 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 6.350 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 6.375 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 6.400 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 6.425 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 6.450 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 6.475 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 6.500 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 6.525 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 6.550 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 6.575 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 6.600 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 6.625 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 6.650 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 6.675 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 6.700 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 6.725 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 6.750 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 6.775 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 6.800 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 6.825 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 6.850 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 6.875 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 6.900 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 6.925 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 6.950 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 6.975 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 7.000 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 7.025 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 7.050 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 7.075 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 7.100 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 7.125 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 7.150 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 7.175 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 7.200 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 7.225 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 7.250 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 7.275 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 7.300 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 7.325 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 7.350 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 7.375 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 7.400 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 7.425 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 7.450 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 7.475 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 7.500 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 7.525 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 7.550 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 7.575 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 7.600 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 7.625 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 7.650 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 7.675 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 7.700 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 7.725 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 7.750 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 7.775 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 7.800 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 7.825 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 7.850 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 7.875 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 7.900 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 7.925 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 7.950 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 7.975 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 8.000 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 8.025 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 8.050 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 8.075 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 8.100 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 8.125 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 8.150 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 8.175 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 8.200 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 8.225 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 8.250 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 8.275 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 8.300 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 8.325 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 8.350 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 8.375 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 8.400 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 8.425 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 8.450 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 8.475 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 8.500 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 8.525 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 8.550 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 8.575 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 8.600 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 8.625 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 8.650 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 8.675 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 8.700 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 8.725 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 8.750 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 8.775 | 132.00 | 132.00 | 132.00 | 132.00 | 132.00 |
| 8.800 | 132.00 | 132.00 | 132.00 | 132.01 | 132.01 |
| 8.825 | 132.01 | 132.01 | 132.01 | 132.01 | 132.01 |
| 8.850 | 132.01 | 132.01 | 132.01 | 132.01 | 132.01 |
| 8.875 | 132.01 | 132.01 | 132.02 | 132.02 | 132.02 |
| 8.900 | 132.02 | 132.02 | 132.02 | 132.02 | 132.02 |
| 8.925 | 132.02 | 132.03 | 132.03 | 132.03 | 132.03 |
| 8.950 | 132.03 | 132.03 | 132.04 | 132.04 | 132.04 |
| 8.975 | 132.04 | 132.04 | 132.04 | 132.04 | 132.04 |
| 9.000 | 132.05 | 132.05 | 132.05 | 132.05 | 132.05 |
| 9.025 | 132.05 | 132.05 | 132.05 | 132.05 | 132.05 |
| 9.050 | 132.06 | 132.06 | 132.06 | 132.06 | 132.06 |
| 9.075 | 132.06 | 132.06 | 132.06 | 132.06 | 132.07 |
| 9.100 | 132.07 | 132.07 | 132.07 | 132.07 | 132.07 |
| 9.125 | 132.07 | 132.07 | 132.08 | 132.08 | 132.08 |
| 9.150 | 132.08 | 132.08 | 132.08 | 132.08 | 132.08 |
| 9.175 | 132.08 | 132.08 | 132.09 | 132.09 | 132.09 |
| 9.200 | 132.09 | 132.09 | 132.09 | 132.09 | 132.09 |
| 9.225 | 132.09 | 132.09 | 132.09 | 132.09 | 132.09 |
| 9.250 | 132.09 | 132.10 | 132.10 | 132.10 | 132.10 |
| 9.275 | 132.10 | 132.10 | 132.10 | 132.10 | 132.10 |
| 9.300 | 132.10 | 132.10 | 132.10 | 132.10 | 132.10 |
| 9.325 | 132.11 | 132.11 | 132.11 | 132.11 | 132.11 |
| 9.350 | 132.11 | 132.11 | 132.11 | 132.11 | 132.11 |
| 9.375 | 132.11 | 132.11 | 132.11 | 132.11 | 132.11 |
| 9.400 | 132.12 | 132.12 | 132.12 | 132.12 | 132.12 |
| 9.425 | 132.12 | 132.12 | 132.12 | 132.12 | 132.12 |
| 9.450 | 132.12 | 132.12 | 132.12 | 132.12 | 132.12 |
| 9.475 | 132.12 | 132.12 | 132.12 | 132.12 | 132.13 |
| 9.500 | 132.13 | 132.13 | 132.13 | 132.13 | 132.13 |
| 9.525 | 132.13 | 132.13 | 132.13 | 132.13 | 132.13 |
| 9.550 | 132.13 | 132.13 | 132.13 | 132.13 | 132.13 |
| 9.575 | 132.13 | 132.13 | 132.13 | 132.13 | 132.13 |
| 9.600 | 132.13 | 132.13 | 132.13 | 132.13 | 132.14 |
| 9.625 | 132.14 | 132.14 | 132.14 | 132.14 | 132.14 |
| 9.650 | 132.14 | 132.14 | 132.14 | 132.14 | 132.14 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 9.675 | 132.14 | 132.14 | 132.14 | 132.14 | 132.14 |
| 9.700 | 132.14 | 132.14 | 132.14 | 132.14 | 132.14 |
| 9.725 | 132.14 | 132.14 | 132.14 | 132.15 | 132.15 |
| 9.750 | 132.15 | 132.15 | 132.15 | 132.15 | 132.15 |
| 9.775 | 132.15 | 132.15 | 132.15 | 132.15 | 132.15 |
| 9.800 | 132.15 | 132.15 | 132.15 | 132.15 | 132.15 |
| 9.825 | 132.15 | 132.15 | 132.15 | 132.16 | 132.16 |
| 9.850 | 132.16 | 132.16 | 132.16 | 132.16 | 132.16 |
| 9.875 | 132.16 | 132.16 | 132.16 | 132.16 | 132.16 |
| 9.900 | 132.16 | 132.16 | 132.16 | 132.16 | 132.16 |
| 9.925 | 132.16 | 132.16 | 132.16 | 132.16 | 132.17 |
| 9.950 | 132.17 | 132.17 | 132.17 | 132.17 | 132.17 |
| 9.975 | 132.17 | 132.17 | 132.17 | 132.17 | 132.17 |
| 10.000 | 132.17 | 132.17 | 132.17 | 132.17 | 132.17 |
| 10.025 | 132.17 | 132.17 | 132.17 | 132.17 | 132.17 |
| 10.050 | 132.17 | 132.17 | 132.18 | 132.18 | 132.18 |
| 10.075 | 132.18 | 132.18 | 132.18 | 132.18 | 132.18 |
| 10.100 | 132.18 | 132.18 | 132.18 | 132.18 | 132.18 |
| 10.125 | 132.18 | 132.18 | 132.18 | 132.18 | 132.18 |
| 10.150 | 132.18 | 132.18 | 132.18 | 132.19 | 132.19 |
| 10.175 | 132.19 | 132.19 | 132.19 | 132.19 | 132.19 |
| 10.200 | 132.19 | 132.19 | 132.19 | 132.19 | 132.19 |
| 10.225 | 132.19 | 132.19 | 132.19 | 132.19 | 132.19 |
| 10.250 | 132.19 | 132.19 | 132.20 | 132.20 | 132.20 |
| 10.275 | 132.20 | 132.20 | 132.20 | 132.20 | 132.20 |
| 10.300 | 132.20 | 132.20 | 132.20 | 132.20 | 132.20 |
| 10.325 | 132.20 | 132.20 | 132.20 | 132.20 | 132.20 |
| 10.350 | 132.21 | 132.21 | 132.21 | 132.21 | 132.21 |
| 10.375 | 132.21 | 132.21 | 132.21 | 132.21 | 132.21 |
| 10.400 | 132.21 | 132.21 | 132.21 | 132.21 | 132.21 |
| 10.425 | 132.21 | 132.21 | 132.21 | 132.21 | 132.21 |
| 10.450 | 132.21 | 132.22 | 132.22 | 132.22 | 132.22 |
| 10.475 | 132.22 | 132.22 | 132.22 | 132.22 | 132.22 |
| 10.500 | 132.22 | 132.22 | 132.22 | 132.22 | 132.22 |
| 10.525 | 132.22 | 132.22 | 132.22 | 132.22 | 132.23 |
| 10.550 | 132.23 | 132.23 | 132.23 | 132.23 | 132.23 |
| 10.575 | 132.23 | 132.23 | 132.23 | 132.23 | 132.23 |
| 10.600 | 132.23 | 132.23 | 132.23 | 132.23 | 132.23 |
| 10.625 | 132.23 | 132.24 | 132.24 | 132.24 | 132.24 |
| 10.650 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 10.675 | 132.24 | 132.24 | 132.24 | 132.24 | 132.24 |
| 10.700 | 132.24 | 132.24 | 132.24 | 132.25 | 132.25 |
| 10.725 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 10.750 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 10.775 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 10.800 | 132.26 | 132.26 | 132.26 | 132.26 | 132.26 |
| 10.825 | 132.26 | 132.26 | 132.26 | 132.26 | 132.26 |
| 10.850 | 132.26 | 132.26 | 132.26 | 132.26 | 132.26 |
| 10.875 | 132.27 | 132.27 | 132.27 | 132.27 | 132.27 |
| 10.900 | 132.27 | 132.27 | 132.27 | 132.27 | 132.27 |
| 10.925 | 132.27 | 132.27 | 132.27 | 132.27 | 132.28 |
| 10.950 | 132.28 | 132.28 | 132.28 | 132.28 | 132.28 |
| 10.975 | 132.28 | 132.28 | 132.28 | 132.28 | 132.28 |
| 11.000 | 132.28 | 132.28 | 132.28 | 132.29 | 132.29 |
| 11.025 | 132.29 | 132.29 | 132.29 | 132.29 | 132.29 |
| 11.050 | 132.29 | 132.29 | 132.29 | 132.29 | 132.29 |
| 11.075 | 132.29 | 132.29 | 132.29 | 132.30 | 132.30 |
| 11.100 | 132.30 | 132.30 | 132.30 | 132.30 | 132.30 |
| 11.125 | 132.30 | 132.30 | 132.30 | 132.30 | 132.30 |
| 11.150 | 132.30 | 132.31 | 132.31 | 132.31 | 132.31 |
| 11.175 | 132.31 | 132.31 | 132.31 | 132.31 | 132.31 |
| 11.200 | 132.31 | 132.31 | 132.32 | 132.32 | 132.32 |
| 11.225 | 132.32 | 132.32 | 132.32 | 132.32 | 132.32 |
| 11.250 | 132.32 | 132.32 | 132.33 | 132.33 | 132.33 |
| 11.275 | 132.33 | 132.33 | 132.33 | 132.33 | 132.33 |
| 11.300 | 132.33 | 132.33 | 132.34 | 132.34 | 132.34 |
| 11.325 | 132.34 | 132.34 | 132.34 | 132.34 | 132.34 |
| 11.350 | 132.34 | 132.35 | 132.35 | 132.35 | 132.35 |
| 11.375 | 132.35 | 132.35 | 132.35 | 132.35 | 132.35 |
| 11.400 | 132.36 | 132.36 | 132.36 | 132.36 | 132.36 |
| 11.425 | 132.36 | 132.36 | 132.36 | 132.37 | 132.37 |
| 11.450 | 132.37 | 132.37 | 132.37 | 132.37 | 132.37 |
| 11.475 | 132.37 | 132.37 | 132.38 | 132.38 | 132.38 |
| 11.500 | 132.38 | 132.38 | 132.38 | 132.38 | 132.38 |
| 11.525 | 132.38 | 132.39 | 132.39 | 132.39 | 132.39 |
| 11.550 | 132.39 | 132.40 | 132.40 | 132.40 | 132.40 |
| 11.575 | 132.40 | 132.41 | 132.41 | 132.41 | 132.42 |
| 11.600 | 132.42 | 132.42 | 132.43 | 132.43 | 132.43 |
| 11.625 | 132.44 | 132.44 | 132.45 | 132.45 | 132.46 |
| 11.650 | 132.46 | 132.47 | 132.48 | 132.48 | 132.49 |
| 11.675 | 132.49 | 132.50 | 132.51 | 132.52 | 132.52 |
| 11.700 | 132.53 | 132.54 | 132.55 | 132.55 | 132.56 |
| 11.725 | 132.57 | 132.58 | 132.59 | 132.60 | 132.60 |
| 11.750 | 132.61 | 132.62 | 132.63 | 132.64 | 132.65 |
| 11.775 | 132.66 | 132.67 | 132.68 | 132.69 | 132.70 |
| 11.800 | 132.71 | 132.72 | 132.73 | 132.74 | 132.75 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 11.825 | 132.76 | 132.77 | 132.78 | 132.79 | 132.80 |
| 11.850 | 132.81 | 132.82 | 132.84 | 132.85 | 132.86 |
| 11.875 | 132.87 | 132.88 | 132.90 | 132.91 | 132.92 |
| 11.900 | 132.94 | 132.95 | 132.96 | 132.97 | 132.99 |
| 11.925 | 133.00 | 133.01 | 133.02 | 133.04 | 133.05 |
| 11.950 | 133.06 | 133.07 | 133.08 | 133.09 | 133.10 |
| 11.975 | 133.11 | 133.12 | 133.13 | 133.14 | 133.14 |
| 12.000 | 133.15 | 133.16 | 133.16 | 133.17 | 133.17 |
| 12.025 | 133.18 | 133.18 | 133.18 | 133.18 | 133.19 |
| 12.050 | 133.19 | 133.19 | 133.19 | 133.19 | 133.19 |
| 12.075 | 133.18 | 133.18 | 133.18 | 133.17 | 133.17 |
| 12.100 | 133.16 | 133.16 | 133.15 | 133.15 | 133.14 |
| 12.125 | 133.13 | 133.12 | 133.11 | 133.11 | 133.10 |
| 12.150 | 133.09 | 133.08 | 133.07 | 133.06 | 133.05 |
| 12.175 | 133.04 | 133.03 | 133.02 | 133.01 | 133.00 |
| 12.200 | 132.99 | 132.98 | 132.97 | 132.96 | 132.94 |
| 12.225 | 132.93 | 132.93 | 132.92 | 132.91 | 132.90 |
| 12.250 | 132.89 | 132.88 | 132.87 | 132.86 | 132.85 |
| 12.275 | 132.84 | 132.84 | 132.83 | 132.82 | 132.81 |
| 12.300 | 132.81 | 132.80 | 132.79 | 132.79 | 132.78 |
| 12.325 | 132.77 | 132.77 | 132.76 | 132.76 | 132.75 |
| 12.350 | 132.75 | 132.74 | 132.74 | 132.73 | 132.73 |
| 12.375 | 132.72 | 132.72 | 132.71 | 132.71 | 132.70 |
| 12.400 | 132.70 | 132.70 | 132.69 | 132.69 | 132.68 |
| 12.425 | 132.68 | 132.68 | 132.67 | 132.67 | 132.67 |
| 12.450 | 132.66 | 132.66 | 132.66 | 132.65 | 132.65 |
| 12.475 | 132.65 | 132.64 | 132.64 | 132.64 | 132.63 |
| 12.500 | 132.63 | 132.63 | 132.62 | 132.62 | 132.62 |
| 12.525 | 132.62 | 132.61 | 132.61 | 132.61 | 132.61 |
| 12.550 | 132.60 | 132.60 | 132.60 | 132.60 | 132.59 |
| 12.575 | 132.59 | 132.59 | 132.59 | 132.58 | 132.58 |
| 12.600 | 132.58 | 132.58 | 132.57 | 132.57 | 132.57 |
| 12.625 | 132.57 | 132.57 | 132.56 | 132.56 | 132.56 |
| 12.650 | 132.56 | 132.56 | 132.55 | 132.55 | 132.55 |
| 12.675 | 132.55 | 132.55 | 132.54 | 132.54 | 132.54 |
| 12.700 | 132.54 | 132.54 | 132.54 | 132.53 | 132.53 |
| 12.725 | 132.53 | 132.53 | 132.53 | 132.53 | 132.53 |
| 12.750 | 132.52 | 132.52 | 132.52 | 132.52 | 132.52 |
| 12.775 | 132.52 | 132.52 | 132.52 | 132.52 | 132.51 |
| 12.800 | 132.51 | 132.51 | 132.51 | 132.51 | 132.51 |
| 12.825 | 132.51 | 132.51 | 132.51 | 132.51 | 132.51 |
| 12.850 | 132.50 | 132.50 | 132.50 | 132.50 | 132.50 |
| 12.875 | 132.50 | 132.50 | 132.50 | 132.50 | 132.50 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 12.900 | 132.50 | 132.50 | 132.50 | 132.49 | 132.49 |
| 12.925 | 132.49 | 132.49 | 132.49 | 132.49 | 132.49 |
| 12.950 | 132.49 | 132.49 | 132.49 | 132.49 | 132.49 |
| 12.975 | 132.49 | 132.49 | 132.49 | 132.49 | 132.48 |
| 13.000 | 132.48 | 132.48 | 132.48 | 132.48 | 132.48 |
| 13.025 | 132.48 | 132.48 | 132.48 | 132.48 | 132.48 |
| 13.050 | 132.48 | 132.48 | 132.48 | 132.48 | 132.47 |
| 13.075 | 132.47 | 132.47 | 132.47 | 132.47 | 132.47 |
| 13.100 | 132.47 | 132.47 | 132.47 | 132.47 | 132.47 |
| 13.125 | 132.47 | 132.47 | 132.47 | 132.47 | 132.47 |
| 13.150 | 132.46 | 132.46 | 132.46 | 132.46 | 132.46 |
| 13.175 | 132.46 | 132.46 | 132.46 | 132.46 | 132.46 |
| 13.200 | 132.46 | 132.46 | 132.46 | 132.46 | 132.46 |
| 13.225 | 132.46 | 132.46 | 132.46 | 132.45 | 132.45 |
| 13.250 | 132.45 | 132.45 | 132.45 | 132.45 | 132.45 |
| 13.275 | 132.45 | 132.45 | 132.45 | 132.45 | 132.45 |
| 13.300 | 132.45 | 132.45 | 132.45 | 132.45 | 132.45 |
| 13.325 | 132.45 | 132.45 | 132.45 | 132.45 | 132.45 |
| 13.350 | 132.45 | 132.44 | 132.44 | 132.44 | 132.44 |
| 13.375 | 132.44 | 132.44 | 132.44 | 132.44 | 132.44 |
| 13.400 | 132.44 | 132.44 | 132.44 | 132.44 | 132.44 |
| 13.425 | 132.44 | 132.44 | 132.44 | 132.44 | 132.44 |
| 13.450 | 132.44 | 132.44 | 132.44 | 132.44 | 132.44 |
| 13.475 | 132.44 | 132.43 | 132.43 | 132.43 | 132.43 |
| 13.500 | 132.43 | 132.43 | 132.43 | 132.43 | 132.43 |
| 13.525 | 132.43 | 132.43 | 132.43 | 132.43 | 132.43 |
| 13.550 | 132.43 | 132.43 | 132.43 | 132.43 | 132.43 |
| 13.575 | 132.43 | 132.43 | 132.43 | 132.43 | 132.42 |
| 13.600 | 132.42 | 132.42 | 132.42 | 132.42 | 132.42 |
| 13.625 | 132.42 | 132.42 | 132.42 | 132.42 | 132.42 |
| 13.650 | 132.42 | 132.42 | 132.42 | 132.42 | 132.42 |
| 13.675 | 132.42 | 132.42 | 132.42 | 132.42 | 132.42 |
| 13.700 | 132.42 | 132.42 | 132.42 | 132.42 | 132.42 |
| 13.725 | 132.41 | 132.41 | 132.41 | 132.41 | 132.41 |
| 13.750 | 132.41 | 132.41 | 132.41 | 132.41 | 132.41 |
| 13.775 | 132.41 | 132.41 | 132.41 | 132.41 | 132.41 |
| 13.800 | 132.41 | 132.41 | 132.41 | 132.41 | 132.41 |
| 13.825 | 132.41 | 132.41 | 132.41 | 132.41 | 132.41 |
| 13.850 | 132.41 | 132.41 | 132.41 | 132.41 | 132.40 |
| 13.875 | 132.40 | 132.40 | 132.40 | 132.40 | 132.40 |
| 13.900 | 132.40 | 132.40 | 132.40 | 132.40 | 132.40 |
| 13.925 | 132.40 | 132.40 | 132.40 | 132.40 | 132.40 |
| 13.950 | 132.40 | 132.40 | 132.40 | 132.40 | 132.40 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 13.975 | 132.40 | 132.40 | 132.40 | 132.40 | 132.40 |
| 14.000 | 132.40 | 132.40 | 132.40 | 132.40 | 132.39 |
| 14.025 | 132.39 | 132.39 | 132.39 | 132.39 | 132.39 |
| 14.050 | 132.39 | 132.39 | 132.39 | 132.39 | 132.39 |
| 14.075 | 132.39 | 132.39 | 132.39 | 132.39 | 132.39 |
| 14.100 | 132.39 | 132.39 | 132.39 | 132.39 | 132.39 |
| 14.125 | 132.39 | 132.39 | 132.39 | 132.39 | 132.39 |
| 14.150 | 132.39 | 132.39 | 132.39 | 132.38 | 132.38 |
| 14.175 | 132.38 | 132.38 | 132.38 | 132.38 | 132.38 |
| 14.200 | 132.38 | 132.38 | 132.38 | 132.38 | 132.38 |
| 14.225 | 132.38 | 132.38 | 132.38 | 132.38 | 132.38 |
| 14.250 | 132.38 | 132.38 | 132.38 | 132.38 | 132.38 |
| 14.275 | 132.38 | 132.38 | 132.38 | 132.38 | 132.38 |
| 14.300 | 132.38 | 132.38 | 132.38 | 132.38 | 132.38 |
| 14.325 | 132.38 | 132.38 | 132.38 | 132.38 | 132.38 |
| 14.350 | 132.38 | 132.38 | 132.38 | 132.38 | 132.38 |
| 14.375 | 132.38 | 132.38 | 132.38 | 132.38 | 132.38 |
| 14.400 | 132.38 | 132.38 | 132.38 | 132.38 | 132.38 |
| 14.425 | 132.37 | 132.37 | 132.37 | 132.37 | 132.37 |
| 14.450 | 132.37 | 132.37 | 132.37 | 132.37 | 132.37 |
| 14.475 | 132.37 | 132.37 | 132.37 | 132.37 | 132.37 |
| 14.500 | 132.37 | 132.37 | 132.37 | 132.37 | 132.37 |
| 14.525 | 132.37 | 132.37 | 132.37 | 132.37 | 132.37 |
| 14.550 | 132.37 | 132.37 | 132.37 | 132.37 | 132.37 |
| 14.575 | 132.37 | 132.37 | 132.37 | 132.37 | 132.37 |
| 14.600 | 132.37 | 132.37 | 132.37 | 132.37 | 132.37 |
| 14.625 | 132.37 | 132.37 | 132.37 | 132.37 | 132.37 |
| 14.650 | 132.37 | 132.37 | 132.37 | 132.37 | 132.37 |
| 14.675 | 132.37 | 132.37 | 132.37 | 132.37 | 132.37 |
| 14.700 | 132.37 | 132.37 | 132.37 | 132.37 | 132.37 |
| 14.725 | 132.37 | 132.37 | 132.37 | 132.37 | 132.37 |
| 14.750 | 132.37 | 132.37 | 132.37 | 132.37 | 132.37 |
| 14.775 | 132.37 | 132.37 | 132.37 | 132.37 | 132.37 |
| 14.800 | 132.37 | 132.37 | 132.37 | 132.36 | 132.36 |
| 14.825 | 132.36 | 132.36 | 132.36 | 132.36 | 132.36 |
| 14.850 | 132.36 | 132.36 | 132.36 | 132.36 | 132.36 |
| 14.875 | 132.36 | 132.36 | 132.36 | 132.36 | 132.36 |
| 14.900 | 132.36 | 132.36 | 132.36 | 132.36 | 132.36 |
| 14.925 | 132.36 | 132.36 | 132.36 | 132.36 | 132.36 |
| 14.950 | 132.36 | 132.36 | 132.36 | 132.36 | 132.36 |
| 14.975 | 132.36 | 132.36 | 132.36 | 132.36 | 132.36 |
| 15.000 | 132.36 | 132.36 | 132.36 | 132.36 | 132.36 |
| 15.025 | 132.36 | 132.36 | 132.36 | 132.36 | 132.36 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 15.050 | 132.36 | 132.36 | 132.36 | 132.36 | 132.36 |
| 15.075 | 132.36 | 132.36 | 132.36 | 132.36 | 132.36 |
| 15.100 | 132.36 | 132.36 | 132.36 | 132.36 | 132.36 |
| 15.125 | 132.36 | 132.36 | 132.36 | 132.36 | 132.36 |
| 15.150 | 132.36 | 132.36 | 132.36 | 132.36 | 132.36 |
| 15.175 | 132.35 | 132.35 | 132.35 | 132.35 | 132.35 |
| 15.200 | 132.35 | 132.35 | 132.35 | 132.35 | 132.35 |
| 15.225 | 132.35 | 132.35 | 132.35 | 132.35 | 132.35 |
| 15.250 | 132.35 | 132.35 | 132.35 | 132.35 | 132.35 |
| 15.275 | 132.35 | 132.35 | 132.35 | 132.35 | 132.35 |
| 15.300 | 132.35 | 132.35 | 132.35 | 132.35 | 132.35 |
| 15.325 | 132.35 | 132.35 | 132.35 | 132.35 | 132.35 |
| 15.350 | 132.35 | 132.35 | 132.35 | 132.35 | 132.35 |
| 15.375 | 132.35 | 132.35 | 132.35 | 132.35 | 132.35 |
| 15.400 | 132.35 | 132.35 | 132.35 | 132.35 | 132.35 |
| 15.425 | 132.35 | 132.35 | 132.35 | 132.35 | 132.35 |
| 15.450 | 132.35 | 132.35 | 132.35 | 132.35 | 132.35 |
| 15.475 | 132.35 | 132.35 | 132.35 | 132.34 | 132.34 |
| 15.500 | 132.34 | 132.34 | 132.34 | 132.34 | 132.34 |
| 15.525 | 132.34 | 132.34 | 132.34 | 132.34 | 132.34 |
| 15.550 | 132.34 | 132.34 | 132.34 | 132.34 | 132.34 |
| 15.575 | 132.34 | 132.34 | 132.34 | 132.34 | 132.34 |
| 15.600 | 132.34 | 132.34 | 132.34 | 132.34 | 132.34 |
| 15.625 | 132.34 | 132.34 | 132.34 | 132.34 | 132.34 |
| 15.650 | 132.34 | 132.34 | 132.34 | 132.34 | 132.34 |
| 15.675 | 132.34 | 132.34 | 132.34 | 132.34 | 132.34 |
| 15.700 | 132.34 | 132.34 | 132.34 | 132.34 | 132.34 |
| 15.725 | 132.34 | 132.34 | 132.34 | 132.34 | 132.34 |
| 15.750 | 132.34 | 132.34 | 132.34 | 132.34 | 132.34 |
| 15.775 | 132.34 | 132.34 | 132.34 | 132.34 | 132.34 |
| 15.800 | 132.34 | 132.34 | 132.33 | 132.33 | 132.33 |
| 15.825 | 132.33 | 132.33 | 132.33 | 132.33 | 132.33 |
| 15.850 | 132.33 | 132.33 | 132.33 | 132.33 | 132.33 |
| 15.875 | 132.33 | 132.33 | 132.33 | 132.33 | 132.33 |
| 15.900 | 132.33 | 132.33 | 132.33 | 132.33 | 132.33 |
| 15.925 | 132.33 | 132.33 | 132.33 | 132.33 | 132.33 |
| 15.950 | 132.33 | 132.33 | 132.33 | 132.33 | 132.33 |
| 15.975 | 132.33 | 132.33 | 132.33 | 132.33 | 132.33 |
| 16.000 | 132.33 | 132.33 | 132.33 | 132.33 | 132.33 |
| 16.025 | 132.33 | 132.33 | 132.33 | 132.33 | 132.33 |
| 16.050 | 132.33 | 132.33 | 132.33 | 132.33 | 132.33 |
| 16.075 | 132.33 | 132.33 | 132.33 | 132.33 | 132.33 |
| 16.100 | 132.33 | 132.33 | 132.33 | 132.33 | 132.33 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 16.125 | 132.32 | 132.32 | 132.32 | 132.32 | 132.32 |
| 16.150 | 132.32 | 132.32 | 132.32 | 132.32 | 132.32 |
| 16.175 | 132.32 | 132.32 | 132.32 | 132.32 | 132.32 |
| 16.200 | 132.32 | 132.32 | 132.32 | 132.32 | 132.32 |
| 16.225 | 132.32 | 132.32 | 132.32 | 132.32 | 132.32 |
| 16.250 | 132.32 | 132.32 | 132.32 | 132.32 | 132.32 |
| 16.275 | 132.32 | 132.32 | 132.32 | 132.32 | 132.32 |
| 16.300 | 132.32 | 132.32 | 132.32 | 132.32 | 132.32 |
| 16.325 | 132.32 | 132.32 | 132.32 | 132.32 | 132.32 |
| 16.350 | 132.32 | 132.32 | 132.32 | 132.32 | 132.32 |
| 16.375 | 132.32 | 132.32 | 132.32 | 132.32 | 132.32 |
| 16.400 | 132.32 | 132.32 | 132.32 | 132.32 | 132.32 |
| 16.425 | 132.32 | 132.32 | 132.32 | 132.32 | 132.32 |
| 16.450 | 132.32 | 132.32 | 132.32 | 132.32 | 132.32 |
| 16.475 | 132.32 | 132.32 | 132.32 | 132.32 | 132.32 |
| 16.500 | 132.32 | 132.32 | 132.32 | 132.32 | 132.32 |
| 16.525 | 132.32 | 132.32 | 132.32 | 132.32 | 132.32 |
| 16.550 | 132.32 | 132.32 | 132.32 | 132.32 | 132.32 |
| 16.575 | 132.32 | 132.32 | 132.32 | 132.32 | 132.32 |
| 16.600 | 132.32 | 132.32 | 132.32 | 132.32 | 132.32 |
| 16.625 | 132.32 | 132.32 | 132.32 | 132.32 | 132.32 |
| 16.650 | 132.32 | 132.32 | 132.32 | 132.32 | 132.32 |
| 16.675 | 132.32 | 132.32 | 132.32 | 132.32 | 132.32 |
| 16.700 | 132.32 | 132.32 | 132.32 | 132.32 | 132.32 |
| 16.725 | 132.32 | 132.32 | 132.31 | 132.31 | 132.31 |
| 16.750 | 132.31 | 132.31 | 132.31 | 132.31 | 132.31 |
| 16.775 | 132.31 | 132.31 | 132.31 | 132.31 | 132.31 |
| 16.800 | 132.31 | 132.31 | 132.31 | 132.31 | 132.31 |
| 16.825 | 132.31 | 132.31 | 132.31 | 132.31 | 132.31 |
| 16.850 | 132.31 | 132.31 | 132.31 | 132.31 | 132.31 |
| 16.875 | 132.31 | 132.31 | 132.31 | 132.31 | 132.31 |
| 16.900 | 132.31 | 132.31 | 132.31 | 132.31 | 132.31 |
| 16.925 | 132.31 | 132.31 | 132.31 | 132.31 | 132.31 |
| 16.950 | 132.31 | 132.31 | 132.31 | 132.31 | 132.31 |
| 16.975 | 132.31 | 132.31 | 132.31 | 132.31 | 132.31 |
| 17.000 | 132.31 | 132.31 | 132.31 | 132.31 | 132.31 |
| 17.025 | 132.31 | 132.31 | 132.31 | 132.31 | 132.31 |
| 17.050 | 132.31 | 132.31 | 132.31 | 132.31 | 132.31 |
| 17.075 | 132.31 | 132.31 | 132.31 | 132.31 | 132.31 |
| 17.100 | 132.31 | 132.31 | 132.31 | 132.31 | 132.31 |
| 17.125 | 132.31 | 132.31 | 132.31 | 132.31 | 132.31 |
| 17.150 | 132.31 | 132.31 | 132.31 | 132.31 | 132.31 |
| 17.175 | 132.31 | 132.31 | 132.31 | 132.31 | 132.31 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 17.200 | 132.31 | 132.31 | 132.31 | 132.31 | 132.31 |
| 17.225 | 132.31 | 132.31 | 132.31 | 132.31 | 132.31 |
| 17.250 | 132.31 | 132.31 | 132.31 | 132.31 | 132.31 |
| 17.275 | 132.31 | 132.31 | 132.31 | 132.31 | 132.31 |
| 17.300 | 132.31 | 132.31 | 132.31 | 132.31 | 132.31 |
| 17.325 | 132.31 | 132.31 | 132.31 | 132.31 | 132.31 |
| 17.350 | 132.31 | 132.31 | 132.31 | 132.31 | 132.31 |
| 17.375 | 132.31 | 132.31 | 132.31 | 132.31 | 132.31 |
| 17.400 | 132.31 | 132.31 | 132.31 | 132.31 | 132.31 |
| 17.425 | 132.31 | 132.31 | 132.31 | 132.31 | 132.31 |
| 17.450 | 132.31 | 132.31 | 132.30 | 132.30 | 132.30 |
| 17.475 | 132.30 | 132.30 | 132.30 | 132.30 | 132.30 |
| 17.500 | 132.30 | 132.30 | 132.30 | 132.30 | 132.30 |
| 17.525 | 132.30 | 132.30 | 132.30 | 132.30 | 132.30 |
| 17.550 | 132.30 | 132.30 | 132.30 | 132.30 | 132.30 |
| 17.575 | 132.30 | 132.30 | 132.30 | 132.30 | 132.30 |
| 17.600 | 132.30 | 132.30 | 132.30 | 132.30 | 132.30 |
| 17.625 | 132.30 | 132.30 | 132.30 | 132.30 | 132.30 |
| 17.650 | 132.30 | 132.30 | 132.30 | 132.30 | 132.30 |
| 17.675 | 132.30 | 132.30 | 132.30 | 132.30 | 132.30 |
| 17.700 | 132.30 | 132.30 | 132.30 | 132.30 | 132.30 |
| 17.725 | 132.30 | 132.30 | 132.30 | 132.30 | 132.30 |
| 17.750 | 132.30 | 132.30 | 132.30 | 132.30 | 132.30 |
| 17.775 | 132.30 | 132.30 | 132.30 | 132.30 | 132.30 |
| 17.800 | 132.30 | 132.30 | 132.30 | 132.30 | 132.30 |
| 17.825 | 132.30 | 132.30 | 132.30 | 132.30 | 132.30 |
| 17.850 | 132.30 | 132.30 | 132.30 | 132.30 | 132.30 |
| 17.875 | 132.30 | 132.30 | 132.30 | 132.30 | 132.30 |
| 17.900 | 132.30 | 132.30 | 132.30 | 132.30 | 132.30 |
| 17.925 | 132.30 | 132.30 | 132.30 | 132.30 | 132.30 |
| 17.950 | 132.30 | 132.30 | 132.30 | 132.30 | 132.30 |
| 17.975 | 132.30 | 132.30 | 132.30 | 132.30 | 132.30 |
| 18.000 | 132.30 | 132.30 | 132.30 | 132.30 | 132.30 |
| 18.025 | 132.30 | 132.30 | 132.30 | 132.30 | 132.30 |
| 18.050 | 132.30 | 132.30 | 132.30 | 132.30 | 132.30 |
| 18.075 | 132.30 | 132.30 | 132.30 | 132.30 | 132.30 |
| 18.100 | 132.30 | 132.30 | 132.30 | 132.30 | 132.30 |
| 18.125 | 132.30 | 132.30 | 132.30 | 132.30 | 132.30 |
| 18.150 | 132.30 | 132.30 | 132.30 | 132.30 | 132.29 |
| 18.175 | 132.29 | 132.29 | 132.29 | 132.29 | 132.29 |
| 18.200 | 132.29 | 132.29 | 132.29 | 132.29 | 132.29 |
| 18.225 | 132.29 | 132.29 | 132.29 | 132.29 | 132.29 |
| 18.250 | 132.29 | 132.29 | 132.29 | 132.29 | 132.29 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 18.275 | 132.29 | 132.29 | 132.29 | 132.29 | 132.29 |
| 18.300 | 132.29 | 132.29 | 132.29 | 132.29 | 132.29 |
| 18.325 | 132.29 | 132.29 | 132.29 | 132.29 | 132.29 |
| 18.350 | 132.29 | 132.29 | 132.29 | 132.29 | 132.29 |
| 18.375 | 132.29 | 132.29 | 132.29 | 132.29 | 132.29 |
| 18.400 | 132.29 | 132.29 | 132.29 | 132.29 | 132.29 |
| 18.425 | 132.29 | 132.29 | 132.29 | 132.29 | 132.29 |
| 18.450 | 132.29 | 132.29 | 132.29 | 132.29 | 132.29 |
| 18.475 | 132.29 | 132.29 | 132.29 | 132.29 | 132.29 |
| 18.500 | 132.29 | 132.29 | 132.29 | 132.29 | 132.29 |
| 18.525 | 132.29 | 132.29 | 132.29 | 132.29 | 132.29 |
| 18.550 | 132.29 | 132.29 | 132.29 | 132.29 | 132.29 |
| 18.575 | 132.29 | 132.29 | 132.29 | 132.29 | 132.29 |
| 18.600 | 132.29 | 132.29 | 132.29 | 132.29 | 132.29 |
| 18.625 | 132.29 | 132.29 | 132.29 | 132.29 | 132.29 |
| 18.650 | 132.29 | 132.29 | 132.29 | 132.29 | 132.29 |
| 18.675 | 132.29 | 132.29 | 132.29 | 132.29 | 132.29 |
| 18.700 | 132.29 | 132.29 | 132.29 | 132.29 | 132.29 |
| 18.725 | 132.29 | 132.29 | 132.29 | 132.29 | 132.29 |
| 18.750 | 132.29 | 132.29 | 132.29 | 132.29 | 132.29 |
| 18.775 | 132.29 | 132.29 | 132.29 | 132.29 | 132.29 |
| 18.800 | 132.29 | 132.29 | 132.29 | 132.29 | 132.29 |
| 18.825 | 132.29 | 132.29 | 132.29 | 132.29 | 132.29 |
| 18.850 | 132.29 | 132.29 | 132.29 | 132.29 | 132.28 |
| 18.875 | 132.28 | 132.28 | 132.28 | 132.28 | 132.28 |
| 18.900 | 132.28 | 132.28 | 132.28 | 132.28 | 132.28 |
| 18.925 | 132.28 | 132.28 | 132.28 | 132.28 | 132.28 |
| 18.950 | 132.28 | 132.28 | 132.28 | 132.28 | 132.28 |
| 18.975 | 132.28 | 132.28 | 132.28 | 132.28 | 132.28 |
| 19.000 | 132.28 | 132.28 | 132.28 | 132.28 | 132.28 |
| 19.025 | 132.28 | 132.28 | 132.28 | 132.28 | 132.28 |
| 19.050 | 132.28 | 132.28 | 132.28 | 132.28 | 132.28 |
| 19.075 | 132.28 | 132.28 | 132.28 | 132.28 | 132.28 |
| 19.100 | 132.28 | 132.28 | 132.28 | 132.28 | 132.28 |
| 19.125 | 132.28 | 132.28 | 132.28 | 132.28 | 132.28 |
| 19.150 | 132.28 | 132.28 | 132.28 | 132.28 | 132.28 |
| 19.175 | 132.28 | 132.28 | 132.28 | 132.28 | 132.28 |
| 19.200 | 132.28 | 132.28 | 132.28 | 132.28 | 132.28 |
| 19.225 | 132.28 | 132.28 | 132.28 | 132.28 | 132.28 |
| 19.250 | 132.28 | 132.28 | 132.28 | 132.28 | 132.28 |
| 19.275 | 132.28 | 132.28 | 132.28 | 132.28 | 132.28 |
| 19.300 | 132.28 | 132.28 | 132.28 | 132.28 | 132.28 |
| 19.325 | 132.28 | 132.28 | 132.28 | 132.28 | 132.28 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 19.350 | 132.28 | 132.28 | 132.28 | 132.28 | 132.28 |
| 19.375 | 132.28 | 132.28 | 132.28 | 132.28 | 132.28 |
| 19.400 | 132.28 | 132.28 | 132.28 | 132.28 | 132.28 |
| 19.425 | 132.28 | 132.28 | 132.28 | 132.28 | 132.28 |
| 19.450 | 132.28 | 132.28 | 132.28 | 132.28 | 132.28 |
| 19.475 | 132.28 | 132.28 | 132.28 | 132.27 | 132.27 |
| 19.500 | 132.27 | 132.27 | 132.27 | 132.27 | 132.27 |
| 19.525 | 132.27 | 132.27 | 132.27 | 132.27 | 132.27 |
| 19.550 | 132.27 | 132.27 | 132.27 | 132.27 | 132.27 |
| 19.575 | 132.27 | 132.27 | 132.27 | 132.27 | 132.27 |
| 19.600 | 132.27 | 132.27 | 132.27 | 132.27 | 132.27 |
| 19.625 | 132.27 | 132.27 | 132.27 | 132.27 | 132.27 |
| 19.650 | 132.27 | 132.27 | 132.27 | 132.27 | 132.27 |
| 19.675 | 132.27 | 132.27 | 132.27 | 132.27 | 132.27 |
| 19.700 | 132.27 | 132.27 | 132.27 | 132.27 | 132.27 |
| 19.725 | 132.27 | 132.27 | 132.27 | 132.27 | 132.27 |
| 19.750 | 132.27 | 132.27 | 132.27 | 132.27 | 132.27 |
| 19.775 | 132.27 | 132.27 | 132.27 | 132.27 | 132.27 |
| 19.800 | 132.27 | 132.27 | 132.27 | 132.27 | 132.27 |
| 19.825 | 132.27 | 132.27 | 132.27 | 132.27 | 132.27 |
| 19.850 | 132.27 | 132.27 | 132.27 | 132.27 | 132.27 |
| 19.875 | 132.27 | 132.27 | 132.27 | 132.27 | 132.27 |
| 19.900 | 132.27 | 132.27 | 132.27 | 132.27 | 132.27 |
| 19.925 | 132.27 | 132.27 | 132.27 | 132.27 | 132.27 |
| 19.950 | 132.27 | 132.27 | 132.27 | 132.27 | 132.27 |
| 19.975 | 132.27 | 132.27 | 132.27 | 132.27 | 132.27 |
| 20.000 | 132.27 | 132.27 | 132.27 | 132.27 | 132.27 |
| 20.025 | 132.27 | 132.26 | 132.26 | 132.26 | 132.26 |
| 20.050 | 132.26 | 132.26 | 132.26 | 132.26 | 132.26 |
| 20.075 | 132.26 | 132.26 | 132.26 | 132.26 | 132.26 |
| 20.100 | 132.26 | 132.26 | 132.26 | 132.26 | 132.26 |
| 20.125 | 132.26 | 132.26 | 132.26 | 132.26 | 132.26 |
| 20.150 | 132.26 | 132.26 | 132.26 | 132.26 | 132.26 |
| 20.175 | 132.26 | 132.26 | 132.26 | 132.26 | 132.26 |
| 20.200 | 132.26 | 132.26 | 132.26 | 132.26 | 132.26 |
| 20.225 | 132.26 | 132.26 | 132.26 | 132.26 | 132.26 |
| 20.250 | 132.26 | 132.26 | 132.26 | 132.26 | 132.26 |
| 20.275 | 132.26 | 132.26 | 132.26 | 132.26 | 132.26 |
| 20.300 | 132.26 | 132.26 | 132.26 | 132.26 | 132.26 |
| 20.325 | 132.26 | 132.26 | 132.26 | 132.26 | 132.26 |
| 20.350 | 132.26 | 132.26 | 132.26 | 132.26 | 132.26 |
| 20.375 | 132.26 | 132.26 | 132.26 | 132.26 | 132.26 |
| 20.400 | 132.26 | 132.26 | 132.26 | 132.26 | 132.26 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 20.425 | 132.26 | 132.26 | 132.26 | 132.26 | 132.26 |
| 20.450 | 132.26 | 132.26 | 132.26 | 132.26 | 132.26 |
| 20.475 | 132.26 | 132.26 | 132.26 | 132.26 | 132.26 |
| 20.500 | 132.26 | 132.26 | 132.26 | 132.26 | 132.26 |
| 20.525 | 132.26 | 132.26 | 132.26 | 132.26 | 132.26 |
| 20.550 | 132.26 | 132.26 | 132.26 | 132.26 | 132.26 |
| 20.575 | 132.26 | 132.26 | 132.26 | 132.26 | 132.26 |
| 20.600 | 132.26 | 132.26 | 132.26 | 132.26 | 132.26 |
| 20.625 | 132.26 | 132.26 | 132.26 | 132.26 | 132.26 |
| 20.650 | 132.26 | 132.26 | 132.26 | 132.26 | 132.26 |
| 20.675 | 132.26 | 132.26 | 132.26 | 132.26 | 132.26 |
| 20.700 | 132.26 | 132.26 | 132.26 | 132.26 | 132.26 |
| 20.725 | 132.26 | 132.26 | 132.26 | 132.26 | 132.26 |
| 20.750 | 132.26 | 132.26 | 132.26 | 132.26 | 132.26 |
| 20.775 | 132.26 | 132.26 | 132.26 | 132.26 | 132.26 |
| 20.800 | 132.26 | 132.26 | 132.26 | 132.26 | 132.26 |
| 20.825 | 132.26 | 132.26 | 132.26 | 132.26 | 132.26 |
| 20.850 | 132.26 | 132.26 | 132.26 | 132.26 | 132.26 |
| 20.875 | 132.26 | 132.26 | 132.26 | 132.26 | 132.26 |
| 20.900 | 132.26 | 132.26 | 132.26 | 132.26 | 132.26 |
| 20.925 | 132.26 | 132.26 | 132.26 | 132.26 | 132.26 |
| 20.950 | 132.26 | 132.26 | 132.26 | 132.26 | 132.26 |
| 20.975 | 132.26 | 132.26 | 132.26 | 132.26 | 132.26 |
| 21.000 | 132.26 | 132.26 | 132.26 | 132.26 | 132.26 |
| 21.025 | 132.26 | 132.26 | 132.26 | 132.26 | 132.26 |
| 21.050 | 132.26 | 132.26 | 132.26 | 132.26 | 132.26 |
| 21.075 | 132.26 | 132.26 | 132.26 | 132.26 | 132.26 |
| 21.100 | 132.26 | 132.26 | 132.26 | 132.26 | 132.26 |
| 21.125 | 132.26 | 132.26 | 132.26 | 132.26 | 132.26 |
| 21.150 | 132.26 | 132.26 | 132.26 | 132.26 | 132.26 |
| 21.175 | 132.26 | 132.26 | 132.26 | 132.26 | 132.26 |
| 21.200 | 132.26 | 132.26 | 132.26 | 132.26 | 132.26 |
| 21.225 | 132.26 | 132.26 | 132.26 | 132.26 | 132.26 |
| 21.250 | 132.26 | 132.26 | 132.26 | 132.26 | 132.26 |
| 21.275 | 132.26 | 132.26 | 132.26 | 132.26 | 132.26 |
| 21.300 | 132.26 | 132.26 | 132.26 | 132.26 | 132.26 |
| 21.325 | 132.26 | 132.26 | 132.26 | 132.26 | 132.26 |
| 21.350 | 132.26 | 132.26 | 132.26 | 132.26 | 132.26 |
| 21.375 | 132.26 | 132.26 | 132.26 | 132.26 | 132.26 |
| 21.400 | 132.26 | 132.26 | 132.26 | 132.26 | 132.26 |
| 21.425 | 132.26 | 132.26 | 132.26 | 132.26 | 132.26 |
| 21.450 | 132.26 | 132.26 | 132.26 | 132.26 | 132.26 |
| 21.475 | 132.26 | 132.26 | 132.26 | 132.26 | 132.26 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 21.500 | 132.26 | 132.26 | 132.26 | 132.26 | 132.26 |
| 21.525 | 132.26 | 132.26 | 132.26 | 132.26 | 132.26 |
| 21.550 | 132.26 | 132.26 | 132.26 | 132.26 | 132.26 |
| 21.575 | 132.26 | 132.26 | 132.26 | 132.26 | 132.26 |
| 21.600 | 132.26 | 132.26 | 132.26 | 132.26 | 132.26 |
| 21.625 | 132.26 | 132.26 | 132.26 | 132.26 | 132.26 |
| 21.650 | 132.26 | 132.26 | 132.26 | 132.26 | 132.26 |
| 21.675 | 132.26 | 132.26 | 132.26 | 132.26 | 132.26 |
| 21.700 | 132.26 | 132.26 | 132.26 | 132.26 | 132.26 |
| 21.725 | 132.26 | 132.26 | 132.26 | 132.26 | 132.26 |
| 21.750 | 132.26 | 132.26 | 132.26 | 132.26 | 132.26 |
| 21.775 | 132.26 | 132.26 | 132.26 | 132.26 | 132.26 |
| 21.800 | 132.26 | 132.26 | 132.26 | 132.26 | 132.26 |
| 21.825 | 132.26 | 132.26 | 132.26 | 132.26 | 132.26 |
| 21.850 | 132.26 | 132.26 | 132.26 | 132.26 | 132.26 |
| 21.875 | 132.26 | 132.26 | 132.26 | 132.26 | 132.26 |
| 21.900 | 132.26 | 132.26 | 132.26 | 132.26 | 132.26 |
| 21.925 | 132.26 | 132.26 | 132.26 | 132.26 | 132.26 |
| 21.950 | 132.26 | 132.26 | 132.26 | 132.26 | 132.26 |
| 21.975 | 132.26 | 132.26 | 132.26 | 132.26 | 132.26 |
| 22.000 | 132.26 | 132.26 | 132.26 | 132.26 | 132.26 |
| 22.025 | 132.26 | 132.25 | 132.25 | 132.25 | 132.25 |
| 22.050 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 22.075 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 22.100 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 22.125 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 22.150 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 22.175 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 22.200 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 22.225 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 22.250 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 22.275 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 22.300 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 22.325 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 22.350 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 22.375 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 22.400 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 22.425 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 22.450 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 22.475 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 22.500 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 22.525 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 22.550 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 22.575 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 22.600 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 22.625 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 22.650 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 22.675 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 22.700 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 22.725 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 22.750 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 22.775 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 22.800 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 22.825 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 22.850 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 22.875 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 22.900 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 22.925 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 22.950 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 22.975 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 23.000 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 23.025 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 23.050 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 23.075 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 23.100 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 23.125 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 23.150 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 23.175 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 23.200 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 23.225 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 23.250 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 23.275 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 23.300 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 23.325 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 23.350 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 23.375 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 23.400 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 23.425 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 23.450 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 23.475 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 23.500 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 23.525 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 23.550 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 23.575 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 23.600 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 23.625 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |

## Time vs. Elevation (ft)

**Output Time increment = 0.005 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 23.650 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 23.675 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 23.700 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 23.725 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 23.750 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 23.775 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 23.800 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 23.825 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 23.850 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 23.875 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 23.900 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 23.925 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 23.950 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 23.975 | 132.25 | 132.25 | 132.25 | 132.25 | 132.25 |
| 24.000 | 132.25 | (N/A) | (N/A) | (N/A) | (N/A) |

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