



# New-Indy Catawba Mill Corrective Action Plan

Submitted: June 15, 2021

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## **1. EXECUTIVE SUMMARY**

New-Indy Catawba LLC (New-Indy) submits this Corrective Action Plan report in response to paragraphs 3, 6 and 7 of the Order issued by the South Carolina Department of Health and Environmental Control (SCDHEC or DHEC) on May 7, 2021. By way of background, until late 2020, New-Indy and its predecessor owners of the mill in Catawba, South Carolina produced bleached paper at the facility. Given the substantial decrease in demand for such paper, the mill was becoming more economically unviable each day. Thus, New-Indy made the decision to convert from producing bleached white paper to unbleached containerboard at the mill. Commencing in spring 2020, the mill replaced the outdated bleached paper-making equipment with state-of-the-art equipment to make lightweight ultra-high strength containerboard and retrained its union workforce to operate and maintain this very sophisticated facility. While the mill began salable production on February 1, 2021, it is still working toward steady-state operations. In late January and February, New-Indy and SCDHEC began receiving complaints from local citizens regarding odors.

At that point, the mill began a concerted effort to identify potential sources of odors and to investigate those potential sources. The mill evaluated its seven (7) major operations and process areas: the woodyard, kraft pulp mill, paper machine, chemical recovery process, utilities, waste treatment, and miscellaneous sources. New-Indy evaluated the seven processes with a series of twelve (12) environmental consultants, including personnel from TRC Companies, Inc. (TRC), ALL4 LLC (ALL4), Weston Solutions, Inc. (Weston), National Council for Air and Stream Improvement (NCASI), Environmental Business Specialists, LLC (EBS), LDX Solutions (LDX), Environmental 360 Solutions, Inc. (E360), Trinity Consultants, Inc. (Trinity), Valmet and Rolf Ryham, SFC Contract Services and Saiia Construction Company. That evaluation included leak detection and repair (LDAR) evaluation, an ambient air screening evaluation and the installation of ambient air monitors, in addition to a focused evaluation of the wastewater treatment system. Based on the evaluation, the mill and its professionals concluded the wastewater treatment system was the only possible source of odors at the mill.

The mill has conducted numerous evaluations and process enhancements at the mill to address the odor issues. As noted above, the mill has engaged at least twelve environmental consulting firms



to assist in the process, including three environmental air consultants, three wastewater consultants, two engineering firms and a toxicologist. Activities that the mill has undertaken to identify and address odors include the following: installing continuous ambient air monitors on the mill property and offsite; completing the screening analysis of hydrogen sulfide (H<sub>2</sub>S) emissions at the mill; restarting the steam stripper; removing the layer of fiber from the surface of the ASB; injecting calcium nitrate and peroxide into the wastewater stream; repairing existing aerators and installing two new aerators. Certain of those activities are ongoing and have been incorporated into the corrective action plan set forth herein. In addition to the ongoing activities, certain activities are planned that will round out the corrective action plan. Those ongoing and upcoming activities set forth in this corrective action plan include the following: feeding calcium nitrate and peroxide into the wastewater stream; increasing the treatment capacity of the stripper; continuing repair of aerators; weekly advanced chemical and microbiological analysis to evaluate biomass health; and continuous ambient air monitoring onsite and offsite.

## **2. BACKGROUND**

New-Indy Catawba, LLC, (New-Indy) operates a kraft pulp and paper mill located at 5300 Cureton Ferry Rd, Catawba, SC, in York County (mill). The mill operates under Title V Operating Permit #2440-0005 that was issued by the South Carolina Department of Health and Environmental Control (DHEC) on May 7, 2019, became effective on July 1, 2019, and expires on June 30, 2024. New-Indy was issued Construction Permit #2440-0005-DF on July 23, 2019, in accordance with state and federal air quality regulations and standards, to allow the mill to modify its processes to convert from bleached paper production to brown paper production. The construction permit was revised on May 13, 2020, to allow the mill to hard pipe its condensates to the wastewater treatment plant. 40 CFR 63, Subpart S, allows this hard piping as a compliance option. New-Indy began operating the mill as an integrated pulp and paper facility manufacturing brown paper on February 1, 2021.

The Maximum Achievable Control Technology (MACT) standard allows hard piping of all the condensates to wastewater treatment plants as a compliance option. New-Indy projected in its construction permit application that the mill modifications and other operational changes could result in an increase in hydrogen sulfide emissions from the mill. The projected increase in hydrogen sulfide emissions was below the “significant net increase” threshold as outlined in S.C. Regulation 61-62.5, Standard 7, and therefore DHEC issued a minor construction air permit for the change on July 23, 2019.

As stated in DHEC’s May 7, 2021 order, after it began receiving complaints in February 2021 about odor in York and Lancaster counties, described as rotten egg and chemical odors, DHEC began an investigation to determine the source of the odors. DHEC staff have also reported observing strong, offsite, odors in the vicinity of the mill and several miles away from the mill that are characteristic of hydrogen sulfide emissions from kraft pulp and paper facilities. On February 22, 23 and 24, 2021, DHEC conducted air, wastewater and landfill inspections at the mill.

On April 7, 2021, DHEC notified New-Indy that based on the results of their investigation into the odor complaints, it appeared to DHEC that New-Indy may be a contributor to the reported odors in the York and Lancaster area. DHEC requested that New-Indy evaluate its operations and

identify and take corrective actions on any potential sources that could be contributing to the odors then being investigated in York and Lancaster counties.

On April 24-27, the US Environmental Protection Agency (EPA) conducted geospatial monitoring of hydrogen sulfide near the mill to identify sources of the odor in the nearby vicinity. EPA monitoring data detected hydrogen sulfide onsite and offsite. DHEC maintains that this validates the determination that the mill is a source of air contaminants at undesirable levels.

DHEC issued a Corrective Order to New-Indy on May 7, 2021, to correct undesirable levels of air contaminants. On May 13, 2021, New-Indy received a Clean Air Act Section 303 Emergency Order from EPA.

### **3. OPERATIONS AND PROCESS DESCRIPTION**

#### **3.1 SITE HISTORY**

New-Indy Catawba LLC (New-Indy) operates an integrated pulp and paper mill located in Catawba, South Carolina. The original pulp mill was constructed in 1959, which included a woodyard area for the processing of raw material, a kraft mill to chemically process wood chips into pulp, a pulp dryer, a chemical recovery area to recycle process chemicals, a utilities area to generate steam and electricity, a waste treatment area, and other operations.

In 1962, a paper machine (No. 1 paper machine) and a groundwood pulping process were added to the facility to facilitate the production of paper. An additional paper machine (No. 3 paper machine) was installed in 1968, as well as the expansion of the groundwood pulping process. A thermo-mechanical pulping (TMP) process was added to the facility in 1978. Eight years later (1986), the groundwood and thermo-mechanical pulping processes were eliminated, while a new paper machine (No. 2 paper machine) was installed to increase the production of paper. Also in 1986, a new thermo-mechanical pulping process was added to replace the original thermo-mechanical pulp (TMP) process.

In 2003, the original kraft pulping system and bleach plant were replaced with a state-of-the-art kraft fiber line and bleaching system. In addition, No. 3 paper machine was converted from newsprint to coated paper production, and TMP was also re-configured to support only coated paper production. In 2011, the kraft pulping system and bleaching system were modified to increase production, while using the same amount of wood furnish and cooking chemicals.

In 2020, the Catawba Mill was converted from manufacturing bleached pulp suitable for manufacturing bleached lightweight coated paper and market pulp to unbleached pulp suitable for manufacturing linerboard and other unbleached pulp and paper products. The conversion resulted in retirement of the bleaching system, the TMP plant, No. 1 paper machine and several other operations. Although not currently running, the No. 2 paper machine remains permitted and is in standby for potential future use as markets allow.

### **3.2 OVERALL PROCESS DESCRIPTION**

The Catawba Mill is comprised of seven (7) distinct process areas, which include the following: the woodyard area, the kraft pulp mill area, the paper mill area, the chemical recovery area, the utilities area, the waste treatment area, and a miscellaneous area. A process flow diagram for these process areas has been included as Figure 3-1. An overall description of the process areas is found below.

Southern pine logs and chips are received by the Catawba Mill at the woodyard. Logs are debarked, chipped, and the chips are screened prior to storage for use within the pulping processes. Likewise, wood chips received at the mill are screened, and processed as needed, prior to use within the pulping processes.

The kraft (sulfate) process area is used to produce pulp. Pulp from the kraft process is produced from “cooking” wood chips in a caustic solution at an elevated temperature and pressure.

Linerboard (the outside layer in a corrugated container) is produced in the paper mill area on one state-of-the-art paper machine. Unbleached market pulp is produced on one pulp dryer.

The recovery furnaces (chemical recovery area), which are auxiliary to the kraft process, burn the organics extracted from the chips and recover cooking chemicals. The causticizing area utilizes the chemicals recovered by the recovery furnaces, and after adding lime, provides the cooking chemicals for the kraft process.

Steam and electricity are produced for facility-wide use by two combination boilers. The recovery furnaces also generate steam.

A waste treatment area receives wastewater and mill waste (solid waste) from the various previously mentioned areas of the facility. Wastewater undergoes biological treatment to remove the dissolved organic wastes prior to discharge into the receiving stream. Mill solid waste is deposited within an on-site landfill for disposal.

The miscellaneous areas include everything which is not captured in one of the aforementioned process operating areas, which includes the facility roads and the pulp storage tanks.

### **3.3 WOODYARD**

Pulp and paper production operations require fibrous vegetative material, or furnish, as a raw material. The Catawba Mill receives virgin fibers in the form of southern pine logs (roundwood furnish) or chips via trucks or railcar. Southern pine materials are off-loaded and stored for processing.

To produce a homogeneous pulping feedstock, roundwood furnish (logs) are transported to the debarking drums for processing. The resulting debarked logs are then cut into chips of equal size through the use of chipper machines. As the wood chips exit the chipper, the material is screened for size using a series of vibrating screens. Oversized chips are isolated and reprocessed to generate acceptably resized chips. Undersized chips, along with the debarking waste, are conveyed to the utilities area for use as a fuel within the facility's boilers.

Raw materials, received in chip form, are screened and processed as noted above. Once the chips, either in-house produced or purchased, are screened, the accepted chips are stored in silos for use by the kraft pulp mill.

The woodyard area was part of the original mill construction in 1959. In 1985, half of the original process equipment was replaced with new equipment. The other half of the woodyard equipment was replaced in 1991. As a result of these changes, the log slashing operation constructed in 1959 was eliminated.

No modifications were required to the woodyard to support manufacturing unbleached pulp. The woodyard operation does not require the use of pollution control devices.

### **3.4 FIBER LINE**

The fiber line utilizes "state-of-the-art" technology for production, process control, environmental control, and energy conservation. Cooking of chips is accomplished in one continuous Kamyr digester. The digester utilizes steam heat and white liquor (a caustic solution) to cook the wood chips into pulp. The outgoing pulp goes to a blow tank for storage at near atmospheric pressure conditions. The pulp is then washed to remove the spent cooking chemicals and dissolved organics (including lignin, the "glue" in wood) extracted from the chips. The washed pulp (called "brown

stock”) undergoes additional processing to separate fiber bundles. The brown stock is adjusted for percent solids and stored in high-density storage chests prior to use in the paper mill.

In late 2020, the fiber line was converted from producing virgin fiber suitable for brightening (bleaching) used to manufacture lightweight coated paper to producing virgin fiber suitable for manufacturing unbleached linerboard. The conversion increased the virgin pulp yield by tripling the Kappa number from less than 30 for bleached pulp to over 90 for unbleached pulp. The Kappa number indicates the “harshness” of the cook: lower Kappa resulting from a harsher cook than higher Kappa. The higher Kappa number (less harsh cooking conditions) dissolves fewer organics from the wood, thereby producing more tons of virgin pulp using the same amount of wood with fewer cooking chemicals.

The oxygen delignification system, bleaching system and chlorine dioxide plant were shut down and retired from service in September 2020 to facilitate the conversion to unbleached paper grades. During the conversion, the washers in the retired oxygen delignification system and bleaching system were repurposed to serve as two parallel three-stage brown stock washers. New refiners and screw presses were also installed to facilitate processing the higher Kappa pulp.

Process vapors from the continuous digester, washers, refiners and other sources in the fiber line are collected and routed to the non-condensable gases (NCG) collection system and then routed to the combination boilers for destruction of total reduced sulfur (TRS) compounds and hazardous air pollutants (HAPs). The fiber line NCG collection system was modified to collect process vapors from the new refiners and screw presses and the repurposed brown stock washers.

### **3.5 PAPER MILL**

#### **3.5.1 Paper Machines**

The No. 3 paper machine utilizes stock (pulp) prepared in the fiber line. Screens, cleaners, and refiners precede the paper machine to develop a uniform stock inventory. The stock is fed to a headbox which evenly distributes the diluted stock across the width of the paper machine. After the headbox, a sheet forms as water is drained via the forming fabric, located on the wet end of the paper machine. After the freestanding water is removed, the sheet proceeds through presses which

remove entrained water. The sheet then enters the dryer sections, which consist of a series of steam heated rotating cylinders, causing the sheet to “snake” around from one dryer to the other. The sheet exits the dryers and is wound onto a jumbo roll which is later cut down to smaller rolls on the winder. The finished rolls are then prepared for shipping.

The No. 3 paper machine was extensively modified to convert from manufacturing coated paper to linerboard. The coating equipment installed in 2003 was removed and the remaining systems were either replaced or upgraded to support linerboard production. The No. 3 paper machine operation does not require pollution control devices.

The No. 2 paper machine was not modified and is not operating but remains available should a market develop for its production capabilities. The No. 2 paper machine operation does not require pollution control devices.

### **3.5.2 Pulp Dryer**

The pulp dryer utilizes stock prepared in the fiber line. Screens precede the pulp dryer to allow for a uniform stock inventory. The pulp dryer is a cylinder machine in which the stock is fed to a “vat” headbox. After the headbox, a sheet forms as water is drained via the vacuum drum located on the wet end of the pulp dryer. After the freestanding water is removed, the sheet proceeds through presses which remove entrained water. The sheet then enters the dryer sections where a Flakt air flotation system is utilized. The pulp dryer has a steam heated booster oven which allows for additional drying, thus ensuring the final product meets customer specifications for percent moisture. The sheet exits the dryers and is cut into sheets and packaged for shipping.

The pulp dryer stock screening system was put into service by modifying the stock supply system from the No. 1 paper machine (which was retired) to support manufacturing unbleached market pulp. The pulp dryer operation does not require pollution control devices.



## **3.6 CHEMICAL RECOVERY**

### **3.6.1 Evaporator System**

The three evaporator sets receive dilute (weak) spent cooking liquor and dissolved organics, otherwise known as black liquor, from the fiber line. The evaporator sets, which are multiple shell and tube heat exchangers, utilize steam to evaporate water and thicken the weak black liquor. This thickened black liquor undergoes additional concentrating in the concentrators until enough water has been removed from the black liquor so it can sustain its own combustion process in the recovery furnaces. This concentrated black liquor is then injected into the two recovery furnaces where the dissolved organics are burned, chemicals are recovered, and steam is produced.

Emissions from the processing of black liquor through the evaporator sets are collected and treated in the low volume high concentration (LVHC) NCG system. The LVHC NCG System collects vapors from the evaporator hotwells and turpentine system vents, while emissions from the weak black liquor tanks are collected in the high volume low concentration (HVLC) system for destruction in one of the Combination Boilers. The LVHC NCG system is equipped with an in-line caustic scrubber to capture non-condensable sulfur compound vapors from the gas stream prior to incineration in either the No. 1 or No. 2 Combination Boiler. The caustic solutions from the smelt dissolving tank scrubber and LVHC in-line scrubber are recycled for the processing of wood chips.

The No. 1 evaporator set was modified to increase the evaporation rate to account for the reduction in the solids content of the weak black liquor from the repurposed washers following the conversion to unbleached pulp. No modifications were required to the No. 2 and No. 3 evaporator sets to support manufacturing unbleached pulp. No modifications were required for the LVHC NCG system to support manufacturing unbleached pulp.

### **3.6.2 Recovery Furnaces**

The No. 2 and No. 3 recovery furnaces combust black liquor from the evaporator sets to remove dissolved organic compounds, recover the sodium and sulfur compounds used in the cooking liquor, and generate steam to operate the kraft pulp mill. The recovery furnaces also have the

potential to burn No. 6 fuel oil and natural gas. Each recovery furnace is equipped with an electrostatic precipitator (ESP) to collect and recover the dried sodium and sulfur compounds and control particulate matter emissions.

No modifications were required to the recovery furnaces to support manufacturing unbleached pulp. No modifications were required for the ESPs serving the No. 2 and No. 3 recovery furnaces to support manufacturing unbleached pulp.

### **3.6.3 Smelt Dissolving Tanks**

Molten sodium and sulfur compounds are collected from the recovery furnace as smelt from the combustion of the black liquor. The resulting smelt is then transported from the recovery furnaces into the two smelt dissolving tanks where the smelt is dissolved with recycled weak cooking chemicals to generate green liquor. This green liquor is then pumped to the Causticizing Area for further processing and re-use in the kraft process.

Smelt dissolving tanks No. 2 and No. 3 are equipped with a caustic scrubber to recycle non-condensable sulfur compounds and prevent these sources from being an odor source. Vapors from the weak black liquor tanks are collected by the HVLC system for destruction in one of the Combination Boilers. The caustic solution from the smelt dissolving tank scrubber is collected to supplement the cooking chemicals used in the fiber line for the processing of wood chips.

No modifications were required to the smelt dissolving tanks to support manufacturing unbleached pulp. No modifications were required for the caustic scrubber serving the No. 2 and No. 3 smelt dissolving tanks to support manufacturing unbleached pulp.

### **3.6.4 Precipitator Mix Tanks**

The precipitator mix tanks recover the dried sodium and sulfur compounds collected from the recovery furnaces for reuse within the kraft pulping process. No modifications were required to the precipitator mix tanks to support manufacturing unbleached pulp. The precipitator mix tanks vent through the recovery furnaces and no modifications to the venting were required to support manufacturing unbleached pulp.

### **3.6.5 Causticizing Area**

The Causticizing Area is designed to regenerate the cooking chemicals for the kraft pulping process. Sodium and sulfur compounds are recovered at the recovery furnaces from the burning of black liquor and are pumped from the smelt dissolving tanks to the Causticizing Area as “green liquor.” Hydrated lime is added to the green liquor to form “white liquor” and calcium carbonate (lime mud). The white liquor, which is a strong caustic/sulfide solution, is used in the fiber line digester for the cooking of chips. The sodium/sulfide chemicals are contained in a closed loop within the green, white, and black liquors. The lime slaker is equipped with a wet scrubber to control nuisance dust.

No modifications were required to the causticizing area to support manufacturing unbleached pulp. No modifications were required for the slaker scrubber to support manufacturing unbleached pulp.

### **3.6.6 Lime Kiln**

The Lime Kiln No. 2 is designed to assist in regenerating the cooking chemicals for the kraft pulping process. Hydrated lime is added to the green liquor to form “white liquor” and calcium carbonate (lime mud). The lime mud is separated from the white liquor, thickened, washed, and then returned in the Lime Kiln to again form lime for converting recovered green liquor to white liquor. The calcium chemicals are contained in a closed loop within the lime, hydrated lime, white liquor, and lime mud constituents. The lime kiln is equipped with an electrostatic precipitator to control particulate emissions.

No modifications were required to the lime kiln to support manufacturing unbleached pulp. No modifications were required for the lime kiln ESP to support manufacturing unbleached pulp.

## **3.7 UTILITIES**

Wood waste, such as bark, sawdust, and undersized chip fractions, is screened at the Woodyard to assure acceptable quality to burn in the No. 1 and No. 2 Combination Boilers. This wood waste is conveyed to the Util/Misc. area. Fuel oil is transported to the facility via truck or rail tanker. Natural gas is supplied by pipeline. Tire derived fuel (TDF) is transported by truck. Each combination boiler is equipped with an ESP to control particulate emissions.

Steam produced by the boilers goes into a common header and a portion is then throttled into the extraction turbine generators. These units receive high pressure steam, extract part of the energy, and discharge steam at lower temperatures and pressures. The lower pressure steam is utilized throughout the facility for process heating purposes. The condensate is returned to the Util/Misc. area for reuse.

The combination boilers also incinerate the NCG gases collected from the kraft pulp mill, the chemical recovery evaporator sets and turpentine recovery system, and the foul condensate steam stripper to control emissions of TRS compounds and HAPs. Incineration of the NCG gases is continuously monitored using the flame failure systems on each boiler. The NCG collection systems are also monitored monthly and annually for leaks following the Catawba Mill Leak Detection and Repair (LDAR) program. The LDAR inspection reports are included in Appendix A.

This area is also responsible for providing the high quality, high purity water which is required for steam production. This is accomplished through the use of flocculation beds, sand filters, and demineralizers.

No modifications were required to the combination boilers to support manufacturing unbleached pulp. No modifications were required for the ESPs serving the No. 1 and No. 2 combination boilers to support manufacturing unbleached pulp.

The fiber line NCG collection system was modified to collect process vapors from the new refiners and screw presses and the repurposed brown stock washers.

### **3.8 WASTE TREATMENT**

#### **3.8.1 Condensate Collection and Treatment System**

The Catawba Mill utilizes a condensate collection tank to accumulate kraft pulping process foul condensate prior to treatment. The condensate collection tank acts as a feed tank for the foul condensate steam stripper and/or the hard pipe to the wastewater treatment system. Contaminants from the foul condensate can be removed in the steam stripper and combusted within a combination boiler or treated biologically in the wastewater system aerated stabilization basin

(ASB). “Clean condensate” from the stripper column is recycled back to the brown stock washers for use as shower water.

The foul condensate treatment system was modified to use the hard piping option to biologically treat the foul condensate in the ASB. This modification was approved by DHEC with permit TV-2440-0005-DF. The hard pipe has no emissions points.

The foul condensate steam stripper was cleaned, repaired, thoroughly checked for proper process control functionality, and returned to service in May 2021. The checkout process also included a complete Pre-Startup Safety Review, requisite Management of Change documentation, P&ID drawing validations, interlock validations, instrumentation calibrations, instrument performance validation, and operator training reviews. No modifications to the stripper-off-gases (SOG) NCG system were required to support returning the steam stripper to service.

### **3.8.2 Wastewater Treatment System**

The Wastewater Treatment System is designed to collect all of the wastewaters from the mill, remove settleable solids, and biologically treat the dissolved organics. Most of the wastewater collects within the mill sewers. The sewers gravity flow to the primary clarifier. The clarifier allows solids to settle to the bottom and be removed and clarified water to overflow to either a settling pond or directly to the aerated stabilization basin (ASB). The solids from the primary clarifier, otherwise known as “sludge,” are pumped to the primary solids EQ Basin that allows additional separation (thickening) of the solids. Decant from the EQ Basin flows into the aeration basin along with clarified wastewater from the clarifier. The condensate hard pipe discharges below the liquid surface of the ASB to biologically treat contaminants in the foul condensate. The treated wastewater from the aeration basin flows into holding ponds. From the holding ponds, the treated wastewater flows by gravity through a Post-Aeration Basin where mechanical aerators increase the dissolved oxygen content of the wastewater prior to discharge into a receiving stream.

Primary clarifier solids that thicken in the EQ Basin are dredged and placed in the No. 4 Sludge Pond for disposal.

The ASB was modified by increasing the diameter of the hard pipe below the liquid surface near the entrance to the ASB. The wastewater treatment system does not operate with control devices.

### **3.8.3 Industrial Landfill**

A 15-acre industrial landfill is located west of the paper machines at the mill. Paper, bark, and other wood product wastes are deposited within the landfill on a daily basis. Fly ash, grits, and dregs are also approved for disposal in the landfill. While mill refuse is disposed on-site, commercial and office waste streams are collected and transported off-site for disposal. Fill dirt is removed from the on-site borrow pits and deposited atop the refuse as daily cover.

No modifications were required to the industrial landfill to support manufacturing unbleached pulp. The landfill does not operate with control devices.

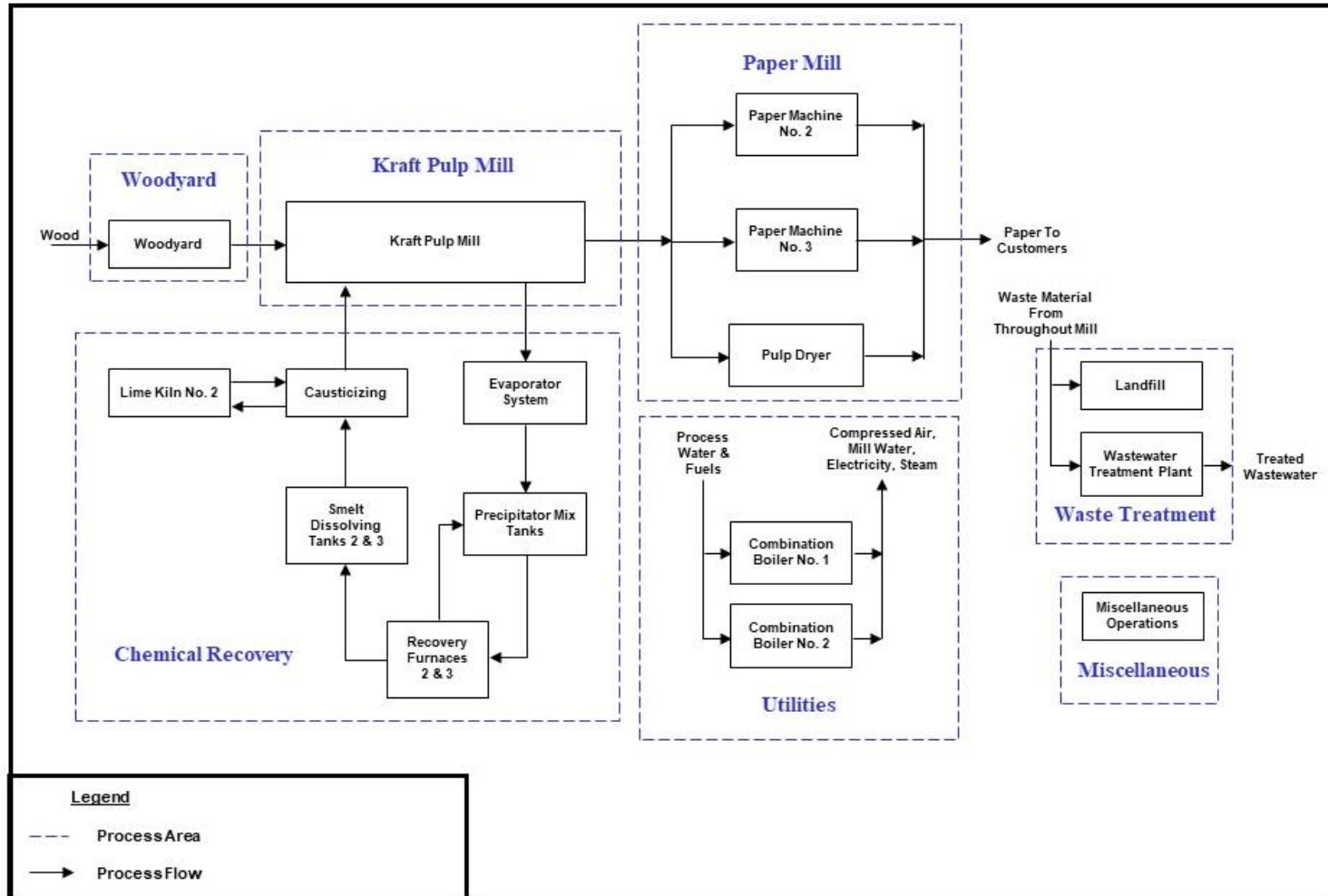
### **3.9 MISCELLANEOUS SOURCES**

The Catawba Mill includes miscellaneous equipment and operations such as facility roads, emergency generators, storage tanks, facility maintenance activities, and lab activities.

The pumps and piping to the high density (HD) pulp storage tanks were modified to re-direct pulp from the retired No. 1 paper machine and better support unbleached pulp. The agitators in each tank were also rebuilt or replaced and the No. 4 HD storage tank was repurposed as a low density (LD) storage tank.

No modifications were required to the tanks storing black liquor, green liquor, or white liquor. The spare and weak liquor tanks are vented to the HVLC system for treatment. The pulp tank and other liquor storage tanks do not operate with control devices.

**Figure 3-1  
Simplified Mill Flow Diagram**



## **4. NEW-INDY EVALUATION OF OPERATIONS AND PROCESSES**

### **4.1 NEW-INDY EVALUATION OF OPERATIONS AND PROCESSES TO IDENTIFY POTENTIAL ODORS CONDUCTED IN CONSULTATION WITH NCASI**

Paragraph 3 of DHEC's May 7, 2021 Order reads:

3. On or before June 1, 2021, complete an evaluation conducted in consultation with a nationally recognized organization, such as the National Council for Air and Stream Improvement (NCASI), to fully evaluate the current operations and processes at the Facility to identify all potential sources that could be contributing to the odors and elevated levels of H<sub>2</sub>S on and off Facility property. The evaluation must include the recent change in operation from making bleached paper to brown paper, the wastewater treatment plant operations, the recent modifications related to the steam stripper and the hard piping of the foul condensate tank to the wastewater treatment plant, any increases in stack emissions, any changes in operation of pollution control equipment, and any uncontrolled emissions to determine if these changes are contributing to the odors in the vicinity of the Facility.

New-Indy submitted an evaluation to DHEC on June 1, 2021. This Section of the CAP describes in additional detail New-Indy's efforts in consultation with NCASI to fully evaluate current operations at the New-Indy mill to identify potential sources that could be contributing to reported odors and hydrogen sulfide emissions. As explained in Section 3, the Catawba Mill is comprised of seven distinct process areas, including the woodyard area, the kraft pulp mill area, the paper mill area, the chemical recovery area, the utilities area, the waste treatment area, and the miscellaneous area. In consultation with numerous consultants and advisors, including NCASI personnel, personnel from New-Indy conducted an evaluation of each process area to identify potential sources that could be contributing to reported odors.

New-Indy understands that the majority of odor complaints describe a "rotten egg" odor that generally is associated with H<sub>2</sub>S. New-Indy conducted its evaluation of operations and processes as they might relate to the different types of odors generally associated with integrated kraft pulping and chemical recovery operation.

Mill personnel at New-Indy conducted the odor evaluation, but New-Indy also engaged the assistance of eight (8) different consultant and engineering firms to assist in the evaluation and corrective action planning, including TRC Consultants (air and wastewater), ALL4, Weston



Solutions (“Weston”), NCASI personnel, Environmental Business Specialists (“EBS”), LDX Solutions (“LDX”), E360 and Trinity. This evaluation included an intensive Leak Detection and Repair (“LDAR”) evaluation by E360, installation of three mobile ambient monitors and meteorological stations by TRC and a screening analysis by Weston, among many other efforts.

#### **4.2 LDAR EVALUATION**

Pursuant to the mill’s Title V air permit, the mill is subject to LDAR requirements under Federal law. Leaks from manufacturing and related equipment, particularly pipes and flanges, can be potential sources of odors. After receiving the initial round of odor complaints in January and February of 2021, New-Indy engaged its LDAR consultant, E360, to conduct an intensive LDAR evaluation at the mill. The LDAR consultant conducted the evaluation of each of the mill’s identified potential leak points and discovered no deficiencies in the mill’s program or in the equipment. *See* Appendix A for E360’s LDAR Evaluation Report.

#### **4.3 SCREENING ANALYSIS**

To attempt to identify concentrations and locations of H<sub>2</sub>S at the mill, New-Indy engaged Weston to conduct a screening analysis of H<sub>2</sub>S emissions. Weston conducted ambient air sampling and drafted a report that is attached hereto as Appendix B.

#### **4.4 AMBIENT AIR MONITORS**

After New-Indy conducted its initial screening with Weston, New-Indy determined that it needed additional data to quantify the impact of potential odor sources at the mill. New-Indy engaged TRC to install two ambient monitors, one on mill property, but across the road from the mill entrance at an adjacent baseball field, and one on-site near the ASB. The unit at the baseball field contained a meteorological station. Later, New-Indy determined that it needed additional monitoring data, so it installed a third monitoring station to the northeast of the mill near the Highway 5 bridge and a new meteorological monitoring station on top of the kraft pulp mill digester structure (250 feet above ground elevation, unencumbered by any nearby building structures). The locations of the three monitors is attached hereto as Appendix C. The data from the three monitors is attached hereto as Appendix D.

#### **4.5 PROCESS AREA REVIEW**

As noted above, New-Indy reviewed its seven process areas to evaluate potential odor issues:

- **Woodyard** - Odors typically associated with the woodyard are “pine” or “wood” type odors, similar to logging and wood milling operations. These are not the types of odors about which complaints are being made. New-Indy, in consultation with its consulting professionals, concluded that the woodyard was not a likely source of the subject odors.
- **Kraft pulp mill** - A kraft pulping process can produce odors similar to “rotten eggs.” However, the chemicals that create these odors are treated in air emission control equipment. The mill is in full compliance with its air permit conditions, including LDAR. New-Indy, in consultation with its consulting professionals, concluded that the kraft pulping process likely was not the source of off-site odors.
- **Paper mill** - A paper machine process can affect the wastewater treatment plant’s operation, but typically only as a result of the impact of sewerage waste losses on the wastewater treatment plant system. The dilution water (white water) from the paper machine overflows into the sewer to the wastewater treatment plant. Upset operating conditions in the pulp mill can cause organic and chemical carryover to the paper machine operations which will get drained out of the pulp on the machine and into the process sewer. Operational upsets in the paper machine operation can also result in pulp fiber being released to the process sewer. Both of these upset scenarios can have an impact on the wastewater treatment plant efficiencies. New-Indy, in consultation with its consulting professionals, concluded that the paper machine process itself likely was not the source of off-site odors.
- **Chemical Recovery** - The Chemical Recovery processes can emit odors similar to “rotten eggs.” However, the chemicals that create these odors are treated in air emission control equipment. The mill is in full compliance with its air permit conditions, including LDAR. New-Indy, in consultation with its consulting professionals, concluded that the chemical recovery process likely was not the source of off-site odors.

- Utilities - The utilities process does not emit the type of odors about which complaints are being made. New-Indy, in consultation with its consulting professionals, concluded that the utilities likely were not the source of off-site odors.
- Miscellaneous sources - The miscellaneous sources do not emit the type of odors about which complaints are being made. New-Indy, in consultation with its consulting professionals, concluded that the miscellaneous sources likely were not the source of off-site odors.
- Waste Treatment - The waste treatment system can emit odors similar to “rotten eggs.” These odors can occur when the wastewater is not efficiently treated in the wastewater treatment process. New-Indy and its consulting professionals concluded that the waste treatment system may be the cause of odors. These low level odors, though, do not explain the intense reactions being reported by local residents who live at long distances from the plant.

After review of the various operations and processes, and upon consultation with NCASI and its other professional consultants, New-Indy narrowed its focus to the wastewater system.

## **5. NEW-INDY EFFORTS TO ADDRESS ODOR COMPLAINTS**

This section details New-Indy's considerable efforts to address odor complaints. New-Indy received the first odor complaint on January 22, 2021. Since that time, New-Indy has worked tirelessly to respond to the complaints, evaluate New-Indy's operations and address reported odors.

Around the time that New-Indy began receiving odor complaints, South Carolina DHEC conducted an air quality inspection, on February 22 and 23, 2021, and a wastewater inspection, on March 15, 2021, at the mill. The wastewater inspection identified a fiber layer on the surface of the ASB. The layer of fiber on the ASB was the result of initial startup operations following the conversion from bleached paper to unbleached containerboard. The layer of fiber made it difficult for personnel to reach the aerators in the ASB and conduct preventive maintenance and repairs. As a result, several aerators became inoperable.

Beginning on March 1, 2021, New-Indy began removing the layer of fiber from the surface of the ASB. This effort has continued using various methods, including cutting the rim from the forty or so feet of fiber closest to the edge of the basin and using a barge to dredge and push the fiber layer toward the edge of the ASB. That fiber layer is hauled to the No. 4 sludge pond where it is processed with other similar waste. These continuing efforts to remove the fiber layer, along with New-Indy's use of an air boat have allowed personnel to reach the aerators, conduct maintenance and repairs on those aerators and return them to service. The ASB has fifty-two aerators, and at present, 38 of those aerators are operating. In the past 30 days, New-Indy has put 10 aerators back into operation.

Also when New-Indy began receiving odor complaints, New-Indy established a community service hotline to identify complaints. New-Indy began logging complaints, including location, time, date, mill operations assessment and wind speed and direction.

On March 5, 2021, New-Indy conducted a full odor survey with its LDAR consultant, E360. The consultant determined that there were no significant leaks that could cause offsite odors and that the plant was in compliance with its LDAR requirements under Federal law. The mill continues to complete monthly LDAR inspections with no significant leaks having been detected, and when

minor leaks are discovered during the inspection, repairs are made as quickly as possible and within compliance guidelines for those repairs.

On March 8, 2021, New-Indy contacted NCASI for assistance in evaluating operations. The next day, on March 9, the mill contacted Trinity Consultants to assist in the evaluation of odor issues. The following day on March 10, 2021, DHEC visited the mill for a senior DHEC management meeting with the mill. That meeting included Myra Reece, Renee Sheeley, Rhonda Banks, Mike Marcus and Henry Porter at DHEC, along with mill personnel. The DHEC representatives and mill personnel reviewed the mill's progress toward identifying sources of odors, and abating odors.

On March 12, 2021, New-Indy began consultation with LDX regarding utilization of the stripper as opposed to hard piping the foul condensate. With the approval of permit TV-2440-0005-DF in July of 2019, New-Indy obtained DHEC approval to idle the foul condensate steam stripper and hard pipe foul condensate to the ASB.

On March 17, 2021, New-Indy hosted two environmental consultants onsite. The first was Weston for sampling ambient emissions and emissions from process vents and stacks and multiple ambient locations throughout the mill property. The second was TRC for onsite ambient monitoring, working in concert with Weston to guide the ambient air monitoring effort and observe the wastewater treatment system. TRC returned on March 19, 2021, to observe the wastewater system and again on March 24, 2021, for additional onsite monitoring evaluations. On March 25, 2021, New-Indy purchased an odor measurement drone and hand-held equipment (delivery scheduled for early to mid-June). On March 30, 2021, TRC and another consultant (ALL 4) conducted an air dispersion modeling review.

It was important for New-Indy to determine the emissions at New-Indy's property boundary and onsite. As such, New-Indy engaged TRC to install three mobile monitoring units at the property. One unit was located on mill property but across the road from the main entrance in a nearby baseball field. That monitor was equipped with a meteorological station. The second monitor was located in the plant property. On April 28, 2021, the third monitor was located on the property near the I-5 bridge. Appendix C indicates the location of the monitors. Appendix D provides the monitoring data for the three monitoring stations. The first onsite data was generated on approximately April 9, 2021.

On April 9, 2021, New-Indy began removing solids from the equalization basin. Four days later, on April 13, 2021, New-Indy began optimizing liquor sulfidity control in the ASB. Ten days later, on April 19, 2021, New-Indy began adding calcium nitrate in the ASB to supplement oxygen as an electronic acceptor and reduce the formation of hydrogen sulfide.

During this time, New-Indy requested that Weston conduct a screening analysis to determine if high levels of H<sub>2</sub>S were being generated at and around the mill. Weston took air samples and generated a screening report that New-Indy provided to DHEC on April 19, 2021. The Weston report is attached as Appendix B. On April 21, 2021, New-Indy began an operations project to return the stripper to operation. On April 28, 2021, TRC installed the third ambient monitor at a location near the bridge on Interstate 5.

The foul condensate steam stripper was returned to operation on May 3, 2021. On that same day, New-Indy hosted consultants Valmet and Rolf Ryham to provide guidance for optimizing the performance of the recovery furnace.

On May 7, 2021, New-Indy received the DHEC order and began implementing the order's requirements, in addition to continuing its odor mitigation efforts independent of the DHEC order. On May 11, 2021, New-Indy continued its No. 1 holding pond oxygen improvement levels by feeding calcium nitrate into the ASB. The site also had an air modeling meeting with TRC and a meeting with NCASI to discuss the need for NCASI to verify the emissions factors the mill used to calculate the actual and potential emissions included in the construction permit application for the change to containerboard. New-Indy had another meeting with NCASI on May 14, 2021, in which NCASI verified the mill used the correct emission factors and validated the calculations.

On May 13, 2021, New-Indy received an order from EPA. Immediately, New-Indy began implementing the requirements of the May 13 EPA order, in addition to continuing its odor mitigation efforts. New-Indy engaged SFC to use a "push boat" that was mobilized on May 16, 2021, to push the fiber layer at the ASB toward the bank. SFC worked with Saiia to transport the solids from the ASB to the No. 4 sludge dewatering pond. This push boat was successful for several days, but as it got progressively deeper into the surface solids, it reached a point where it could no longer push into the material to push it towards the dike for removal by the long arm excavator. Throughout April and May, New-Indy continued to return aerators to service. On

May 26, 2021, New-Indy moved its three ambient air monitors to new locations pursuant to the EPA order. Attached as Exhibit E is the current location of the monitors. Attached as Exhibit F is the air emissions data generated by the monitors.

On May 26, 2021, New-Indy launched a website dedicated to facilitating communication and transparency with local residents and regulatory agencies ([www.newindycatawba.com](http://www.newindycatawba.com)). This website includes daily reports explaining the EPA's independent hydrogen sulfide data collection as well as information about the mill. The mill also posts its daily ambient air emissions monitoring report on the website in an effort to provide transparency to the public. The website also includes public notices of any mill activities that may generate increased odor levels.

On June 8, 2021, New-Indy consulted with LDX regarding current stripper capacity and the repaired trim reflux condenser, which is used to polish the methanol capture efficiency for the stripper operation. On June 8, 2021, New-Indy personnel participated in Scentroid TR8 and Pollutracker training to learn how to use the instrument to measure ambient concentrations on both instantaneous and longer term (24-hour) measurement periods. New-Indy also removed the trim reflux condenser from the stripper for repairs in an effort to increase stripper capacity. On June 9, 2021, New-Indy improved the oxygen transfer into No. 1 Holding Pond by installing two aerators and injecting peroxide into the waste stream. On June 9, 2021, the Post-Aeration Basin tank at the wastewater outfall was upfitted with a new cover and carbon filter. Also on that day, personnel began using the TR8 and Pollutracker handheld devices in the field to measure ambient levels of H<sub>2</sub>S at various locations and evaluate the initial inlet and discharge concentrations around the pilot activated carbon filtration system. Also in June, the plant continued to remove ASB fiber layer using a barged-mounted long-reach excavator in addition to a long-reach excavator from the bank.

## **6. CORRECTIVE ACTION PLAN – CONDITION 6**

### **6.1 H<sub>2</sub>S SOURCE EVALUATION**

Condition 3 of the DHEC Order required New-Indy to complete the following:

On or before June 1, 2021, complete an evaluation conducted in consultation with a nationally recognized organization, such as the National Council for Air and Stream Improvement (NCASI), to fully evaluate the current operations and processes at the Facility to identify all potential sources that could be contributing to the odors and elevated levels of H<sub>2</sub>S on and off Facility property. The evaluation must include the recent change in operation from making bleached paper to brown paper, the wastewater treatment plant operations, the recent modifications related to the steam stripper and the hard piping of the foul condensate tank to the wastewater treatment plant, any increases in stack emissions, any changes in operation of pollution control equipment, and any uncontrolled emissions to determine if these changes are contributing to the odors in the vicinity of the Facility.

New-Indy consulted with NCASI in May 2021 and confirmed the emissions estimates contained in the 2019 and 2020 air permit applications were correctly applied and generally representative of the conversion from manufacturing bleached paper to brown paper.

The H<sub>2</sub>S and TRS (H<sub>2</sub>S, methyl mercaptan, dimethyl disulfide and dimethyl sulfide) emissions from each area of the mill are reviewed in the following sections. A summary of the H<sub>2</sub>S and TRS emissions are provided in Table 6-1.

#### **6.1.1 Woodyard**

No modifications were required to the woodyard to support manufacturing unbleached pulp. The woodyard does not operate with control devices. There are no known H<sub>2</sub>S or TRS emissions from the woodyard.

#### **6.1.2 Kraft Pulp Mill**

The conversion to brown paper increased the virgin pulp yield by tripling the Kappa number from less than 30 for bleached pulp to over 90 for unbleached pulp. Kappa number is a key test method



for determining the level of lignin remaining in a sample of digested pulp. The Kappa number indicates the “harshness” of the cook, lower Kappa being a harsher cook than higher Kappa. The higher Kappa number (less harsh cooking conditions) dissolves fewer organics from the wood, thereby producing more tons of virgin pulp using the same amount of raw materials (wood and with fewer cooking liquor chemicals).

With the exception of the pulp storage tanks after pulp washing, the kraft pulp mill sources are collected and routed to the non-condensable (NCG) system, and H<sub>2</sub>S and TRS emissions are controlled through incineration in the combination boilers.

Source testing of both the No. 1 and No. 2 combination boilers will be conducted by New-Indy, in accordance with Condition 5 of the DHEC order to confirm the original H<sub>2</sub>S and TRS emissions estimates based on information from, and verified by, NCASI.

### **6.1.3 No. 2 Paper Machine**

The No. 2 paper machine was not modified and remains available should market conditions create an opportunity for its production capabilities to be utilized. The No. 2 off-machine coaters have been retired from service. The No. 2 paper machine does not operate with control devices. The No. 2 paper machine has not returned to operation following the conversion.

### **6.1.4 No. 3 Paper Machine**

The No. 3 paper machine was extensively modified to convert from manufacturing coated paper to linerboard. The No. 3 paper machine does not operate with control devices. New-Indy conducted a screening study of one No. 3 paper machine vent, and no measurable TRS emissions were present in the vent gases. Source testing of the No. 3 paper machine will be conducted by New-Indy in accordance with Condition 5 of the DHEC order to confirm the original H<sub>2</sub>S and TRS emissions estimates based on information from NCASI.

### **6.1.5 Pulp Dryer**

The pulp dryer stock screening system was configured by modifying the stock screening system from the No. 1 paper machine (which was retired) to support manufacturing unbleached market pulp. The pulp dryer does not operate with control devices. Source testing of the pulp dryer will

be conducted by New-Indy in accordance with Condition 5 of the DHEC order to confirm the original H<sub>2</sub>S and TRS emissions estimates based on information from NCASI.

#### **6.1.6 Evaporator System**

The No. 1 evaporator set was modified to operate as a five-effect system to increase the evaporation rate to account for the reduction in the solids content of the weak black liquor from the repurposed washers following the conversion to unbleached pulp. No modifications were required to the No. 2 and No. 3 evaporator sets to support manufacturing unbleached pulp.

Emissions from the processing of black liquor through the evaporator sets are collected and treated in the low volume high concentration (LVHC) NCG system. The LVHC NCG System collects vapors from the evaporator hotwells and turpentine system vents. The LVHC NCG system is equipped with an in-line caustic scrubber to capture non-condensable sulfur compound vapors from the gas stream prior to incineration in either the No. 1 or No. 2 combination boiler.

No modifications were required for the LVHC NCG system to support manufacturing unbleached pulp. The Kappa change results in TRS emissions 16% lower per ton of pulp production based on information provided by NCASI.

Source testing of both the No. 1 and No. 2 combination boilers will be conducted by New-Indy in accordance with Condition 5 of the DHEC order to confirm the original H<sub>2</sub>S and TRS emissions estimates based on information from NCASI.

#### **6.1.7 Recovery Furnaces**

No modifications were required to the No. 2 and No. 3 recovery furnaces to support manufacturing unbleached pulp. No modifications were required for the ESPs serving the No. 2 and No. 3 recovery furnaces to support manufacturing unbleached pulp.

#### **6.1.8 Smelt Dissolving Tanks**

Smelt dissolving tanks No. 2 and No. 3 are equipped with a caustic scrubber to reduce particulate matter (PM) and TRS emissions.

No modifications were required to the smelt dissolving tanks to support manufacturing unbleached pulp. No modifications were required for the caustic scrubber serving the No. 2 and No. 3 smelt dissolving tanks to support manufacturing unbleached pulp.

New-Indy will conduct source testing of the smelt dissolving tank vent to confirm the original H<sub>2</sub>S and TRS emissions estimates based on information from NCASI.

#### **6.1.9 Precipitator Mix Tanks**

No modifications were required to the precipitator mix tanks to support manufacturing unbleached pulp. The precipitator mix tanks vent through the recovery furnaces, and no modifications to the venting were required to support manufacturing unbleached pulp. Therefore, emissions reported from the recovery furnaces reflect the emissions from these sources.

#### **6.1.10 Causticizing Area**

No modifications were required to the causticizing area to support manufacturing unbleached pulp. No modifications were required for the slaker scrubber to support manufacturing unbleached pulp. The causticizing area is a high pH process, and no H<sub>2</sub>S emissions are expected. In addition, the causticizing area uses fresh water and no change in TRS emissions is expected.

#### **6.1.11 Lime Kiln**

No modifications were required to the No. 2 lime kiln to support manufacturing unbleached pulp. No modifications were required for the lime kiln ESP to support manufacturing unbleached pulp.

#### **6.1.12 Combination Boilers**

The combination boilers also incinerate the NCG gases collected from the kraft pulp mill, the chemical recovery evaporator sets and turpentine recovery system, and the foul condensate steam stripper to control emissions of TRS compounds and HAPs. The kraft pulp mill NCG collection system was modified to collect gases from the new refiners and screw presses and the repurposed brown stock washers.

No modifications were required to the combination boilers to support manufacturing unbleached pulp. No modifications were required for the ESPs serving the No. 1 and No. 2 combination boilers to support manufacturing unbleached pulp.

Incineration of the NCG gases is continuously monitored using the flame failure systems on each boiler. The NCG collection systems are also monitored monthly and annually for leaks following the Catawba Mill Leak Detection and Repair (LDAR) program.

Source testing of both the No. 1 and No. 2 combination boilers will be conducted by New-Indy in accordance with Condition 5 of the DHEC order to confirm the original H<sub>2</sub>S and TRS emissions estimates based on information from NCASI.

#### **6.1.13 Condensate Collection and Treatment System**

The condensate treatment system was modified to use the hard piping option to biologically treat the foul condensate in the ASB. The hard pipe has no emissions points.

The foul condensate steam stripper was repaired and returned to service in May 2021. No modifications to the stripper-off-gases (SOG) NCG system were required to support returning the steam stripper to service or manufacturing unbleached pulp.

Source testing of the steam stripper will be conducted by New-Indy in accordance with Condition 5 of the DHEC order to confirm the original H<sub>2</sub>S and TRS emissions estimates based on information from NCASI.

#### **6.1.14 Wastewater Treatment System**

The ASB was modified by increasing the diameter of the hard pipe below the liquid surface near the entrance to the ASB. The wastewater treatment system does not operate with control devices.

Please see Section 7 for a detailed discussion of the wastewater treatment system.

### **6.1.15 Industrial Landfill**

No modifications were required to the industrial landfill to support manufacturing unbleached pulp. The landfill does not operate with control devices. There are no known H<sub>2</sub>S or TRS emissions from the landfill.

### **6.1.16 Miscellaneous Sources**

The pumps and piping to the high density (HD) pulp storage tanks were modified to re-direct pulp from the retired No. 1 paper machine and better support unbleached pulp. The agitators in each tank were also rebuilt or replaced, and the No. 4 HD storage tank was repurposed as a low density (LD) storage tank.

No modifications were required to the tanks storing black liquor, green liquor, or white liquor. Emissions from the spare and weak liquor tanks are vented to the HVLC system for treatment. The remaining pulp and liquor storage tanks do not operate with control devices. The emissions from all storage tanks were estimated using information from NCASI. No change to the storage tank emissions is expected based on the reduction in TRS due to the Kappa change.

No modifications were required to the other miscellaneous sources to support manufacturing unbleached pulp.

## **6.2 CORRECTIVE ACTION PLAN – CONDITION 6**

Condition 6 of the DHEC Order required New-Indy to complete the following:

On or before June 15, 2021, submit to the Department a report of the evaluation conducted in Step 3 above and, for review, comment, and approval; a corrective action plan (CAP) (developed and stamped by a South Carolina-registered Professional Engineer (PE)) and a schedule of implementation, which addresses operational issues identified in the above-referenced evaluation as contributing to the odor. The schedule of implementation shall include specific dates or timeframes for initiation and the completion of each action and details as to how each action addresses the odor and operational issues noted above.

The corrective actions for each area of the mill are reviewed in the following sections.

### **6.2.1 Woodyard**

No operational issues or corrective actions have been identified for the woodyard.

### **6.2.2 Kraft Pulp Mill**

Source testing of both the No. 1 and No. 2 combination boilers will be conducted by New-Indy in accordance with Condition 5 of the DHEC Order to confirm the original H<sub>2</sub>S and TRS emissions estimates based on information from NCASI.

No operational issues or corrective actions have been identified for the kraft pulp mill pending the results of the source testing required by Condition 5 of the DHEC Order.

### **6.2.3 No. 2 Paper Machine**

No operational issues or corrective actions have been identified for the No. 2 paper machine.

### **6.2.4 No. 3 Paper Machine**

Source testing of the No. 3 paper machine will be conducted by New-Indy in accordance with Condition 5 of the DHEC order to confirm the original H<sub>2</sub>S and TRS emissions estimates based on information from NCASI.

No operational issues or corrective actions have been identified for the No. 3 paper machine pending the results of the source testing required by Condition 5 of the DHEC Order.

### **6.2.5 Pulp Dryer**

Source testing of the pulp dryer will be conducted by New-Indy in accordance with Condition 5 of the DHEC order to confirm the original H<sub>2</sub>S and TRS emissions estimates based on information from NCASI.

No operational issues or corrective actions have been identified for the pulp dryer pending the results of the source testing required by Condition 5 of the DHEC Order.

### **6.2.6 Evaporator System**

Source testing of both the No. 1 and No. 2 combination boilers will be conducted by New-Indy in accordance with Condition 5 of the DHEC order to confirm the original H<sub>2</sub>S and TRS emissions estimates based on information from NCASI.

No operational issues or corrective actions have been identified for the evaporator system pending the results of the source testing required by Condition 5 of the DHEC Order.

### **6.2.7 Recovery Furnaces**

TRS emissions from the recovery furnaces are continuously monitored and recorded. The Mill will continue to meet the applicable TRS emissions limits for both recovery furnaces.

No operational issues or corrective actions have been identified for the No. 2 and No. 3 recovery furnaces.

### **6.2.8 Smelt Dissolving Tanks**

New-Indy will conduct source testing of the smelt dissolving tank vent to confirm the original H<sub>2</sub>S and TRS emissions estimates based on information from NCASI.

No operational issues or corrective actions have been identified for the No. 2 and No. 3 smelt dissolving tanks pending the results of the source testing conducted by New-Indy.

### **6.2.9 Precipitator Mix Tanks**

The precipitator mix tanks are vented through the recovery furnaces and would be reflected in the emissions from those sources.

No operational issues or corrective actions have been identified for the precipitator mix tanks.

### **6.2.10 Causticizing Area**

The causticizing area is a high pH process, and no H<sub>2</sub>S emissions are expected. The causticizing area uses fresh water, and no change in TRS emissions is expected.

No operational issues or corrective actions have been identified for the causticizing area.

#### **6.2.11 Lime Kiln**

TRS emissions from the lime kiln are continuously monitored and recorded. The Mill will continue to meet the applicable TRS emissions limits for the lime kiln. No operational issues or corrective actions have been identified for the No. 2 Lime Kiln.

#### **6.2.12 Combination Boilers**

Incineration of the NCG gases is continuously monitored using the flame failure systems on each boiler. The NCG collection systems are also monitored monthly and annually for leaks following the Catawba Mill Leak Detection and Repair (LDAR) program.

Source testing of both the No. 1 and No. 2 combination boilers will be conducted by New-Indy, in accordance with Condition 5 of the DHEC order to confirm the original H<sub>2</sub>S and TRS emissions estimates based on information from NCASI.

#### **6.2.13 Condensate Collection and Treatment System**

Source testing of the foul condensate steam stripper will be conducted by New-Indy in accordance with Condition 5 of the DHEC order to confirm the original H<sub>2</sub>S and TRS emissions estimates based on information from NCASI.

No operational issues or corrective actions have been identified for the foul condensate steam stripper pending the results of the source testing required by Condition 5 of the DHEC Order.

#### **6.2.14 Wastewater Treatment System**

Please see Section 7 for a detailed discussion of the wastewater treatment system operational issues and corrective actions.

#### **6.2.15 Industrial Landfill**

No operational issues or corrective actions have been identified for the landfill.



### **6.2.16 Miscellaneous Sources**

No operational issues or corrective actions have been identified for the miscellaneous sources.

6.3 Professional Engineering Certification

Name: Sheryl Watkins, P.E.

S.C. Registration No. 34347

Company: ALL4 LLC

COA No. 6409



**Table 6-1  
Summary of H<sub>2</sub>S and Other TRS Compound Emissions**

SOURCE OF H <sub>2</sub> S	H <sub>2</sub> S		H <sub>2</sub> S		H <sub>2</sub> S		TRS		TRS		TRS		TRS/H <sub>2</sub> S Control	Compliance Monitoring	Condition 3 Operational Evaluation	Condition 6 Corrective Action Plan
	Bleached Mill (Stripper)		Brown Mill (Hard Pipe)		Brown Mill (Combo)		Bleached Mill (Stripper)		Brown Mill (Hard Pipe)		Brown Mill (Combo)					
	Controlled maximum lb/hr	Percent percent of total	Controlled maximum lb/hr	Percent percent of total	Controlled maximum lb/hr	Percent percent of total	Controlled maximum lb/hr	Percent percent of total	Controlled maximum lb/hr	Percent percent of total	Controlled maximum lb/hr	Percent percent of total				
Kraft Mill NCG System	0.35	6.7%	0.43	8.1%	0.43	8.2%	1.24	1.9%	1.60	2.8%	1.60	3.1%	Incineration in Combination Boilers	Flame Failure System CMS	Source test required by Condition 5 to confirm expected emissions	No corrective actions identified pending source test results
Stripper Off Gases	0.70	13.3%	N/A	N/A	0.37	7.0%	3.48	5.4%	N/A	N/A	1.84	3.5%	Incineration in Combination Boilers	Flame Failure System CMS	Source test required by Condition 5 to confirm expected emissions	No corrective actions identified pending source test results
Recovery Furnace #2	0.16	3.0%	0.16	3.0%	0.16	3.0%	0.27	0.4%	0.27	0.5%	0.27	0.5%	Good combustion practices	TRS CEMS	maintain TRS emissions limit and monitoring	No corrective actions identified
Smelt Dissolving Tank #2	0.28	5.4%	0.28	5.3%	0.28	5.3%	0.37	0.6%	0.37	0.7%	0.37	0.7%	scrubber flow and pressure drop	Stack testing and scrubber CMS	Source test being conducted to confirm current emissions	No corrective actions identified pending source test results
Recovery Furnace #3	0.29	5.5%	0.29	5.4%	0.29	5.5%	0.49	0.8%	0.49	0.9%	0.49	0.9%	Good combustion practices	TRS CEMS	maintain TRS emissions limit and monitoring	No corrective actions identified
Smel Dissolving Tank #3	0.51	9.7%	0.51	9.6%	0.51	9.7%	0.67	1.0%	0.67	1.2%	0.67	1.3%	scrubber flow and pressure drop	Stack testing and scrubber CMS	Source test being conducted to confirm current emissions	No corrective actions identified pending source test results
Lime Kiln #2	0.97	18.4%	0.97	18.2%	0.97	18.3%	0.97	1.5%	0.97	1.7%	0.97	1.9%	Good combustion practices	TRS CEMS	maintain TRS emissions limit and monitoring	No corrective actions identified
Causticizing Area	N/A	N/A	N/A	N/A	N/A	N/A	0.40	0.6%	0.40	0.7%	0.40	N/A	none	none	no change in emissions identified	No corrective actions identified
Precipitator Mix Tanks	N/A	N/A	N/A	N/A	N/A	N/A	0.02	0.0%	0.02	0.0%	0.02	N/A	none	none	no vents to atmosphere, sources vent into recovery furnaces	No corrective actions identified
Paper Machine #2	N/A	N/A	N/A	N/A	N/A	N/A	0.75	1.2%	0.75	1.3%	0.75	N/A	none	none	source not currently in operation	No corrective actions identified
Paper Machine #3	N/A	N/A	N/A	N/A	N/A	N/A	3.13	4.8%	3.13	5.6%	3.13	N/A	none	none	Source test required by Condition 5 to confirm expected emissions	No corrective actions identified pending source test results
Pulp Dryer	N/A	N/A	N/A	N/A	N/A	N/A	0.85	1.3%	0.85	1.5%	0.85	N/A	none	none	Source test required by Condition 5 to confirm expected emissions	No corrective actions identified pending source test results
HD Pulp Storage Tanks	N/A	N/A	N/A	N/A	N/A	N/A	9.20	14.2%	9.20	16.4%	9.20	N/A	none	none	no change in emissions identified	No corrective actions identified
LD Pulp Storage Tanks	N/A	N/A	N/A	N/A	N/A	N/A	3.30	5.1%	3.30	5.9%	3.30	N/A	none	none	no change in emissions identified	No corrective actions identified
Weak Black Liquor Storage Tanks	0.15	2.9%	0.15	2.9%	0.15	2.9%	1.41	2.2%	1.41	2.5%	1.41	2.7%	none	none	no change in emissions identified	No corrective actions identified
Strong Black Liquor Storage Tanks	0.25	4.6%	0.25	4.6%	0.25	4.6%	1.35	2.1%	1.35	2.4%	1.35	2.6%	none	none	no change in emissions identified	No corrective actions identified
White Liquor Storage Tanks	0.02	0.3%	0.02	0.3%	0.02	0.3%	1.77	2.7%	1.77	3.2%	1.77	3.4%	none	none	no change in emissions identified	No corrective actions identified
Green Liquor Storage Tanks	N/A	N/A	N/A	N/A	N/A	N/A	0.20	0.3%	0.20	0.4%	0.20	0.4%	none	none	no change in emissions identified	No corrective actions identified
ASB Zone 1	0.81	15.4%	1.64	30.7%	1.22	23.2%	17.76	27.4%	21.22	37.8%	15.46	29.7%	none	none	See Condition 7	See Condition 7
ASB Zone 2	0.44	8.4%	0.36	6.8%	0.36	6.7%	9.75	15.0%	4.66	8.3%	4.49	8.6%	none	none	See Condition 7	See Condition 7
ASB Zone 3	0.34	6.5%	0.27	5.2%	0.27	5.1%	7.47	11.5%	3.56	6.3%	3.43	6.6%	none	none	See Condition 7	See Condition 7
TOTAL EMISSIONS (stk + fug)	5.27		5.33		5.28		64.85		56.18		51.98					

## **7. CORRECTIVE ACTION PLAN – WASTEWATER TREATMENT IMPROVEMENTS NEW-INDY – CATAWBA, SC**

### **7.1 INTRODUCTION**

Paragraph 7 of the SC DHEC’s May 7, 2021 Order reads:

On or before June 15, 2021, and to the extent not included in Step 6 above, submit to the Department, for review, comment and approval, a corrective action plan (CAP) (developed and stamped by a South Carolina-registered Professional Engineer (PE)) and a schedule of implementation, which addresses operational issues at the Facility wastewater treatment plant that may be causing or contributing to odor and elevated levels of H<sub>2</sub>S. This CAP shall include, but not be limited to, a comprehensive evaluation of the wastewater treatment plant to determine if adequate and appropriate facultative waste treatment is occurring in the aerated stabilization basin (ASB) and the potential for odors resulting from the discharge of foul condensate into the wastewater treatment plant. The CAP shall address the significant fiber and sludge accumulation and foam occurring in the ASB and identify their respective source(s). Additionally, the CAP shall include a study of the microbial concentration in the ASB to determine if there is an adequate microbial population to aid in the reduction of foam on the ASB. The schedule of implementation shall include specific dates or timeframes for initiation and the completion of each action and details as to how each action addresses the odor and wastewater treatment system operational issues noted above. The schedule of implementation of specific corrective action steps proposed under the CAP will be evaluated by the Department and comments provided to New-Indy within five calendar days. New-Indy shall address all comments by the Department and submit a final approvable CAP within five calendar days of Department comment. Upon Department approval, the schedules(s) and corrective actions contained within the CAP shall be incorporated into and become an enforceable part of this Order.

This CAP has been written to meet the requirements of Paragraph 7.

## **7.2 COMPREHENSIVE EVALUATION OF WASTEWATER TREATMENT SYSTEM**

New-Indy retained EBS and TRC to evaluate the wastewater treatment system with regards the following:

- Operational issues that may be causing or contributing to odor and elevated levels of hydrogen sulfide;
- Whether adequate and appropriate waste treatment is occurring in the ASB;
- The potential for odors resulting from the discharge of foul condensate into the treatment system;
- The accumulation of fiber, foam, and sludge accumulation and their sources; and
- A study of the microbial population in the ASB with regards to reducing the fiber/foam layer and providing biological degradation of BOD5.

### **7.2.1 Operational issues that may be causing or contributing to odor and elevated levels of hydrogen sulfide**

H<sub>2</sub>S emissions can originate in a wastewater treatment basin in two ways. The first source of emissions is H<sub>2</sub>S that has been produced upstream of the wastewater treatment system and volatilizes when exposed to mixing or agitation in the aeration basin or holding pond. Minimization of this source of H<sub>2</sub>S is generally accomplished via proper subservice diffusion and adequate oxygenation of the wastewater through proper aeration and mixing. The second source of H<sub>2</sub>S is the formation of H<sub>2</sub>S by sulfate reducing bacteria in unaerated or poorly aerated areas in the ASB or holding pond.

A properly operated aerobic biological treatment system utilizes aeration and bacterial metabolism to convert biodegradable compounds (BOD) in the wastewater into additional bacteria, water, and carbon dioxide, an odorless gas. In the absence of sufficient dissolved oxygen, the bacterial population will shift to a sulfate reducing scenario, where sulfate replaces oxygen as the terminal electron acceptor, with resultant H<sub>2</sub>S formation.

TRC performed site visits to the facility on March 17 and March 19, 2021, to observe the conditions of the wastewater treatment system. EBS performed site visits on May 11, May 25, and June 9, 2021, to observe system conditions and to collect process evaluation samples. Discussions regarding EBS's process control data is provided in Section 7.2.2 below, but in general, the conditions observed indicated a floating layer of fiber/foam on portions of the ASB

and accumulated solids in the EQ Basin. Effluent from the primary clarifier weir appeared typical of effluent from paper mill primary clarifiers.

The predominant issues that have hindered aeration and mixing in the ASB have been the formation of the floating layer of foam and fiber and the accumulation of settled solids. Excess fiber loading into the ASB combined with production liquor losses has led to the formation of a thick, floating layer of fiber and foam covering much of the early aerated zone. The fiber and liquors losses arose during mill conversion and recommissioning. The floating solids layer contributed to the breakdown of multiple aerators in the front end of the system. This loss of aeration capacity led to a reduction in biological treatment capacity and resulted in reduced aerobic and even anaerobic conditions. Sulfate reducing bacteria when present under anaerobic conditions metabolize BOD by utilizing sulfate as a terminal electron acceptor when there is no dissolved oxygen present, thus producing H<sub>2</sub>S as a byproduct. The floating solids also represent biodegradable material that dissolve over time, adding additional oxygen demand to the system.

The accumulated solids in the ASB have reduced the hydraulic residence time in the basin for treatment and impacted the flow path through the basin. Solids accumulation occurs from solids loading in the influent as well as settling of biomass generated as part of normal biological treatment. The influent loading comes from solids that may not have been removed during the primary clarification process or primary solids that have become re-entrained in wastewater due to the primary clarifier underflow in the EQ Basin.

The reduced treatment efficiency and poorly aerated conditions caused by the floating fiber/foam layer and accumulated solids and H<sub>2</sub>S production contributed to elevated concentrations of H<sub>2</sub>S in the effluent from the ASB to No. 1 Holding Pond. No. 1 Holding Pond retains wastewater prior to undergoing post-treatment aeration in the post-aeration basin. In the post-aeration basin, large surface aerator/mixers aerate the wastewater in a rectangular, concrete basin. This aeration has the potential of releasing hydrogen sulfide that may be in the wastewater. On June 9, 2021, the facility installed a flexible cover, blower and carbon filtration system to capture emissions from the post-aeration basin and treat the off gasses through a carbon filtration system to reduce the H<sub>2</sub>S concentration.

The increase of foul condensate loading to the ASB through the hard pipe option under the Title V permit and NSPS Subpart S increased the load of both BOD5 and sulfur compounds. The loading of the anticipated foul condensate and anticipated wastewater from the converted, unbleached manufacturing operations into the ASB was modeled in 2019 utilizing NCASI's Simulated Aerated Stabilization Basin Model (Version 4.2). The ASB parameters in the model were set up using the 2015 solids survey results based on the facility's assumption that additional sludge accumulation since 2015 was approximately equal to the amount of sludge that was removed as part of maintenance dredging since that time. The 2019 modeling indicated that the ASB could sufficiently treat the foul condensate and enable the wastewater treatment system and comply with current (and anticipated) NPDES permit requirements. After the conversion and restarting of the mill, however, the thick layer of foam/fiber formed on the basin reducing the aeration capacity of the basin. This reduced aeration capacity and sludge accumulation that has reduced mixing and disruption of the flow path through the basin have hindered the basin's ability to perform as modeled.

The two main operational issues in the ASB that pose the potential of causing or contributing to elevated levels of hydrogen sulfide have been the formation of the floating fiber/foam layer and the accumulation of settled solids. Addressing the floating fiber/foam layer and regaining a portion of treatment volume by removing sufficient solids in strategic areas of the ASB are recommended and included as corrective actions in Section 7.3.

### **7.2.2 Adequacy and appropriateness of waste treatment that is occurring in the Aerated Stabilization Basin**

New-Indy's ASB is of typical design for an integrated pulp and paper mill. An ASB operates by both providing sufficient residence time for biological treatment of organic wastes as well as providing for the settling and digestion of biomass essential to the operation of the basin. An ASB accomplishes biological treatment and sludge digestion through two layers. The upper layer is typically well mixed and aerated with the use of floating aerators. Soluble BOD5 serves as a food source to microscopic biota in this upper layer thus reducing the BOD5 concentration in the wastewater. As the BOD5 is consumed, additional biomass is produced to continue the treatment process. As biomass accumulates, some of the solids settle to the basin bottom and begin to undergo digestion in anoxic conditions, which are by design out of reach of the aeration and mixing

energy from the surface aerators. As the biomass degrades, it releases some BOD5 and nutrients. The released BOD5 gets treated in the upper layer, and the released nutrients get reused in the process to support continued biomass growth. This release of nutrients and BOD5 from the degradation of biomass at the bottom is referred to as “benthic feedback” and is an important step in the ASB treatment process. Not all the biomass that settles to the basin bottom digests, and this accumulated sludge can begin reducing the working volume of the basin thus reducing the residence time for treatment.

Unlike an activated sludge system that concentrates biomass in the mixed liquor through the return of a portion of settled secondary sludge, an ASB operates with a much lower density of biomass and achieves high removal efficiencies, not through high concentrations of mixed liquor biomass but instead through extended residence times. The large volumes of typical ASBs that provide the high residence time for treatment also makes ASBs less susceptible to slug discharges of high organic strength, pH swings, and hydraulic loading spikes that can plague activated sludge systems. In addition, by design, ASBs generate less sludge for disposal than activated sludge systems and require less energy to operate. ASBs also require less nutrient loading because of the inherent “benthic feedback” nutrient recycle process.

New-Indy has routinely collected samples from the ASB influent, effluent and within the ASB for process control parameters such as BOD5, TSS, pH and temperature. As part of preparations for full scale unbleached operations and foul condensate hard pipe loading, New-Indy revised the ASB sampling regimen to include methanol sampling as well as sampling of the foul condensate stream in January 2021.

In terms of BOD loading to the ASB, the conversion from bleached paper to unbleached containerboard included two considerations for determining the ASB’s ability to support the converted mill operations. Although the planned hard pipe solution would result in a higher loading of BOD to the ASB from the chemical recovery operations, the overall BOD loading to the ASB would not change due to correspondingly reduced BOD loading from the paper making operation (elimination of starch, coatings and sub-sized fibrous “fines” from the paper machine operation). By design, this validated the decision to implement the hard pipe solution for methanol



destruction, as the ASB would continue to be more than adequate to treat the planned post-construction BOD loading.

The mill experienced a rough operational startup, which was more difficult than anticipated. Additional factors that complicated the wastewater treatment plant startup conditions were the time of year (cold weather) and an anomalous influx of solids from the EQ basin (because the primary clarifier was out of service). The normal flow of effluent from the primary clarifier is to route the underflow sludge to the EQ basin for solids settling with the clarifier overflow going directly to the ASB inlet. With the primary clarifier out of service for rake repairs, all mill effluent was routed through the EQ basin, which resulted in a hydraulic washing of solids from that basin into the ASB. Fiber losses from the mill's operational startup compounded the buildup of solids in the ASB. The fibrous sludge floated and matted on the ASB surface, which caused surface aerators to shut down. The floating solids mat then built to the point where access to the aerators was prohibited, and the aerators could not be returned to service as would otherwise normally take place. This situation was further exacerbated by extremely wet weather in January through March 2021, which resulted in restricted access to the No. 4 sludge holding pond, thus preventing solids removal from the ASB surface until March 2021. Therefore, the ASB's reduced aeration efficiency was a primary factor in creating treatment inefficiencies through the ASB.

New-Indy retained EBS to evaluate the treatment system in May 2021. EBS collected samples from the ASB inlet, effluent, ASB midpoint and from the No. 1 Holding Pond and analyzed for pH, temperature, dissolved oxygen, Oxidation-Reduction Potential (ORP), ammonia, ortho-phosphate, Sulfide, dissolved oxygen uptake rate, TSS, Volatile Suspended Solids (VSS) and Chemical Oxygen Demand (COD). These samples were collected on May 11, May 25 and June 9, 2021. Continued sampling is conducted weekly going forward. EBS also evaluated the microbiology of samples from the ASB midpoint and ASB effluent during each sampling event, and the details of the microbiology evaluation are discussed more in Section 7.2.5. The complete EBS reports are provided in Appendix D but are summarized below for COD removal along with estimates of loading calculated by TRC based on information provided by the facility and EBS.

- May 11, 2021 EBS Evaluation:

- Wastewater flow into the ASB (minus foul condensate) was recorded at 27.4 MGD, the measured soluble COD in that influent (minus foul condensate) was 873 mg/L, giving a soluble COD loading in the ASB influent (minus foul condensate) of approximately 200,000 pounds per day (lbs./day).
- The foul condensate hard pipe flow that day was approximately 0.158 MGD. The COD of the foul condensate was not measured that day, but the average from the four measurements collected that month was approximately 3,850 mg/L for total COD, giving a COD loading of approximately 5,100 lbs./day from the foul condensate.
- The total influent COD loading was approximately 205,100 lbs./day.
- The ASB effluent soluble COD concentration that day was 510 mg/L, giving an approximate mass loading from the ASB of 117,200 lbs./day, or a removal efficiency of approximately 43%.
- May 25, 2021 EBS Evaluation:
  - Wastewater flow into the ASB (minus foul condensate) was recorded at 30 MGD, the measured soluble COD in that influent (minus foul condensate) was 1303 mg/L, giving a soluble COD loading in the ASB influent (minus foul condensate) of approximately 326,000 pounds per day (lbs./day).
  - The foul condensate hard pipe flow that day was approximately 0.307 MGD. The COD of the foul condensate that day was measured to be 4,300 mg/L for total COD, giving a COD loading of approximately 11,000 lbs./day from the foul condensate.
  - The total influent COD loading was approximately 337,000 lbs./day.
  - The ASB effluent soluble COD concentration that day was 231 mg/L, giving an approximate mass loading from the ASB of 58,388 lbs./day, or a removal efficiency of approximately 83%.
- June 9, 2021 EBS Evaluation:
  - Wastewater flow into the ASB (minus foul condensate) was recorded at 29.4 MGD, the measured soluble COD in that influent (minus foul condensate) was 1,059 mg/L, giving a soluble COD loading in the ASB influent (minus foul condensate) of approximately 260,000 pounds per day (lbs./day).
  - The foul condensate hard pipe flow that day was approximately 0.307 MGD. A total COD value for the foul condensate was not available for that day as of the

writing of this CAP; therefore, the average of the previous three measurements was used (4,733 mg/L), giving a COD loading of approximately 16,600 lbs./day from the foul condensate.

- The total influent COD loading was approximately 276,000 lbs./day.
- The ASB effluent soluble COD concentration that day was 376 mg/L, giving an approximate mass loading from the ASB of 93,500 lbs./day, or a removal efficiency of approximately 66%.

Historically, the ASB has generally removed greater than 85% of the influent BOD. The ASB is capable of treating mill wastewater as demonstrated by historical sampling and modeling. A properly operated and maintained primary clarifier, ASB and treated effluent retaining capabilities along with management and disposal of primary clarifier solids is an appropriate treatment regimen and can provide adequate treatment for this type of wastewater to enable compliance with the NPDES permit. Continued efforts to address the floating fiber/foam layer, strategic maintenance dredging, and continuing the revised monitoring of ASB process control parameters is recommended and included as corrective actions in Section 7.3.

### **7.2.3 The potential for odors resulting from the discharge of foul condensate into the treatment system**

The foul condensate represent an organic and sulfide load to the ASB. In a system facing aeration challenges due to the floating fiber/foam layer and lost volume due to solids accumulation, this additional organic loading can exacerbate the aeration difficulties leading to poorly aerobic and even anaerobic conditions. These conditions can cause the bacteria population to shift to sulfate reducing bacteria where sulfate replaces oxygen as the terminal electron acceptor resulting in H<sub>2</sub>S formation. The additional sulfide from the foul condensate provides an additional sulfur source to the system. Improving conditions in the ASB, including addressing the floating fiber/foam layer and regaining treatment volume through removal of solids will improve the ability of the ASB to treat foul condensate in an aerobic environment reducing the biological factors that contribute to the formation of H<sub>2</sub>S.

The 2019 ASB modeling of the loading from the unbleached mill operations and the full foul condensate loading indicated the ASB as modeled could meet the oxygen demand requirements of BOD<sub>5</sub> in maintaining aerobic conditions in the upper pond layer as designed. H<sub>2</sub>S emissions was

estimated using NCASI's Wastewater Hydrogen Sulfide Emissions Simulator (H2SSIM, version 1.3) in January 2020. As with the 2019 ASB modeling, the ASB inputs were based on anticipated wastewater and H<sub>2</sub>S loading and that the accumulated solids conditions in January 2020 were approximately the same as those observed in 2015 based on the facility's assumption that additional accumulation was approximately equal to the amount of solids removed through maintenance dredging conducted since 2015. That modeling indicated that based on the assumptions and inputs used, the additional emissions of hydrogen sulfide with the addition of the full condensate stream would be less than 1 ton per year.

With the understanding that ASB conditions have changed since early 2020 when the H<sub>2</sub>S modeling was performed and that there is actual data for the foul condensate and process wastewater characteristics from unbleached operations, additional ASB treatment and H<sub>2</sub>S emissions modeling is recommended and included as part of the corrective actions in Section 7.3.

#### **7.2.4 The accumulation of fiber, foam and sludge and their sources**

As discussed above, the formation of the floating layer of fiber and foam has contributed to the reduction in aeration and mixing capacity in the ASB, while accumulated sludge has impacted the flow path of wastewater through the basin and reduced the effectiveness of mixing and aeration in the basin. The floating layer is a combination of excessive fiber in the wastewater and foaming caused by production liquors, fatty acid soaps, and cellulose breakdown products. Production upsets during recommissioning contributed to the high losses of fiber and production material the facility's process sewer system. Addressing fiber and process liquor losses in the mill is recommended and included as corrective actions in Section 7.3.

The accumulation of sludge in the ASB is a result of elevated primary solids loading in the influent to the ASB and biomass generation from BOD<sub>5</sub> treatment. The source of the elevated solids in the influent flow is from solids being entrained in effluent from the primary solids EQ Basin. Sludge from the primary clarifier is pumped to the EQ Basin to thicken and homogenize before being removed and placed in the No. 4 Sludge Pond. If the solids aren't removed frequently enough, suspended solids can be entrained in the supernatant that leaves the EQ Basin into the ASB inlet ditch ultimately settling out in the ASB. While the use of the EQ Basin served as an urgently needed means of addressing inadequate primary sludge dewatering, ultimately managing

primary solids in an alternative manner is recommended and is included as corrective action in Section 7.3.

Biomass generated in the ASB during the BOD5 treatment process settles to the basin bottom and undergoes digestion. Digestion alone does not eliminate the solids, as some of it is inert, so maintenance dredging must be performed to keep accumulation in check. If maintenance dredging does not keep up with the accumulation of solids in the basin, the settled solids will begin reducing the working volume of the basin available for treatment. Increasing the maintenance dredging program in the ASB, and even dredging to recover lost volume to regain sufficient treatment volume, is recommended and is included as corrective action in Section 7.3.

#### **7.2.5 A study of the microbial population in the ASB with regards to reducing the fiber/foam layer and providing biological degradation of BOD5**

As part of their evaluations on May 11, May 25, and June 9, 2021, EBS performed microscopic examinations. Their reports can be found in Appendix D but are summarized with regards to the micro exams below.

- May 11, 2021 EBS Evaluation: The micro exam showed a moderate to high abundance of dispersed bacteria in the ASB Midpoint and ASB Effluent samples, as well as a moderate abundance of pin floc in both samples. No higher life forms (protozoa/metazoa) were observed at the ASB Midpoint, but the ASB Effluent showed several flagellates and a few free-swimming ciliates. Ciliates are generally considered indicators of aerobic, non-toxic conditions in ASB treatment systems. A low to moderate abundance of fiber was observed at the ASB midpoint sample, and a moderate abundance of grit and debris were observed in both samples.
- May 25, 2021 EBS Evaluation: The micro exam showed higher life forms (protozoa) in both the ASB midpoint and ASB Effluent. Two stalked ciliates were observed at the ASB Midpoint: these are sensitive microorganisms that generally exist in non-toxic, aerobic environments. Two free swimming ciliates were observed at the ASB Outfall as well. The ASB midpoint sample showed a high abundance of grit and debris, as well as pin floc and a few small compact pieces of floc. There was no floc larger than pin floc observed at the ASB Outfall, and the abundance of grit/debris decreased in this sample. Dispersed bacteria abundance was high in the midpoint (2.5 out of 3) and moderate to high in the ASB Effluent (2 out of 3).

- June 9, 2021 EBS Evaluation: The micro exam showed stalked ciliates and free-swimming ciliates at the ASB Mid and ASB Out sample points. Stalked ciliates are generally considered indicators of good biomass health, as they are sensitive microorganisms that don't survive in toxic or anaerobic conditions. There was abundant grit and debris observed in the ASB Mid sample, with the abundance decreasing in the ASB Out sample. This corresponds with the lower percent VSS (volatile suspended solids) observed in the ASB Mid sample, as there is a higher fraction of inorganic grit/debris in this part of the ASB.

As discussed, ASBs do not have the highly concentrated population of microbial life in the mixed liquor that activated sludge systems require for treatment.

Continued evaluations of the ASB mixed liquor microbiology is recommended along with continuous, in situ biomonitoring, and are included to support corrective actions in Section 7.3.

### **7.3 CORRECTIVE ACTIONS AND TIMELINE**

A properly operated aerobic biological treatment system utilizes aeration and bacterial metabolism to convert biodegradable compounds (BOD) in the wastewater into additional bacteria, water, and carbon dioxide, an odorless gas. In the absence of sufficient dissolved oxygen, the bacterial population will shift to a sulfate reducing scenario, where sulfate replaces oxygen as the terminal electron acceptor resulting in H<sub>2</sub>S formation. The floating layer of fiber and foam contributed to the reduction in aeration and mixing capacity in the ASB. The accumulation of settled solids in the ASB contributed to the reduction in treatment residence time, reduced mixing efficiency, and altered the flow path of wastewater undergoing treatment through the ASB. The following corrective actions have been developed to address these operational issues.

This corrective action plan employs the concept of the Eight Growth Pressures necessary for optimum aerobic metabolism as outlined in "Aerated Stabilization Basins in the Pulp and Paper Industry" by Paul Klopping and Michael Foster published in 2003. Each of the eight growth pressures (BOD Loading, pH, Hydraulic Retention Time, Dissolved Oxygen, Nutrients, Temperature, Toxicity, and Biomass Viability) play a role in the health of a system with BOD Loading, Dissolved Oxygen, pH, Temperature, and Hydraulic Retention Time being most impactful in terms of H<sub>2</sub>S formation and emission. The intent of this document is to provide a

corrective action plan to improve the health of the wastewater treatment system and mitigate H<sub>2</sub>S formation.

### **Item 1: Removal of Floating Solids in the Aerated Stabilization Basin (ASB)**

#### *Basic Description:*

- Remove floating solids in the ASB. Floating solids removal will allow access to out-of-commission aerators.

#### *Technical Rationale:*

- Excess fiber loading into the ASB has led to floating solids covering much of the early aerated zone. The floating solids have contributed to the breakdown of multiple aerators in the front end of the system. Removal of these solids will be necessary to repair the aerators, which will lead to higher BOD removal efficiency, more aerobic conditions in the wastewater treatment system and reduce the potential for H<sub>2</sub>S formation. The floating solids also represent biodegradable material that dissolve over time, adding additional oxygen demand to the system.

#### *Timeline:*

- Long arm excavators are currently removing solids that can be reached from shore. In addition, two other contracting firms will begin work over the next weeks to remove the floating solids from barge and vessel-based equipment.
- Address fiber and liquor losses in production that may have contributed to the formation of the floating fiber/foam layer.

### **Item 2: Removal of Settled Solids in the Aerated Stabilization Basin (ASB)**

#### *Basic Description:*

- Remove sufficient settled solids in the ASB to meet treatment and sludge management needs. Dredging settled sludge will improve the hydraulic retention time of the ASB, improve mixing, and the flow path through the ASB. In addition, a sludge accumulation rate needs to be estimated to plan maintenance dredging rates to stay ahead of accumulation.

#### *Technical Rationale:*

- Settled solids removal will also be necessary to provide additional retention time for BOD removal. Additional volume in the ASB will be created by dredging solids from the bottom of the basin.

*Timeline:*

- Long arm excavators began removing solids that can be reached from shore in March 2021 and will continue until removal is completed.
- Sludge maintenance dredging is ongoing. The facility is currently in the process of identifying a dredging contractor(s) that can dredge at a faster rate.
- EBS began a lithium tracer study on June 8, 2021 to determine the hydraulic retention time of the ASB. In addition, lithium profile samples were collected throughout the ASB five and twenty-four hours after the lithium was introduced to determine the current flow patterns.
  - Preliminary results from the lithium profile sampling will be available by June 21, 2021.
- Perform ASB modeling using up-to-date information about the ASB to guide settled solids removal actions.

**Item 3: Primary Clarifier Sludge Handling Improvements**

*Basic Description:*

- While solids removal from the ASB is critically important, it will be subsequently important to ensure solids loading is minimized in the future. Improving primary clarification and preventing dumps of process solids that bypass or overwhelm the primary clarifier will decrease the amount of fiber and other solids that are entering the ASB from the mill. In the short term, this can be mitigated by dredging the EQ basin that the underflow of the secondary clarifier feeds into. In the long term, the underflow of the primary clarifier will be pressed and removed from the wastewater treatment system. Reducing non-wastewater loads of solids to the primary clarifier, such as boiler ash, lime mud, grits and slaker dregs will also reduce the solids loading.

*Technical Rationale:*

- The underflow of the primary clarifier is currently feeding into an EQ basin that is largely full of solids. The lack of settling volume in the EQ [basin?] is leading to elevated TSS entering the ASB. These solids will settle in the ASB and reduce the hydraulic retention time. Especially during/after dredging, this will be important as the volume gained from dredging will be quickly cancelled out if influent solids aren't reduced.
  - Keeping primary sludge removed in the clarifier from becoming remixed with wastewater is important.
  - Mechanical dewatering through the use of a belt press is essential to improving the solids removal.
  - Returning the EQ Basin to use for attenuating hydraulic and concentration swings in the primary clarifier effluent will provide a more evenly distributed loading to the ASB.



#### **Item 4: Existing Aeration Repair**

##### *Basic Description:*

- Repair out-of-commission splash aerators in the early zones of the ASB.

##### *Technical Rationale:*

- Each hp of aeration in the ASB theoretically removes 25-35 lbs. of BOD per day. Using the midpoint of 30 lbs. of BOD removal per hp, each 75 hp splash aerator that is repaired will remove approximately 2,250 lbs. of additional BOD per day. Sulfate reducing bacteria when present under anaerobic conditions metabolize BOD by utilizing sulfate as a terminal electron acceptor when there is no dissolved oxygen present and produce H<sub>2</sub>S as a byproduct. Repairing aerators will decrease the oxygen demand in the ASB and No. 1 Holding Pond, promoting the growth of aerobic bacteria and reduce the conditions favorable to sulfate-reducing bacteria.
- In addition to supplying oxygen, aeration will strip any sulfide present under the right pH conditions, so it is important to reduce any potential sulfide formation from upstream sources prior to entering the ASB.

##### *Timeline:*

- Aerator repairs are ongoing.
- Gradually turn on the aerators as they become operational.
- On April 19, 2021, New-Indy began adding calcium nitrate in the ASB to supplement oxygen as an electronic acceptor and reduce the formation of hydrogen sulfide.
- On June 9, 2021, New-Indy began adding hydrogen peroxide and supplemental oxygen to the ASB inlet to provide supplement dissolved oxygen until aeration conditions improve in the ASB.

#### **Item 5: Add Aeration to No. 1 Holding Pond**

##### *Basic Description:*

- Add two 75 hp splash aerators to the front end of the No. 1 Holding Pond.

##### *Technical Rationale:*

- Adding additional aerators to the No. 1 Holding Pond will provide additional D.O. that will reduce the potential for H<sub>2</sub>S formation from sulfate reducing bacteria. These aerators will be installed in the early zones of the No. 1 Holding Pond to prevent stirring up solids before the outfall. The permanent need for these will be evaluated as treatment efficiencies improve in the ASB.

##### *Timeline:*

- Two 75 hp splash aerators were installed June 9, 2021, near the inlet of No. 1 Holding Pond.

### **Item 6: ASB Biomass Monitoring: EBS Advanced Microscopic and Chemical Analysis**

#### **(Weekly)**

##### *Basic Description:*

- ASB Influent, ASB Midpoint, and ASB Outfall samples will be sent to EBS weekly for an advanced chemical and microbiological analysis that evaluates biomass health and related parameters.

##### *Technical Rationale:*

- These analyses will provide weekly trended data on parameters related to wastewater performance. This analysis will evaluate biomass health, biomass abundance, soluble BOD removal efficiency, and other parameters related to wastewater treatment performance.
  - The analysis will include:
    - *Microscopic Examination* – Protozoa/Metazoa abundance, floc formation, and dispersed bacteria abundance
    - *Flow Cytometry* – Analysis of percent live/dead bacterial cells in the sample
    - *Culturable Cell Counts*
    - *Total Cell Counts*
    - *Live Cell Counts*
    - *Basic chemical analysis*
      - *Soluble BOD*
      - *NH<sub>3</sub>-N and PO<sub>4</sub><sup>3-</sup>-P Concentrations*
      - *DOUR*
      - *TSS/VSS*

##### *Timeline:*

- Weekly sample shipment will begin on June 16.

### **Item 7: ASB Biomass Monitoring: Sentry Probe Installation**

##### *Basic Description:*

- EBS will install an in-line probe which will monitor biomass activity at the ASB Midpoint sample. *SENTRY: Bio-Electrode Technology* monitors biological activity by measuring electron transfer as the resident ASB biomass metabolizes soluble organic compounds. This data can be viewed 24/7 on the online SENTRY data page.

##### *Technical Rationale:*

- The SENTRY unit consists of a metal screen that allows biological material to grow on the screen. As the biology consumes organic material, the electrons that normally would be accepted by oxygen/nitrate/sulfate go into an anode and are measured by the unit. This electron transfer will fluctuate up and down based on how much soluble BOD is present at this point in the system. The electron transfer is measured as MET (microbial electron transfer) and is plotted out on the SENTRY data page. This data can also help alert us to potential inhibitory/toxic compounds moving through the system, as that will decrease oxygen uptake/electron transfer.

*Timeline:*

- EBS will install the Sentry Probe by mid-July 2021.

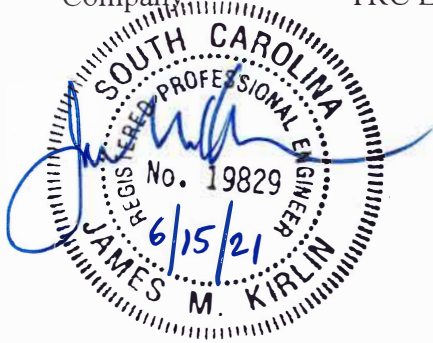
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**7.4 WASTEWATER PROFESSIONAL ENGINEERING CERTIFICATION**

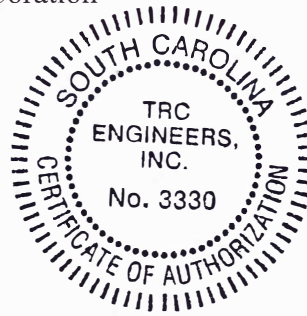
Name: James M. Kirlin, P.E.

S.C. Registration No. 19,829

Company: TRC Environmental Corporation



(Seal)



(TRC COA Seal)

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# APPENDIX A - LEAK DETECTION AND REPAIR (LDAR) INSPECTION REPORTS

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Inspection Date: January 26-27, 2021



New Indy Containerboard - Catawba Mill  
5300 Cureton Ferry Rd.  
Catawba, SC 29704

### 2021 Monthly LDAR Inspection Summary Report

**Table 1: Visual Inspection Summary Table**

Equipment Number	Date	Description of Leak or Visual Defect
MV-1137	1/26/2021	Manual Valve MV-1137 is located on foul condensate line at outlet of HVLC Foul Condensate Tank No. 3 and prior to the pump. The drain valve is open and dripping from spout.
NA	1/27/2021	The 1A Screw Press Dilution Conveyor is puffing from top hatch door.
NA	1/27/2021	The 1B Screw Press Dilution Conveyor is puffing from top hatch door.
NA	1/27/2021	The 1A Brown Stock Washer is puffing from three open hatch doors.
NA	1/27/2021	The 1B Brown Stock Washer is puffing from four open hatch doors.
NA	1/27/2021	The 2A Brown Stock Washer is puffing from four open hatch doors.
NA	1/27/2021	The 2B Brown Stock Washer is puffing from four open hatch doors.
NA	1/27/2021	The 3A Brown Stock Washer is puffing from one open hatch door.
NA	1/27/2021	The 3B Brown Stock Washer is puffing from four open hatch doors
<b>First Attempt to Repair must be completed by:</b>		5 Days from Inspection Date Not Applicable if no leaks were found.
<b>Repairs must be completed by:</b>		15 Days from Inspection Date Not Applicable if no leaks were found.

This report provides a summary of leaks and visual defects found during the visual inspection of the closed-vent and condensate-collection systems and complies with the record keeping requirements of 63.454(b)(1-2, 4-5).

The facility must initiate repairs to any defects within five (5) calendar days from this inspection and the defects must be repaired within fifteen (15) calendar days of the inspection. If the leak or defect requires the system to be shutdown in order to make repairs, or more emissions would occur from attempting the repair than delaying the repair, then the repairs may be delayed until the next process unit shutdown. A report must be supplied with the repair date and associated information, or the reason for the delay if the repairs are not completed within the 15-day period. These response requirements are specific to 40 CFR 63, specifically 63.453(k)(6), 63.453(l)(3), and 63.964(b)(1-2). Documentation of all repair attempts made and any leaks/defects requiring a process unit shutdown must be completed according to 63.454(b)(6-11).

I certify that the results of the visual inspection are accurate and complete to the best of my knowledge.

Inspector Name: Josh Howard

Signature: Josh Howard



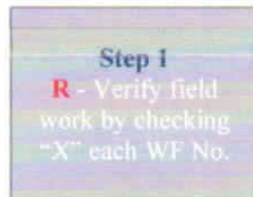
## Inspection QA/QC Procedure

E360 Project Number?	New Indy - Catawba
Task Number (if applicable)?	January 2021 Monthly LOAR

### Purpose of Form

To verify field work meets each critical element.

### Visual Work Flow (WF)

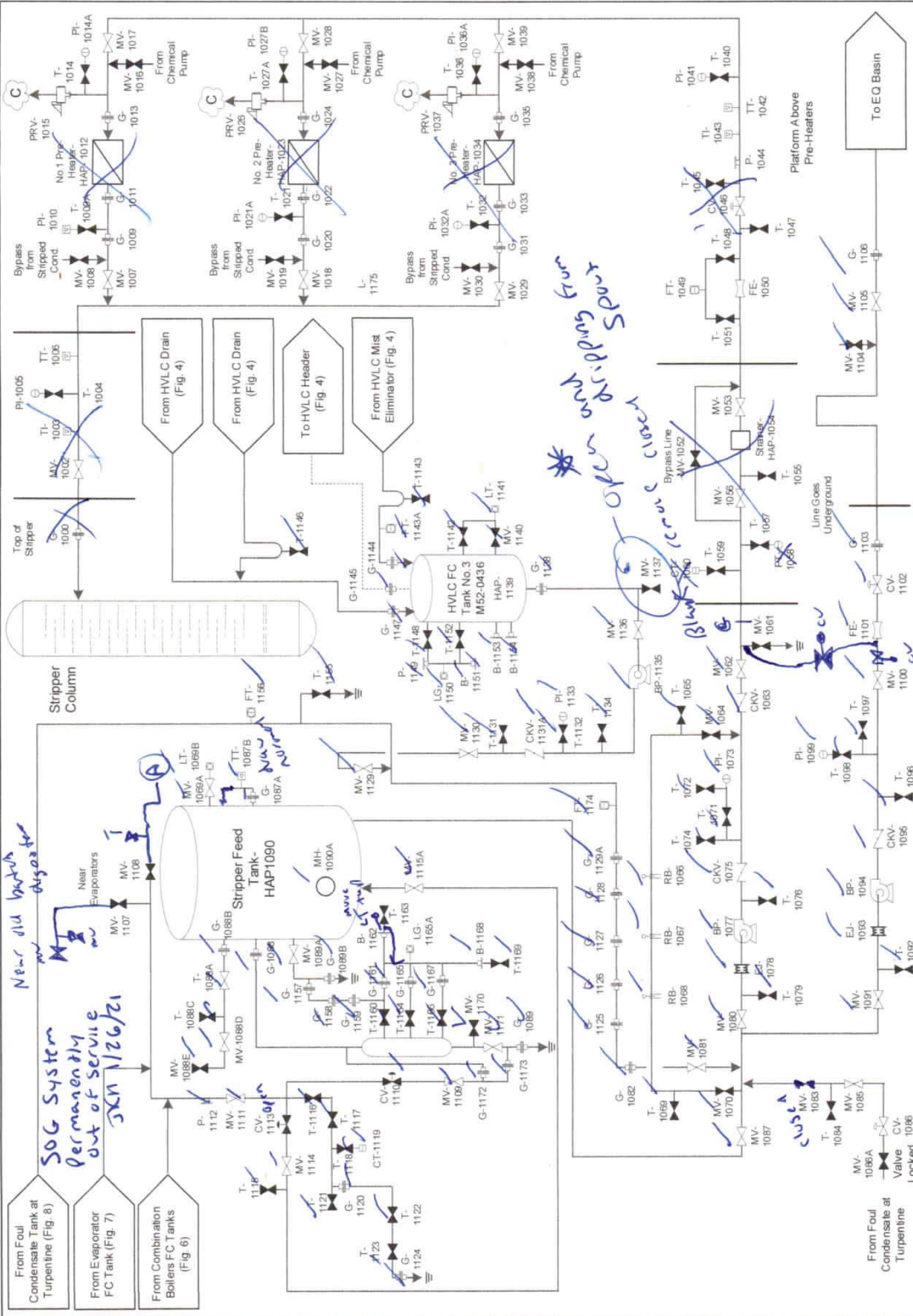


### Verification of Critical Elements

WF No.	Requirement	Yes?
	Work-flow step	1
	Verifier of critical elements for work-flow step	R
1	Was a bump test performed on the personal H <sub>2</sub> S monitor?	✓
2	Have the most recent versions of the inspection forms been used?	✓
3	Were all inspection points identified correctly and inspected correctly?	✓
4	Did the operator/ contact verify to our inspector that all equipment was operating under normal operating conditions?	✓
5	Were any deficiencies identified in person to the client?	✓
6	Were all inspection questions answered with either a Yes, No, or NA?	NA
7	Were inspections performed during the required regulatory time frame?	✓

### Approvals

Role	WF Step	Name	Approval (insert date)
Responsible Person (R)	1	Josh Howard	1/27/21



Near old tanks  
 SOG System Permanently out of service  
 New 1/26/21

Blank  
 Open  
 Remove check valve  
 multiplying from

Rev. Date  
 July 2020  
 Figure 1

New-Indy - Catawba Mill  
 LDAR Inspection and Testing Diagrams  
 Stripper System Foul Condensate

ENVIRONMENTAL 360

To Another Page and Indicated Equipment  
 From Another Page and Indicated Equipment  
 Vent Gases  
 Condensates  
 Liquor/Stock Lines  
 Process Lines



1/26/21

Stripper System Foul Condensate  
Completed Date/Time:

Number	Type	Equip. Number	Pressure (psi)	Background	VOC Reading	In Component Free of Leaks or Defects?	Comments
1000	G						
1002	MV	51-MV-0580					
1003	TI	TI-032B					
1004	T						
1005	PI	PI-031B					
1006	TI						
1007	MV	51-MV-0550					
1008	MV	51-MV-0541					
1009	G						
1009A	PI						
1010	G						
1011	HAP						
1012							
1013	T						
1014	T						
1014A	PI						
1015	PRV	PSV-034A					
1016	MV	51-MV-0554					
1017	MV	51-MV-0563					
1018	MV	51-MV-0567					
1019	MV	51-MV-0549					
1020	G						
1021	T						
1021A	PI						
1022	G						
1023	HAP						
1024	G						
1026	PRV	PSV-034C					
1027	MV	51-MV-0555					
1027A	T						
1027B	PI						
1028	MV	51-MV-0564					
1029	MV						
1030	MV	51-MV-0548					
1031	G						
1032	T						
1032A	PI						
1033	G						
1034	HAP						
1035	G						
1036	T						
1036A	PI						
1037	PRV	PSV-034E					
1038	MV	51-MV-0556					
1039	MV	51-MV-0565					
1040	T						
1041	PI	PI-031D					
1042	TI						
1043	TI						
1044	P						
1045	T						
1046	CV	51-FCV-001					
1047	T	51-MV-0562					
1048	PI						
1049	PI						
1050	PI	51-PI-001					
1051	T						
1052	MV	51-MV-0560					
1053	MV	51-MV-0561					
1054	HAP						
1055	T						
1056	MV	51-MV-0578					
1057	T						
1058	PI						
1059	T	51-AT-007					
1060	CT						
1061	MV	24-MV-0361					
1062	MV	24-MV-0359					
1063	CKV						
1064	MV	24-MV-0445					
1065	T						
1066	RB						
1067	RB						
1068	RB						
1069	T						
1069A	MV						
1069B	LT	51-LT-265					
1070	MV	24-MV-445					
1071	T						
1072	T						
1073	PI						
1074	T						
1075	CKV						
1076	T						
1077	BP						
1078	EJ						
1079	T						
1080	MV	24-MV-363					
1081	G						
1082	G						
1083	MV	V704F					
1084	T						
1085	MV						
1086	CV	51-HV-269					
1086A	MV						
1087	MV	24-MV-362					
1087A	G						

OPEN WITH

YES

REMOVED

REMOVED

Y

Y

Y

Y

Y

Y

Y

Y

Y

Y

Y

Y

Y

Y

Y

Y

Y

51-TT-266

24-MV-0352

24-MV-360

51-FCV-267

VBB4F

M52-0435

TT

1088

1088A

1088B

1088C

1088D

1088E

1089A

1089B

1090

1088

1088A

1088B

1088C

1088D

1088E

1089A

1089B

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1120

1121

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1124

1125

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1131A

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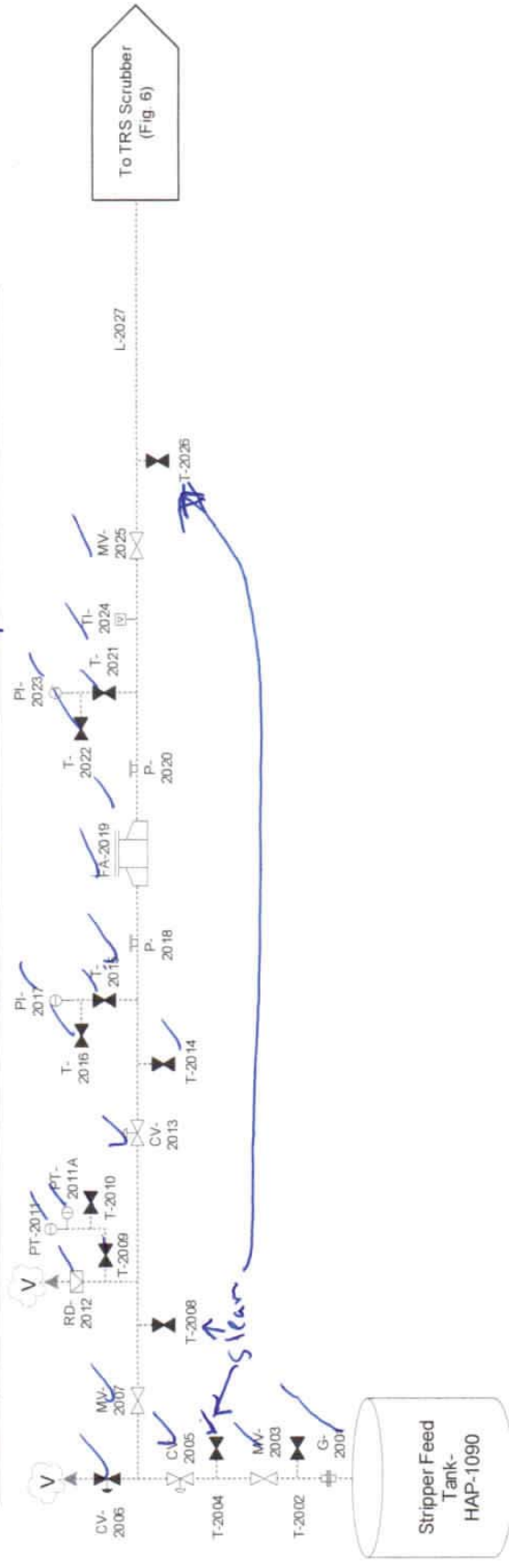
1225

1

Stripper Feed Tank

Completed Date/Time: 1/26/21

Number	Type	Equip. Number	Pressure (+/-)	Background	VOC Reading	Is Component Free of Leaks or Defects?	Comments
2001	G					✓	
2002	T					✓	
2003	MV					✓	
2004	T					✓	
2005	CV	51-PCV-264				✓	
2006	CV	51-HV-262				✓	
2007	MV	51-MV-0672				✓	
2008	T					✓	
2009	T					✓	
2010	T					✓	
2011	PT	51-PSH-261				✓	
2011A	PT					✓	
2012	RD					✓	
2013	CV	51-HV-260				✓	
2014	T	51-MV-0675				✓	
2015	T					✓	
2016	T					✓	
2017	PI					✓	
2018	P					✓	
2019	FA	M51-0546				✓	
2020	P					✓	
2021	T					✓	
2022	T					✓	
2023	PI	51-PI-268B				✓	
2024	TI	O1-TI-274				✓	
2025	MV	51-MV-0673				✓	
2026	T	24-MV-0353				✓	
2027	L					✓	



\* Indicates car seal present

- Vent Gases
- Condensates
- Liquor/Stock Lines
- Process Lines
- To Another Page and Indicated Equipment
- From Another Page and Indicated Equipment



New-Indy – Catawba Mill  
LDAR Inspection and Testing Diagrams  
Stripper Feed Tank

Rev. Date  
July 2020

Figure 2

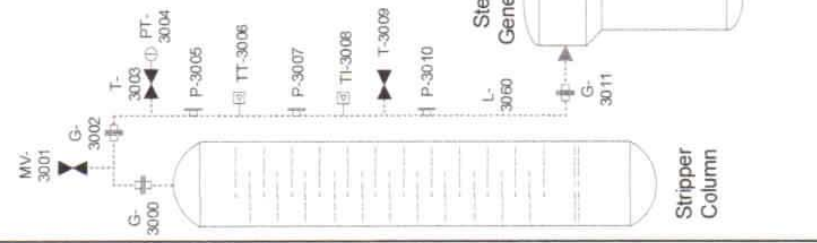
Stripper Column SOGs

Completed Date/Time: 1/26/21

Number	Type	Equip. Number	Pressure (+/-)	Background	VOC Reading	Is Component Free of Leaks or Defects?	Comments
3031	TT	51-TT-028					
3032	B						
3033	PT						
3034	T						
3035	PI						
3036	CV	51-PCV-030					
3037	MV	51-MV-0602					
3038	MV	51-MV-0633					Car seal present.
3039	MV	51-MV-0632					
3040	T						
3040A	T						
3041	PT	51-PSH-036					
3041A	PT						
3042	G						
3043	RD						
3044	T						
3045	T						Car seal present.
3046	PI						
3047	FA						
3048	T						
3049	T						Car seal present.
3050	PI	51-PT-038					
3051	T						
3051A	T						
3051A	T						
3052	PT	51-PT-038					
3053	TI	51-MV-0634					
3054	MV						
3055	G						
3056	T						
3057	FT	51-FT-040					
3058	T						
3059	G						
3060	L						

Remove

SOG system is out of service Remove JKM 1/26/21



\* Indicates car seal present



New-Indy - Catawba Mill  
 LDAR Inspection and Testing Diagrams  
 Stripper Column SOGs



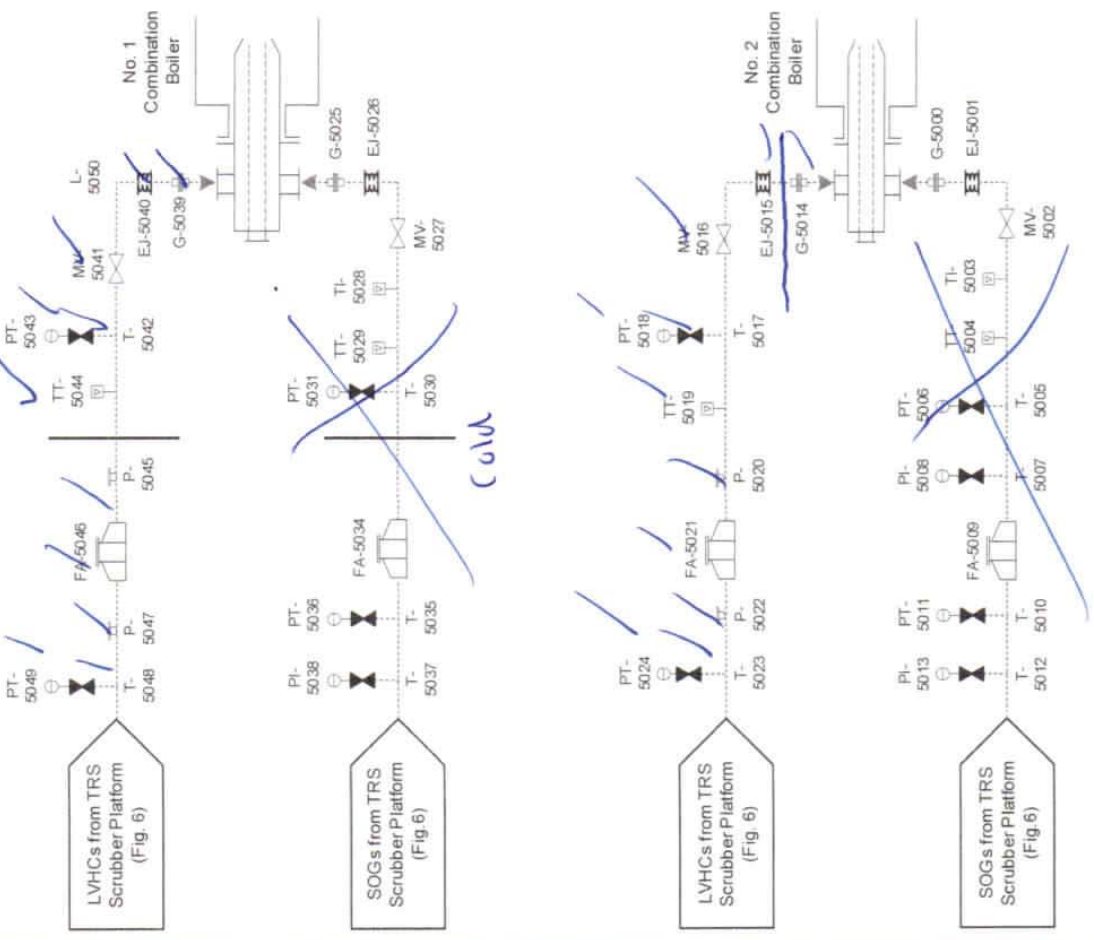
Rev. Date  
 July 2020  
 Figure 3



Combination Boiler SOG and LVHC Incineration  
 Completed Date/Time: 1/26/21

Number	Type	Equip. Number	Pressure (+/-)	Background	VOC Reading	Is Component Free of Leaks or Defects?	Comments
5000	G						
5001	EJ						
5002	MV	37-MV-0283					
5003	TI						
5004	TT						
5005	T						
5006	PT	37-PT-032					
5007	T						
5008	PI						
5009	FA						
5010	T						
5011	PT						
5012	T						
5013	PI						
5014	G						
5015	EJ						
5016	MV	37-MV-0313					
5017	T						
5018	PT	37-PT-385					
5019	TT	37-TT-384					
5020	P						
5021	FA						
5022	P						
5023	T						
5024	PT	37-PT-383					
5025	G						
5026	EJ						
5027	MV						
5028	TI						
5029	TT	26-TT-034					
5030	T						
5031	PT	26-PT-033					
5034	FA						
5035	T						
5036	PT	26-PT-031					
5037	T						
5038	PI						
5039	G						
5040	EJ						
5041	MV	26-MV-0532					
5042	T						
5043	PT	26-PT-377					
5044	TT						
5045	P						
5046	FA						
5047	P						
5048	T						
5049	PT	26-PT-375					
5050	L						

SOG system permanently out of service  
 to SKA 1/26/21



Vent Gases  
 Condensates  
 Liquor/Stock Lines  
 Process Lines

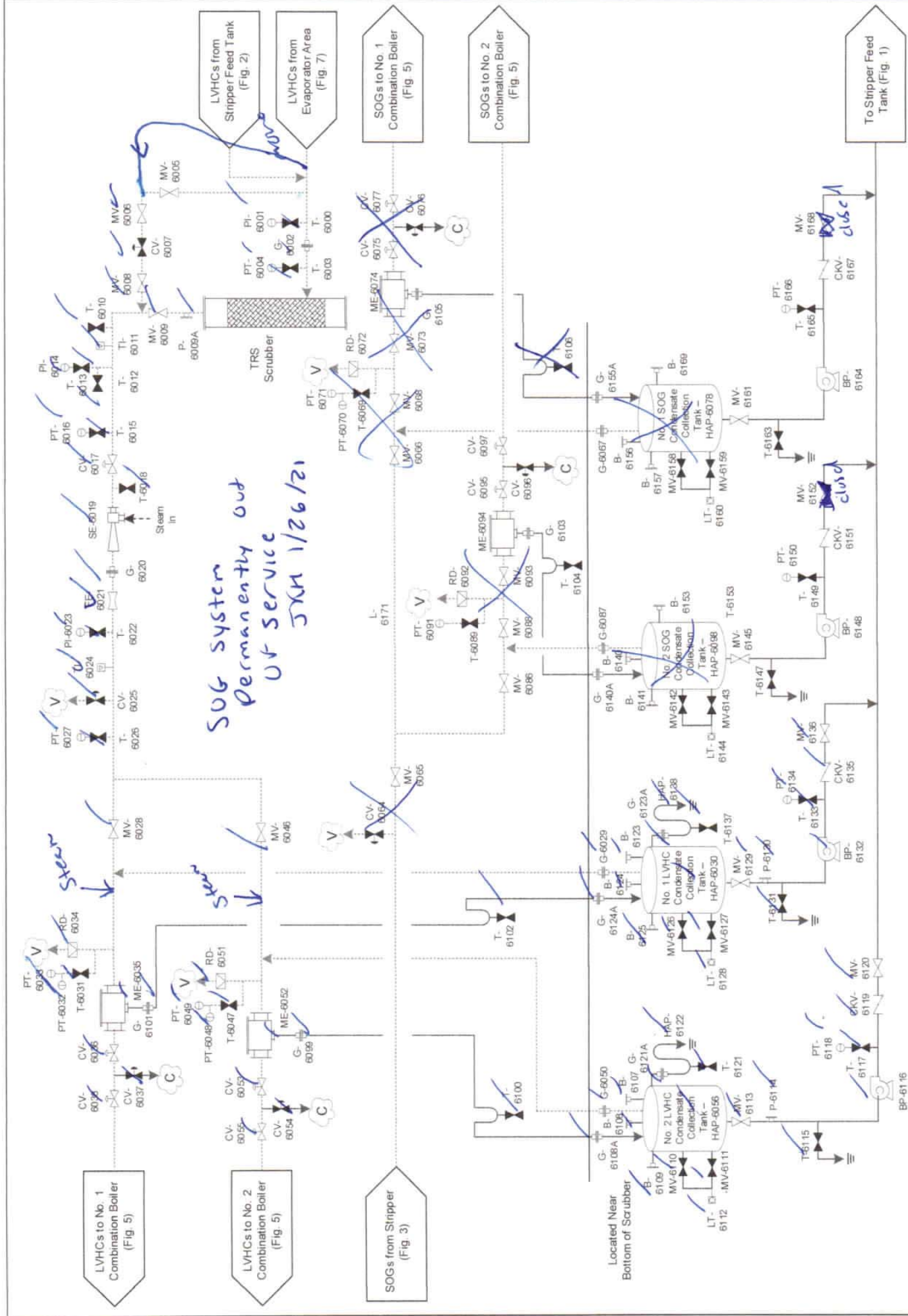
To Another Page and Indicated Equipment  
 From Another Page and Indicated Equipment



ENVIRONMENTAL 360

New-Indy - Catawba Mill  
 LDAR Inspection and Testing Diagrams  
 Combination Boiler SOG and LVHC Incineration

Rev. Date July 2020  
 Figure 5



*SUG system Permanently out of service JKH 1/26/21*

*Steam*

*Steam*

*close*

*close*

<p>Vent Gases Condensates Liquor/Stock Lines Process Lines</p>	<p>To Another Page and Indicated Equipment</p> <p>From Another Page and Indicated Equipment</p>		<p>New-Indy – Catawba Mill</p>	<p>Rev. Date July 2020</p>
			<p>LDAR Inspection and Testing Diagrams</p>	<p>Figure 6</p>

TRS Scrubber Platform  
 Completed Date/Time: 1/26/21

Number	Type	Equip. Number	Pressure (+/-)	Background	VOC Reading	Is Component Free of Leaks or Defects?	Comments
6000	T					Y	
6001	PI					Y	
6002	G					Y	
6003	T					Y	
6004	PT					Y	
6005	MV	26-MV-0485				Y	
6006	MV	26-MV-0486				Y	
6007	CV	26-HV-364				Y	
6008	MV	26-MV-0575				Y	
6009	MV	26-MV-0507				Y	
6009A	P					Y	
6010	T					Y	
6011	TI					Y	
6012	T					Y	
6013	T					Y	
6014	PI					Y	
6015	T					Y	
6016	PT					Y	
6017	CV	26-PCV-365				Y	
6018	T					Y	
6019	SE					Y	
6020	G					Y	
6021	FE					Y	
6022	T					Y	
6023	PI					Y	
6024	TI					Y	
6025	CV					Y	
6026	T					Y	
6027	PT	26-PT-372				Y	
6028	MV					Y	
6029	G					Y	
6030	HAP					Y	
6031	T					Y	
6032	PT					Y	
6033	PT	26-PSH-373				Y	
6034	RD					Y	
6035	ME					Y	
6036	CV					Y	
6037	CV					Y	
6038	CV					Y	
6046	MV					Y	
6047	T					Y	
6048	PT	37-PSH-381				Y	
6049	PT					Y	
6050	G					Y	
6051	RD					Y	
6052	ME					Y	
6053	CV	37-HV-382A				Y	
6054	CV	37-HV-043				Y	
6055	CV	37-HV-382B				Y	
6056	HAP					Y	
6064	CV					Y	
6065	MV	51-MV-637				Y	
6066	MV	51-MV-638				Y	
6067	G					Y	
6068	MV	51-MV-474				Y	
6069	T					Y	
6070	PT	26-PSH-028				Y	
6071	PT					Y	
6072	RD					Y	
6073	MV	26-MV-0475				Y	
6074	ME					Y	
6075	CV	26-HV-030A				Y	
6076	CV	26-HV-043				Y	
6077	CV	26-HV-030B				Y	
6078	HAP					Y	
6086	MV	51-MV-0283				Y	
6087	G					Y	
6088	MV					Y	
6089	T					Y	
6091	PT	37-PSH-025				Y	
6092	RD					Y	
6093	MV	37-MV-0282				Y	
6094	ME					Y	

Remove

Y

Remove  
 Remove  
 Remove  
 Remove

Y

Y

Y

Y

Y

Y

Y

Y

Y

Y

Y

Y

Y

Y

Y

Y

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Y

Y

Y

Y

Remove

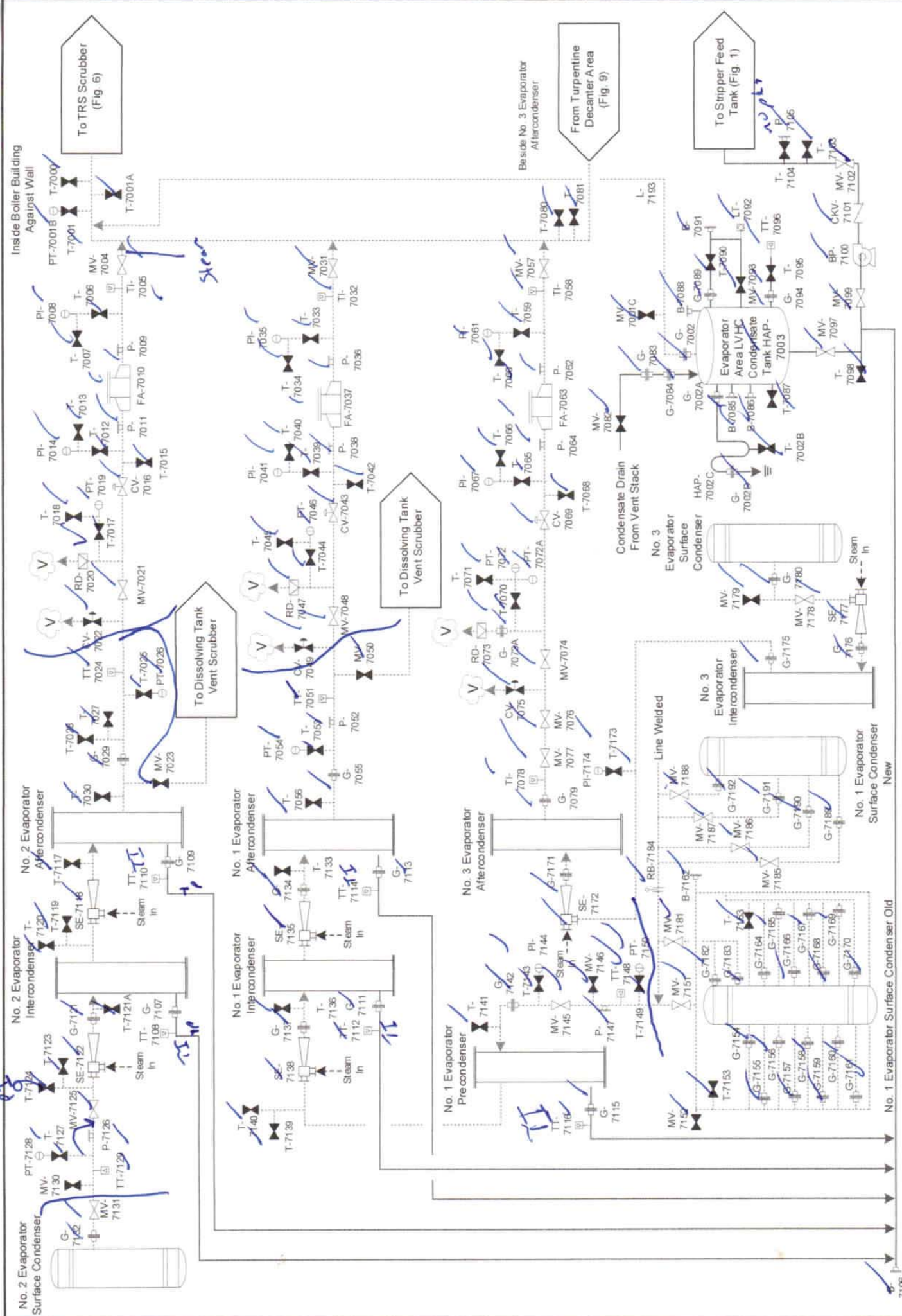
Remove

Remove

37-HV-027A

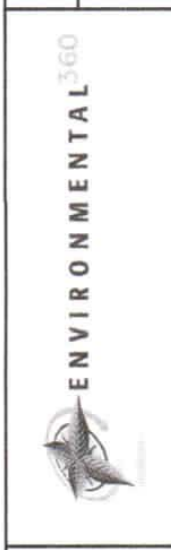
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6168  
6169  
6171

CV  
CV  
CV  
HAP  
G  
T  
G  
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G  
T  
B  
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B  
B  
MV  
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CKV  
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CKV  
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MV  
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MV  
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BP  
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PT  
CKV  
MV  
B  
L



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July 2020

New-Indy – Catawba Mill  
LDAR Inspection and Testing Diagrams  
Evaporator System



To Another Page and Indicated Equipment  
From Another Page and Indicated Equipment  
Vent Gases  
Condensates  
Liquor/Stock Lines  
Process Lines

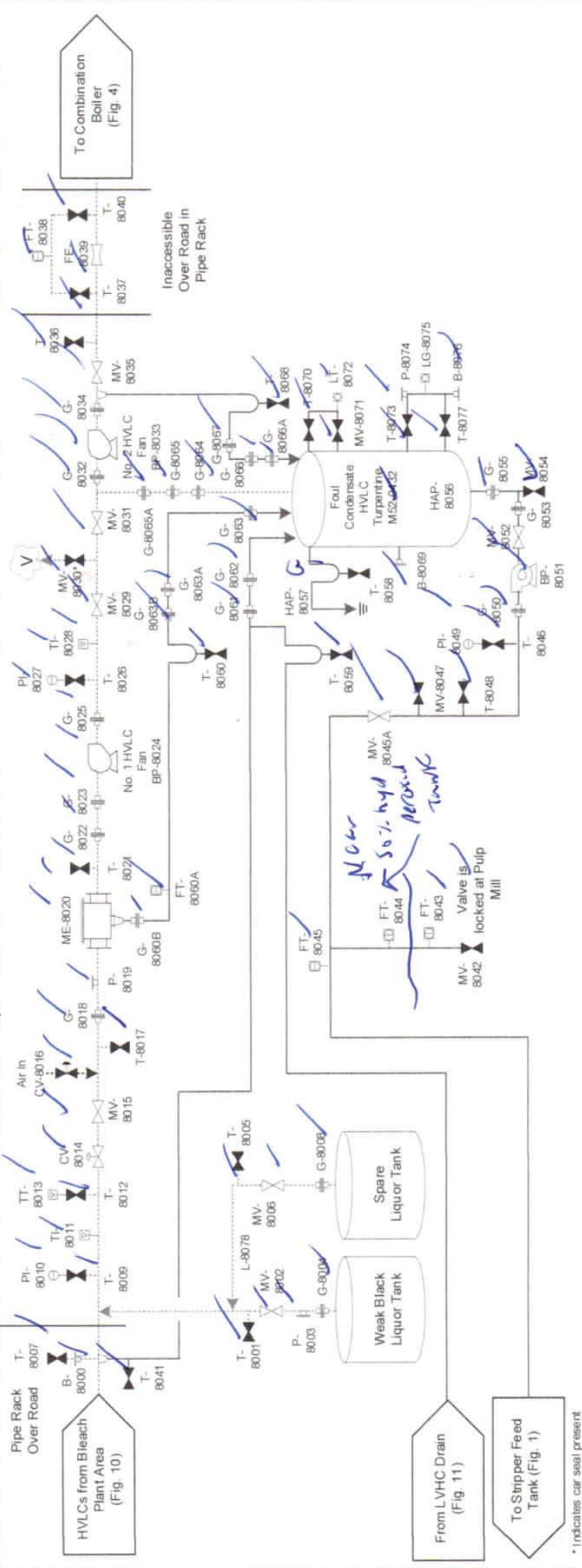
Figure 7





1/26/21

Number	Type	Equip. Number	Pressure (psi)	Background	VOC Reading	IS Component	Comments
SD41	MV						
SD42	FT						
SD43	FT						
SD44	FT						
SD45	FT						
SD46	MV						
SD47	MV						
SD48	T						
SD49	PI						
SD50	G						
SD51	BP						
SD52	MV						
SD53	MV						
SD54	MV						
SD55	G						
SD56	HAP						
SD57	HAP						
SD58	T						
SD59	T						
SD60	FT						
SD61	FT						
SD62	G						
SD63	G						
SD64	G						
SD65	G						
SD66	G						
SD67	G						
SD68	T						
SD69	T						
SD70	MV						
SD71	LT						
SD72	LT						
SD73	P						
SD74	P						
SD75	LG						
SD76	B						
SD77	T						
SD78	T						



**ENVIRONMENTAL 360**

New-Indy – Catawba Mill

LDAR Inspection and Testing Diagrams

HVLCL Blower Platform

Rev. Date  
July 2020

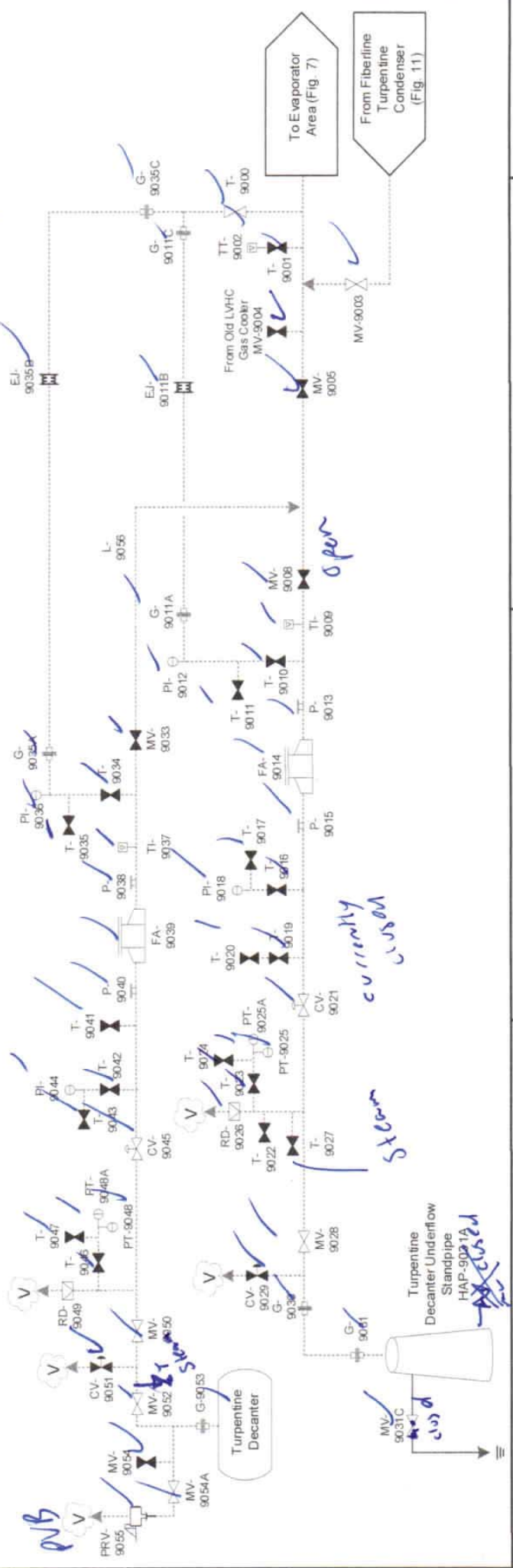
Figure 8

\* Indicates car seal present

..... To Another Page and Indicated Equipment  
 ——— Condensates  
 ——— Liquor/Stock Lines  
 ——— Process Lines

Number	Type	Equip. Number	Pressure (+/-)	Background	VOC Reading	Is Component Free of Leaks or Defects?	Comments
9000	T					Y	
9001	T					Y	
9002	TT					Y	
9003	MV	14-MV-0312				Y	
9004	MV					Y	
9005	MV					Y	
9008	MV	14-TI/TW-125				Y	
9009	TI					Y	
9010	T					Y	
9011	T					Y	
9011A	G					Y	
9011B	EJ					Y	
9011C	G					Y	
9012	PI					Y	
9013	P					Y	
9014	FA					Y	
9015	P					Y	
9016	T					Y	
9017	T	14-PI-125A				Y	
9018	PI					Y	
9019	T					Y	
9020	T					Y	
9021	CV	14-HV-127				Y	
9022	T					Y	
9023	T					Y	
9024	T					Y	
9025	PT	14-PSH-122				Y	
9025A	PT	14-PSH-122				Y	
9026	RD					Y	
9027	T					Y	
9028	MV					Y	

9029	CV	14-HV-126					
9030	G						
9031	G						
9031A	HAP						
9031C	MV	14-MV-0330					
9033	MV						
9034	T						
9035	T						
9035A	G						
9035B	EJ						
9035C	G						
9036	PI						
9037	TI	14-TI/TW-304B					
9038	P						
9039	FA	M14-0121					
9040	P						
9041	T						
9042	T						
9043	T						
9044	PI						
9045	CV	14-HV-314					
9046	T						
9047	T						
9048	PT	14-PSH-313					
9048A	PT	14-PSH-313					
9049	RD						
9050	MV	14-MV-0342					
9051	CV	14-HV-312					
9052	MV	14-MV-0343					
9053	G						
9054	MV						
9054A	MV						
9055	PRV						
9056	L						



Completed Date/Time: 1/26/21

Rev. Date  
July 2020

New-Indy - Catawba Mill

Figure 9

LDAR Inspection and Testing Diagrams

Turpentine Decanter and Standpipe

Vent Gases

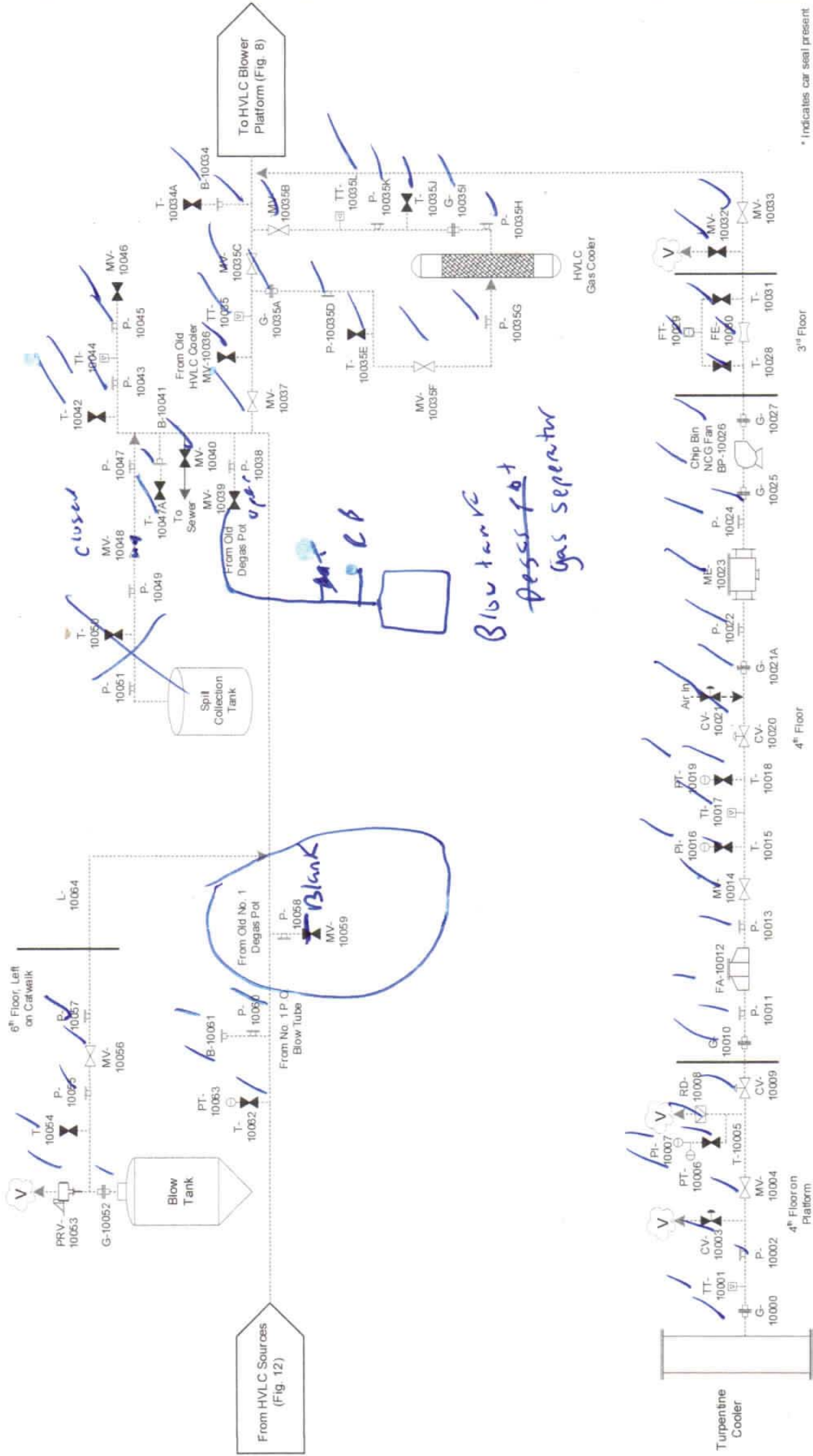
Condensates

Liquor/Stock Lines

Process Lines

To Another Page and Indicated Equipment

From Another Page and Indicated Equipment



\* Indicates air seal present

Rev. Date  
July 2020

Figure 10

New-Indy - Catawba Mill  
LDAR Inspection and Testing Diagrams  
Turpentine Cooler and Blow Tank

ENVIRONMENTAL 360



To Another Page and Indicated Equipment  
From Another Page and Indicated Equipment

Vent Gases  
Condensates  
Liquor/Stock Lines  
Process Lines

**Turpentine Cooler and Blow Tank**

Completed Date/Time: 1/27/21

Number	Type	Equip. Number	Pressure (+/-)	Background	VOC Reading	Is Component Free of Leaks or Defects?	Comments
10000	G					yes	
10001	TT	52-TE-230				y	
10002	P					y	
10003	CV	52-QV-937				y	
10004	MV	52-MV-1021				y	
10005	T					y	
10006	PT	52-PSH-934				y	
10007	PI					y	
10008	RD					y	
10009	CV	52-EV-938				y	
10010	G					y	
10011	P					y	
10012	FA	M52-0429				y	
10013	P					y	
10014	MV	52-MV-1022				y	
10015	T					y	
10016	PI					y	
10017	TI					y	
10018	T					y	
10019	PT					y	
10020	CV	52-PV-941				y	
10021	CV					y	
10021A	G					y	
10022	P					y	
10023	ME	M52-0415				y	
10024	P					y	
10025	G					y	
10026	BP	M52-0411				y	
10027	G					y	
10028	T					y	
10029	FT					y	
10030	FE					y	
10031	T					y	
10032	MV					y	
10033	MV					y	
10034	B					y	
10034A	T					y	
10035	TT	52-TT-947				y	
10035A	G					y	
10035B	MV					y	
10035C	MV					y	

Number	Type	Equip. Number	Pressure (+/-)	Background	VOC Reading	Is Component Free of Leaks or Defects?	Comments
10035D	P					y	
10035E	T					y	
10035F	MV					y	
10035G	P					y	
10035H	P					y	
10035I	G					y	
10035J	T					y	
10035K	P					y	
10035L	TT					y	
10036	MV					y	
10037	MV					y	
10038	P					y	
10039	MV					y	
10040	MV					y	
10041	B					y	
10042	T					y	
10043	P					y	
10044	TI					y	
10045	P					y	
10046	MV					y	
10047	P					y	
10047A	T					y	
10048	MV	A507				y	
10049	P					y	
10050	T					y	
10051	P					y	
10052	G					y	
10053	PRV					y	
10054	T					y	
10055	P					y	
10056	MV					y	
10057	P					y	
10058	P					y	
10059	<del>MV</del> Blank					y	
10060	P					y	
10061	B					y	
10062	T					y	
10063	PT	52-PT-215				y	
10064	L					y	

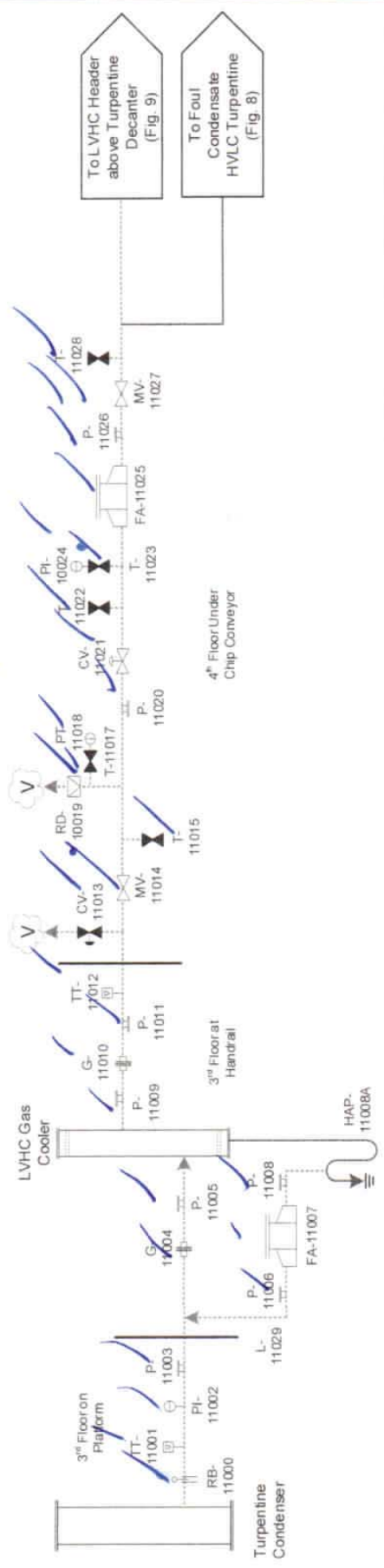
Remove

Car seal present.

**Turpentine Condenser and LVHC Gas Cooler**

Completed Date/Time: 1/27/21

Number	Type	Equip. Number	Pressure (+/-)	Background	VOC Reading	Is Component Free of Leaks or Defects?	Comments
11000	RB					Yes	
11001	TT	52-TE-222A				Y	
11002	PI					Y	
11003	P					Y	
11004	G					Y	
11005	P					Y	
11006	P					Y	
11007	FA	M52-0512				Y	
11008	P					Y	
11008A	HAP					Y	
11009	P					Y	
11010	G					Y	
11011	P					Y	
11012	TT	52-TE-225				Y	
11013	CV	52-HV-174B				Y	
11014	MV	52-A-368				Y	
11015	T					Y	
11017	T					Y	
11018	PT	52-PSH-226				Y	
11019	RD					Y	
11020	P					Y	
11021	CV	52-HV-174A				Y	
11022	T	52-A-428				Y	
11023	T					Y	
11024	PI	52-PI-226				Y	
11025	FA	Z00-0395M				Y	
11026	P					Y	
11027	MV	52-A-541				Y	
11028	T	52-A-437				Y	
11029	L					Y	



**ENVIRONMENTAL** 360

**New-Indy – Catawba Mill**

LDAR Inspection and Testing Diagrams

Turpentine Condenser and LVHC Gas Cooler

**Rev. Date**  
July 2020

**Figure** 11

**Legend:**

- Vent Gases
- Condensates
- Liquor/Stock Lines
- Process Lines

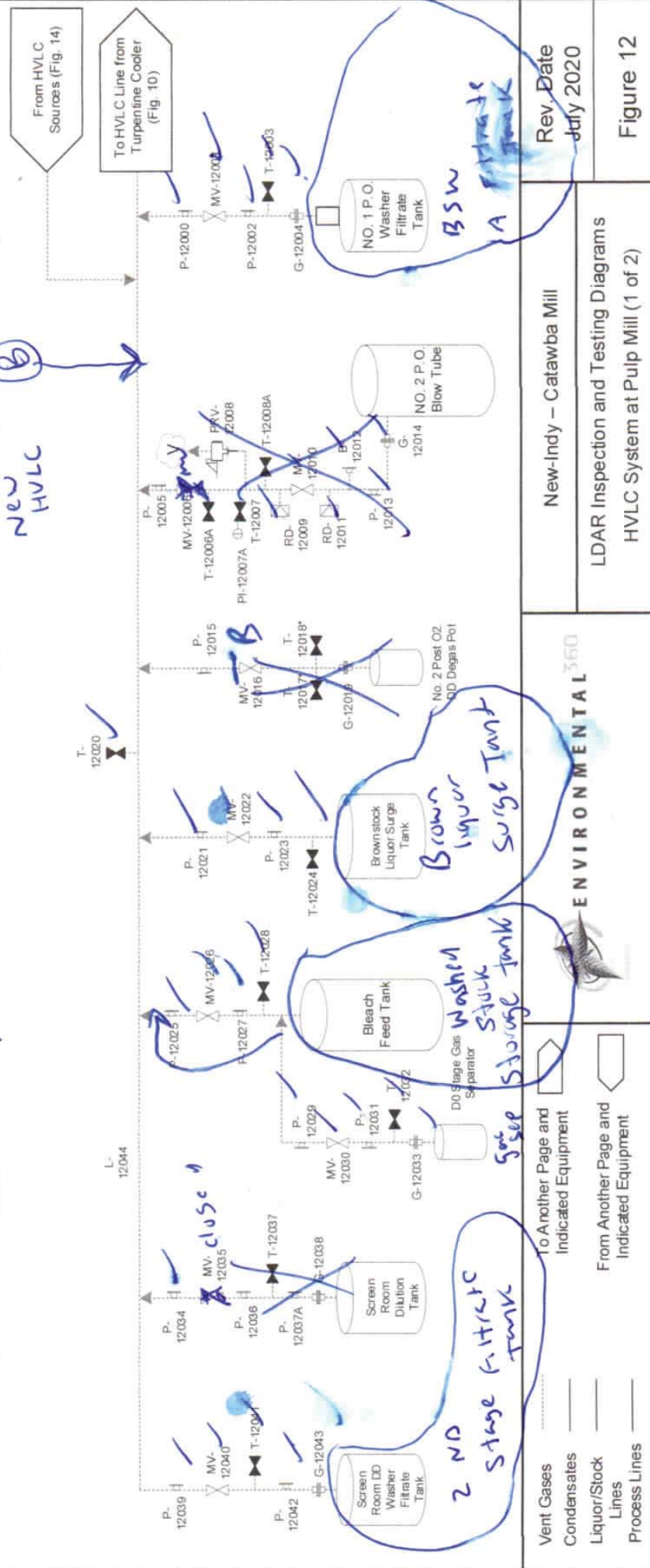
To Another Page and Indicated Equipment

From Another Page and Indicated Equipment

HVLC System at Pulp Mill (1 of 2) 7/27/20

Number	Type	Equip. Number	Pressure (+/-)	Background	VOC Reading	Is Component Free of Leaks or Defects?	Comments
12000	P					yes	
12001	MV					y	
12003	T	X182				y	
12004	G					y	
12005	P					y	
12006	MV					y	
12006A	T						Remove
12007	T						
12007A	PI						
12008	PRV						
12008A	T						
12009	RD						
12010	MV						
12011	RD						
12012	B						
12013	P						
12014	G						
12015	P					yes	
12016	MV	Blank				Remove	Car seal present.
12017	T					yes	
12018	T	X176					Car seal present.
12019	G						
12020	T	V4454					

12021	P	0598-22-HY					
12022	MV						
12023	P						
12024	T	D060					
12025	P						
12026	MV						
12027	P						
12028	T						
12029	P						
12030	MV	F543					
12031	P						
12032	T	F541					
12033	G						
12034	P						
12035	MV	SR307					
12036	P						
12037	T	SR314					
12037A	P						
12038	G						
12039	P						
12040	MV	SR308					
12041	T						
12042	P						
12043	G						
12044	L						



Rev. Date  
July 2020

New-Indy - Catawba Mill  
LDAR Inspection and Testing Diagrams  
HVLC System at Pulp Mill (1 of 2)

ENVIRONMENTAL 360

To Another Page and Indicated Equipment  
From Another Page and Indicated Equipment

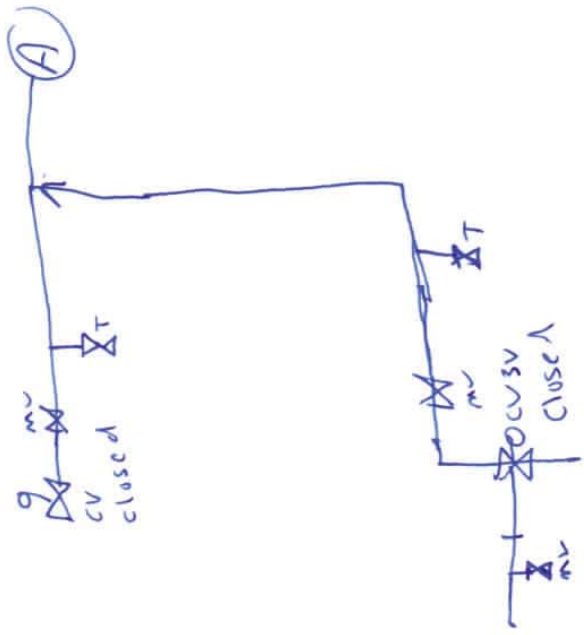
Figure 12



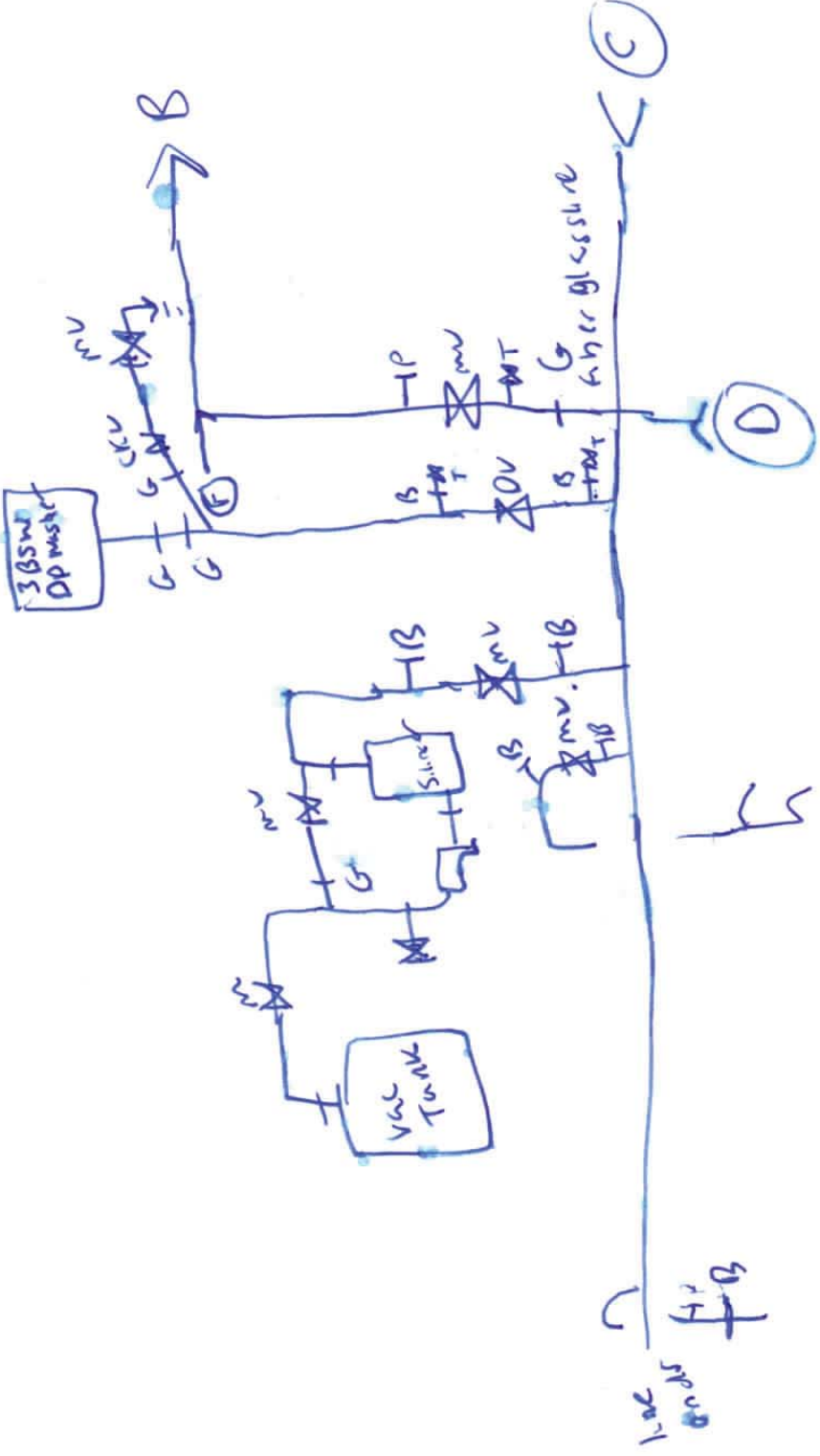




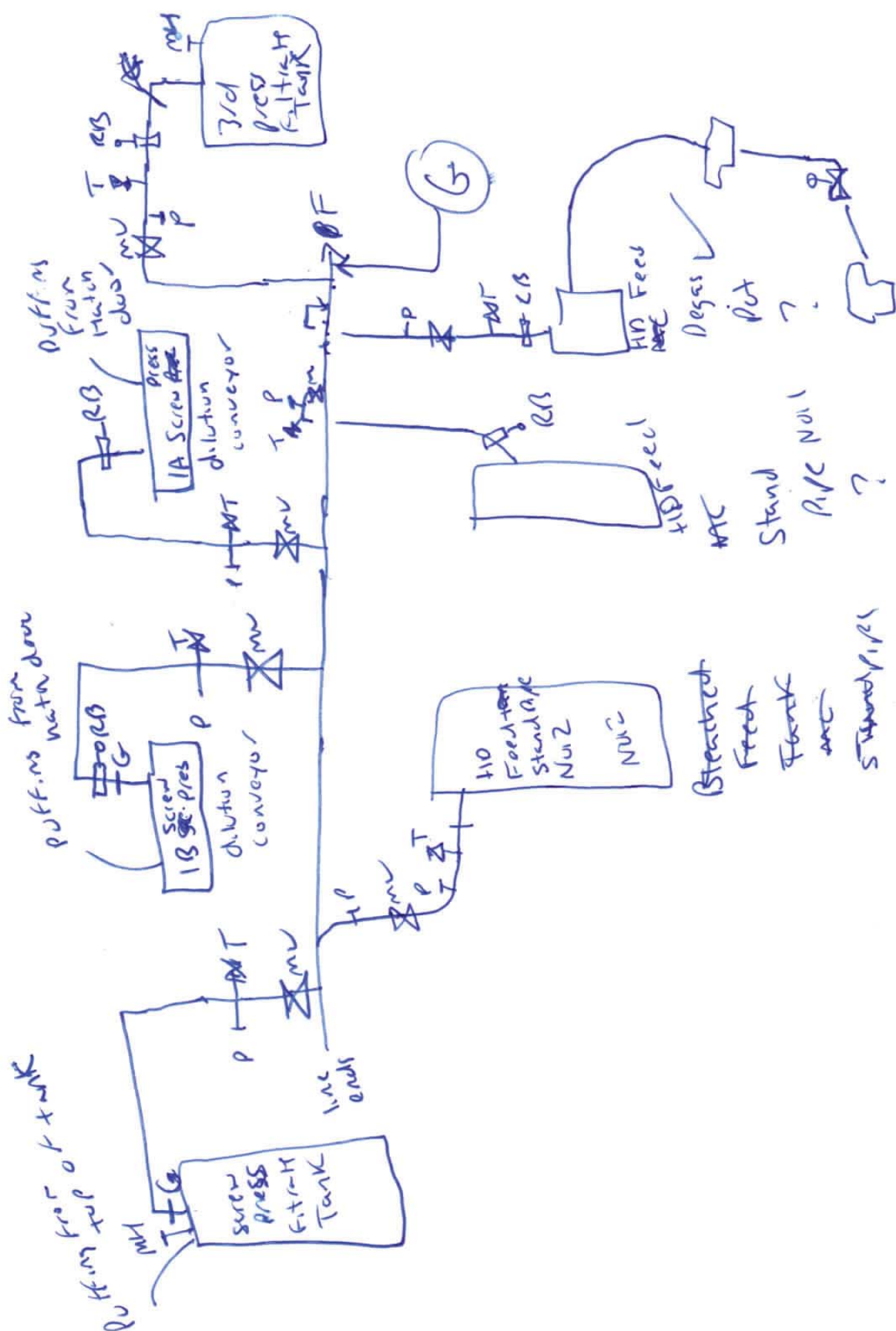




test washer







Breached  
 Feed  
 Feed  
 Stand No. 1  
 Stand No. 2

Stand  
 Pipe No. 1  
 ?

Stand No. 1  
 Stand No. 2

Inspection Date: February 17, 2021



New Indy Containerboard - Catawba Mill  
5300 Cureton Ferry Rd.  
Catawba, SC 29704

### 2021 Monthly LDAR Inspection Summary Report

**Table 1: Visual Inspection Summary Table**

Equipment Number	Date	Description of Leak or Visual Defect
T-8060	2/17/2021	Tap valve T-8060 is located on foul condensate low point drain, coming from mist eliminator on HVLC line at inlet of No. 1 HVLC fan. The valve is open and dripping.
T-8068	2/17/2021	Tap valve T-8068 is located on foul condensate low point drain, coming from HVLC line at outlet of No. 2 HVLC fan. The valve is open and dripping.
HAP13007	2/17/2021	The 1A Screw Press Dilution Conveyor is puffing from top hatch door.
HAP-13013	2/17/2021	The 1B Screw Press Dilution Conveyor is puffing from top hatch door.
HAP-13117	2/17/2021	The 2B Brown Stock Washer is puffing from four open hatch doors.
<b>First Attempt to Repair must be completed by:</b>	5 Days from Inspection Date	Not Applicable if no leaks were found.
<b>Repairs must be completed by:</b>	15 Days from Inspection Date	Not Applicable if no leaks were found.

This report provides a summary of leaks and visual defects found during the visual inspection of the closed-vent and condensate-collection systems and complies with the record keeping requirements of 63.454(b)(1-2, 4-5).

The facility must initiate repairs to any defects within five (5) calendar days from this inspection and the defects must be repaired within fifteen (15) calendar days of the inspection. If the leak or defect requires the system to be shutdown in order to make repairs, or more emissions would occur from attempting the repair than delaying the repair, then the repairs may be delayed until the next process unit shutdown. A report must be supplied with the repair date and associated information, or the reason for the delay if the repairs are not completed within the 15-day period. These response requirements are specific to 40 CFR 63, specifically 63.453(k)(6), 63.453(l)(3), and 63.964(b)(1-2). Documentation of all repair attempts made and any leaks/defects requiring a process unit shutdown must be completed according to 63.454(b)(6-11).

I certify that the results of the visual inspection are accurate and complete to the best of my knowledge.

Inspector Name: Josh Howard

Signature: Josh Howard



## Inspection QA/QC Procedure

E360 Project Number?	New Indy Catawba
Task Number (if applicable)?	February 2020 Monthly LDAR

### Purpose of Form

To verify field work meets each critical element.

### Visual Work Flow (WF)

**Step 1**  
**R** - Verify field work by checking "X" each WF No.

### Verification of Critical Elements

WF No.	Requirement	Yes?
	Work-flow step	1
	Verifier of critical elements for work-flow step	R
1	Was a bump test performed on the personal H <sub>2</sub> S monitor?	✓
2	Have the most recent versions of the inspection forms been used?	✓
3	Were all inspection points identified correctly and inspected correctly?	✓
4	Did the operator/ contact verify to our inspector that all equipment was operating under normal operating conditions?	✓
5	Were any deficiencies identified in person to the client?	✓
6	Were all inspection questions answered with either a Yes, No, or NA?	✓
7	Were inspections performed during the required regulatory time frame?	✓

### Approvals

Role	WF Step	Name	Approval (insert date)
Responsible Person (R)	1	<i>John Lee</i>	2/17/2021





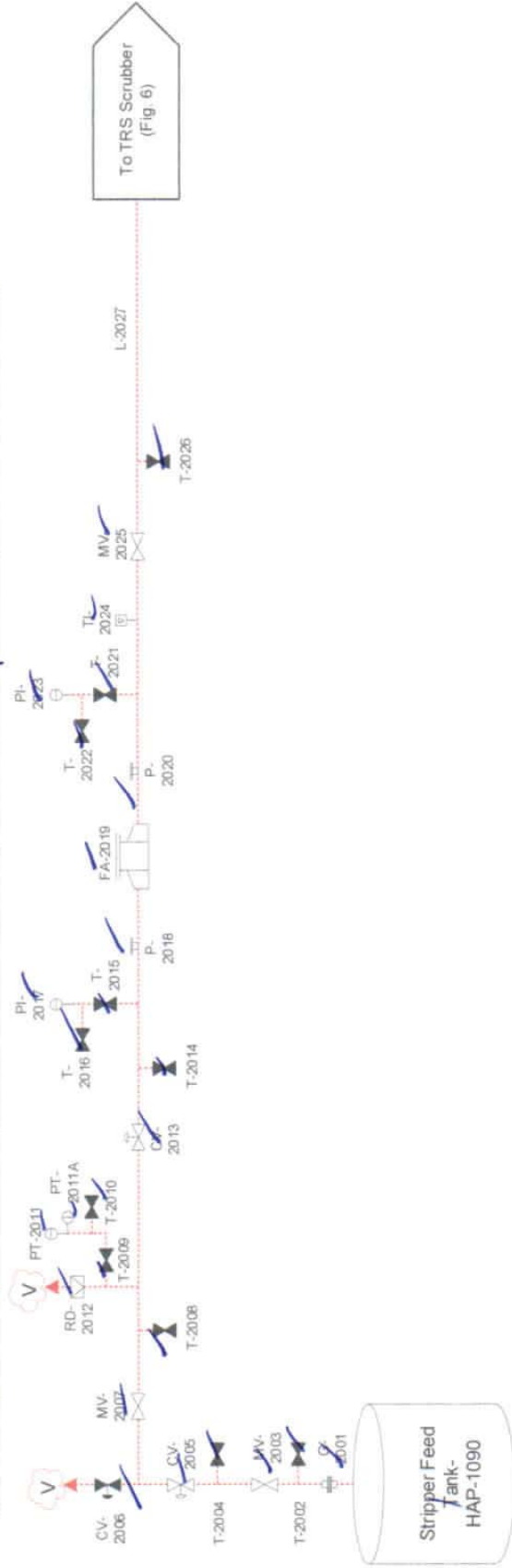
Stripper System Foul Condensate  
 Completed Date/Time: 2/17/21

Number	Type	Equip. Number	Pressure (+/-)	Background	VOG Reading	Is Component Free of Leaks or Defects?	Comments
1060	B					Y	
1061	MV	24-MV-0361				Y	
1062	MV	24-MV-0359				Y	
1062A	LT					Y	
1063	CKV					Y	
1064	MV	24-MV-0445				Y	
1065	T					Y	
1066	RB					Y	
1067	RB					Y	
1068	RB					Y	
1069	T					Y	
1069A	MV					Y	
1069B	LT	51-LT-265				Y	
1070	MV	24-MV-445				Y	
1071	T					Y	
1072	T					Y	
1073	PI					Y	
1074	T					Y	
1075	CKV					Y	
1076	T					Y	
1077	BP					Y	
1078	EJ					Y	
1079	T					Y	
1080	MV	24-MV-363				Y	
1081	MV					Y	
1082	G					Y	
1083	MV	V704F				Y	
1084	T					Y	
1085	MV					Y	
1086	CV	51-HV-269				Y	
1086A	MV					Y	
1087	MV	24-MV-362				Y	
1087A	G					Y	
1087B	TT	51-TT-266				Y	
1088	G					Y	
1088A	T					Y	
1088B	G					Y	
1088C	T					Y	
1088D	MV					Y	
1088E	MV					Y	
1089	G					Y	
1089A	MV	24-MV-0352				Y	
1089B	G					Y	
1090	HAP					Y	
1090A	MH					Y	
1091	MV	24-MV-0365				Y	
1092	T					Y	
1093	EJ					Y	
1094	BP					Y	
1095	CKV	V884F				Y	
1096	T					Y	
1097	T					Y	
1098	T					Y	
1099	PI					Y	
1100	MV	24-MV-360				Y	
1100A	CV					Y	
1100B						Y	
1101	FE					Y	
1102	CV	51-FCV-267				Y	
1103	G					Y	
1104	MV					Y	
1105	MV					Y	
1106	G					Y	
1107	MV					Y	
1108	MV					Y	
1109	MV					Y	
1110	CV					Y	
1111	MV					Y	
1112	P					Y	
1113	CV					Y	
1114	MV					Y	
1115	T					Y	
1115A	MV					Y	
1116	T					Y	
1117	T					Y	
1118	CT					Y	
1120	G					Y	
1121	T					Y	
1122	T					Y	
1123	T					Y	
1124	G					Y	
1125	G					Y	
1126	G					Y	
1127	G					Y	
1128	G					Y	
1129	MV					Y	
1129A	G					Y	
1130	MV					Y	
1131	T					Y	
1131A	CKV					Y	
1132	T					Y	
1133	PI					Y	
1134	T					Y	
1135	BP					Y	
1136	MV					Y	
1137	MV					Y	
1138	G					Y	
1139	HAP					Y	
1140	MV	M152-0436				Y	
1141	LT					Y	
1142	T					Y	
1143	T					Y	
1143A	FT					Y	
1144	G					Y	
1145	G					Y	
1146	T					Y	
1147	G					Y	
1148	T					Y	
1149	P					Y	
1150	LG					Y	
1151	B					Y	
1152	T					Y	
1153	B					Y	
1154	B					Y	
1155	T					Y	
1156	FT					Y	
1157	G					Y	
1158	G					Y	
1159	G					Y	
1160	T					Y	
1161	G					Y	
1162	B					Y	
1163	T					Y	
1164	T					Y	
1165	G					Y	
1165A	LG					Y	
1166	T					Y	
1167	G					Y	
1168	B					Y	
1169	T					Y	
1170	MV					Y	
1171	MV					Y	
1172	G					Y	
1173	G					Y	
1174	FT					Y	
1175	L					Y	

Stripper Feed Tank

Completed Date/Time: 2/17/21

Number	Type	Equip. Number	Pressure (+/-)	Background	VOC Reading	Is Component Free of Leaks or Defects?	Comments
2001	G					Yes	
2002	T					Y	
2003	MV					Y	
2004	T					Y	
2005	CV	51-PCV-264				Y	
2006	CV	51-HV-262				Y	
2007	MV	51-MV-0672				Y	
2008	T					Y	
2009	T					Y	
2010	T					Y	
2011	PT	51-PSH-261				Y	
2011A	PT					Y	
2012	RD					Y	
2013	CV	51-HV-260				Y	
2014	T	51-MV-0675				Y	
2015	T					Y	
2016	T					Y	
2017	PI					Y	
2018	P					Y	
2019	FA	M51-0546				Y	
2020	P					Y	
2021	T					Y	
2022	T					Y	
2023	PI	51-PI-268B				Y	
2024	TI	01-TI-274				Y	
2025	MV	51-MV-0673				Y	
2026	T	24-MV-0353				Y	
2027	L					Y	



\* Indicates air seal present

--- Vent Gases  
--- Condensates  
--- Liquor/Stock Lines  
--- Process Lines

  To Another Page and Indicated Equipment  
  From Another Page and Indicated Equipment

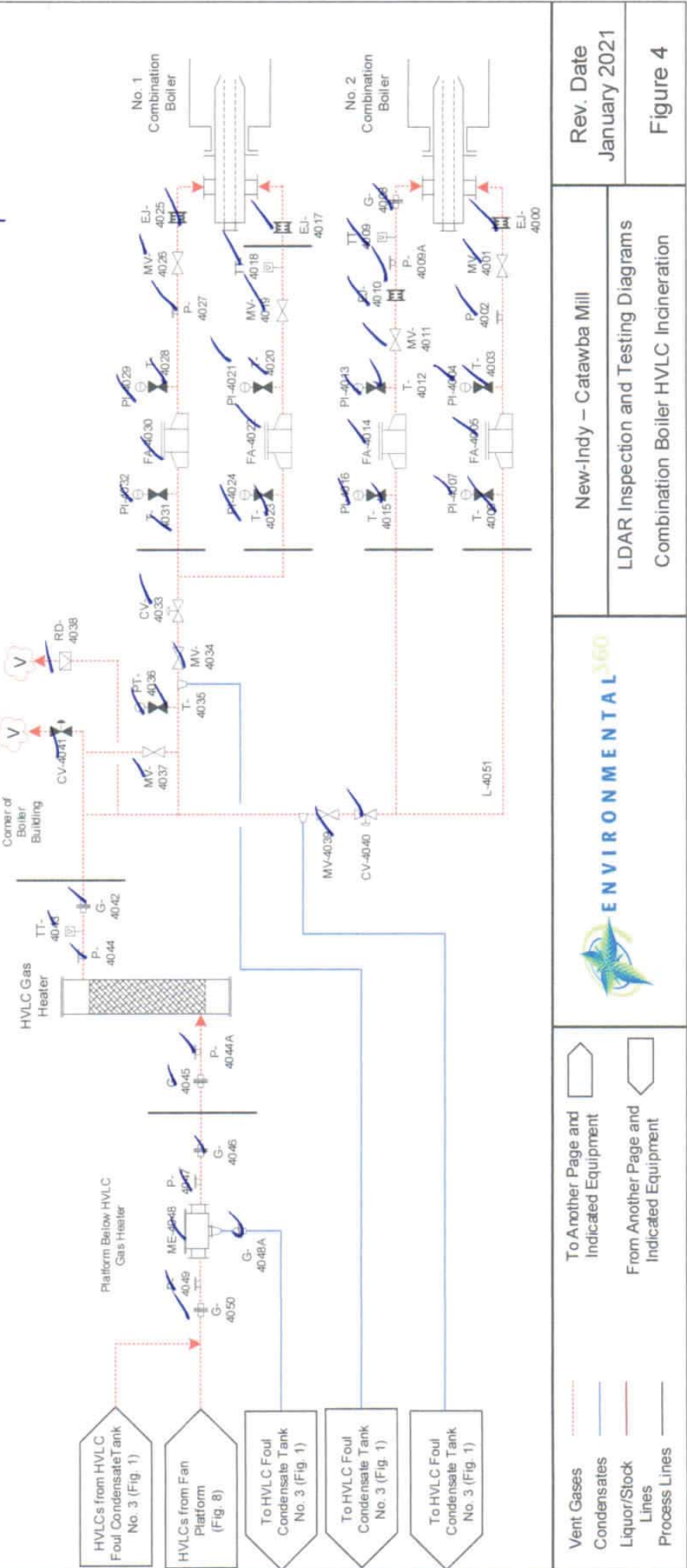


New-Indy – Catawba Mill  
 LDAR Inspection and Testing Diagrams  
 Stripper Feed Tank

Rev. Date  
 January 2021  
 Figure 2

Combination Boiler HVLC Incinerator  
 Completed Date/Time: 2/17/21

Number	Type	Equip. Number	Pressure (+/-)	Background	VOC Reading	Is Component Free of Leaks or Defects?	Comments
4000	EJ					Yes	
4001	MV	37-MV-0271				Yes	
4002	P					Yes	
4003	T					Yes	
4004	PI					Yes	
4005	FA					Yes	
4006	T					Yes	
4007	PI					Yes	
4008	G					Yes	
4009	TT					Yes	
4009A	P					Yes	
4010	EJ					Yes	
4011	MV	37-MV-0270				Yes	
4012	T					Yes	
4013	PI					Yes	
4014	FA					Yes	
4015	T					Yes	
4016	PI					Yes	
4017	EJ					Yes	
4018	TT					Yes	
4019	MV	26-MV-0628				Yes	
4020	T	BOP271				Yes	
4021	PI					Yes	
4022	FA	M52-0426				Yes	
4023	T	BOP270				Yes	
4024	PI	52-PI-930				Yes	
4025	EJ					Yes	
4026	MV					Yes	
4027	P					Yes	
4028	T					Yes	
4029	PI					Yes	
4030	FA					Yes	
4031	T					Yes	
4032	PI					Yes	
4033	CV	26-MV-0626				Yes	
4034	MV					Yes	
4035	T					Yes	
4036	PT	52-PSH-960				Yes	
4037	MV	52-MV-0625				Yes	
4038	RD					Yes	
4039	MV					Yes	
4040	CV					Yes	
4041	CV					Yes	
4042	G					Yes	
4043	TT	52-TT-965				Yes	
4044	P					Yes	
4044A	P					Yes	
4045	G					Yes	
4046	G					Yes	
4047	P					Yes	
4048	ME					Yes	
4048A	G					Yes	
4049	P					Yes	
4050	G					Yes	
4051	L					Yes	



Rev. Date  
January 2021

New-Indy - Catawba Mill  
 LDAR Inspection and Testing Diagrams  
 Combination Boiler HVLC Incinerator



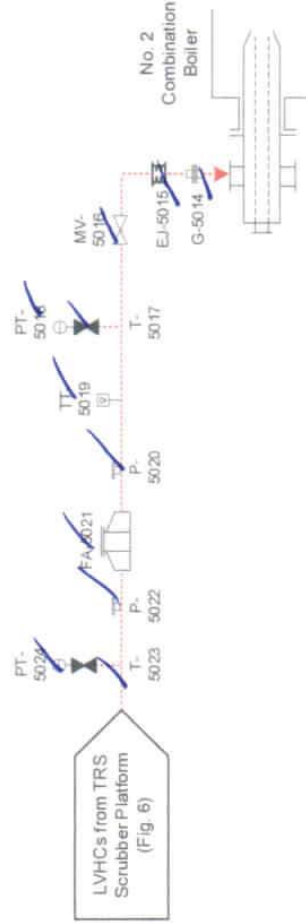
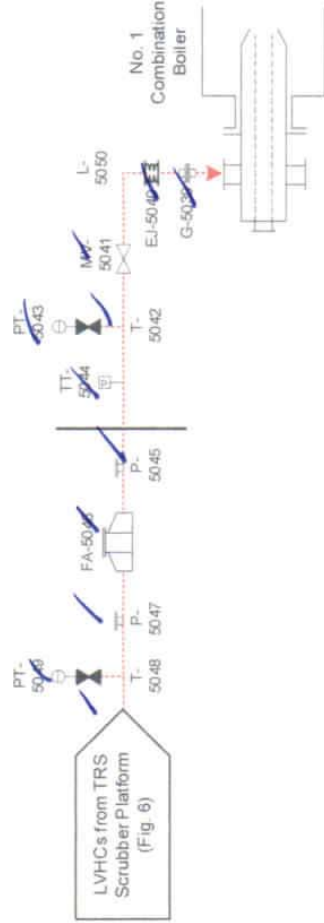
To Another Page and Indicated Equipment  
 From Another Page and Indicated Equipment  
 Vent Gases  
 Condensates  
 Liquor/Stock Lines  
 Process Lines

Figure 4

Combination Boiler SOG and LVHC Incineration

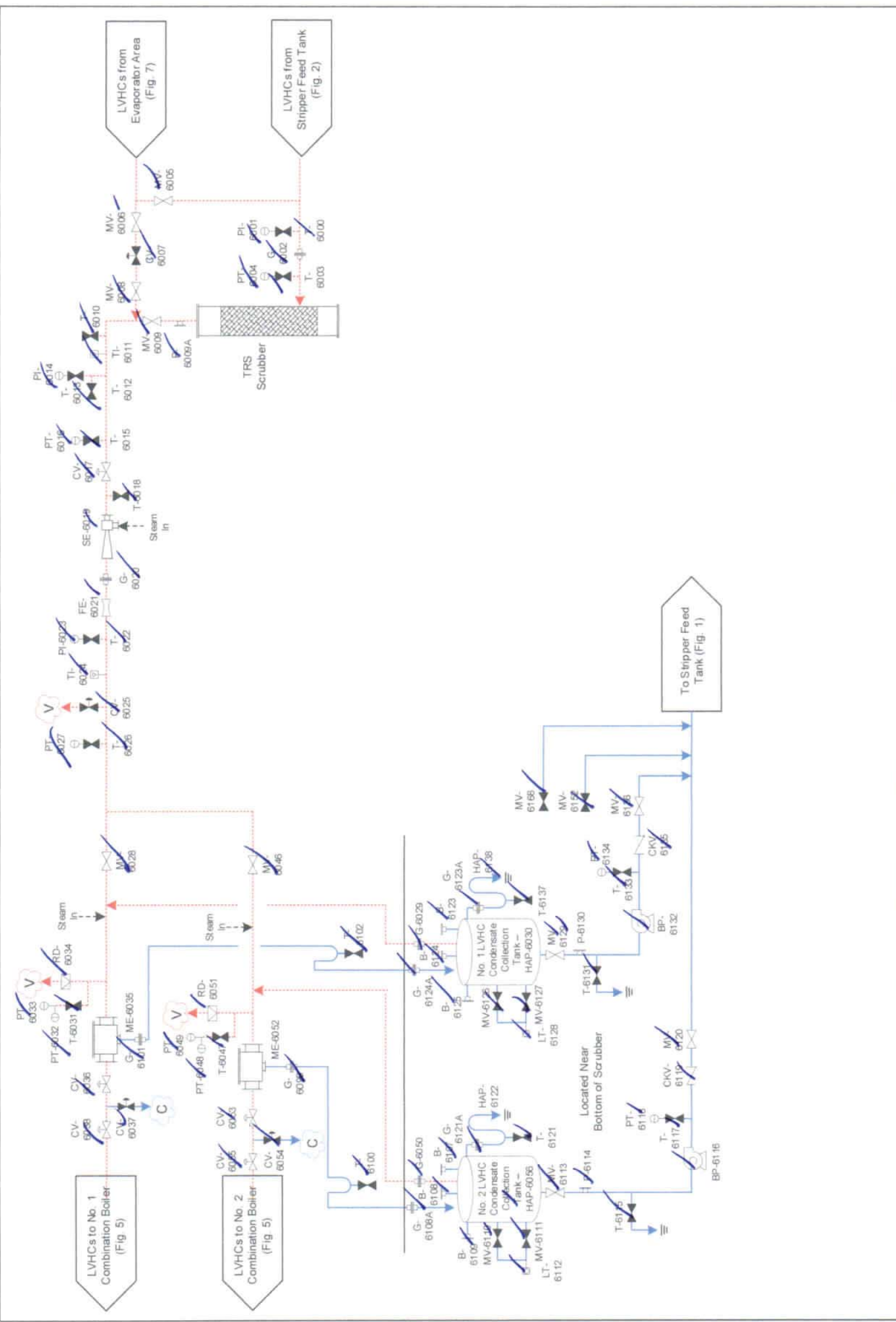
Completed Date/Time: 2/17/21

Number	Type	Equip. Number	Pressure (+/-)	Background	VOC Reading	Is Component Free of Leaks or Defects?	Comments
5014	G					Yes	
5015	EJ					Y	
5016	MV	37-MV-0313				Y	
5017	T					Y	
5018	PT	37-PT-385				Y	
5019	TT	37-TT-384				Y	
5020	P					Y	
5021	FA					Y	
5022	P					Y	
5023	T					Y	
5024	PT	37-PT-383				Y	
5039	G					Y	
5040	EJ					Y	
5041	MV	26-MV-0532				Y	
5042	T					Y	
5043	PT	26-PT-377				Y	
5044	TT					Y	
5045	P					Y	
5046	FA					Y	
5047	P					Y	
5048	T					Y	
5049	PT	26-PT-375				Y	
5050	L					Y	



New-Indy – Catawba Mill  
 LDAR Inspection and Testing Diagrams  
 Combination Boiler SOG and LVHC Incineration

Rev. Date  
 January 2021  
 Figure 5



Vent Gases  
 Condensates  
 Liquor/Stock Lines  
 Process Lines

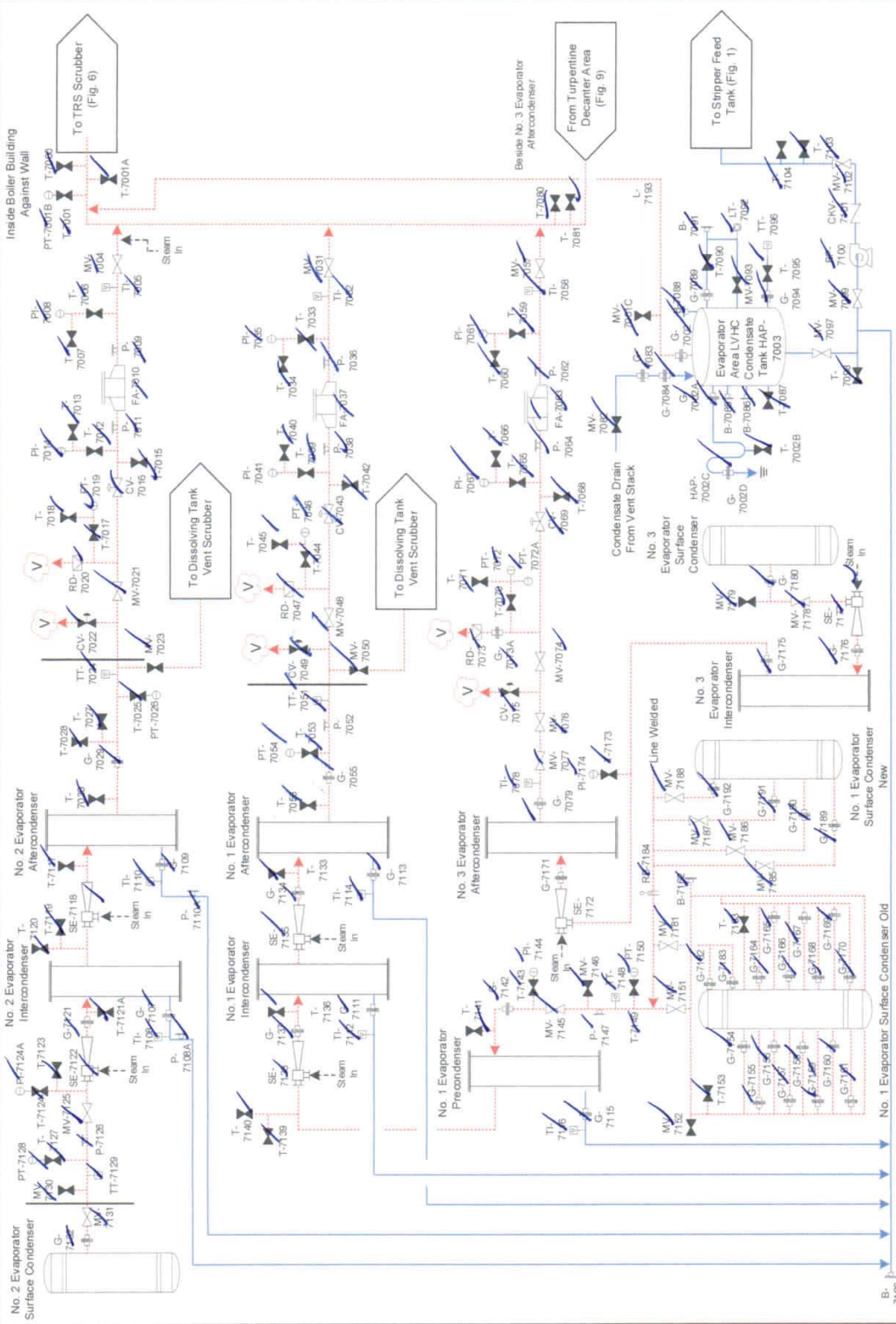
To Another Page and Indicated Equipment  
 From Another Page and Indicated Equipment



New-Indy – Catawba Mill  
 LDAR Inspection and Testing Diagrams  
 TRS Scrubber Platform

Rev. Date  
 January 2021  
 Figure 6



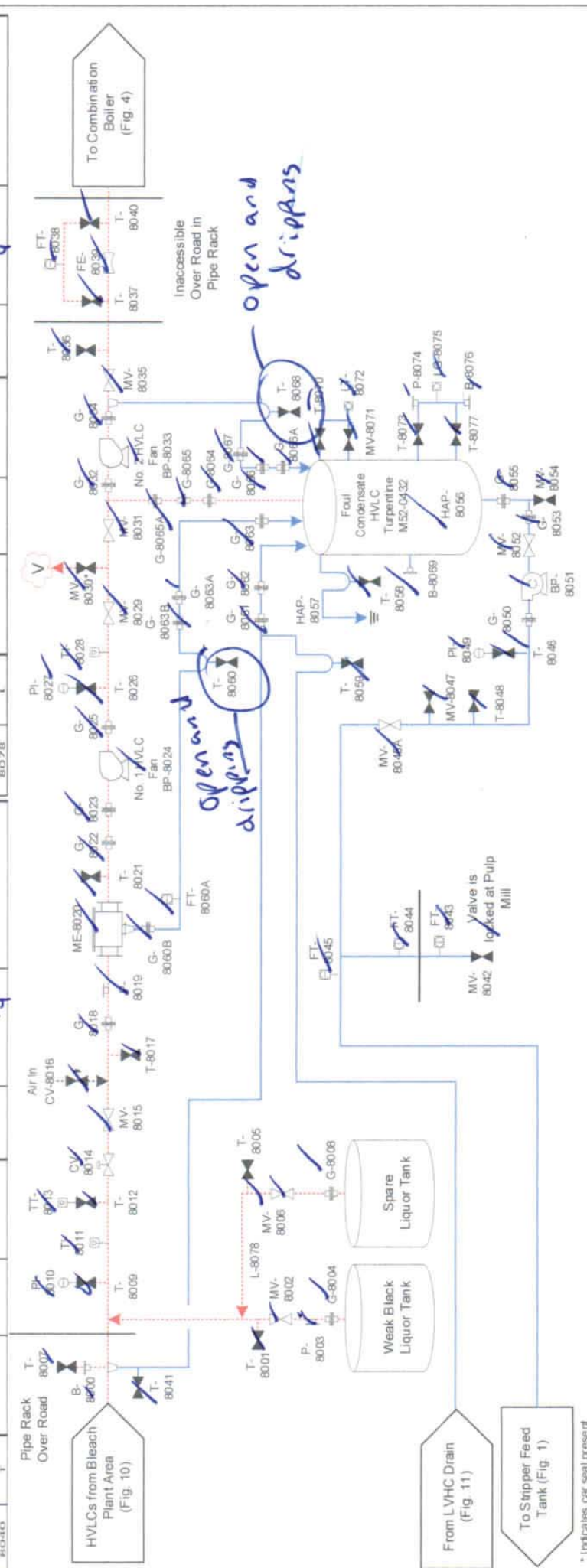


			<p>Rev. Date January 2021</p> <p>New-Indy – Catawba Mill LDAR Inspection and Testing Diagrams Evaporator System</p> <p>Figure 7</p>
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HVLC Blower Platform		2/17/21	
Number	Type	Equip. Number	Pressure (psig)
8000	B		
8001	T		
8002	MV		
8003	P		
8004	G		
8005	T		
8006	MV		
8007	T		
8008	G		
8009	PI		
8010	PI		
8011	TI		
8012	T		
8013	TI		
8014	CV	54-PV-953	
8015	MV	26-MV-0618	
8016	CV		
8017	T	26-MV-0619	
8018	G		
8019	P		
8020	M/E		
8021	T		
8022	G		
8023	G		
8024	BP	M52-0412	
8025	G		
8026	T		
8027	PI	52-PI-958	
8028	TI		
8029	MV	26-MV-0670	
8030	MV		
8031	MV		
8032	BP		
8033	BP	M52	
8034	G		
8035	MV	26-MV-0622	
8036	T		
8037	FT		
8038	FT		
8039	FT		
8040	T		



Number	Type	Equip. Number	Pressure (psig)	Is Component Free of Leaks or Defects?	Comments
8041	T			Yes	
8042	MV			Yes	
8043	FT			Yes	
8044	FT			Yes	
8045	MV			Yes	
8046	T			Yes	
8047	MV			Yes	
8048	T			Yes	
8049	G			Yes	
8050	G			Yes	
8051	BP			Yes	
8052	MV			Yes	
8053	G			Yes	
8054	MV			Yes	
8055	G			Yes	
8056	HAP			Yes	
8057	HAP			Yes	
8058	T			Yes	
8059	T			Yes	
8060	T			Yes	
8060A	FT			Yes	
8060B	G			Yes	
8061	G			Yes	
8062	G			Yes	
8063	G			Yes	
8064	G			Yes	
8065	G			Yes	
8065A	G			Yes	
8066	G			Yes	
8066A	G			Yes	
8067	G			Yes	
8068	G			Yes	
8069	PI			Yes	
8070	TI			Yes	
8071	MV			Yes	
8072	LT			Yes	
8073	T			Yes	
8074	P			Yes	
8075	LG			Yes	
8076	B			Yes	
8077	T			Yes	
8078	T			Yes	

Number	Type	Equip. Number	Pressure (psig)	Background	VOC Reading	Comments
8041	T					
8042	MV					
8043	FT					
8044	FT					
8045	MV					
8046	T					
8047	MV					
8048	T					
8049	G					
8050	G					
8051	BP					
8052	MV					
8053	G					
8054	MV					
8055	G					
8056	HAP					
8057	HAP					
8058	T					
8059	T					
8060	T					
8060A	FT					
8060B	G					
8061	G					
8062	G					
8063	G					
8064	G					
8065	G					
8065A	G					
8066	G					
8066A	G					
8067	G					
8068	G					
8069	PI					
8070	TI					
8071	MV					
8072	LT					
8073	T					
8074	P					
8075	LG					
8076	B					
8077	T					
8078	T					

Number	Type	Equip. Number	Pressure (psig)	Background	VOC Reading	Comments
8041	T					
8042	MV					
8043	FT					
8044	FT					
8045	MV					
8046	T					
8047	MV					
8048	T					
8049	G					
8050	G					
8051	BP					
8052	MV					
8053	G					
8054	MV					
8055	G					
8056	HAP					
8057	HAP					
8058	T					
8059	T					
8060	T					
8060A	FT					
8060B	G					
8061	G					
8062	G					
8063	G					
8064	G					
8065	G					
8065A	G					
8066	G					
8066A	G					
8067	G					
8068	G					
8069	PI					
8070	TI					
8071	MV					
8072	LT					
8073	T					
8074	P					
8075	LG					
8076	B					
8077	T					
8078	T					

ENVIRONMENTAL 360

New-Indy - Catawba Mill

LDAR Inspection and Testing Diagrams

HVLC Blower Platform

Rev. Date

January 2021

Figure 8

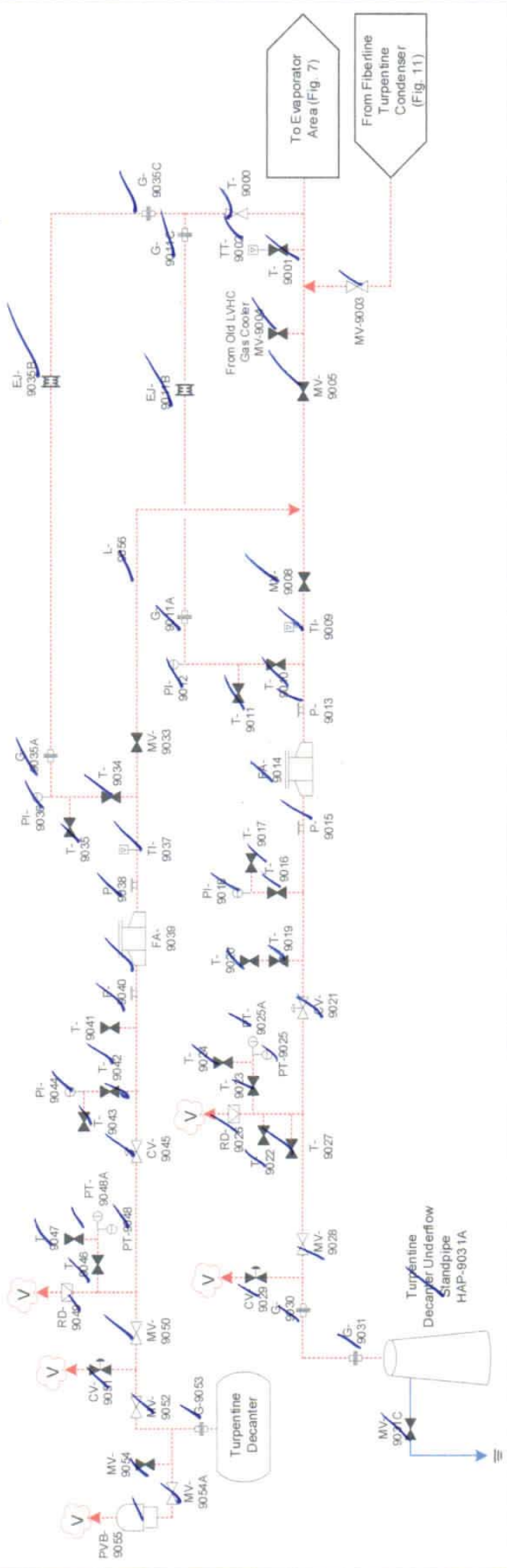
\* Indicates car seal present

Legend:

- Vent Gases
- Condensates
- Liquor/Stock Lines
- Process Lines
- ◁ To Another Page and Indicated Equipment
- ▷ From Another Page and Indicated Equipment

Number	Type	Equip. Number	Pressure (#/in)	Background	VOC Reading	Is Component Free of Leaks or Defects?	Comments
9000	T					Yes	
9001	T					Yes	
9002	TT					Yes	
9003	MV	14-MV-0312				Yes	
9004	MV					Yes	
9005	MV					Yes	
9008	MV	14-TI/TW-125				Yes	
9009	TI					Yes	
9010	T					Yes	
9011	T					Yes	
9011A	G					Yes	
9011B	EJ					Yes	
9011C	G					Yes	
9012	PI					Yes	
9013	P					Yes	
9014	FA					Yes	
9015	P					Yes	
9016	T					Yes	
9017	T					Yes	
9018	PI	14-PI-125A				Yes	
9019	T					Yes	
9020	T					Yes	
9021	CV	14-HV-127				Yes	
9022	T					Yes	
9023	T					Yes	
9024	T					Yes	
9025	PT	14-PSH-122				Yes	
9025A	PT	14-PSH-122				Yes	
9026	RD					Yes	
9027	T					Yes	
9028	MV					Yes	

9029	CV	14-HV-126					
9030	G						
9031	G						
9031A	HAP						
9031C	MV						
9033	MV	14-MV-0330					
9034	T						
9035	T						
9035A	G						
9035B	EJ						
9035C	G						
9036	PI						
9037	TI	14-TI/TW-304B					
9038	P						
9039	FA	M14-0121					
9040	P						
9041	T						
9042	T						
9043	T						
9044	PI						
9045	CV	14-HV-314					
9046	T						
9047	T						
9048	PT	14-PSH-313					
9048A	PT	14-PSH-313					
9049	RD						
9050	MV	14-MV-0342					
9051	CV	14-HV-312					
9052	MV	14-MV-0343					
9053	G						
9054	MV						
9054A	MV						
9055	PRV						
9056	L						



Completed Date/Time: 2/19/21

Rev. Date  
January 2021

New-Indy - Catawba Mill

LDAR Inspection and Testing Diagrams

Turpentine Decanter and Standpipe

Figure 9

To Another Page and Indicated Equipment

From Another Page and Indicated Equipment

Vent Gases

Condensates

Liquor/Stock Lines

Process Lines

To Evaporator Area (Fig. 7)

From Fiberline Turpentine Condenser (Fig. 11)



**Turpentine Cooler and Blow Tank**

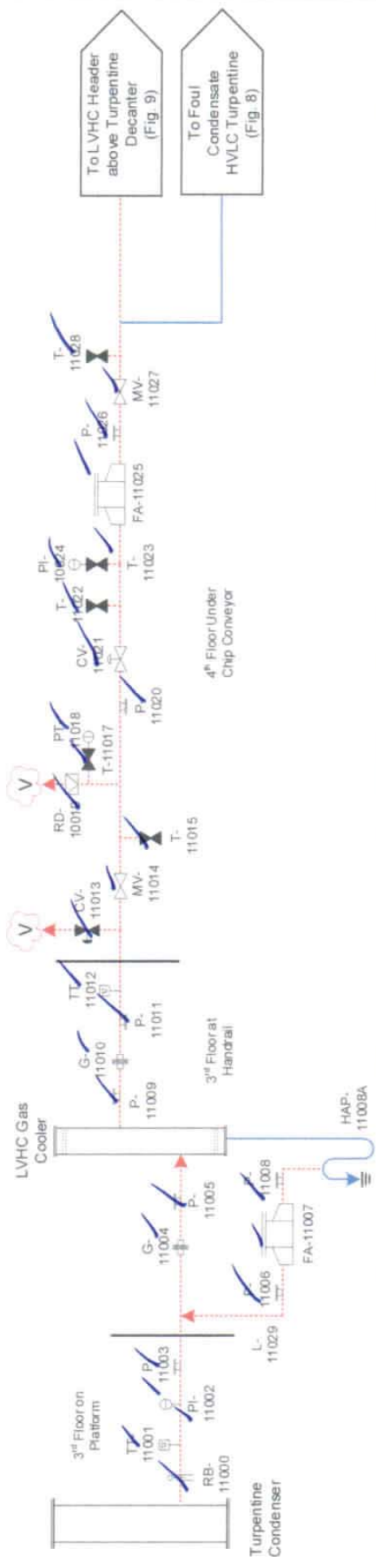
Completed Date/Time: 2/17/21

Number	Type	Equip. Number	Pressure (+/-)	Background	VOC Reading	Is Component Free of Leaks or Defects?	Comments
10000	G					yes	
10001	TT	52-TE-230				y	
10002	P					y	
10003	CV	52-QV-937				y	
10004	MV	52-MV-1021				y	
10005	T					y	
10006	PT	52-PSH-934				y	
10007	PI					y	
10008	RD					y	
10009	CV	52-EV-938				y	
10010	G					y	
10011	P					y	
10012	FA	M52-0429				y	
10013	P					y	
10014	MV	52-MV-1022				y	
10015	T					y	
10016	PI					y	
10017	TI					y	
10018	T					y	
10019	PT					y	
10020	CV	52-PV-941				y	
10021	CV					y	
10021A	G					y	
10022	P					y	
10023	ME	M52-0415				y	
10024	P					y	
10025	G					y	
10026	BP	M52-0411				y	
10027	G					y	
10028	T					y	
10029	FT					y	
10030	FE					y	
10031	T					y	
10032	MV					y	Car seal present.
10033	MV					y	
10034	B					y	
10034A	T					y	
10035	TT	52-TT-947				y	

10035A	G						yes
10035B	MV						y
10035C	MV						y
10035D	P						y
10035E	T						y
10035F	MV						y
10035G	P						y
10035H	P						y
10035I	G						y
10035J	T						y
10035K	P						y
10035L	TT						y
10036	MV						y
10037	MV						y
10038	P						y
10039	MV						y
10039A	T						y
10039B	RB						y
10040	MV						y
10041	B						y
10042	T						y
10043	P						y
10044	TI						y
10045	P						y
10046	MV						y
10047	P						y
10047A	T						y
10048	MV	A507					y
1052	G						y
1053	PRV						y
1054	T						y
1055	P						y
1056	MV						y
1057	P						y
1058	P						y
1059	B						y
1060	P						y
1061	B						y
1062	T						y
1063	PT	52-PT-215					y
1064	L						y

**Turpentine Condenser and LVHC Gas Cooler**  
 Completed Date/Time: 2/17/21

Number	Type	Equip. Number	Pressure (+/-)	Background	VOC Reading	Is Component Free of Leaks or Defects?	Comments
11000	RB					YES ✓	
11001	TT	52-TE-222A				✓	
11002	PI					✓	
11003	P					✓	
11004	G					✓	
11005	P					✓	
11006	P					✓	
11007	FA	M52-0512				✓	
11008	P					✓	
11008A	HAP					✓	
11009	P					✓	
11010	G					✓	
11011	P					✓	
11012	TT	52-TE-225				✓	
11013	CV	52-HV-174B				✓	
11014	MV	52-A-368				✓	
11015	T					✓	
11017	T					✓	
11018	PT	52-PSH-226				✓	
11019	RD					✓	
11020	P					✓	
11021	CV	52-HV-174A				✓	
11022	T	52-A-428				✓	
11023	T					✓	
11024	PI	52-PI-226				✓	
11025	FA	Z00-0395M				✓	
11026	P					✓	
11027	MV	52-A-541				✓	
11028	T	52-A-437				✓	
11029	L					✓	



**ENVIRONMENTAL 360**

To Another Page and Indicated Equipment

From Another Page and Indicated Equipment

Vent Gases (dotted line)

Condensates (blue line)

Liquor/Stock Lines (red line)

Process Lines (black line)

New-Indy – Catawba Mill

LDAR Inspection and Testing Diagrams

Turpentine Condenser and LVHC Gas Cooler

Rev. Date  
January 2021

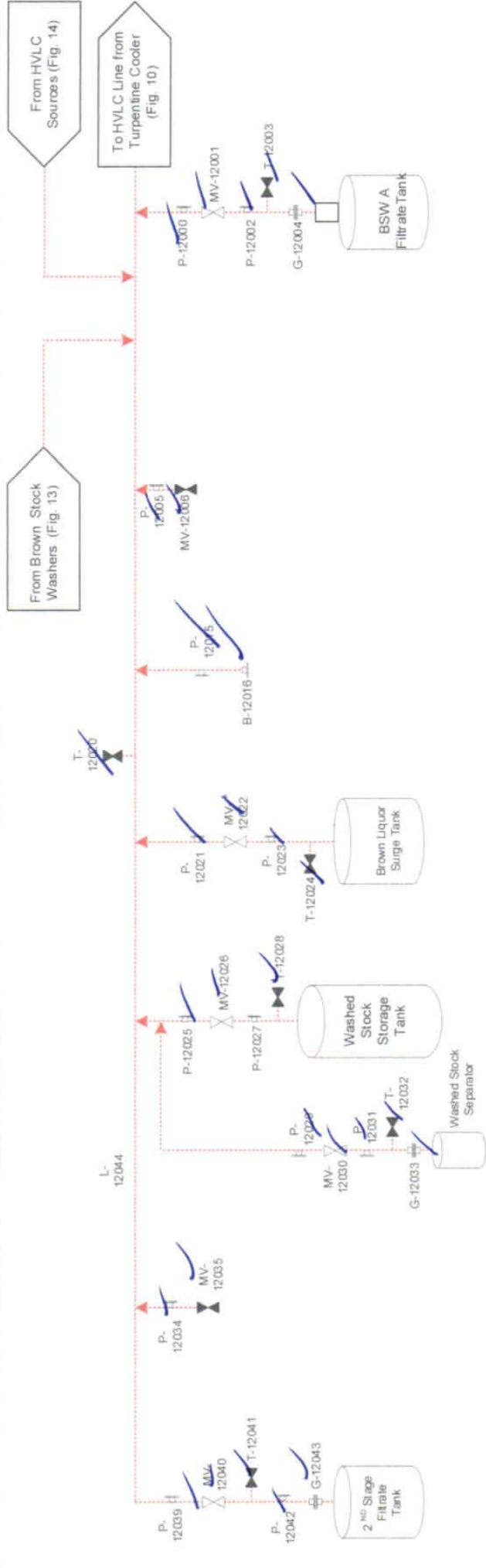
Figure 11

### HVLC System at Pulp Mill (1 of 2)

Completed Date/Time: 2/17/21

Number	Type	Equip. Number	Pressure (+/-)	Background	VOC Reading	Is Component Free of Leaks or Defects?	Comments
12000	P					Yes	
12001	MV					Y	
12002	P					Y	
12003	T	X182				Y	
12004	G					Y	
12005	P					Y	
12006	MV					Y	
12015	P					Y	
12016	B					Y	
12020	T	V4454				Y	
12021	P					Y	
12022	MV	0598-22-HY				Y	
12023	P					Y	
12024	T	D060				Y	

12025	P					Yes	
12026	MV					Y	
12027	P					Y	
12028	T					Y	
12029	P					Y	
12030	MV	F543				Y	
12031	P					Y	
12032	T	F541				Y	
12033	G					Y	
12034	P					Y	
12035	MV	SR307				Y	
29039	P					Y	
29040	MV	SR308				Y	
29041	T					Y	
29042	P					Y	
29043	G					Y	
29044	L					Y	



--- Vent Gases  
--- Condensates  
--- Liquor/Stock Lines  
--- Process Lines

  To Another Page and Indicated Equipment  
  From Another Page and Indicated Equipment

**ENVIRONMENTAL 360**

New-Indy – Catawba Mill

LDAR Inspection and Testing Diagrams  
HVLC System at Pulp Mill (1 of 2)

Rev. Date  
January 2021

Figure 12





Bleach Plant Completed Date/Time: 2/17/21

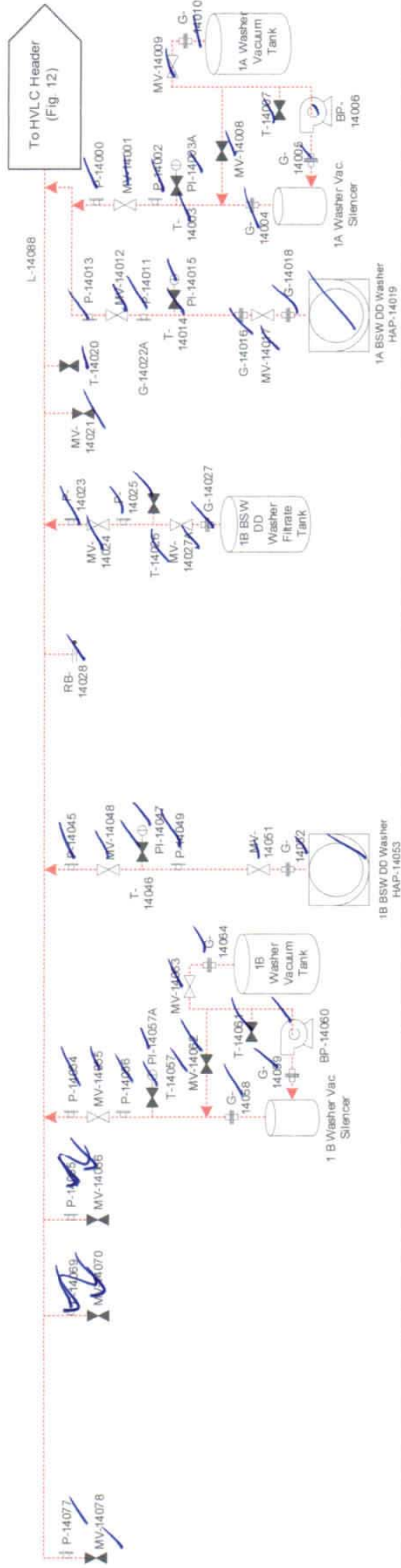
Number	Type	Equip. Number	Pressure (+/-)	Background	VOC Reading	Is Component Free of Leaks or Defects?	Comments
13026	B					Y	
13026A	T					Y	
13027	DV					Y	
13028	B					Y	
13028A	T					Y	
13031	G					Y	
13032	G					Y	
13033	HAP					Y	
13034	B					Y	
13035	MV	F532				Y	
13036	B					Y	
13037	G					Y	
13038	G					Y	
13039	BP	E53-0021				Y	
13040	G					Y	
13041	T	F56				Y	
13042	G					Y	
13043	MV	F99				Y	
13044	MV					Y	
13045	G					Y	
13046	B					Y	
13047	MV					Y	
13050	P					Y	
13051	B					Y	
13054	P					Y	
13055	B					Y	
13057	B					Y	
13058	P					Y	
13059	B					Y	
13061	P					Y	
13062	B					Y	
13064	B					Y	
13065	B					Y	
13066	B					Y	
13067	T					Y	
13068	PI					Y	
13069	MV					Y	
13070	B					Y	
13071	G					Y	
13072	B					Y	
13073	MV	F530				Y	
13074	B					Y	
13075	G					Y	
13076	G					Y	
13077	BP	E53-0046				Y	
13078	G					Y	
13079	T	F195				Y	
13080	MV	F101				Y	
13081	G					Y	
13082	MV					Y	
13083	G					Y	
13084	B					Y	
13084A	T					Y	
13085	MV	F529				Y	
13086	B					Y	
13086A	T					Y	
13088	G					Y	
13088A	B					Y	
13088B	T					Y	
13090	G					Y	
13091	G					Y	
13092	HAP					Y	
13093	P					Y	

13094	B	F528				Y	
13097	B					Y	
13098	MV	F527				Y	
13099	B					Y	
13100	G					Y	
13101	G					Y	
13102	BP					Y	
13103	G					Y	
13104	T	F262				Y	
13105	MV	F248				Y	
13106	G					Y	
13107	MV					Y	
13108	G					Y	
13109	B					Y	
13109A	T					Y	
13110	MV					Y	
13111	B					Y	
13111A	T					Y	
13115	G					Y	
13116	G					Y	
13117	HAP					Y	
13118	B					Y	
13119	DV	F524				Y	
13120	B					Y	
13121	G					Y	
13122	G					Y	
13123	BP	E53-0106				Y	
13124	G					Y	
13125	T	F356				Y	
13126	MV	F293				Y	
13127	G					Y	
13128	MV					Y	
13129	G					Y	
13130	B					Y	
13130A	T					Y	
13131	MV					Y	
13132	B					Y	
13132A	T					Y	
13135	G					Y	
13136	G					Y	
13137	HAP					Y	
13138	P					Y	
13139	B					Y	
13144	L					Y	
13145	HAP					Y	
13146	HAP					Y	
13147	HAP					Y	

**HVLC System at Pulp Mill (2 of 2)**  
 Completed Date/Time: 2/17/21

Number	Type	Equip. Number	Pressure (+/-)	Background	VOC Reading	Is Component Free of Leaks or Defects?	Comments
14000	P					Yes	
14001	MV	X170				Y	
14002	P					Y	
14003	T					Y	
14003A	PI	52-PI-353				Y	
14004	G					Y	
14005	G					Y	
14006	BP	M52-0092				Y	
14007	T	X74				Y	
14008	MV	X240				Y	
14009	MV					Y	
14010	G					Y	
14011	P					Y	
14012	MV	X169				Y	
14013	P					Y	
14014	T	X179				Y	
14015	PI					Y	
14016	G					Y	
14017	MV					Y	
14018	G					Y	
14019	HAP					Y	
14020	T					Y	
14021	MV					Y	
14023	P					Y	
14024	MV	X171				Y	
14025	P					Y	
14026	T					Y	
14027	G					Y	
14027A	MV					Y	
14028	RB					Y	
14045	P					Y	
14046	T					Y	
14047	PI					Y	
14048	MV	X168				Y	
14049	P					Y	
14051	MV					Y	
14052	G					Y	
14053	HAP					Y	
14054	P					Y	
14055	MV	X167				Y	
14056	P					Y	
14057	T					Y	
14057A	PI					Y	
14058	G					Y	
14059	G					Y	
14060	BP	E52-0128				Y	
14061	T	X159				Y	
14062	MV	X265				Y	
14063	MV					Y	
14064	G					Y	
14065	P					Y	
14066	MV	SR313				Y	
14069	P					Y	
14070	MV	SR312				Y	
14077	P					Y	
14078	MV					Y	
14088	L					Y	

Number	Type	Equip. Number	Pressure (+/-)	Background	VOC Reading	Is Component Free of Leaks or Defects?	Comments
14000	P					Yes	
14001	MV	X170				Y	
14002	P					Y	
14003	T					Y	
14003A	PI	52-PI-353				Y	
14004	G					Y	
14005	G					Y	
14006	BP	M52-0092				Y	
14007	T	X74				Y	
14008	MV	X240				Y	
14009	MV					Y	
14010	G					Y	
14011	P					Y	
14012	MV	X169				Y	
14013	P					Y	
14014	T	X179				Y	
14015	PI					Y	
14016	G					Y	
14017	MV					Y	
14018	G					Y	
14019	HAP					Y	
14020	T					Y	
14021	MV					Y	
14023	P					Y	
14024	MV	X171				Y	
14025	P					Y	
14026	T					Y	



--- Vent Gases  
--- Condensates  
--- Liquor/Stock Lines  
--- Process Lines  
  To Another Page and Indicated Equipment  
  From Another Page and Indicated Equipment



New-Indy – Catawba Mill  
 LDAR Inspection and Testing Diagrams  
 HVLC System at Pulp Mill (2 of 2)

Rev. Date  
 January 2021  
 Figure 14

Inspection Date: March 15, 2021



New Indy Containerboard - Catawba Mill  
5300 Cureton Ferry Rd.  
Catawba, SC 29704

**2021 Monthly LDAR Inspection Summary Report**

**Table 1: Visual Inspection Summary Table**

Equipment Number	Date	Description of Leak or Visual Defect
HAP-13092	3/15/2021	The 3A Brown Stock Washer is puffing from hatch door
HAP-13117	3/15/2021	The 2B Brown Stock Washer is puffing from hatch door.
HAP-14053	3/15/2021	The 1B Brown Stock Washer is puffing from hatch door.
<b>First Attempt to Repair must be completed by:</b>	5 Days from Inspection Date	Not Applicable if no leaks were found.
<b>Repairs must be completed by:</b>	15 Days from Inspection Date	Not Applicable if no leaks were found.

This report provides a summary of leaks and visual defects found during the visual inspection of the closed-vent and condensate-collection systems and complies with the record keeping requirements of 63.454(b)(1-2, 4-5).

The facility must initiate repairs to any defects within five (5) calendar days from this inspection and the defects must be repaired within fifteen (15) calendar days of the inspection. If the leak or defect requires the system to be shutdown in order to make repairs, or more emissions would occur from attempting the repair than delaying the repair, then the repairs may be delayed until the next process unit shutdown. A report must be supplied with the repair date and associated information, or the reason for the delay if the repairs are not completed within the 15-day period. These response requirements are specific to 40 CFR 63, specifically 63.453(k)(6), 63.453(l)(3), and 63.964(b)(1-2). Documentation of all repair attempts made and any leaks/defects requiring a process unit shutdown must be completed according to 63.454(b)(6-11).

I certify that the results of the visual inspection are accurate and complete to the best of my knowledge.

Inspector Name: Josh Howard

Signature: Josh Howard



## Inspection QA/QC Procedure

E360 Project Number?	New Indy Catawba
Task Number (if applicable)?	March 2021 Monthly LOAR

### Purpose of Form

To verify field work meets each critical element.

### Visual Work Flow (WF)

**Step 1**

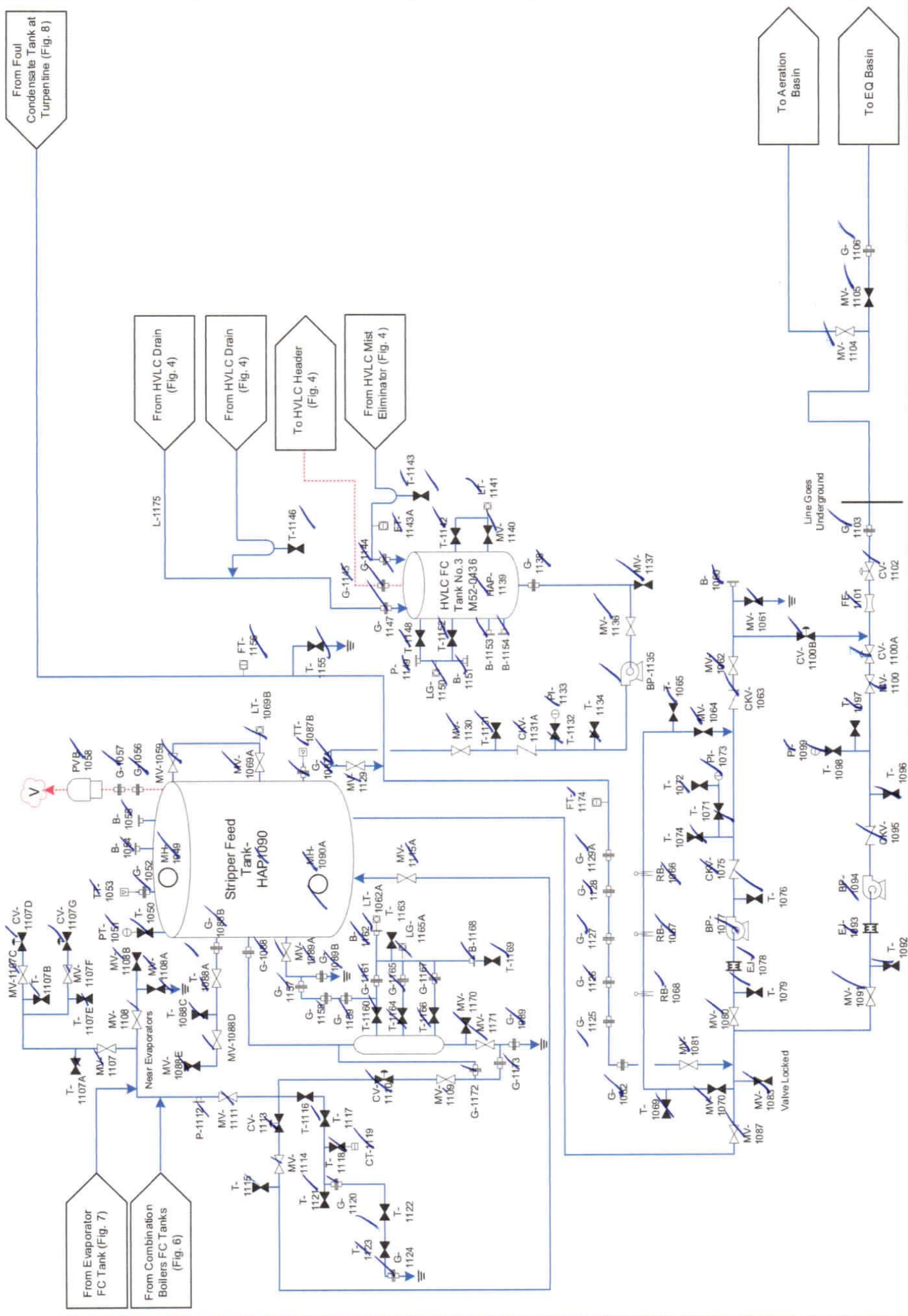
**R** - Verify field work by checking "X" each WF No.

### Verification of Critical Elements

WF No.	Requirement	Yes?
	Work-flow step	1
	Verifier of critical elements for work-flow step	R
1	Was a bump test performed on the personal H <sub>2</sub> S monitor?	✓
2	Have the most recent versions of the inspection forms been used?	✓
3	Were all inspection points identified correctly and inspected correctly?	✓
4	Did the operator/ contact verify to our inspector that all equipment was operating under normal operating conditions?	✓
5	Were any deficiencies identified in person to the client?	✓
6	Were all inspection questions answered with either a Yes, No, or NA?	✓
7	Were inspections performed during the required regulatory time frame?	✓

### Approvals

Role	WF Step	Name	Approval (insert date)
Responsible Person (R)	1	Josh Helet	03/15/2021



From Foul Condensate Tank at Turpentine (Fig. 8)

From HVLC Drain (Fig. 4)  
 From HVLC Drain (Fig. 4)  
 To HVLC Header (Fig. 4)  
 From HVLC Mist Eliminator (Fig. 4)

To Aeration Basin  
 To EQ Basin

Rev. Date  
 February 2021  
 Figure 1

New-Indy - Catawba Mill  
 LDAR Inspection and Testing Diagrams  
 Stripper System Foul Condensate



Vent Gases  
 Condensates  
 Liquor/Stock Lines  
 Process Lines

To Another Page and Indicated Equipment  
 From Another Page and Indicated Equipment

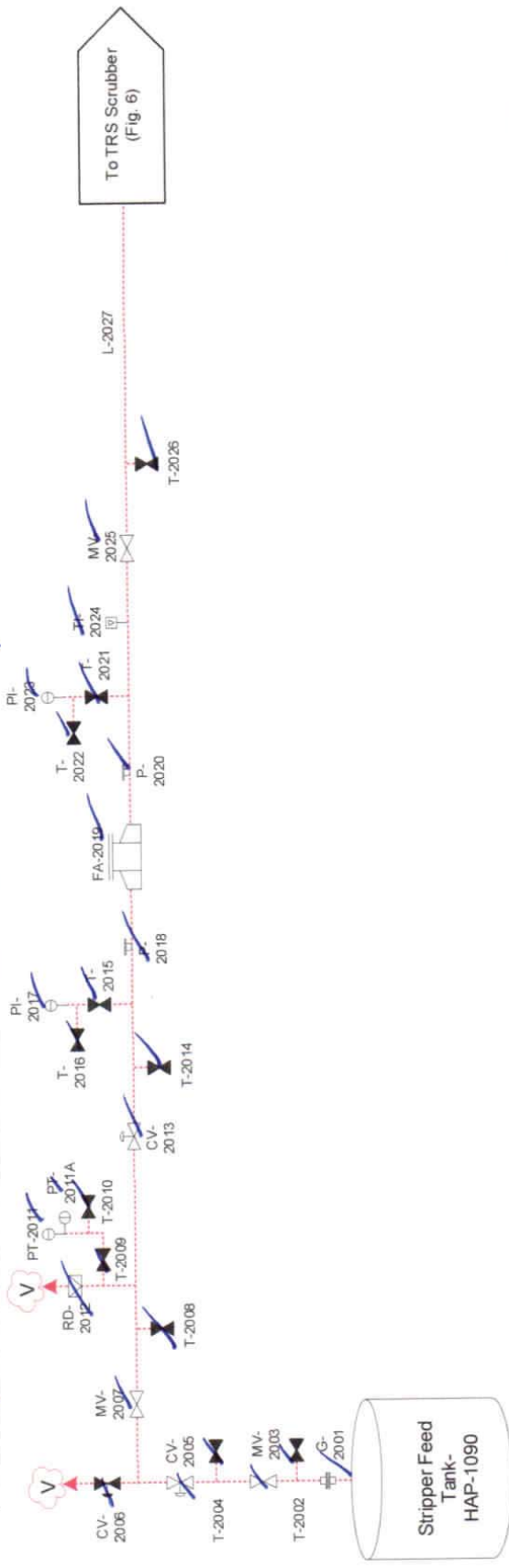
Stripper system roui Conceptual  
 Completed Date/Time: 3/15/21

Number	Type	Equip. Number	Pressure (+/-)	Background	VOC Reading	Is Component Free of Leaks or Defects?	Comments
1049	MH					Yes	
1050	T					Y	
1051	PT					Y	
1052	G					Y	
1053	TT					Y	
1054	B					Y	
1055	B					Y	
1056	G					Y	
1057	G					Y	
1058	PVB					Y	
1059	MV					Y	
1060	B					Y	
1061	MV	24-MV-0361				Y	
1062	MV	24-MV-0359				Y	
1062A	LT					Y	
1063	CKV					Y	
1064	MV	24-MV-0445				Y	
1065	T					Y	
1066	RB					Y	
1067	RB					Y	
1068	RB					Y	
1069	T					Y	
1069A	MV					Y	
1069B	LT					Y	
1070	MV	51-LT-265 24-MV-445				Y	
1071	T					Y	
1072	T					Y	
1073	PI					Y	
1074	T					Y	
1075	CKV					Y	
1076	T					Y	
1077	BP					Y	
1078	EJ					Y	
1079	T					Y	
1080	MV	24-MV-363				Y	
1081	MV					Y	
1082	G					Y	
1083	MV	V704F				Y	
1087	MV	24-MV-362				Y	
1087A	G					Y	
1087B	TT	51-TT-266				Y	
1088	G					Y	
1088A	T					Y	
1088B	G					Y	
1088C	T					Y	
1088D	MV					Y	
1088E	MV					Y	
1089	G					Y	
1089A	MV	24-MV-0352				Y	
1089B	G					Y	
1090	HAP					Y	
1090A	MH					Y	
1091	MV	24-MV-0365				Y	
1092	T					Y	
1093	EJ					Y	
1094	BP					Y	
1095	CKV	V884F				Y	
1096	T					Y	
1097	T					Y	
1098	T					Y	
1099	PI					Y	
1100	MV	24-MV-360				Y	
1100A	CV					Y	
1100B	CV					Y	
1101	FE					Y	
1102	CV	51-FCV-267				Y	
1103	G					Y	
1104	MV					Y	
1105	MV					Y	
1106	G					Y	
1107	MV					Y	
1107A	T					Y	
1107B	T					Y	
1107C	MV					Y	
1107E	T					Y	
1107F	MV					Y	
1107G	CV					Y	
1108	MV					Y	
1108A	MV					Y	
1108B	MV					Y	
1109	MV					Y	
1110	CV					Y	
1111	MV					Y	
1112	P					Y	
1113	CV					Y	
1114	MV					Y	
1115	T					Y	
1115A	MV					Y	
1116	T					Y	
1117	T					Y	
1118	T					Y	
1119	CT					Y	
1120	G					Y	
1121	T					Y	
1122	T					Y	
1123	T					Y	
1124	G					Y	
1125	G					Y	
1126	G					Y	
1127	G					Y	
1128	G					Y	
1129	MV					Y	
1129A	G					Y	
1130	MV					Y	
1131	T					Y	
1131A	CKV					Y	
1132	T					Y	
1133	PI					Y	
1134	T					Y	
1135	BP					Y	
1136	MV					Y	
1137	MV					Y	
1138	G					Y	
1139	HAP	M52-0436				Y	
1140	MV					Y	
1141	LT					Y	
1142	T					Y	
1143	T					Y	
1143A	FT					Y	
1144	G					Y	
1145	G					Y	
1146	T					Y	
1147	G					Y	
1148	T					Y	
1149	P					Y	
1150	LG					Y	
1151	B					Y	
1152	T					Y	
1153	B					Y	
1154	B					Y	
1155	T					Y	
1156	FT					Y	
1157	G					Y	
1158	G					Y	
1159	G					Y	
1160	T					Y	
1161	G					Y	
1162	B					Y	
1163	T					Y	
1164	T					Y	
1165	G					Y	
1165A	LG					Y	
1166	T					Y	
1167	G					Y	
1168	B					Y	
1169	T					Y	
1170	MV					Y	
1171	MV					Y	
1172	G					Y	
1173	G					Y	
1174	FT					Y	

**Stripper Feed Tank**

Completed Date/Time: 3/15/21

Number	Type	Equip. Number	Pressure (+/-)	Background	VOC Reading	Is Component Free of Leaks or Defects?	Comments
2001	G					Yes	
2002	T					Y	
2003	MV					Y	
2004	T					Y	
2005	CV	51-PCV-264				Y	
2006	CV	51-HV-262				Y	
2007	MV	51-MV-0672				Y	
2008	T					Y	
2009	T					Y	
2010	T					Y	
2011	PT	51-PSH-261				Y	
2011A	PT					Y	
2012	RD					Y	
2013	CV	51-HV-260				Y	
2014	T	51-MV-0675				Y	
2015	T					Y	
2016	T					Y	
2017	PI					Y	
2018	P					Y	
2019	FA	M51-0546				Y	
2020	P					Y	
2021	T					Y	
2022	T					Y	
2023	PI	51-PI-268B				Y	
2024	TI	01-TI-274				Y	
2025	MV	51-MV-0673				Y	
2026	T	24-MV-0353				Y	
2027	L					Y	



\* Indicates car seal present



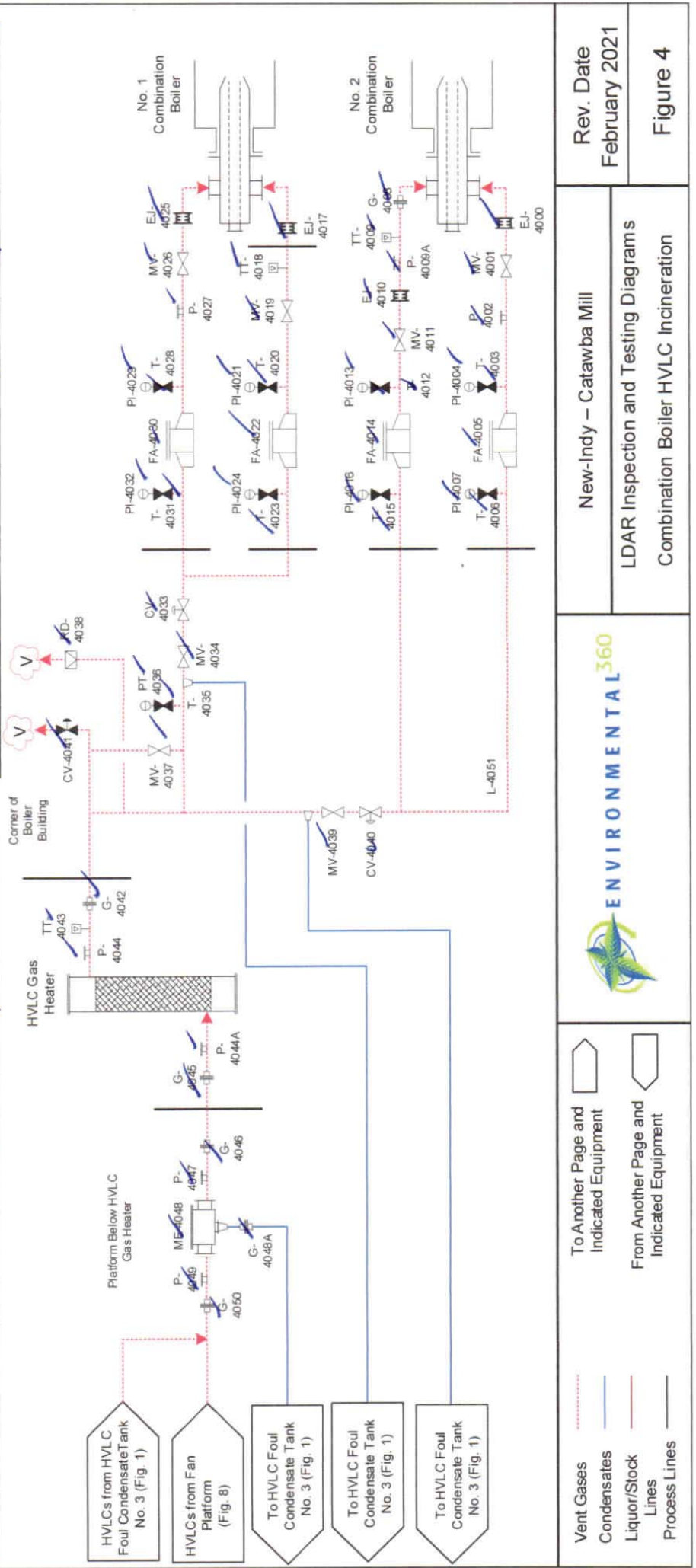
New-Indy – Catawba Mill  
LDAR Inspection and Testing Diagrams  
Stripper Feed Tank

Rev. Date  
February 2021

Figure 2

Number	Type	Equip. Number	Pressure (+/-)	Background	VOC Reading	Is Component Free of Leaks or Defects?	Comments
4000	EJ					YES	
4001	MV	37-MV-0271				Y	
4002	P					Y	
4003	T					Y	
4004	PI					Y	
4005	FA					Y	
4006	T					Y	
4007	PI					Y	
4008	G					Y	
4009	TT					Y	
4009A	P					Y	
4010	EJ					Y	
4011	MV	37-MV-0270				Y	
4012	T					Y	
4013	PI					Y	
4014	FA					Y	
4015	T					Y	
4016	PI					Y	
4017	EJ					Y	
4018	TT					Y	
4019	MV	26-MV-0628				Y	
4020	T	BOP271				Y	
4021	PI					Y	
4022	FA	M52-0426				Y	
4023	T	BOP270				Y	
4024	PI	52-PI-930				Y	
4025	EJ					Y	
4026	MV					Y	
4027	P					Y	
4028	T					Y	
4029	PI					Y	
4030	FA					Y	
4031	T					Y	
4032	PI					Y	
4033	CV					Y	
4034	MV	26-MV-0626				Y	
4035	T					Y	
4036	PT	52-PSH-960				Y	
4037	MV	52-MV-0625				Y	
4038	RD					Y	
4039	MV					Y	
4040	CV					Y	
4041	CV					Y	
4042	G	52-TT-965				Y	
4043	TT					Y	
4044	P					Y	
4044A	P					Y	
4045	G					Y	
4046	G					Y	
4047	P					Y	
4048	ME					Y	
4048A	G					Y	
4049	P					Y	
4050	G					Y	
4051	L					Y	

Combination Boiler HVLC Incinerator!	Completed Date/Time:	3/15/21					
Number	Type	Equip. Number	Pressure (+/-)	Background	VOC Reading	Is Component Free of Leaks or Defects?	Comments
4000	EJ					YES	
4001	MV	37-MV-0271				Y	
4002	P					Y	
4003	T					Y	
4004	PI					Y	
4005	FA					Y	
4006	T					Y	
4007	PI					Y	
4008	G					Y	
4009	TT					Y	
4009A	P					Y	
4010	EJ					Y	
4011	MV	37-MV-0270				Y	
4012	T					Y	
4013	PI					Y	
4014	FA					Y	
4015	T					Y	
4016	PI					Y	
4017	EJ					Y	
4018	TT					Y	
4019	MV	26-MV-0628				Y	
4020	T	BOP271				Y	
4021	PI					Y	
4022	FA	M52-0426				Y	
4023	T	BOP270				Y	



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New-Indy – Catawba Mill  
LDAR Inspection and Testing Diagrams  
Combination Boiler HVLC Incineration



To Another Page and Indicated Equipment  
From Another Page and Indicated Equipment

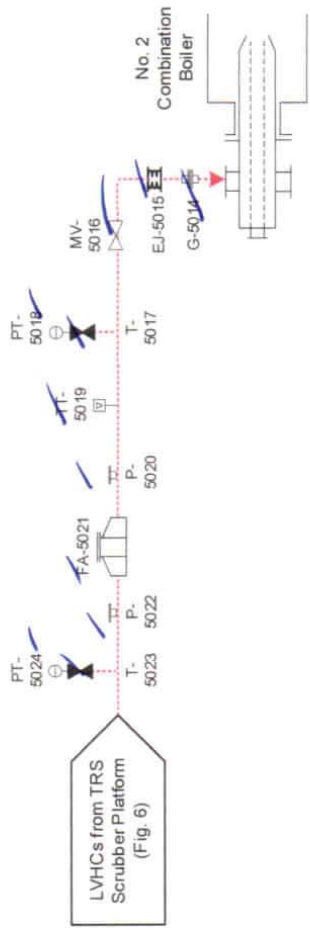
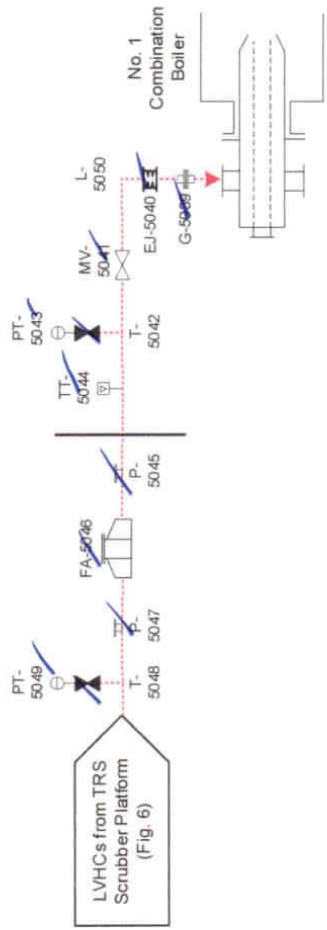
Vent Gases  
Condensates  
Liquor/Stock Lines  
Process Lines



Combination Boiler LVHC Incineration

Completed Date/Time: 3/15/21

Number	Type	Equip. Number	Pressure (+/-)	Background	VOC Reading	Is Component Free of Leaks or Defects?	Comments
5014	G					Yes	
5015	EJ					Y	
5016	MV	37-MV-0313				Y	
5017	T					Y	
5018	PT	37-PT-385				Y	
5019	TT	37-TT-384				Y	
5020	P					Y	
5021	FA					Y	
5022	P					Y	
5023	T					Y	
5024	PT	37-PT-383				Y	
5039	G					Y	
5040	EJ					Y	
5041	MV	26-MV-0532				Y	
5042	T					Y	
5043	PT	26-PT-377				Y	
5044	TT					Y	
5045	P					Y	
5046	FA					Y	
5047	P					Y	
5048	T					Y	
5049	PT	26-PT-375				Y	
5050	L					Y	



Vent Gases: Condensates: Liquor/Stock Lines: Process Lines:

To Another Page and Indicated Equipment: From Another Page and Indicated Equipment:



New-Indy – Catawba Mill  
 LDAR Inspection and Testing Diagrams  
 Combination Boiler LVHC Incineration

Rev. Date  
 February 2021  
 Figure 5

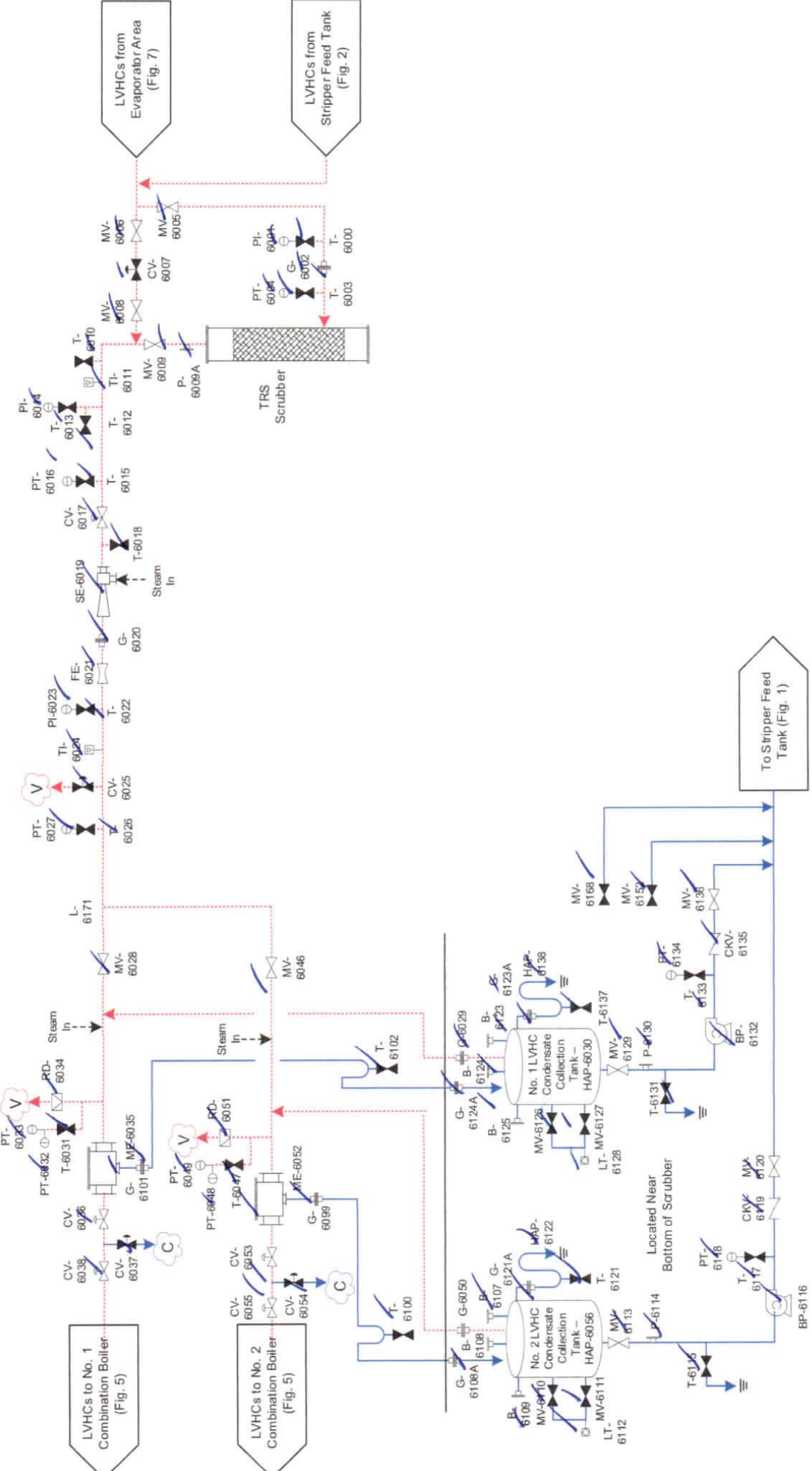
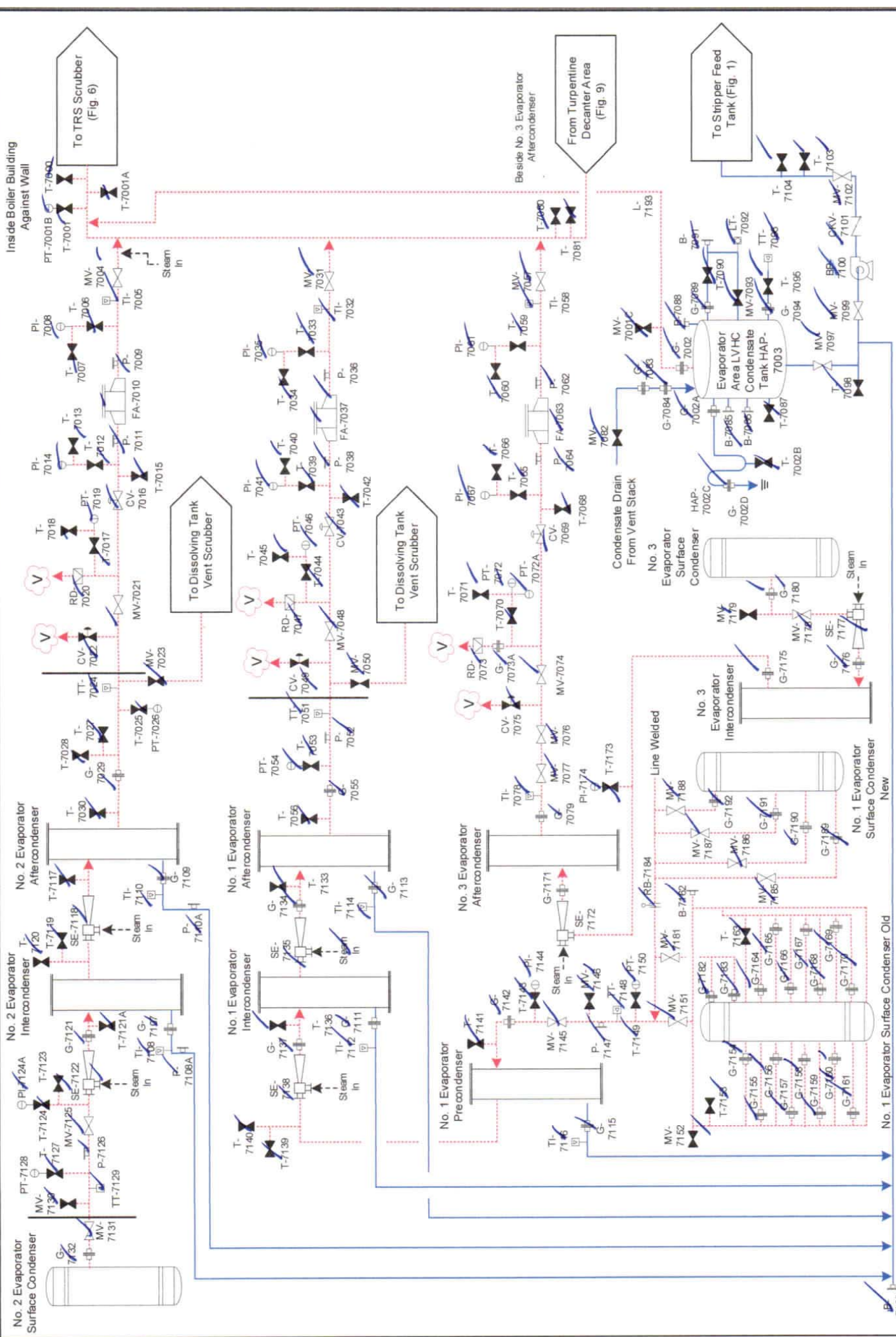


Figure 6





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New-Indy – Catawba Mill  
LDAR Inspection and Testing Diagrams  
Evaporator System

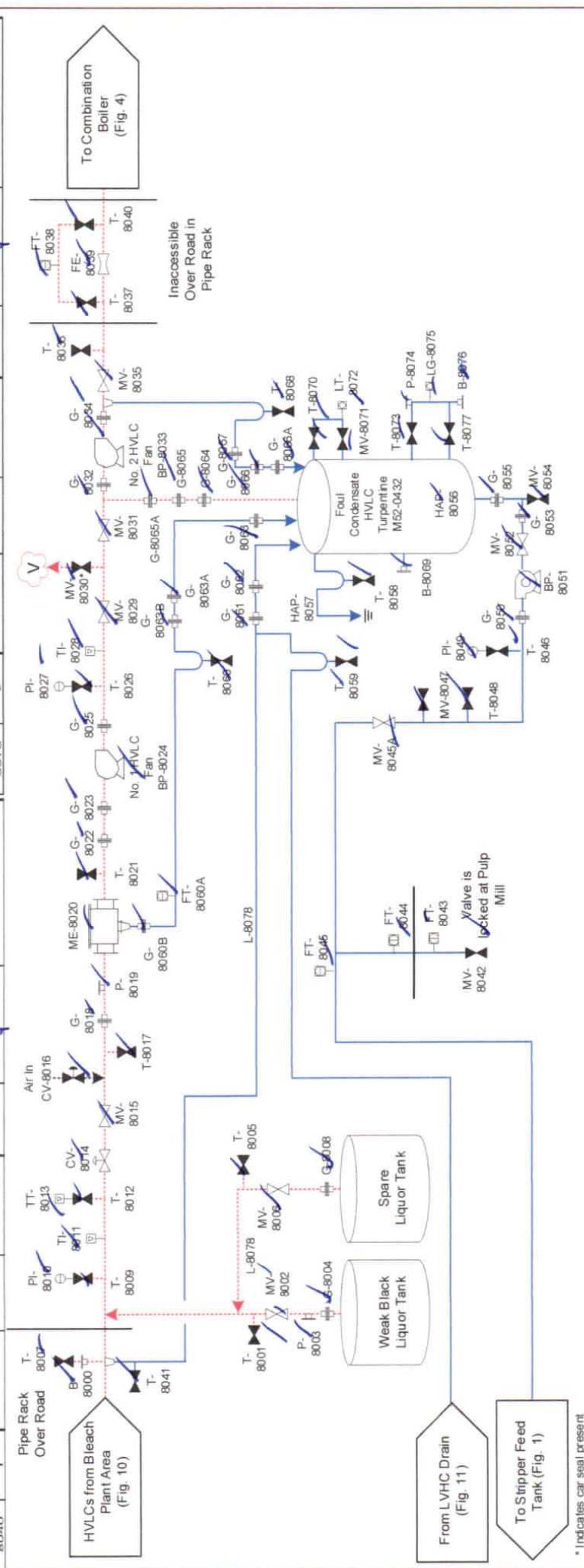


To Another Page and Indicated Equipment  
From Another Page and Indicated Equipment

Vent Gases  
Condensates  
Liquor/Stock Lines  
Process Lines



HVLC Blower Platform				
Number	Type	Equip. Number	Pressure (P/S)	Background
8000	B			
8001	B			
8002	MV			
8003	P			
8004	G			
8005	MV			
8007	T			
8008	T			
8009	P			
8010	PI			
8011	TI			
8012	T			
8013	TT			
8014	CV	54-PV-953		
8015	MV	26-MV-0618		
8016	CV	26-MV-0619		
8017	T			
8018	G			
8019	P			
8020	ME			
8021	T			
8022	G			
8023	T			
8024	BP	M52-0412		
8025	G			
8026	T			
8027	PI	5.2-PI-958		
8028	TI			
8029	MV	26-MV-0670		
8030	MV			
8031	MV			
8032	CV			
8033	BP	M52		
8034	G			
8035	MV	26-MV-0622		
8036	T			
8037	T			
8038	FE			
8039	T			
8040	T			



Completed Date/Time: 3/15/21

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February 2021

Is Component Free of Leaks of Detects? **YES**

New-Indy – Catawba Mill  
LDAR Inspection and Testing Diagrams  
HVLC Blower Platform

Legend:

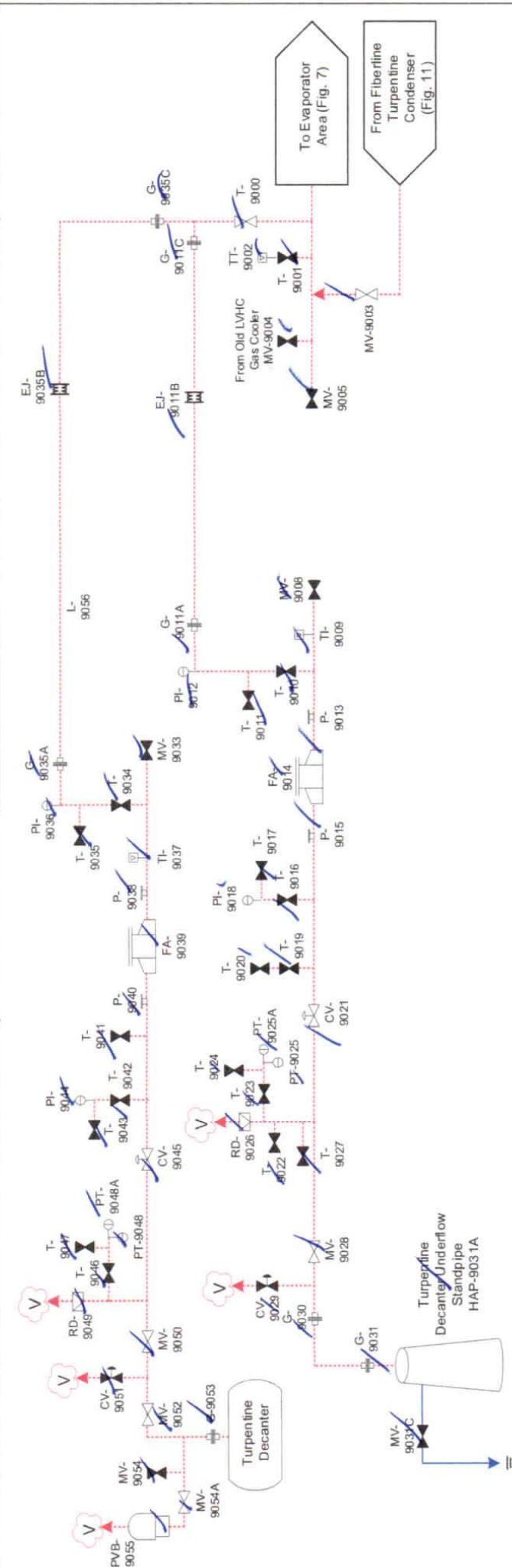
- Vent Gases
- Condensates
- Liquor/Stock Lines
- Process Lines

- To Another Page and Indicated Equipment
- From Another Page and Indicated Equipment

\* Indicates car seal present

**Turpentine Decanter and Standpipe**  
 Completed Date/Time: **3/15/21**

Number	Type	Equip. Number	Pressure (+/-)	Background	VOC Reading	Is Component Free of Leaks or Defects?	Comments
9000	T					Yes	
9001	T					Y	
9002	TT					Y	
9003	MV	14-MV-0312				Y	
9004	MV					Y	
9005	MV					Y	
9008	MV	14-TI/TW-125				Y	
9009	TI					Y	
9010	T					Y	
9011	T					Y	
9011A	G					Y	
9011B	EJ					Y	
9011C	G					Y	
9012	PI					Y	
9013	P					Y	
9014	FA					Y	
9015	P					Y	
9016	T					Y	
9017	T					Y	
9018	PI	14-PI-125A				Y	
9019	T					Y	
9020	T					Y	
9021	CV	14-HV-127				Y	
9022	T					Y	
9023	T					Y	
9024	T					Y	
9025	PT	14-PSH-122				Y	
9025A	PT	14-PSH-122				Y	
9026	RD					Y	
9027	T					Y	
9028	MV					Y	



ENVIRONMENTAL 360

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New-Indy – Catawba Mill

LDAR Inspection and Testing Diagrams

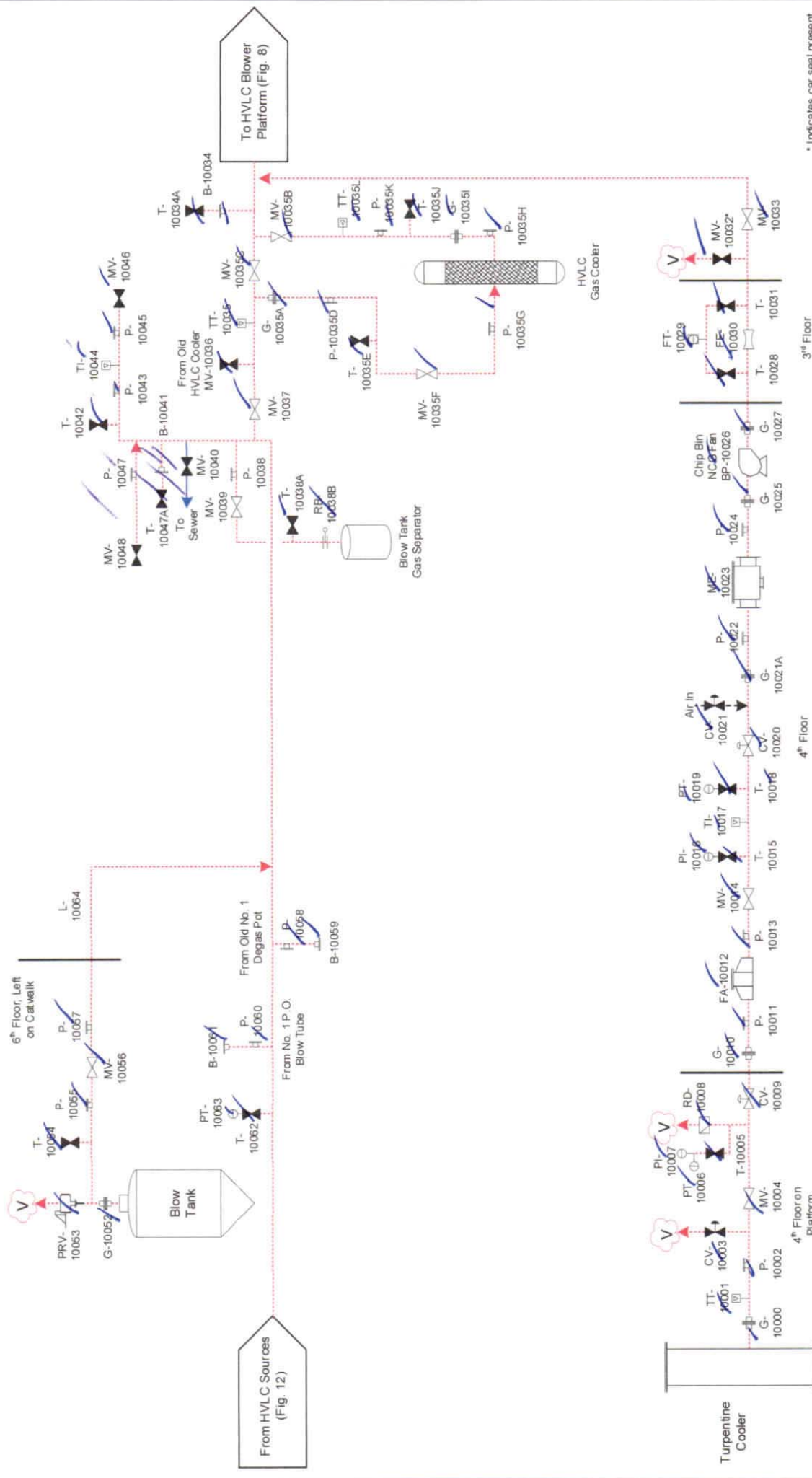
Turpentine Decanter and Standpipe

To Another Page and Indicated Equipment

From Another Page and Indicated Equipment

To Evaporator Area (Fig. 7)

From Fibertine Turpentine Condenser (Fig. 11)



\* Indicates car seal present

Rev. Date	February 2021
Figure	Figure 10

New-Indy – Catawba Mill
LDAR Inspection and Testing Diagrams
Turpentine Cooler and Blow Tank



<p>--- Vent Gases</p> <p>— Condensates</p> <p>— Liquor/Stock Lines</p> <p>— Process Lines</p>	<p>◁ To Another Page and Indicated Equipment</p> <p>▷ From Another Page and Indicated Equipment</p>
---	---



**Turpentine Cooler and Blow Tank**

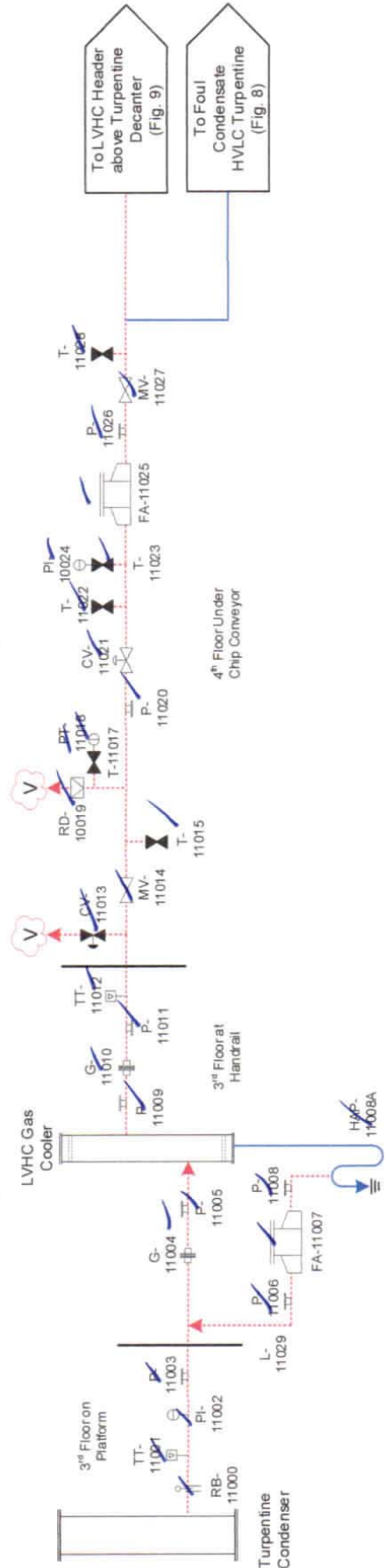
Completed Date/Time: 3/15/21

Number	Type	Equip. Number	Pressure (+/-)	Background	VOC Reading	Is Component Free of Leaks or Defects?	Comments
10000	G					yes	
10001	TT	52-TE-230				y	
10002	P					y	
10003	CV	52-QV-937				y	
10004	MV	52-MV-1021				y	
10005	T					y	
10006	PT	52-PSH-934				y	
10007	PI					y	
10008	RD					y	
10009	CV	52-EV-938				y	
10010	G					y	
10011	P					y	
10012	FA	M52-0429				y	
10013	P					y	
10014	MV	52-MV-1022				y	
10015	T					y	
10016	PI					y	
10017	TI					y	
10018	T					y	
10019	PT					y	
10020	CV	52-PV-941				y	
10021	CV					y	
10021A	G					y	
10022	P					y	
10023	ME	M52-0415				y	
10024	P					y	
10025	G					y	
10026	BP	M52-0411				y	
10027	G					y	
10028	T					y	
10029	FT					y	
10030	FE					y	
10031	T					y	
10032	MV					y	Car seal present.
10033	MV					y	
10034	B					y	
10034A	T					y	
10035	TT	52-TT-947				y	
10035A	G					y	

10035B	MV					y	
10035C	MV					y	
10035D	P					y	
10035E	T					y	
10035F	MV					y	
10035G	P					y	
10035H	P					y	
10035I	G					y	
10035J	T					y	
10035K	P					y	
10035L	TT					y	
10036	MV					y	
10037	MV					y	
10038	P					y	
10038A	T					y	
10038B	RB					y	
10039	MV					y	
10040	MV					y	
10041	B					y	
10042	T					y	
10043	P					y	
10044	TI					y	
10045	P					y	
10046	MV					y	
10047	P					y	
10047A	T					y	
10048	MV	A507				y	
10052	G					y	
10053	PRV					y	
10054	T					y	
10055	P					y	
10056	MV					y	
10057	P					y	
10058	P					y	
10059	B					y	
10060	P					y	
10061	B					y	
10062	T					y	
10063	PT	52-PT-215				y	
10064	L					y	

**Turpentine Condenser and LVHC Gas Cooler**  
 Completed Date/Time: 3/15/24

Number	Type	Equip. Number	Pressure (+/-)	Background	VOC Reading	Is Component Free of Leaks or Defects?	Comments
11000	RB					Yes	
11001	TT	52-TE-222A				Y	
11002	PI					Y	
11003	P					Y	
11004	G					Y	
11005	P					Y	
11006	P					Y	
11007	FA	M52-0512				Y	
11008	P					Y	
11008A	HAP					Y	
11009	P					Y	
11010	G					Y	
11011	P					Y	
11012	TT	52-TE-225				Y	
11013	CV	52-HV-174B				Y	
11014	MV	52-A-368				Y	
11015	T					Y	
11017	T					Y	
11018	PT	52-PSH-226				Y	
11019	RD					Y	
11020	P					Y	
11021	CV	52-HV-174A				Y	
11022	T	52-A-428				Y	
11023	T					Y	
11024	PI	52-PI-226				Y	
11025	FA	Z00-0395M				Y	
11026	P					Y	
11027	MV	52-A-541				Y	
11028	T	52-A-437				Y	
11029	L					Y	



**ENVIRONMENTAL360**

New-Indy – Catawba Mill

LDAR Inspection and Testing Diagrams

Turpentine Condenser and LVHC Gas Cooler

Rev. Date  
February 2021

Figure 11

To Another Page and Indicated Equipment

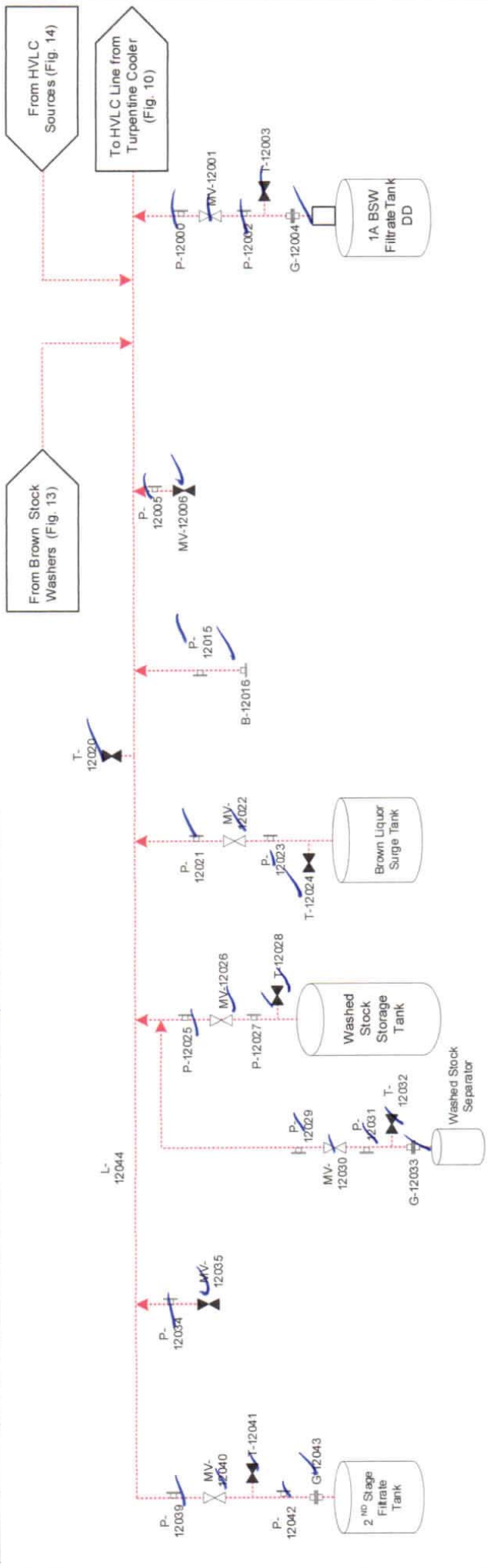
From Another Page and Indicated Equipment

HVLC System at Pulp Mill (1 of 2)

Completed Date/Time: 3/15/21

Number	Type	Equip. Number	Pressure (+/-)	Background	VOC Reading	Is Component Free of Leaks or Defects?	Comments
12000	P					yes	
12001	MV					y	
12002	P					y	
12003	T	X182				y	
12004	G					y	
12005	P					y	
12006	MV					y	
12015	P					y	
12016	B					y	
12020	T	V4454				y	
12021	P					y	
12022	MV	0598-22-HY				y	
12023	P					y	
12024	T	D060				y	

12025	P						yes
12026	MV						y
12027	P						y
12028	T						y
12029	P						y
12030	MV	F543					y
12031	P						y
12032	T	F541					y
12033	G						y
12034	P						y
12035	MV	SR307					y
12039	P						y
12040	MV	SR308					y
12041	T						y
12042	P						y
12043	G						y
12044	L						y



ENVIRONMENTAL 360

To Another Page and Indicated Equipment

From Another Page and Indicated Equipment

Vent Gases

Condensates

Liquor/Stock Lines

Process Lines

New-Indy – Catawba Mill

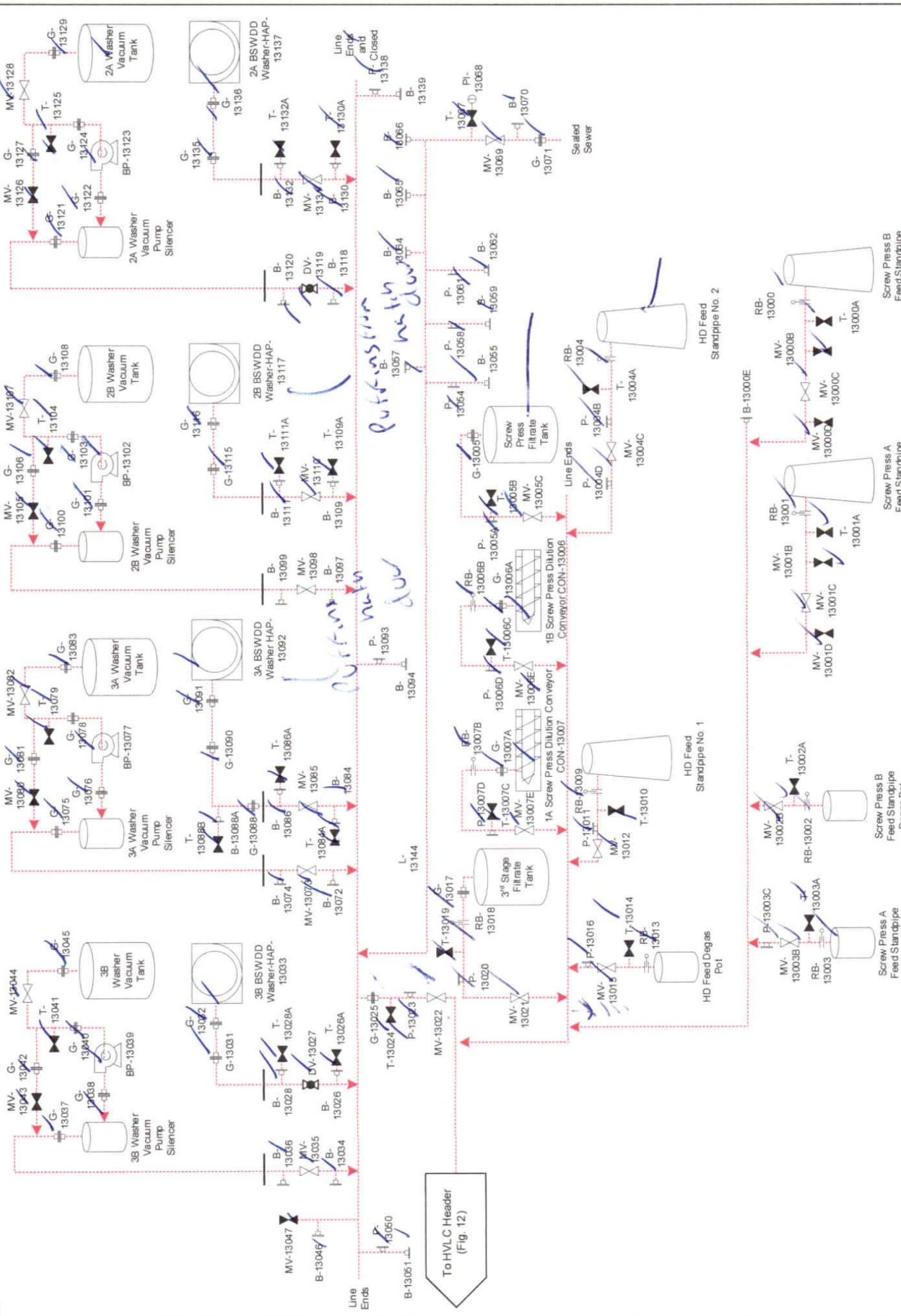
LDAR Inspection and Testing Diagrams

HVLC System at Pulp Mill (1 of 2)

Rev. Date

February 2021

Figure 12



Rev. Date  
February 2021

New-Indy – Catawba Mill  
LDAR Inspection and Testing Diagrams  
Pulp Mill BSWs



To Another Page and Indicated Equipment  
From Another Page and Indicated Equipment

Vent Gases  
 Bleach Gases  
 Condensates  
 Liquor/Stock Lines  
 Process Lines

To Another Page and Indicated Equipment  
 From Another Page and Indicated Equipment

Screw Press A Feed Standpipe  
 Screw Press B Feed Standpipe  
 HD Feed Standpipe No. 1  
 HD Feed Standpipe No. 2  
 Screw Press A Feed Standpipe Degas Pot  
 Screw Press B Feed Standpipe Degas Pot

Pulp Mill BSWs Completed Date/Time: 3/15/21

Number	Type	Equip. Number	Pressure (+/-)	Background	VOC Reading	Is Component Free of Leaks or Defects?	Comments
13000	RB					Y	
13000A	T					Y	
13000B	MV					Y	
13000C	MV					Y	
13000D	MV					Y	
13000E	B					Y	
13001	RB					Y	
13001A	T					Y	
13001B	MV					Y	
13001C	MV					Y	
13001D	MV					Y	
13002	RB					Y	
13002A	T					Y	
13002B	MV					Y	
13003	RB					Y	
13003A	T					Y	
13003B	MV					Y	
13003C	P					Y	
13004	RB					Y	
13004A	T					Y	
13004B	P					Y	
13004C	MV					Y	
13004D	P					Y	
13005	G					Y	
13005A	P					Y	
13005B	T					Y	
13005C	MV					Y	
13006	CON					Y	
13006A	G					Y	
13006B	RB					Y	
13006C	T					Y	
13006D	P					Y	
13006E	MV					Y	
13007	CON					Y	
13007A	A					Y	
13007B	RB					Y	
13007C	T					Y	
13007D	P					Y	
13007E	MV					Y	
13009	RB					Y	
13010	T					Y	
13011	P					Y	
13012	MV					Y	
13013	RB					Y	
13014	T					Y	
13015	MV					Y	
13016	P					Y	
13017	G					Y	
13018	RB					Y	
13019	T					Y	
13020	P					Y	
13021	MV					Y	
13022	MV					Y	
13023	P					Y	
13024	T					Y	
13025	G					Y	
13026	B					Y	
13026A	T					Y	
13027	DV					Y	
13028	B					Y	
13028A	T					Y	
13031	G					Y	
13032	G					Y	
13033	HAP					Y	
13034	B					Y	
13035	MV					Y	
13036	B					Y	
13037	G					Y	
13038	G					Y	
13039	BP					Y	
13040	G					Y	
13041	T					Y	
13042	G					Y	
13043	MV					Y	
13044	MV					Y	
13045	G					Y	
13046	B					Y	
13047	MV					Y	
13050	P					Y	
13051	B					Y	
13054	P					Y	
13055	B					Y	
13057	B					Y	
13058	P					Y	
13059	B					Y	
13061	P					Y	
13062	B					Y	
13064	B					Y	
13065	B					Y	
13066	B					Y	
13067	T					Y	
13068	PI					Y	
13069	MV					Y	
13070	B					Y	
13071	G					Y	
13072	B					Y	
13073	MV	F530				Y	
13074	B					Y	
13075	G					Y	
13076	G					Y	
13077	BP	E53-0046				Y	
13078	G					Y	
13079	T	F195				Y	
13080	MV	F101				Y	
13081	G					Y	
13082	MV					Y	
13083	G					Y	
13084	B					Y	
13084A	T					Y	
13085	MV	F529				Y	
13086	B					Y	
13086A	T					Y	
13088	G					Y	
13088A	B					Y	
13088B	T					Y	
13090	G					Y	
13091	G					Y	
13092	HAP					Y	
13093	P					Y	
13094	B	F528				Y	
13097	B					Y	
13098	MV	F527				Y	
13099	B					Y	
13100	G					Y	
13101	G					Y	
13102	BP					Y	
13103	G					Y	
13104	T	F262				Y	
13105	MV	F248				Y	
13106	G					Y	
13107	MV					Y	
13108	G					Y	
13109	B					Y	
13109A	T					Y	
13110	MV					Y	
13111	B					Y	
13111A	T					Y	
13115	G					Y	
13116	G					Y	
13117	HAP					Y	
13118	B					Y	
13119	DV	F524				Y	
13120	B					Y	
13121	G					Y	
13122	G					Y	
13123	BP	E53-0106				Y	
13124	G					Y	
13125	T	F356				Y	
13126	MV	F293				Y	
13127	G					Y	
13128	MV					Y	
13129	G					Y	
13130	B					Y	
13130A	T					Y	
13131	MV					Y	
13132	B					Y	
13132A	T					Y	
13135	G					Y	
13136	G					Y	
13137	HAP					Y	
13138	P					Y	
13139	B					Y	
13144	L					Y	

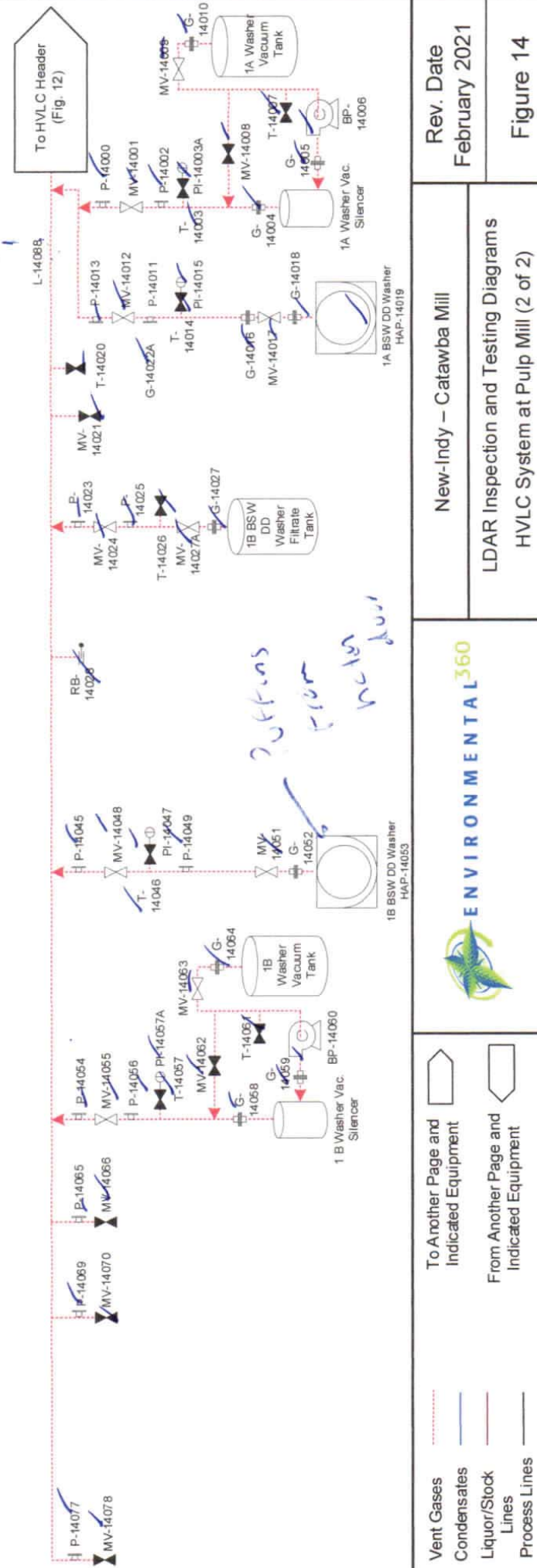
PUFFINS

PUFFINS

Number	Type	Equip. Number	Pressure (+/-)	Background	VOC Reading	Is Component Free of Leaks or Defects?	Comments
14000	P					Yes	
14001	MV	X170				Y	
14002	P					Y	
14003	T					Y	
14003A	PI	52-PI-353				Y	
14004	G					Y	
14005	G					Y	
14006	BP	M52-0092				Y	
14007	T	X74				Y	
14008	MV	X240				Y	
14009	MV					Y	
14010	G					Y	
14011	P					Y	
14012	MV	X169				Y	
14013	P					Y	
14014	T	X179				Y	
14015	PI					Y	
14016	G					Y	
14017	MV					Y	
14018	G					Y	
14019	HAP					Y	
14020	T					Y	
14021	MV					Y	
14023	P					Y	
14024	MV	X171				Y	
14025	P					Y	
14026	T					Y	

Number	Type	Equip. Number	Pressure (+/-)	Background	VOC Reading	Is Component Free of Leaks or Defects?	Comments
14027	G					Y	
14027A	MV					Y	
14028	RB					Y	
14045	P					Y	
14046	T					Y	
14047	PI					Y	
14048	MV	X168				Y	
14049	P					Y	
14051	MV					Y	
14052	G					Y	
14053	HAP					Y	
14054	P					Y	
14055	MV	X167				Y	
14056	P					Y	
14057	T					Y	
14057A	PI					Y	
14058	G					Y	
14059	G					Y	
14060	BP	E52-0128				Y	
14061	T	X159				Y	
14062	MV	X265				Y	
14063	MV					Y	
14064	G					Y	
14065	P					Y	
14066	MV	SR313				Y	
14069	P					Y	
14070	MV	SR312				Y	
14077	P					Y	
14078	MV					Y	
14088	L					Y	

Completed Date/Time: 3/15/21



Inspection Date: April 5, 2021



New Indy Containerboard - Catawba Mill  
5300 Cureton Ferry Rd.  
Catawba, SC 29704

### 2021 Monthly LDAR Inspection Summary Report

**Table 1: Visual Inspection Summary Table**

Equipment Number	Date	Description of Leak or Visual Defect
N/A	4/5/2021	No leaks or defects to report.
<b>First Attempt to Repair must be completed by:</b>	5 Days from Inspection Date	Not Applicable if no leaks were found.
<b>Repairs must be completed by:</b>	15 Days from Inspection Date	Not Applicable if no leaks were found.

This report provides a summary of leaks and visual defects found during the visual inspection of the closed-vent and condensate-collection systems and complies with the record keeping requirements of 63.454(b)(1-2, 4-5).

The facility must initiate repairs to any defects within five (5) calendar days from this inspection and the defects must be repaired within fifteen (15) calendar days of the inspection. If the leak or defect requires the system to be shutdown in order to make repairs, or more emissions would occur from attempting the repair than delaying the repair, then the repairs may be delayed until the next process unit shutdown. A report must be supplied with the repair date and associated information, or the reason for the delay if the repairs are not completed within the 15-day period. These response requirements are specific to 40 CFR 63, specifically 63.453(k)(6), 63.453(l)(3), and 63.964(b)(1-2). Documentation of all repair attempts made and any leaks/defects requiring a process unit shutdown must be completed according to 63.454(b)(6-11).

I certify that the results of the visual inspection are accurate and complete to the best of my knowledge.

Inspector Name: Josh Howard

Signature: Josh Howard



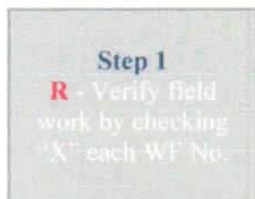
## Inspection QA/QC Procedure

E360 Project Number?	New Lady catawba
Task Number (if applicable)?	April 2021 <del>AAAR</del> <sup>JPR</sup> LOR monthly

### Purpose of Form

To verify field work meets each critical element.

### Visual Work Flow (WF)



### Verification of Critical Elements

WF No.	Requirement	Yes?
	Work-flow step	1
	Verifier of critical elements for work-flow step	R
1	Was a bump test performed on the personal H <sub>2</sub> S monitor?	✓
2	Have the most recent versions of the inspection forms been used?	✓
3	Were all inspection points identified correctly and inspected correctly?	✓
4	Did the operator/ contact verify to our inspector that all equipment was operating under normal operating conditions?	✓
5	Were any deficiencies identified in person to the client?	NA
6	Were all inspection questions answered with either a Yes, No, or NA?	✓
7	Were inspections performed during the required regulatory time frame?	✓

### Approvals

Role	WF Step	Name	Approval (insert date)
Responsible Person (R)	1	John Akel	04/05/2021



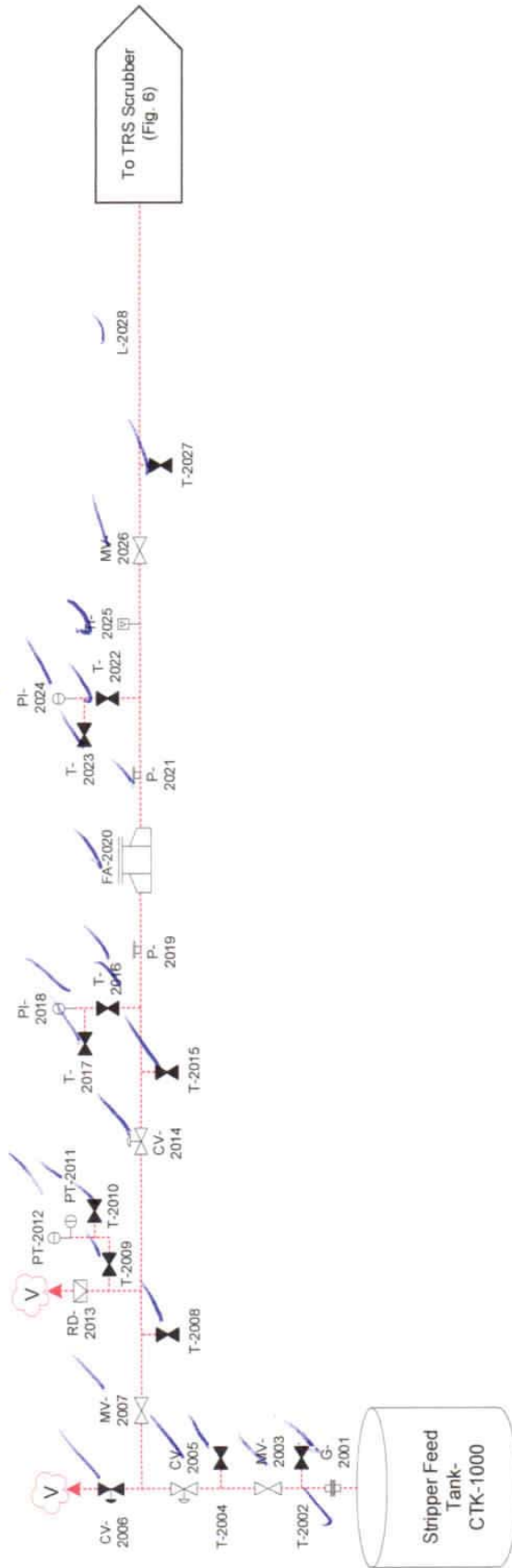




**Stripper Feed Tank**

Completed Date/Time: 4/5/2021

Number	Type	Equip. Number	Pressure (+/-)	Background	VOC Reading	Is Component Free of Leaks or Defects?	Comments
2001	G					Yes	
2002	T					Yes	
2003	MV					Yes	
2004	T					Yes	
2005	CV					Yes	
2006	CV					Yes	
2007	MV					Yes	
2008	T					Yes	
2009	T					Yes	
2010	T					Yes	
2011	PT					Yes	
2012	PT					Yes	
2013	RD					Yes	
2014	CV					Yes	
2015	T					Yes	
2016	T					Yes	
2017	T					Yes	
2018	PI					Yes	
2019	P					Yes	
2020	FA					Yes	
2021	P					Yes	
2022	T					Yes	
2023	T					Yes	
2024	PI					Yes	
2025	TI					Yes	
2026	MV					Yes	
2027	T					Yes	
2028	L					Yes	



\* Indicates car seal present

--- Vent Gases  
--- Condensates  
--- Liquor/Stock Lines  
--- Process Lines

To Another Page and Indicated Equipment  
From Another Page and Indicated Equipment

**ENVIRONMENTAL<sup>360</sup>**

New-Indy – Catawba Mill

LDAR Inspection and Testing Diagrams

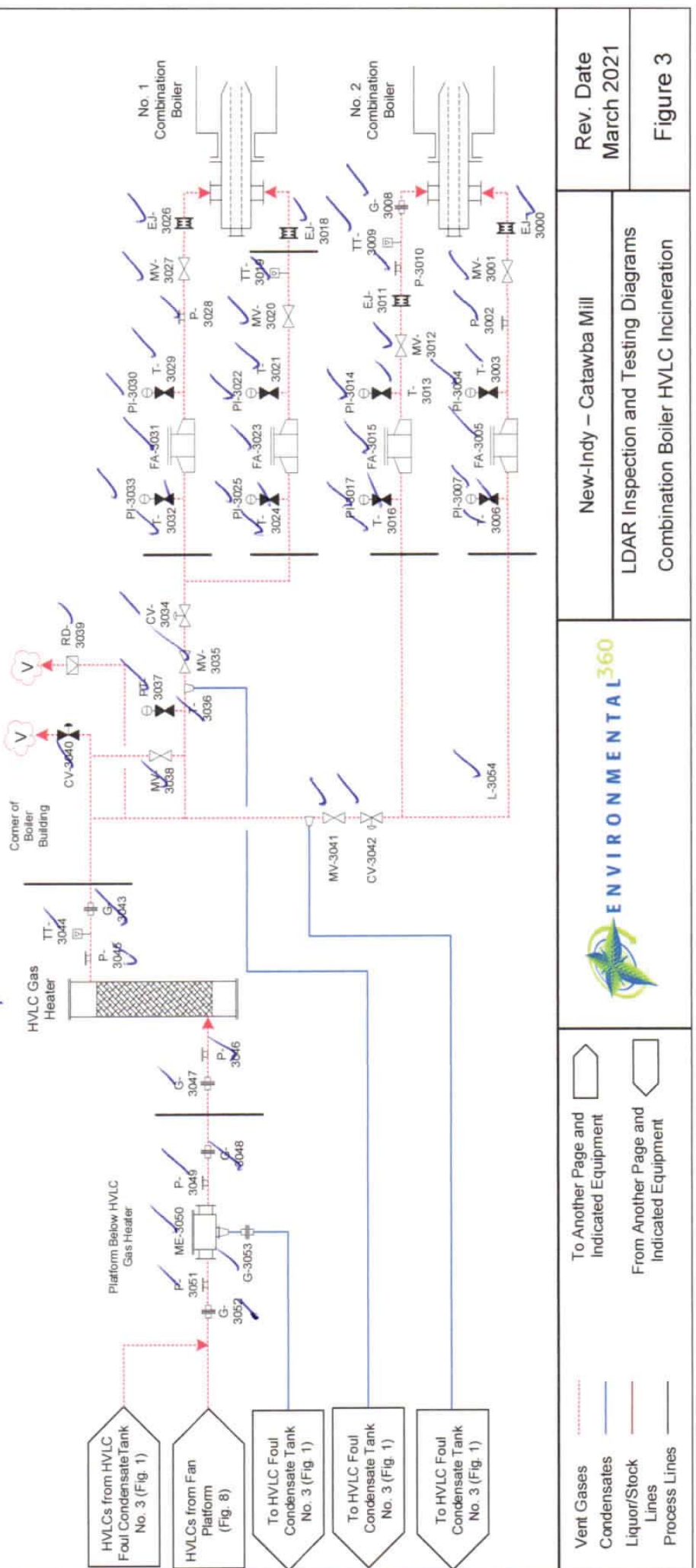
Stripper Feed Tank

Rev. Date  
March 2021

Figure 2

Number	Type	Equip. Number	Pressure (+/-)	Background	VOC Reading	Is Component Free of Leaks or Defects?	Comments
3000	EJ					YES	
3001	MV					Y	
3002	P					Y	
3003	T					Y	
3004	PI					Y	
3005	FA					Y	
3006	T					Y	
3007	PI					Y	
3008	G					Y	
3009	TT					Y	
3010	P					Y	
3011	EJ					Y	
3012	MV					Y	
3013	T					Y	
3014	PI					Y	
3015	FA					Y	
3016	T					Y	
3017	PI					Y	
3018	EJ					Y	
3019	TT					Y	
3020	MV					Y	
3021	T					Y	
3022	PI					Y	
3023	FA					Y	
3024	T					Y	
3025	PI					Y	
3026	EJ					Y	
3027	MV					Y	
3028	P					Y	
3029	T					Y	
3030	PI					Y	
3031	FA					Y	
3032	T					Y	
3033	PI					Y	
3034	CV					Y	
3035	MV					Y	
3036	T					Y	
3037	PT					Y	
3038	MV					Y	
3039	RD					Y	
3040	CV					Y	
3041	MV					Y	
3042	CV					Y	
3043	G					Y	
3044	TT					Y	
3045	P					Y	
3046	P					Y	
3047	G					Y	
3048	G					Y	
3049	P					Y	
3050	ME					Y	
3051	P					Y	
3052	G					Y	
3053	G					Y	
3054	L					Y	

Number	Type	Equip. Number	Pressure (+/-)	Background	VOC Reading	Is Component Free of Leaks or Defects?	Comments
3026	EJ					Y	
3027	MV					Y	
3028	P					Y	
3029	T					Y	
3030	PI					Y	
3031	FA					Y	
3032	T					Y	
3033	PI					Y	
3034	CV					Y	
3035	MV					Y	
3036	T					Y	
3037	PT					Y	
3038	MV					Y	
3039	RD					Y	
3040	CV					Y	
3041	MV					Y	
3042	CV					Y	
3043	G					Y	
3044	TT					Y	
3045	P					Y	
3046	P					Y	
3047	G					Y	
3048	G					Y	
3049	P					Y	
3050	ME					Y	
3051	P					Y	
3052	G					Y	
3053	G					Y	
3054	L					Y	



Rev. Date  
March 2021

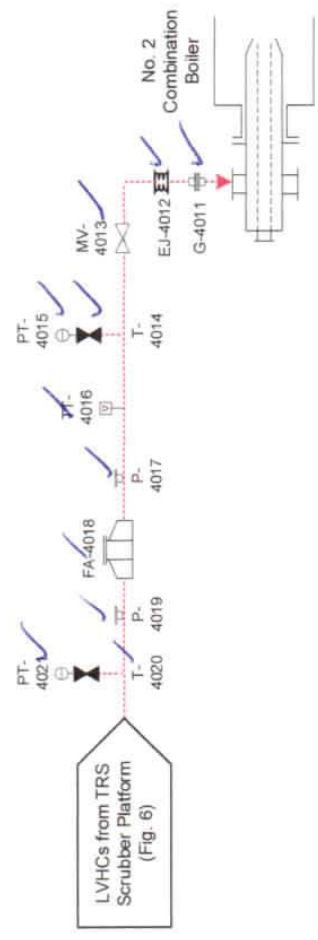
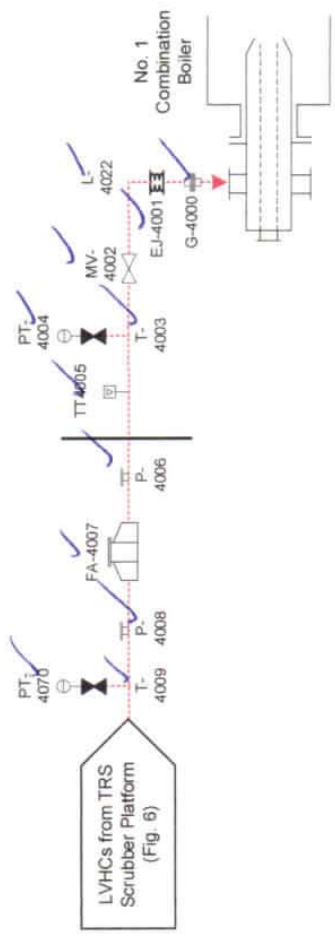
New-Indy - Catawba Mill  
LDAR Inspection and Testing Diagrams  
Combination Boiler HVLIC Incineration



Figure 3

Combination Boiler LVHC Incineration  
 Completed Date/Time: 4/15/2021

Number	Type	Equip. Number	Pressure (+/-)	Background	VOC Reading	Is Component Free of Leaks or Defects?	Comments
4000	G					YES	
4001	EJ					Y	
4002	MV					Y	
4003	T					Y	
4004	PT					Y	
4005	TT					Y	
4006	P					Y	
4007	FA					Y	
4008	P					Y	
4009	T					Y	
4010	PT					Y	
4011	G					Y	
4012	EJ					Y	
4013	MV					Y	
4014	T					Y	
4015	PT					Y	
4016	TT					Y	
4017	P					Y	
4018	FA					Y	
4019	P					Y	
4020	T					Y	
4021	PT					Y	
4022	L					Y	



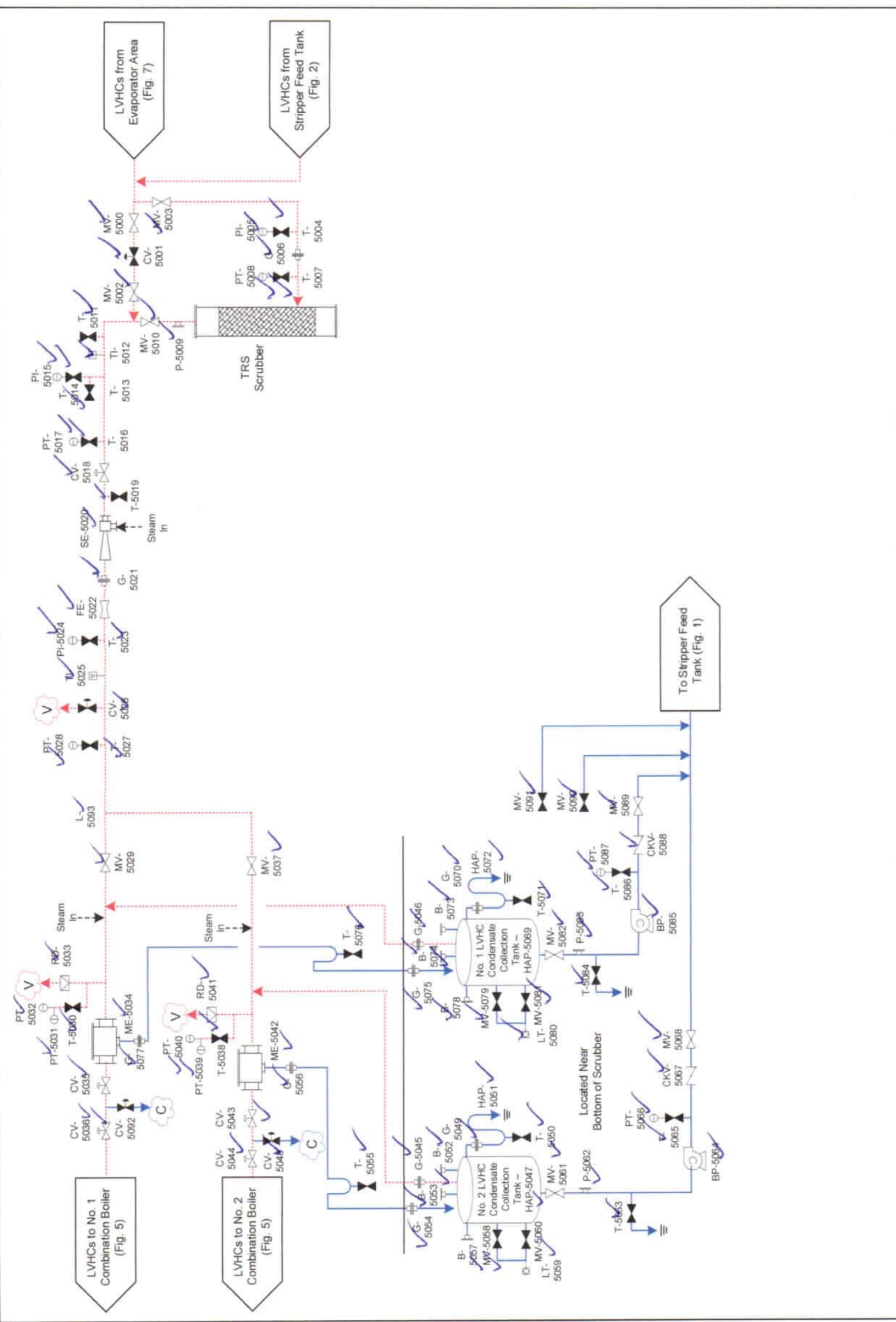
Vent Gases  
 Condensates  
 Liquor/Stock Lines  
 Process Lines

To Another Page and Indicated Equipment  
 From Another Page and Indicated Equipment



New-Indy – Catawba Mill  
 LDAR Inspection and Testing Diagrams  
 Combination Boiler LVHC Incineration

Rev. Date  
 March 2021  
 Figure 4

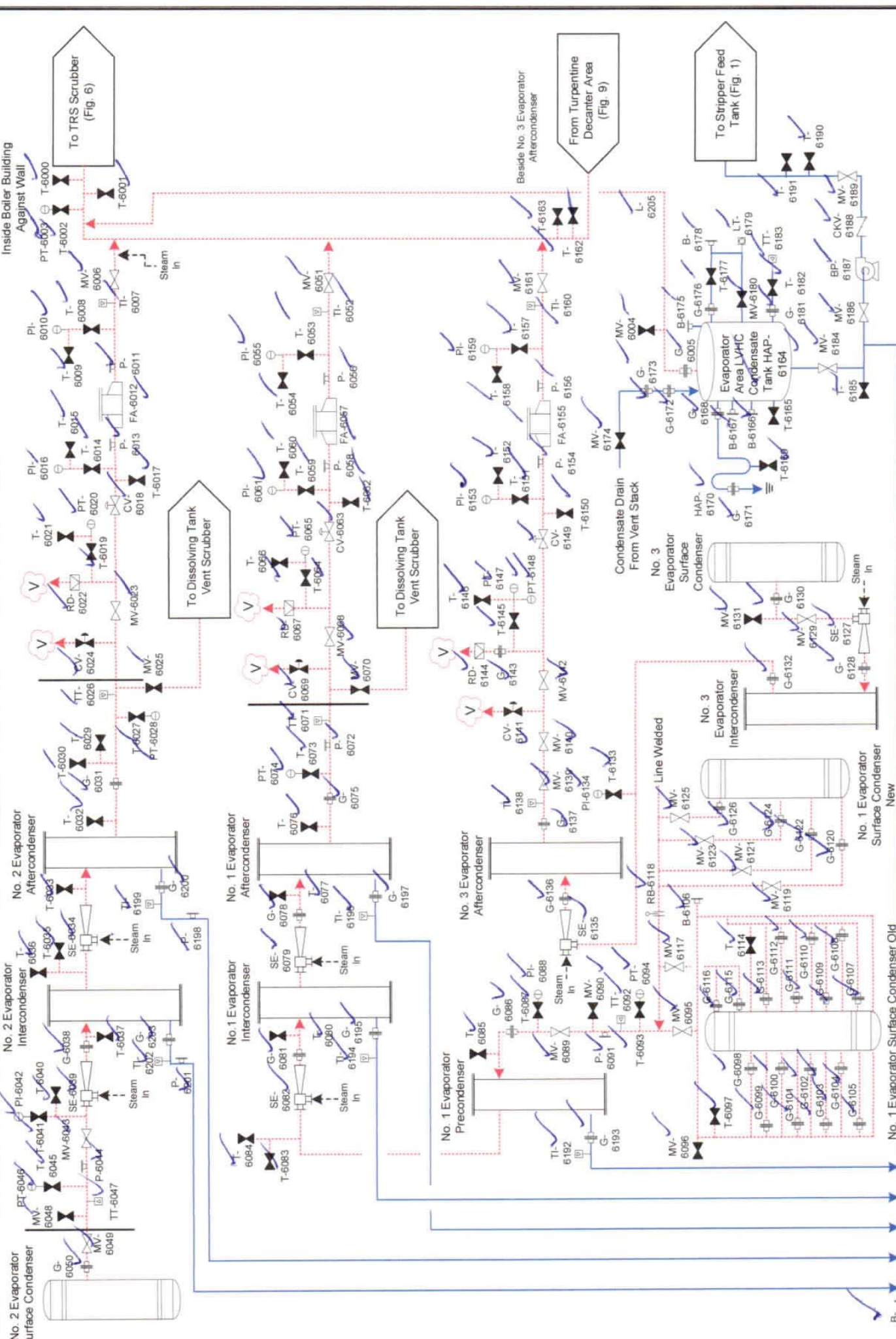


<p>Vert Gases Condensates Liquor/Stock Lines Process Lines</p>	<p>To Another Page and Indicated Equipment From Another Page and Indicated Equipment</p>	<p>ENVIRONMENTAL 360</p>	<p>To Another Page and Indicated Equipment From Another Page and Indicated Equipment</p>
<p>LDAR Inspection and Testing Diagrams TRS Scrubber Platform</p>		<p>New-Indy – Catawba Mill</p>	<p>Rev. Date March 2021</p> <p>Figure 5</p>

TRS Scrubber Platform

Completed Date/Time: 6/15/2021

Number	Type	Equip. Number	Pressure (+/-)	Background	VOC Reading	Is Component Free of Leaks or Defects?	Comments
5000	MV					YES	
5001	CV					Y	
5002	MV					Y	
5003	MV					Y	
5004	T					Y	
5005	PI					Y	
5006	G					Y	
5007	T					Y	
5008	PT					Y	
5009	P					Y	
5010	MV					Y	
5011	T					Y	
5012	TI					Y	
5013	T					Y	
5014	T					Y	
5015	PI					Y	
5016	T					Y	
5017	PT					Y	
5018	T					Y	
5019	SE					Y	
5020	G					Y	
5021	FE					Y	
5022	T					Y	
5023	PI					Y	
5024	TI					Y	
5025	TI					Y	
5026	CV					Y	
5027	T					Y	
5028	PT					Y	
5029	MV					Y	
5030	T					Y	
5031	PT					Y	
5032	PT					Y	
5033	RD					Y	
5034	ME					Y	
5035	CV					Y	
5036	CV					Y	
5037	MV					Y	
5038	T					Y	
5039	PT					Y	
5040	PT					Y	
5041	RD					Y	
5042	ME					Y	
5043	CV					Y	
5044	CV					Y	
5045	G					Y	
5046	G					Y	
5047	HAP						
5048	CV						
5049	G						
5050	T						
5051	HAP						
5052	B						
5053	B						
5054	G						
5055	T						
5056	G						
5057	B						
5058	MV						
5059	LT						
5060	MV						
5061	MV						
5062	P						
5063	T						
5064	BP						
5065	T						
5066	PT						
5067	CKV						
5068	MV						
5069	HAP						
5070	G						
5071	T						
5072	HAP						
5073	B						
5074	B						
5075	G						
5076	T						
5077	G						
5078	B						
5079	MV						
5080	LT						
5081	MV						
5082	MV						
5083	P						
5084	T						
5085	BP						
5086	T						
5087	PT						
5088	CKV						
5089	MV						
5090	MV						
5091	MV						
5092	CV						
5093	L						



<p>Rev. Date March 2021</p>	<p>New-Indy – Catawba Mill</p> <p>LDAR Inspection and Testing Diagrams</p> <p>Evaporator System</p>		<p>To Another Page and Indicated Equipment</p> <p>From Another Page and Indicated Equipment</p> <p>Vent Gases</p> <p>Condensates</p> <p>Liquor/Stock Lines</p> <p>Process Lines</p>
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Figure 6









HVLC Blower Platform

Completed Date/Time: 4/15/2021

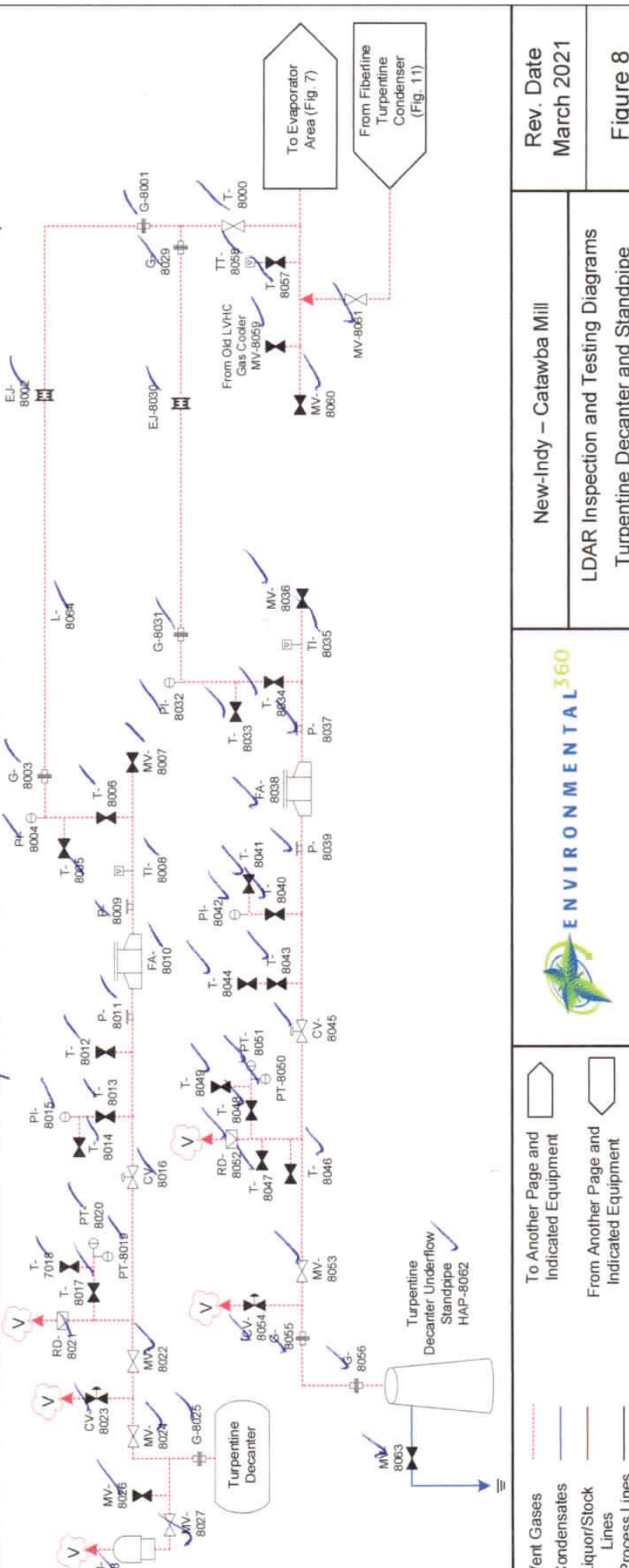
Number	Type	Equip. Number	Pressure (+/-)	Background	VOC Reading	Is Component Free of Leaks or Defects?	Comments
7000	B					YES	
7001	Type					Y	
7002	Type					Y	
7003	PI					Y	
7004	TI					Y	
7005	T					Y	
7006	TT					Y	
7007	CV					Y	
7008	MV					Y	
7009	CV					Y	
7010	T					Y	
7011	G					Y	
7012	PI					Y	
7013	ME					Y	
7014	T					Y	
7015	G					Y	
7016	G					Y	
7017	BP					Y	
7018	G					Y	
7019	T					Y	
7020	PI					Y	
7021	TI					Y	
7022	MV					Y	
7023	MV					Y	
7024	MV					Y	
7025	G					Y	
7026	BP					Y	
7027	G					Y	
7028	MV					Y	
7029	T					Y	
7030	T					Y	
7031	FT					Y	
7032	FE					Y	
7033	T					Y	
7034	T					Y	
7035	MV					Y	
7036	P					Y	
7037	G					Y	
7038	T					Y	
7039	MV					Y	
7040							G
7041							G
7042							G
7043							G
7044							HAP
7045							G
7046							MV
7047							G
7048							MV
7049							BP
7050							G
7051							T
7052							PI
7053							T
7054							MV
7055							MV
7056							FT
7057							FT
7058							MV
7059							FT
7060							B
7061							T
7062							HAP
7063							G
7064							G
7065							T
7066							T
7067							G
7068							G
7069							G
7070							T
7071							FT
7072							G
7073							G
7074							G
7075							G
7076							T
7077							T
7078							LT
7079							MV
7080							T
7081							P
7082							LG
7083							B
7084							T
7085							L

Car seal present

Number	Type	Equip. Number	Pressure (%)	Background	VOC Reading	In Component Free of Leaks or Defects?	Comments
8000	Type						
8001	G						
8002	EJ						
8003	G						
8004	PI						
8005	Type						
8006	MV						
8007	TI						
8008	PI						
8009	FA						
8010	PI						
8011	T						
8012	T						
8013	T						
8014	PI						
8015	PI						
8016	CV						
8017	T						
8018	T						
8019	PT						
8020	PT						
8021	RD						
8022	MV						
8023	CV						
8024	MV						
8025	G						
8026	MV						
8027	MV						
8028	PVB						
8029	G						
8030	EJ						

Number	Type	Equip. Number	Pressure (%)	Background	VOC Reading	In Component Free of Leaks or Defects?	Comments
8031	G						
8032	PI						
8033	T						
8034	T						
8035	TI						
8036	MV						
8037	P						
8038	FA						
8039	P						
8040	T						
8041	T						
8042	PI						
8043	T						
8044	T						
8045	CV						
8046	T						
8047	T						
8048	T						
8049	T						
8050	PT						
8051	PT						
8052	RD						
8053	MV						
8054	CV						
8055	G						
8056	G						
8057	T						
8058	TT						
8059	MV						
8060	MV						
8061	MV						
8062	HAP						
8063	MV						
8064	L						

Turpentine Decanter and Standpipe  
 Completed Date/Time: 4/15/2021



Rev. Date  
 March 2021

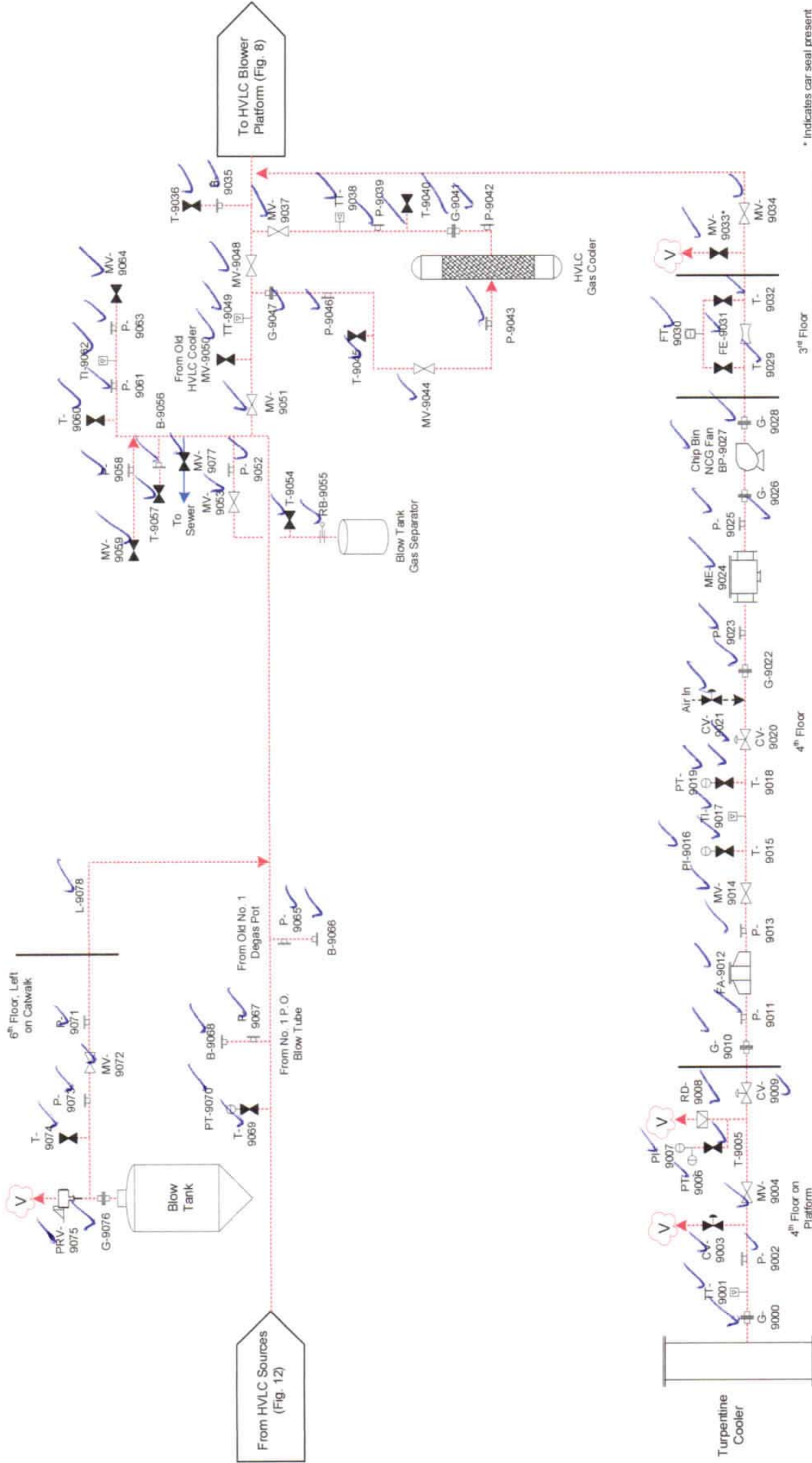
New-Indy – Catawba Mill  
 LDAR Inspection and Testing Diagrams  
 Turpentine Decanter and Standpipe



To Another Page and Indicated Equipment  
 From Another Page and Indicated Equipment

Vent Gases  
 Condensates  
 Liquor/Stock Lines  
 Process Lines

Figure 8



<p>* Indicates car seal present</p>	<p>Rev. Date March 2021</p>
<p>New-Indy – Catawba Mill LDAR Inspection and Testing Diagrams Turpentine Cooler and Blow Tank</p>	
<p>Vert Gases (Red dashed line)</p> <p>Condensates (Blue solid line)</p> <p>Liquor/Stock Lines (Green solid line)</p> <p>Process Lines (Black solid line)</p> <p>To Another Page and Indicated Equipment (Red arrow)</p> <p>From Another Page and Indicated Equipment (Blue arrow)</p>	<p>Figure 9</p>

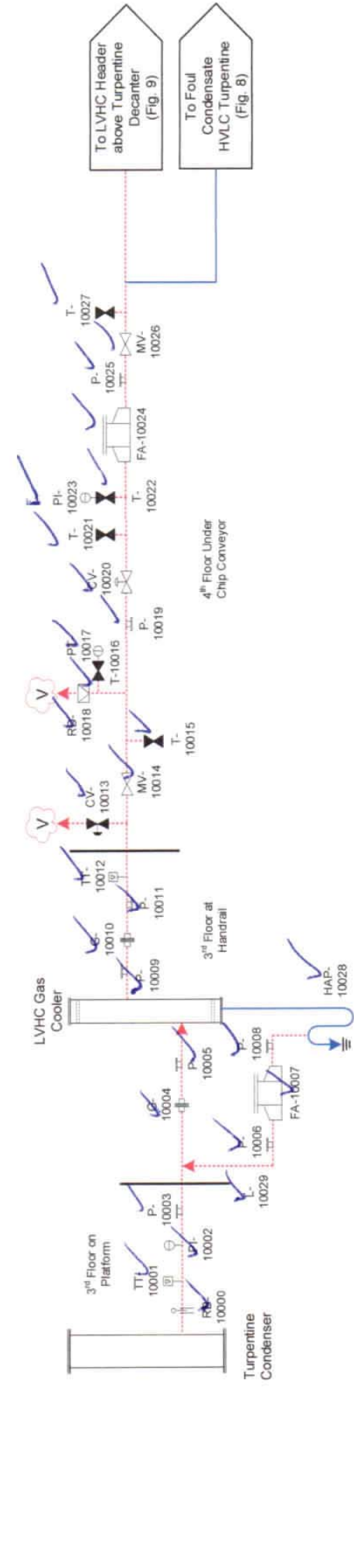


**Turpentine Condenser and LVHC Gas Cooler**

Completed Date/Time: 4/5/2021

Number	Type	Equip. Number	Pressure (+/-)	Background	VOC Reading	Is Component Free of Leaks or Defects?	Comments
10000	RB					Yes	
10001	TT					Y	
10002	PI					Y	
10003	PI					Y	
10004	G					Y	
10005	PI					Y	
10006	PI					Y	
10007	FA					Y	
10008	PI					Y	
10009	PI					Y	
10010	G					Y	
10011	PI					Y	
10012	TT					Y	

10013	CV						yes
10014	MV						Y
10015	T						Y
10016	T						Y
10017	PT						Y
10018	RD						Y
10019	P						Y
10020	CV						Y
10021	T						Y
10022	T						Y
10023	PI						Y
10024	FA						Y
10025	P						Y
10026	MV						Y
10027	T						Y
10028	HAP						Y
10029	L						Y



**ENVIRONMENTAL 360**

Legend:

- Vent Gases
- Condensates
- Liquor/Stock Lines
- Process Lines
- To Another Page and Indicated Equipment
- From Another Page and Indicated Equipment

New-Indy – Catawba Mill

LDAR Inspection and Testing Diagrams

Turpentine Condenser and LVHC Gas Cooler

Rev. Date  
March 2021

Figure 10

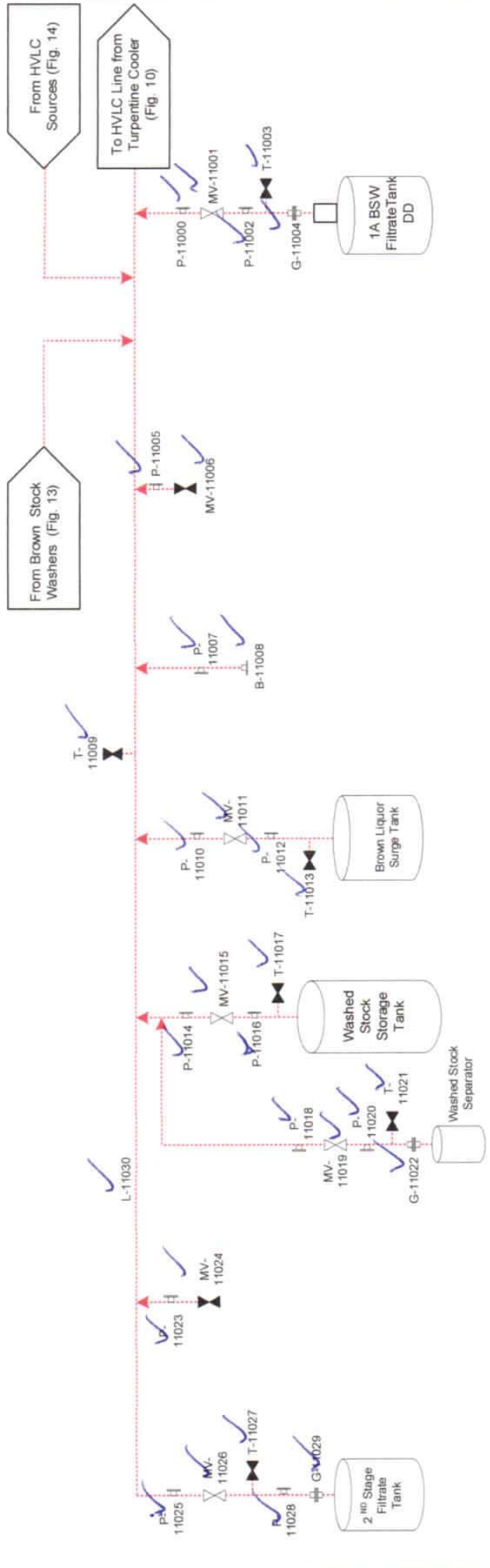


**HVLC System at Pulp Mill (1 of 2)**

Completed Date/Time: 4/5/2021

Number	Type	Equip. Number	Pressure (+/-)	Background	VOC Reading	Is Component Free of Leaks or Defects?	Comments
11000	P					yes	
11001	MV					y	
11002	P					y	
11003	T					y	
11004	G					y	
11005	P					y	
11006	MV					y	
11007	P					y	
11008	B					y	
11009	T					y	
11010	P					y	
11011	MV					y	
11012	P					y	

11013	T						yes
11014	P						y
11015	MV						y
11016	P						y
11017	T						y
11018	P						y
11019	MV						y
11020	P						y
11021	T						y
11022	G						y
11023	P						y
11024	MV						y
11025	P						y
11026	MV						y
11027	T						y
11028	P						y
11029	G						y
11030	L						y



ENVIRONMENTAL 360

New-Indy – Catawba Mill

LDAR Inspection and Testing Diagrams

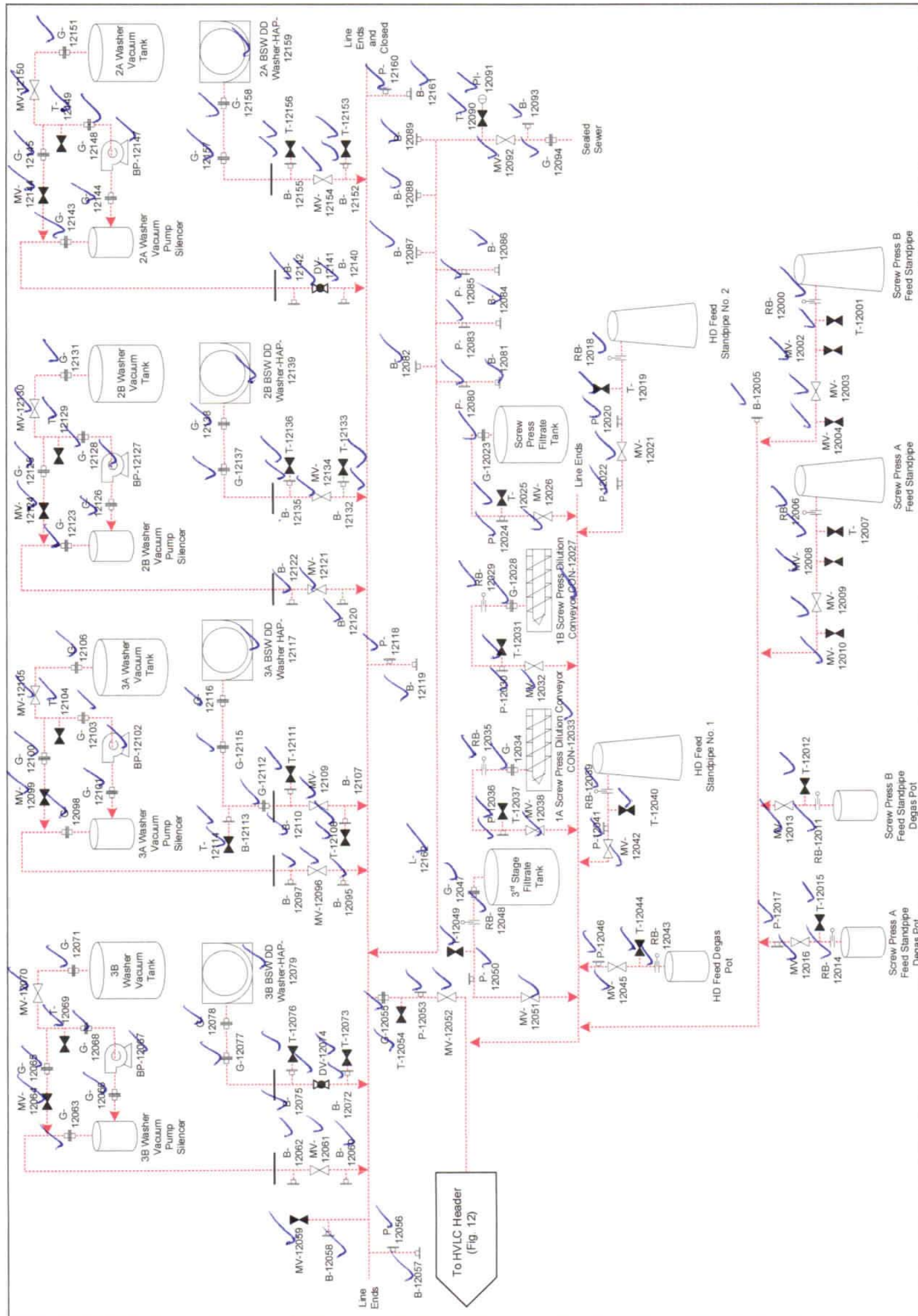
HVLC System at Pulp Mill (1 of 2)

Rev. Date  
March 2021

Figure 11

Legend:

- Vent Gases
- Condensates
- Liquor/Stock Lines
- Process Lines
- To Another Page and Indicated Equipment
- From Another Page and Indicated Equipment



Rev. Date  
March 2021

Figure 12

New-Indy – Catawba Mill

LDAR Inspection and Testing Diagrams

Pulp Mill BSWs



	To Another Page and Indicated Equipment
	From Another Page and Indicated Equipment
	From Another Page and Indicated Equipment
	From Another Page and Indicated Equipment
	Process Lines

Pulp Mill BSWs

Completed Date/Time: 4/5/2021

Number	Type	Equip. Number	Pressure (+/-)	Background	VOC Reading	Is Component Free of Leaks or Defects?	Comments
12000	RB					Yes	
12001	T					Y	
12002	MV					Y	
12003	MV					Y	
12004	MV					Y	
12005	B					Y	
12006	RB					Y	
12007	T					Y	
12008	MV					Y	
12009	MV					Y	
12010	MV					Y	
12011	RB					Y	
12012	T					Y	
12013	MV					Y	
12014	RB					Y	
12015	T					Y	
12016	MV					Y	
12017	P					Y	
12018	RB					Y	
12019	T					Y	
12020	P					Y	
12021	MV					Y	
12022	P					Y	
12023	G					Y	
12024	P					Y	
12025	T					Y	
12026	MV					Y	
12027	CON					Y	
12028	G					Y	
12029	RB					Y	
12030	P					Y	
12031	T					Y	
12032	MV					Y	
12033	CON					Y	
12034	G					Y	
12035	RB					Y	
12036	P					Y	
12037	T					Y	
12038	MV					Y	
12039	RB					Y	
12040	T					Y	
12041	P					Y	
12042	MV					Y	
12043	RB					Y	
12044	T					Y	
12045	MV					Y	
12046	P					Y	
12047	G					Y	
12048	RB					Y	
12049	T					Y	
12050	P					Y	
12051	MV					Y	
12052	MV					Y	
12053	P					Y	
12054	T					Y	
12055	G					Y	
12056	P					Y	
12057	B					Y	
12058	B					Y	
12059	MV					Y	
12060	B					Y	
12061	MV					Y	
12062	B					Y	
12063	G					Y	
12064	MV					Y	
12065	G					Y	
12066	G					Y	
12067	BP					Y	
12068	G					Y	
12069	T					Y	
12070	MV					Y	
12071	G					Y	
12072	B					Y	
12073	T					Y	
12074	DV					Y	
12075	T					Y	
12076	T					Y	
12077	G					Y	
12078	G					Y	
12079	HAP					Y	
12080	P					Y	
12081	B					Y	
12082	B					Y	
12083	P					Y	
12084	B					Y	
12085	P					Y	
12086	B					Y	

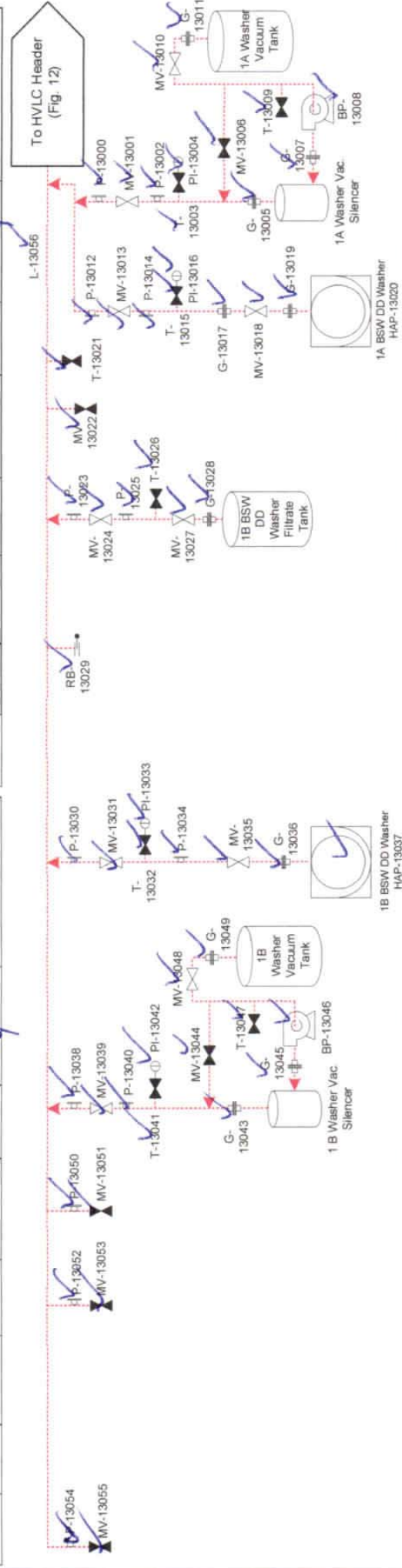


**HVLC System at Pulp Mill (2 of 2)**

Completed Date/Time: 4/5/2021

Number	Type	Equip. Number	Pressure (+/-)	Background	VOC Reading	Is Component Free of Leaks or Defects?	Comments
13000	P					YES	
13001	MV					YES	
13002	P					YES	
13003	T					YES	
13004	PI					YES	
13005	G					YES	
13006	MV					YES	
13007	G					YES	
13008	BP					YES	
13009	T					YES	
13010	MV					YES	
13011	G					YES	
13012	P					YES	
13013	MV					YES	
13014	P					YES	
13015	T					YES	
13016	PI					YES	
13017	G					YES	
13018	MV					YES	
13019	G					YES	
13020	HAP					YES	
13021	T					YES	
13022	MV					YES	
13023	P					YES	
13024	MV					YES	

13025	P					YES	
13026	T					YES	
13027	MV					YES	
13028	G					YES	
13029	RB					YES	
13030	P					YES	
13031	MV					YES	
13032	T					YES	
13033	PI					YES	
13034	P					YES	
13035	MV					YES	
13036	G					YES	
13037	HAP					YES	
13038	P					YES	
13039	MV					YES	
13040	P					YES	
13041	T					YES	
13042	PI					YES	
13043	G					YES	
13044	MV					YES	
13045	G					YES	
13046	BP					YES	
13047	T					YES	
13048	MV					YES	
13049	G					YES	
13050	P					YES	
13051	MV					YES	
13052	P					YES	
13053	MV					YES	
13054	P					YES	
13055	MV					YES	
13056	L					YES	



**ENVIRONMENTAL360**

**New-Indy – Catawba Mill**

LDAR Inspection and Testing Diagrams

HVLC System at Pulp Mill (2 of 2)

**Rev. Date**  
March 2021

**Figure 13**

--- Vent Gases  
--- Condensates  
--- Liquor/Stock Lines  
--- Process Lines

To Another Page and Indicated Equipment  
From Another Page and Indicated Equipment

Inspection Date: May 3-7, 2021

New Indy Containerboard - Catawba Mill  
5300 Cureton Ferry Rd.  
Catawba, SC 29704



**2021 LDAR Annual Method 21 Testing and Negative-Pressure Certification Summary Report**

Equipment Number	Date	Description of Leak or Visual Defect
CV-5026	5/4/2021	Control valve CV-5026 is located on the LVHC line at outlet of Steam Ejector and prior to the mist eliminators. The valve is not collecting gasses and had a VOC reading of 1558 ppm. Maintenance made first attempt by tightening shaft of valve, but was unsuccessful.
WSR-12079	5/3/2021	The 3B BSW DD Washer is puffing from an open hatch door.
<b>First Attempt to Repair must be completed by:</b>	5 Days from Inspection Date	Not Applicable if no leaks were found.
<b>Repairs must be completed by:</b>	15 Days from Inspection Date	Not Applicable if no leaks were found.

This report provides a summary of leaks and defects found during the Annual Method 21 Testing, Negative-Pressure Certification, and Visual inspection of the closed-vent and condensate collection systems and complies with the record keeping requirements of 63.454(b)(1-5).

The facility must initiate repairs to any defects within five (5) calendar days from this inspection and the defects must be repaired within fifteen (15) calendar days of the inspection. If the leak or defect requires the system to be shutdown in order to make repairs, or more emissions would occur from attempting the repair than delaying the repair, then the repairs may be delayed until the next process unit shutdown. A report must be supplied with the repair date and associated information, or the reason for the delay if the repairs are not completed within the 15-day period. These response requirements are specific to 40 CFR 63, specifically 63.453(k)(6), 63.453(l)(3), and 63.964(b)(1-2). Documentation of all repair attempts made and any leaks/defects requiring a process unit shutdown must be completed according to 63.454(b)(6-11).

I certify that the results of the Annual Method 21 Testing, Negative-Pressure Certification, and Visual inspection are accurate and complete to the best of my knowledge.

Inspector Name: Josh Howard

Signature: Josh Howard

Daily Calibration Sheet



Name: Josh Howard

Company: Environmental 360, Inc.

Date: 5/4/2021

Time: 9:26 AM

Client Name: New Indy Containerboard  
 Closed-Vent and Condensate-Collection Systems Cartkinton  
 Method 21 Testing

VOC Analyzer Model #: TVA2020-A2S1B1  
 VOC Analyzer Serial #: 2020504799

Zero Gas Concentration:	Zero Grade Air	Expiration Date:	Lot#:	Actual Value:
Span Gas Concentration:	500 PPM Methane	<u>9/24/24</u>	<u>304-401906627-1</u>	<u>20.1</u>
Span Gas Concentration:	<10,000 PPM Methane	<u>5/01/24</u>	<u>304-401804749-1</u>	<u>506</u>
		<u>11/20/24</u>	<u>304-401969514-1</u>	<u>9989</u>

Cylinder calibration gases must be analyzed and certified by the manufacturer within 2% accuracy.

	Reading	Actual Value	Precision (%)
500 PPM Methane Calibration Precision 1:	<u>499</u>	<u>506</u>	<u>1</u>
500 PPM Methane Calibration Precision 2:	<u>498</u>	<u>506</u>	<u>2</u>
500 PPM Methane Calibration Precision 3:	<u>497</u>	<u>506</u>	<u>2</u>
500 PPM Methane Calibration Precision 1 w/ Tubing:	<u>483</u>	<u>506</u>	<u>5</u>
500 PPM Methane Calibration Precision 2 w/ Tubing:	<u>489</u>	<u>506</u>	<u>3</u>
500 PPM Methane Calibration Precision 3 w/ Tubing:	<u>488</u>	<u>506</u>	<u>4</u>
<10,000 PPM Methane Calibration Precision 1:	<u>9993</u>	<u>9989</u>	<u>0</u>
<10,000 PPM Methane Calibration Precision 2:	<u>9983</u>	<u>9988</u>	<u>0</u>
<10,000 PPM Methane Calibration Precision 3:	<u>9884</u>	<u>9989</u>	<u>1</u>
<10,000 PPM Methane Calibration Precision 1 w/ Tubing:	<u>9964</u>	<u>9989</u>	<u>0</u>
<10,000 PPM Methane Calibration Precision 2 w/ Tubing:	<u>9950</u>	<u>9989</u>	<u>0</u>
<10,000 PPM Methane Calibration Precision 3 w/ Tubing:	<u>9996</u>	<u>9989</u>	<u>0</u>

The Calibration Precision must **not** have variability greater than 10%.

Response Factor: 1

The Response Factor must **not** be greater than 10.

Response Time: 3 sec

The Response Time must **not** be greater than 30 seconds. All probes and extensions used during the testing must be attached while measuring the response time.

Response Time with 20 Ft. Extension Tubing: 8 sec

Calibration Check: 481 / 506 = 5%  
 Calibration Check Time: 6:39 PM

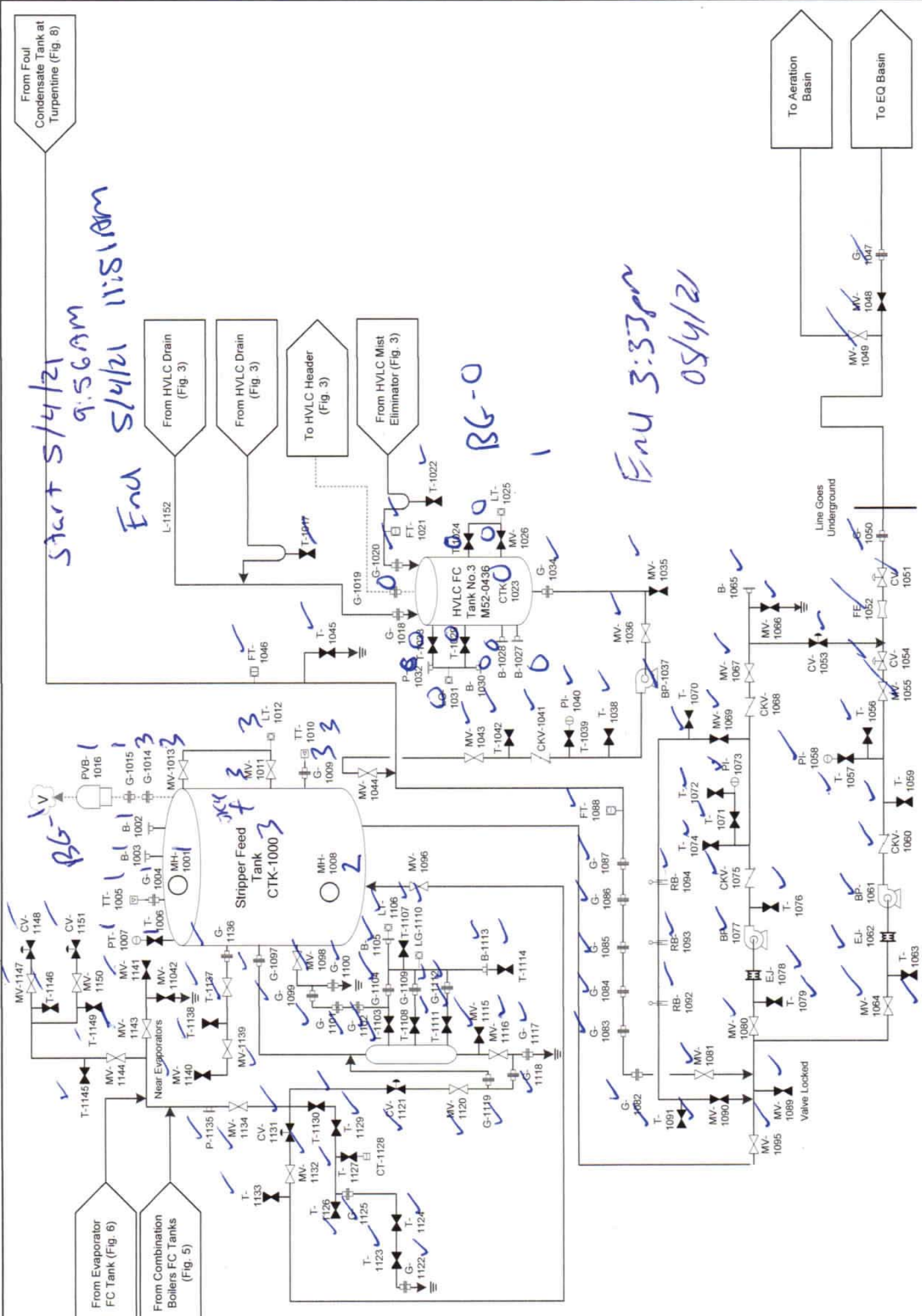
Comments: \_\_\_\_\_

I certify that calibration occurred prior to use and that all regulations and requirements were met.

Signed: Josh Howard

From Foul  
Condensate Tank at  
Turpentine (Fig. 8)

Start 5/4/21  
9:56 AM  
End  
5/4/21 11:51 AM



BG-0

End 5/4/21 11:51 AM

To Aeration Basin  
To EQ Basin

Rev. Date  
March 2021

Figure 1

New Indy Containerboard – Catawba Mill  
LDAR Inspection and Testing Diagrams  
Stripper System Foul Condensate

ENVIRONMENTAL 360



To Another Page and Indicated Equipment  
 From Another Page and Indicated Equipment  
 Vent Gases  
 Condensates  
 Liquor/Stock Lines  
 Process Lines



3:33 PM

Stripper System Foul Condensate  
Completed Date/Time: 8/4/2021

Number	Type	Pressure (+/-)	Background	VOC Reading	Is Component Free of Leaks or Defects?	Comments
1000	CTK	Cond	1	3	Yes	
1001	MH			1	Y	
1002	B			1	Y	
1003	B			1	Y	
1004	G			1	Y	
1005	TT			1	Y	
1006	T			1	Y	
1007	PT			1	Y	
1008	MH			2	Y	
1009	G			3	Y	
1010	TT			3	Y	
1011	MV			3	Y	
1012	LT			3	Y	
1013	MV			3	Y	
1014	G			3	Y	
1015	G			3	Y	
1016	PVB			3	Y	
1017	T	Cond		1	Y	
1018	G				Y	
1019	G				Y	
1020	G				Y	
1021	FT	Cond			Y	
1022	T				Y	
1023	CTK				Y	
1024	T	Cond			Y	
1025	LT	Cond			Y	
1026	MV	Cond			Y	
1027	B				Y	
1028	B				Y	
1029	T				Y	
1030	B				Y	
1031	LG				Y	
1032	P				Y	
1033	T				Y	
1034	G				Y	
1035	MV				Y	
1036	MV				Y	
1037	BP				Y	
1038	T				Y	
1039	T				Y	
1040	PI				Y	
1041	CKV				Y	
1042	T				Y	
1043	MV				Y	
1044	MV				Y	
1045	T				Y	
1046	FT				Y	
1047	G				Y	
1048	MV				Y	
1049	MV				Y	
1050	G				Y	
1051	CV				Y	
1052	FE				Y	
1053	CV				Y	
1054	CV				Y	
1055	MV				Y	
1056	T				Y	
1057	T				Y	
1058	PI				Y	
1059	T				Y	
1060	CKV				Y	
1061	BP				Y	
1062	EJ				Y	
1063	T				Y	
1064	MV				Y	
1065	B				Y	
1066	MV				Y	
1067	MV				Y	
1068	CKV				Y	
1069	MV				Y	
1070	T				Y	
1071	T				Y	
1072	T				Y	
1073	PI				Y	
1074	T				Y	

Number	Type	Pressure (+/-)	Background	VOC Reading	Is Component Free of Leaks or Defects?	Comments
1075	CKV					
1076	T					
1077	BP					
1078	EJ					
1079	T					
1080	MV					
1081	MV					
1082	G					
1083	G					
1084	G					
1085	G					
1086	G					
1087	G					
1088	FT					
1089	MV					
1090	MV					
1091	T					
1092	RB					
1093	RB					
1094	RB					
1095	MV					
1096	MV					
1097	G					
1098	MV					
1099	G					
1100	G					
1101	G					
1102	G					
1103	T					
1104	G					
1105	B					
1106	LT					
1107	T					
1108	T					
1109	G					
1110	LG					
1111	T					
1112	G					
1113	B					
1114	T					
1115	MV					
1116	MV					
1117	G					
1118	G					
1119	G					
1120	MV					
1121	CV					
1122	G					
1123	T					
1124	T					
1125	G					
1126	T					
1127	T					
1128	CT					
1129	T					
1130	T					
1131	CV					
1132	MV					
1133	T					
1134	MV					
1135	P					
1136	G					
1137	T					
1138	T					
1139	MV					
1140	MV					
1141	MV					
1142	MV					
1143	MV					
1144	MV					
1145	T					
1146	T					
1147	MV					
1148	CV					
1149	T					
1150	MV					
1151	CV					
1152	L					

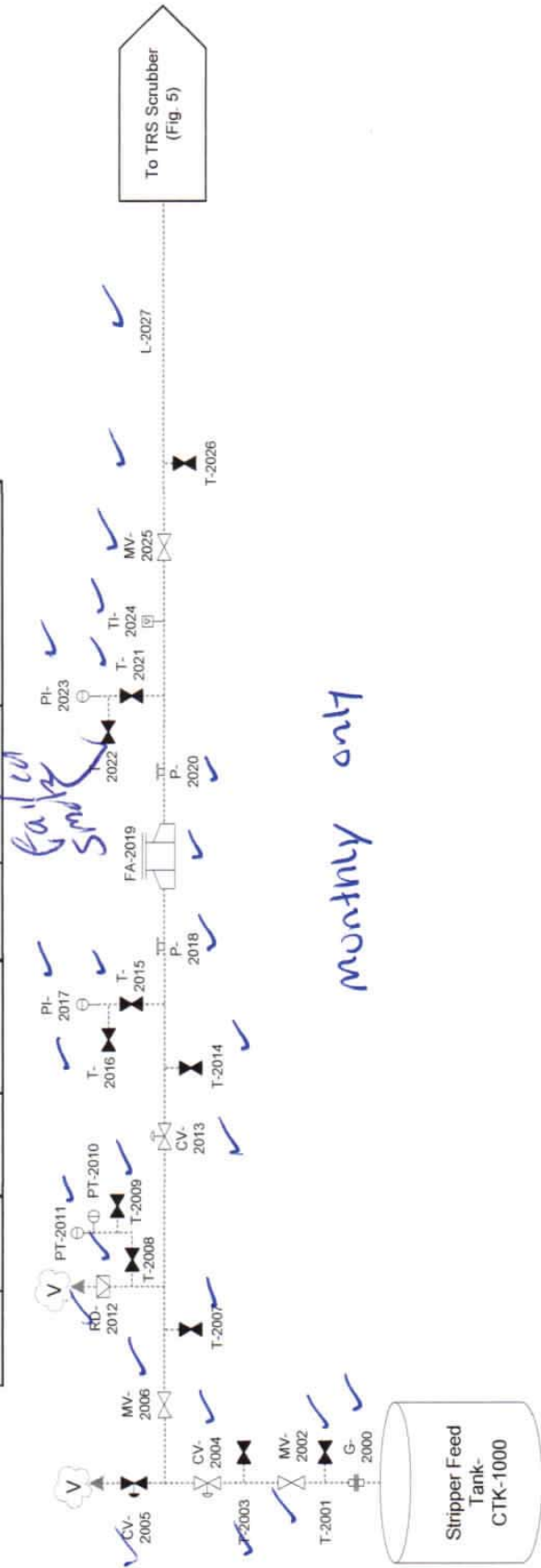
Cond

Cond

Stripper Feed Tank

Completed Date/Time: 5/14/2021 / ND

Number	Type	Pressure (+/-)	Background	VOC Reading	Is Component Free of Leaks or Defects?	Comments
2000	G				yes	
2001	T				Y	
2002	MV				Y	
2003	T				Y	
2004	CV				Y	
2005	CV				Y	
2006	MV				Y	
2007	T				Y	
2008	T				Y	
2009	T				Y	
2010	PT				Y	
2011	PT				Y	
2012	RD				Y	
2013	CV				Y	
2014	T				Y	
2015	T				Y	
2016	T				Y	
2017	PI				Y	
2018	P				Y	
2019	FA				Y	
2020	P				Y	
2021	T				Y	
2022	T				Y	
2023	PI				Y	
2024	TI				Y	
2025	MV				Y	
2026	T				Y	
2027	L				Y	Failed 5 mtc



- ..... Vent Gases
- Condensates
- Liquor/Stock Lines
- Process Lines

- To Another Page and Indicated Equipment
- From Another Page and Indicated Equipment



New Indy Containerboard – Catawba Mill  
LDAR Inspection and Testing Diagrams  
Stripper Feed Tank

Rev. Date  
March 2021  
Figure 2



Start 11:34AM  
05/04/21

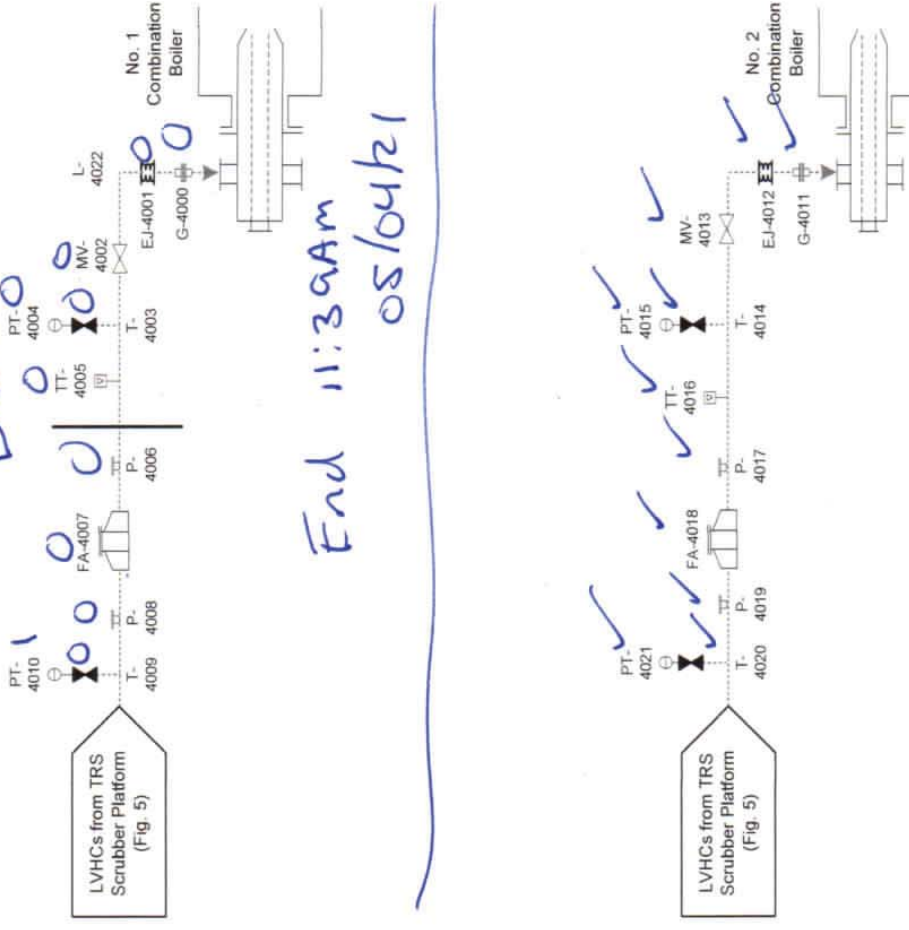
Combination Boiler LVHC Incineration

Completed Date/Time: 5/4/21 11:39AM

BGO

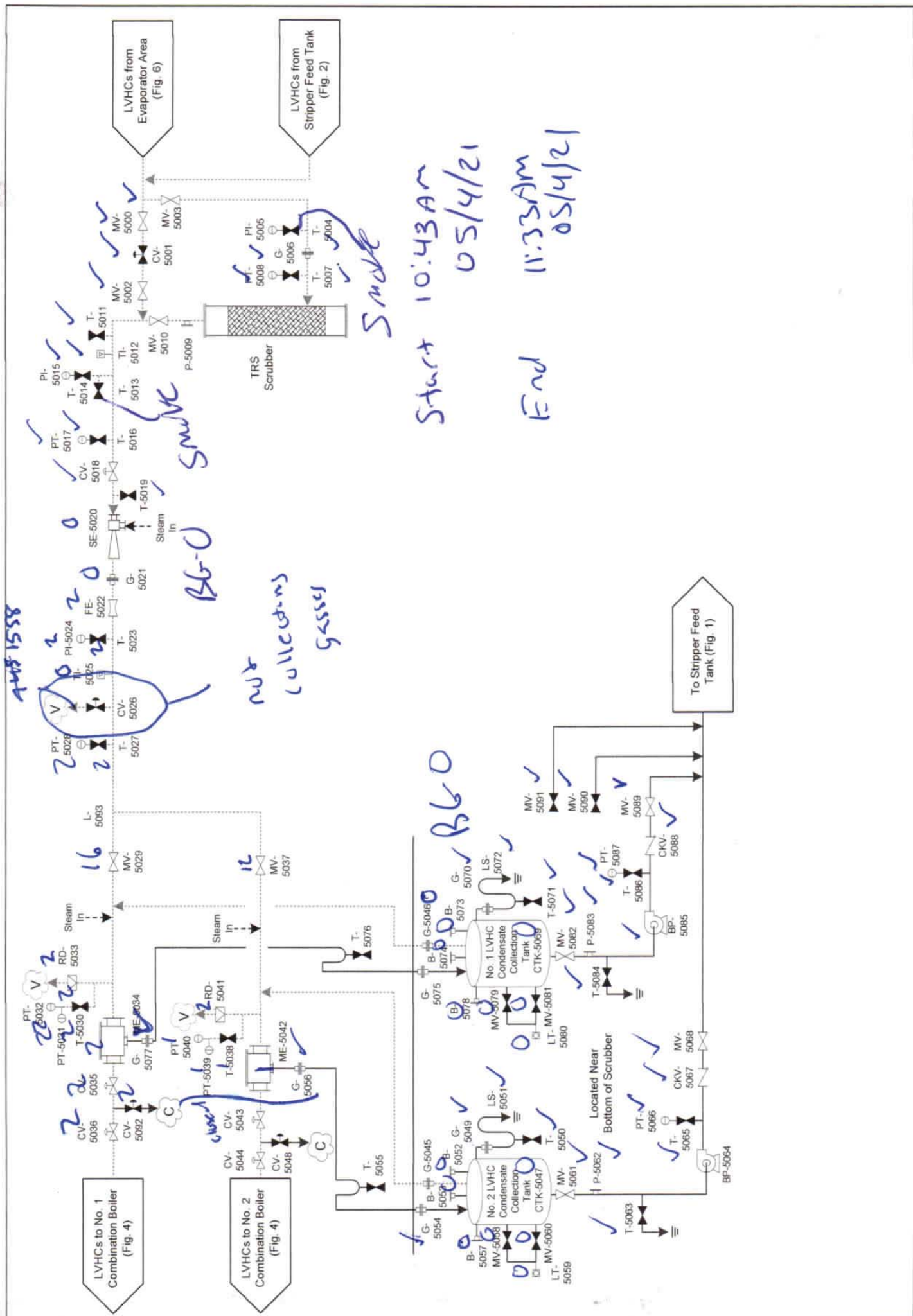
End 11:39AM  
05/04/21

Number	Type	Pressure (+/-)	Background	VOC Reading	Is Component Free of Leaks or Defects?	Comments
4000	G	+	0	0	yes	
4001	EJ			0	y	
4002	MV			0	y	
4003	T			0	y	
4004	PT			0	y	
4005	TT			0	y	
4006	P			0	y	
4007	FA			0	y	
4008	P			0	y	
4009	T			0	y	
4010	PT			0	y	
4011	G			1	y	monthly
4012	EJ				y	
4013	MV				y	
4014	T				y	
4015	PT				y	
4016	TT				y	
4017	P				y	
4018	FA				y	
4019	P				y	
4020	T				y	
4021	PT				y	
4022	L	NA			y	



New Indy Containerboard – Catawba Mill  
LDAR Inspection and Testing Diagrams  
Combination Boiler LVHC Incineration

Rev. Date  
March 2021  
Figure 4



Rev. Date  
March 2021

New Indy Containerboard – Catawba Mill  
LDAR Inspection and Testing Diagrams  
TRS Scrubber Platform

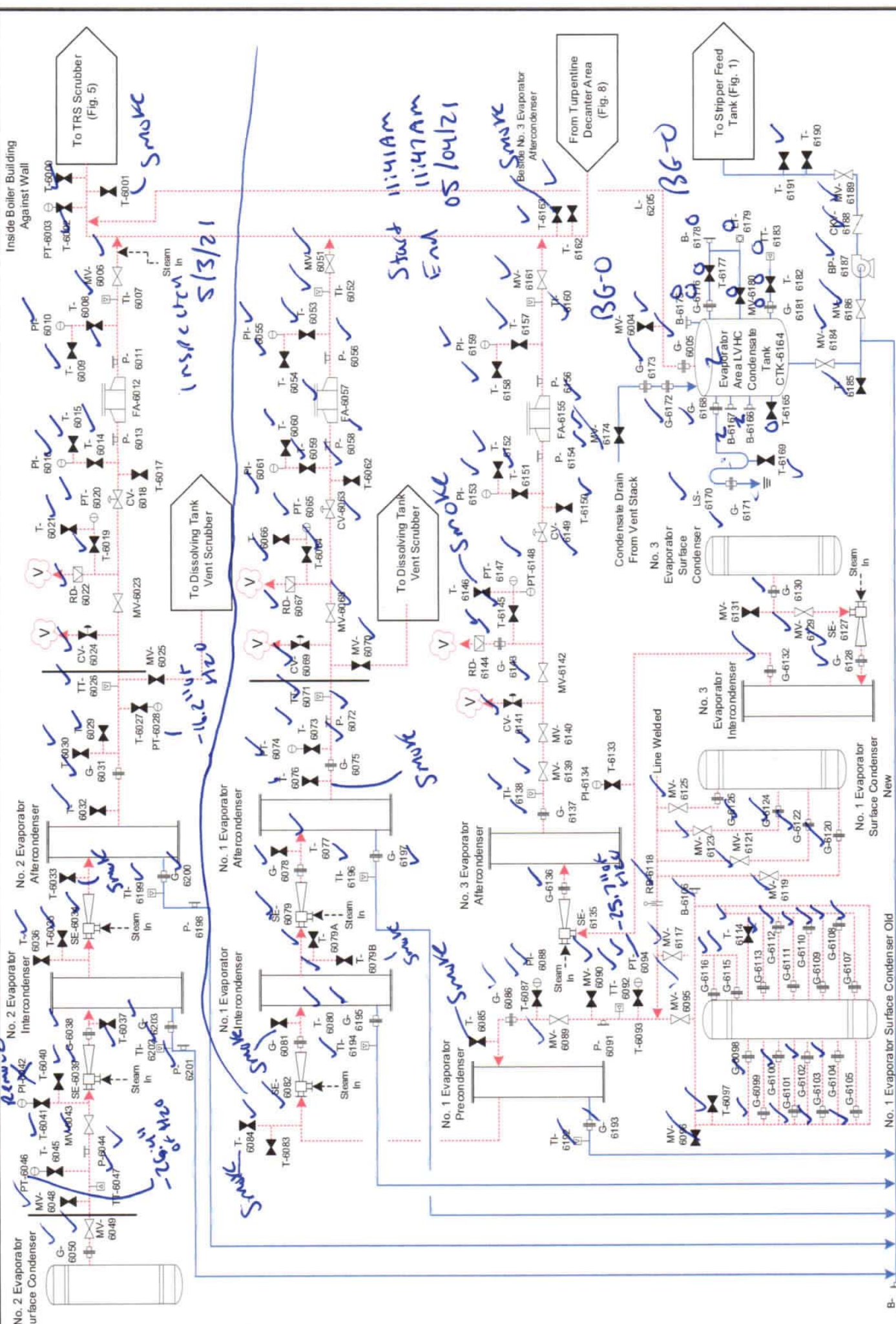


To Another Page and Indicated Equipment  
From Another Page and Indicated Equipment

Vent Gases  
Condensates  
Liquor/Stock Lines  
Process Lines

Figure 5





Rev. Date  
March 2021

New Indy Containerboard – Catawba Mill  
LDAR Inspection and Testing Diagrams  
Evaporator System



To Another Page and Indicated Equipment  
From Another Page and Indicated Equipment

--- Vent Gases  
 --- Condensates  
 --- Liquor/Stock Lines  
 --- Process Lines

Evaporator System

Completed Date/Time: 5/13/21 11:47 AM

Number	Type	Pressure (+/-)	Background	VOC Reading	Is Component Free of Leaks or Defects?	Comments
6000	T	—			Yes	
6001	T				Y	Smoke
6002	T				Y	
6003	PT				Y	
6004	MV				Y	
6005	G				Y	
6006	MV				Y	
6007	TI				Y	
6008	T				Y	
6009	T				Y	
6010	PI				Y	
6011	P				Y	
6012	FA				Y	
6013	P				Y	
6014	T				Y	
6015	T				Y	
6016	PI				Y	
6017	T				Y	
6018	CV				Y	
6019	T				Y	
6020	PT				Y	
6021	T				Y	
6022	RD				Y	
6023	MV				Y	
6024	CV				Y	
6025	MV				Y	
6026	TT				Y	
6027	T				Y	
6028	PT				Y	
6029	T				Y	
6030	T				Y	
6031	G				Y	
6032	T				Y	
6033	T				Y	
6034	SE				Y	
6035	T				Y	
6036	T				Y	
6037	T				Y	
6038	G				Y	
6039	SE				Y	
6040	T				Y	
6041	T				Y	
6042	PI				Y	Removal
6043	MV				Yes	
6044	P				Y	
6045	T				Y	
6046	PT				Y	
6047	TT				Y	
6048	MV				Y	

— 26.2 uoFHa

Smoke

Removal

— 26.4 uoFHa

6049	MV					
6050	G					Yes
6051	MV					Y
6052	TI					Y
6053	T					Y
6054	T					Y
6055	PI					Y
6056	P					Y
6057	FA					Y
6058	P					Y
6059	T					Y
6060	T					Y
6061	PI					Y
6062	T					Y
6063	CV					Y
6064	T					Y
6065	PT					Y
6066	T					Y
6067	RD					Y
6068	MV					Y
6069	CV					Y
6070	MV					Y
6071	TT					Y
6072	P					Y
6073	T					Y
6074	PT					Y
6075	G					Y
6076	T					Smoke
6077	T					Y
6078	G					Y
6079	SE					Smoke
6079A	T					Smoke
6079B	T					Smoke
6080	T					Y
6081	G					Y
6082	SE					Y
6083	T					Y
6084	T					Smoke
6085	T					Smoke
6086	G					Y
6087	T					Y
6088	PI					Y
6089	MV					Y
6090	MV					Y
6091	P					Y
6092	TT					Y
6093	T					Y
6094	PT					Y
6095	MV					Y
6096	MV					Y
6097	T					Y
6098	G					Y
6099	G					Y

— 26.2 uoFHa

Removal

— 26.4 uoFHa



Number	Type	Pressure (+/-)	Background	VOC Reading	Is Component Free of Leaks or Defects?	Comments
6100	G				Yes	
6101	G				Y	
6102	G				Y	
6103	G				Y	
6104	G				Y	
6105	G				Y	
6106	B				Y	
6107	G				Y	
6108	G				Y	
6109	G				Y	
6110	G				Y	
6111	G				Y	
6112	G				Y	
6113	G				Y	
6114	T				Y	
6115	G				Y	
6116	G				Y	
6117	MV				Y	
6118	RB				Y	
6119	MV				Y	
6120	G				Y	
6121	MV				Y	
6122	G				Y	
6123	MV				Y	
6124	G				Y	
6125	MV				Y	
6126	G				Y	
6127	SE				Y	
6128	G				Y	
6129	MV				Y	
6130	G				Y	
6131	MV				Y	
6132	G				Y	
6133	T				Y	
6134	PI				Y	
6135	SE				Y	
6136	G				Y	
6137	G				Y	
6138	TI				Y	
6139	MV				Y	
6140	MV				Y	
6141	CV				Y	
6142	MV				Y	
6143	G				Y	
6144	RD				Y	
6145	T				Y	
6146	T				Y	
6147	PT				Y	
6148	PT				Y	
6149	CV				Y	
6150	T				Y	
6151	T				Y	
6152	T				Y	

Number	Type	Pressure (+/-)	Background	VOC Reading	Is Component Free of Leaks or Defects?	Comments
6153	PI				Yes	
6154	P				Y	
6155	FA				Y	
6156	P				Y	
6157	T				Y	
6158	T				Y	
6159	PI				Y	
6160	TI				Y	
6161	MV				Y	
6162	T				Y	
6163	T				Y	
6164	CTK				Y	
6165	T				Y	
6166	B				Y	
6167	B				Y	
6168	G				Y	
6169	T				Y	
6170	LS				Y	
6171	G				Y	
6172	G				Y	
6173	G				Y	
6174	MV				Y	
6175	B				Y	
6176	G				Y	
6177	T				Y	
6178	B				Y	
6179	LT				Y	
6180	MV				Y	
6181	G				Y	
6182	T				Y	
6183	TT				Y	
6184	MV				Y	
6185	T				Y	
6186	MV				Y	
6187	BP				Y	
6188	CKV				Y	
6189	MV				Y	
6190	T				Y	
6191	T				Y	
6192	TI				Y	
6193	G				Y	
6194	TI				Y	
6195	G				Y	
6196	TI				Y	
6197	G				Y	
6198	P				Y	
6199	TI				Y	
6200	G				Y	
6201	P				Y	
6202	TI				Y	
6203	G				Y	
6204	B				Y	
6205	L				Y	

Evaporator System  
 Completed Date/Time: 5/4/21 11:47AM

smute

Cond

smute  
 26/4/21

Start 12:00 PM  
 05/04/21

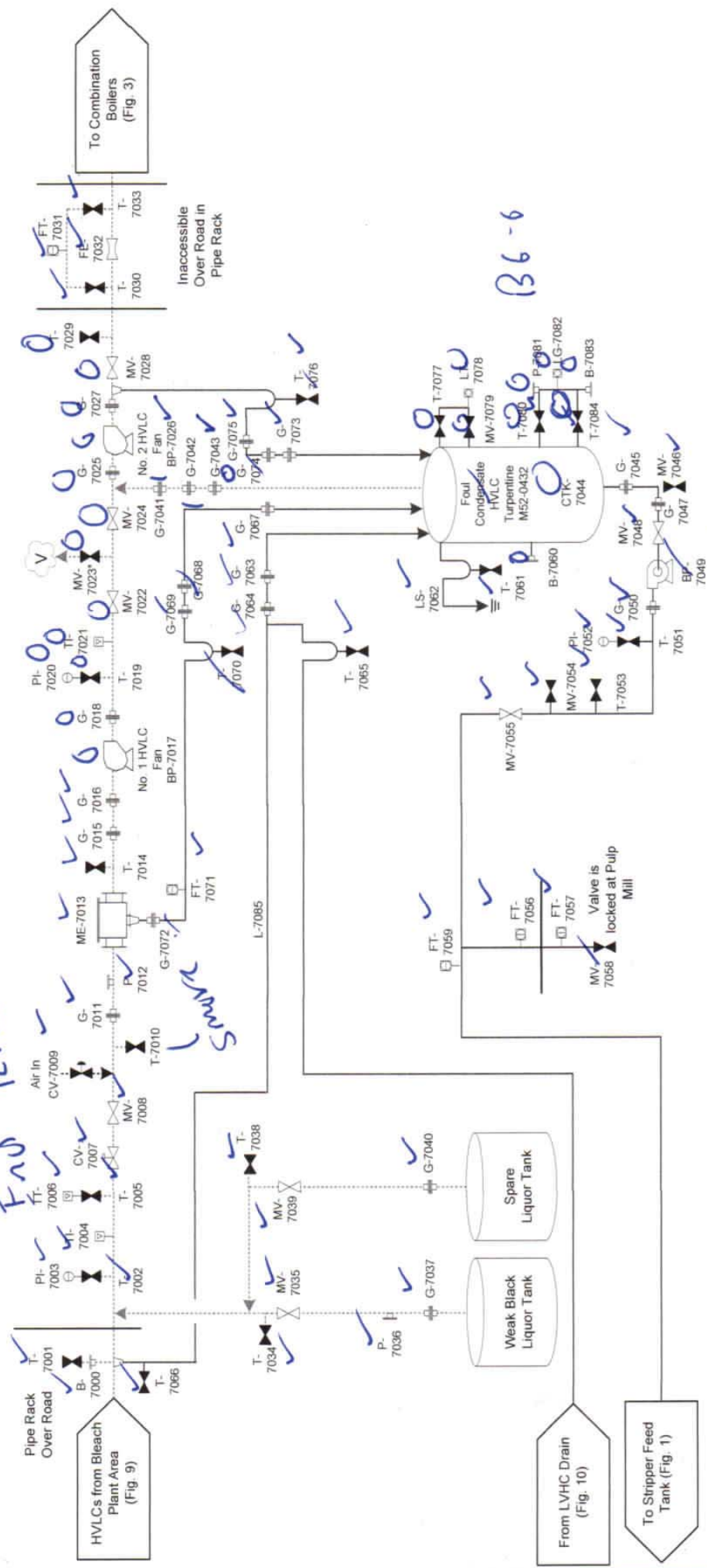
End 12:16 PM

BGO

SMMS

B6-6

Emy 3:42 PM 05/07/21



• Indicates car seal present

- Vent Gases
- Condensates
- Liquor/Stock Lines
- Process Lines
- To Another Page and Indicated Equipment
- From Another Page and Indicated Equipment



ENVIRONMENTAL 360

New Indy Containerboard – Catawba Mill  
 LDAR Inspection and Testing Diagrams  
 HVLC Blower Platform

Rev. Date  
 March 2021

Figure 7









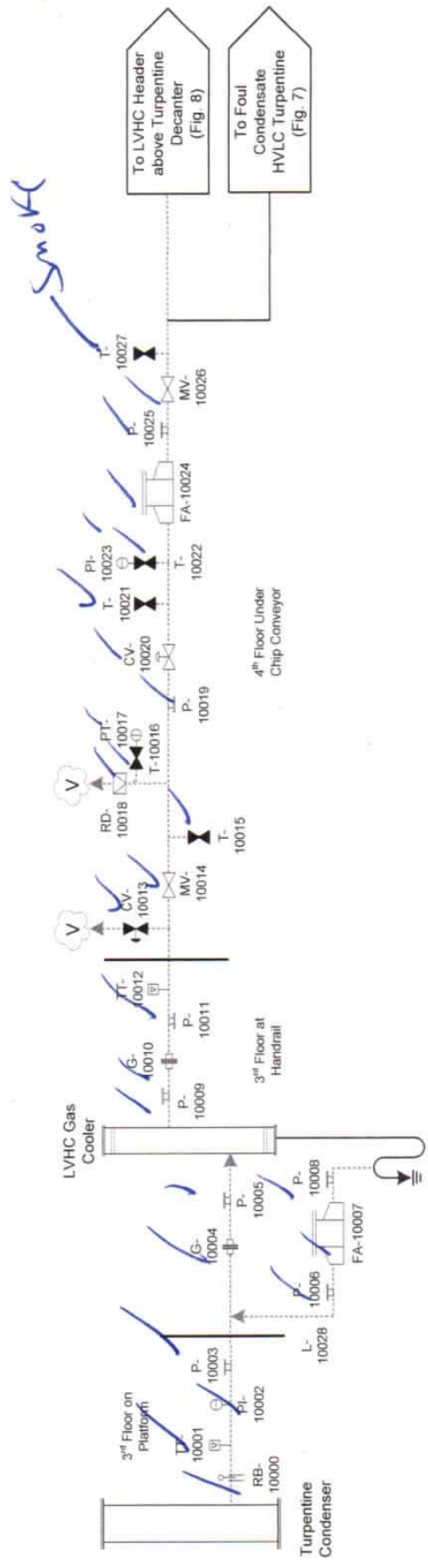
Turpentine Condenser and LVHC Gas Cooler

Completed Date/Time: 5/3/21 11:07 AM

Number	Type	Pressure (+/-)	Background	VOC Reading	Is Component Free of Leaks or Defects?	Comments
10000	RB				YES	
10001	TT				Y	
10002	PI				Y	
10003	P				Y	
10004	G				Y	
10005	P				Y	
10006	P				Y	
10007	FA				Y	
10008	P				Y	
10009	P				Y	
10010	G				Y	
10011	P				Y	
10012	TT				Y	

10013	CV							
10014	MV							
10015	T							
10016	T							
10017	PT							
10018	RD							
10019	P							
10020	CV							
10021	T							
10022	T							
10023	PI							
10024	FA							
10025	P							
10026	MV							
10027	T							
10028	L							

End 11:07 AM 5/3/21



**ENVIRONMENTAL 360**

- Vent Gases: [Symbol]
- Condensates: [Symbol]
- Liquor/Stock Lines: [Symbol]
- Process Lines: [Symbol]
- To Another Page and Indicated Equipment: [Symbol]
- From Another Page and Indicated Equipment: [Symbol]

New Indy Containerboard – Catawba Mill  
 LDAR Inspection and Testing Diagrams  
 Turpentine Condenser and LVHC Gas Cooler

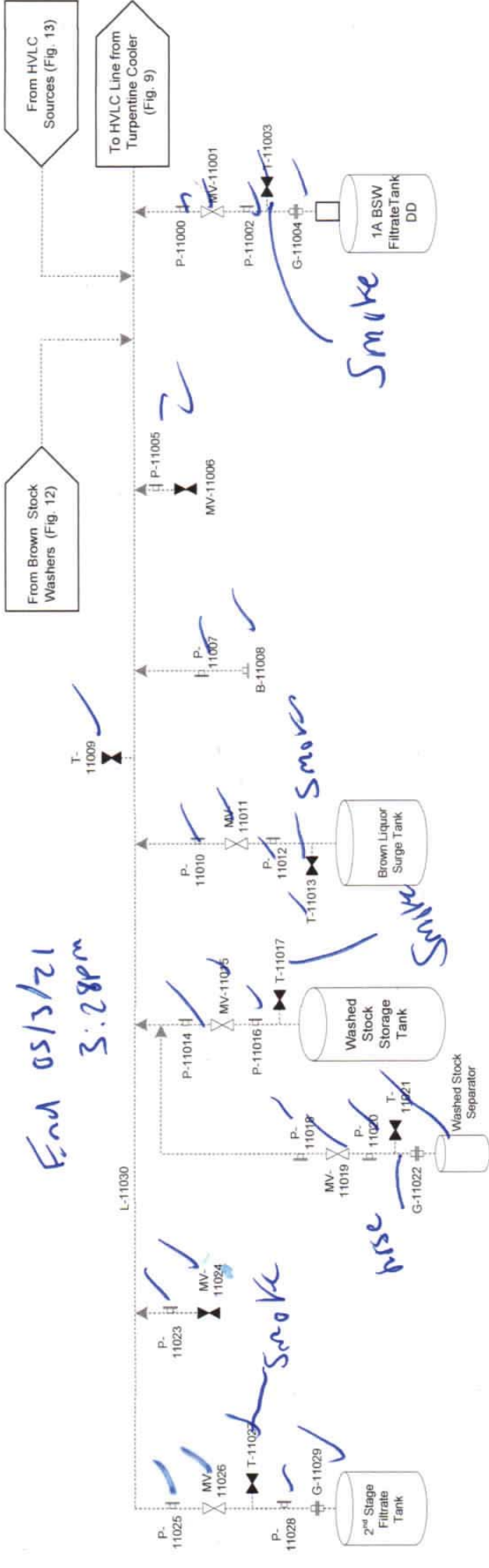
Rev. Date  
 March 2021  
 Figure 10

HVLC System at Pulp Mill (1 of 2)

Completed Date/Time: 5/13/21 3:28 PM

Number	Type	Pressure (+/-)	Background	VOC Reading	Is Component Free of Leaks or Defects?	Comments
11000	P	—			yes	
11001	MV				Y	
11002	P				Y	
11003	T				Y	Smoke
11004	G				Y	
11005	P				Y	
11006	MV				Y	
11007	P				Y	
11008	B				Y	
11009	T				Y	
11010	P				Y	
11011	MV				Y	
11012	P				Y	
11013	T				Y	Smoke

11014	P				Y	yes
11015	MV				Y	
11016	P				Y	
11017	T				Y	Smoke
11018	P				Y	
11019	MV				Y	
11020	P				Y	
11021	T				Y	
11022	G				Y	
11023	P				Y	
11024	MV				Y	
11025	P				Y	
11026	MV				Y	
11027	T				Y	Smoke
11028	P				Y	
11029	G				Y	
11030	L				Y	



ENVIRONMENTAL 360

To Another Page and Indicated Equipment

From Another Page and Indicated Equipment

Vent Gases

Condensates

Liquor/Stock Lines

Process Lines

New Indy Containerboard – Catawba Mill

LDAR Inspection and Testing Diagrams

HVLC System at Pulp Mill (1 of 2)

Rev. Date

March 2021

Figure 11



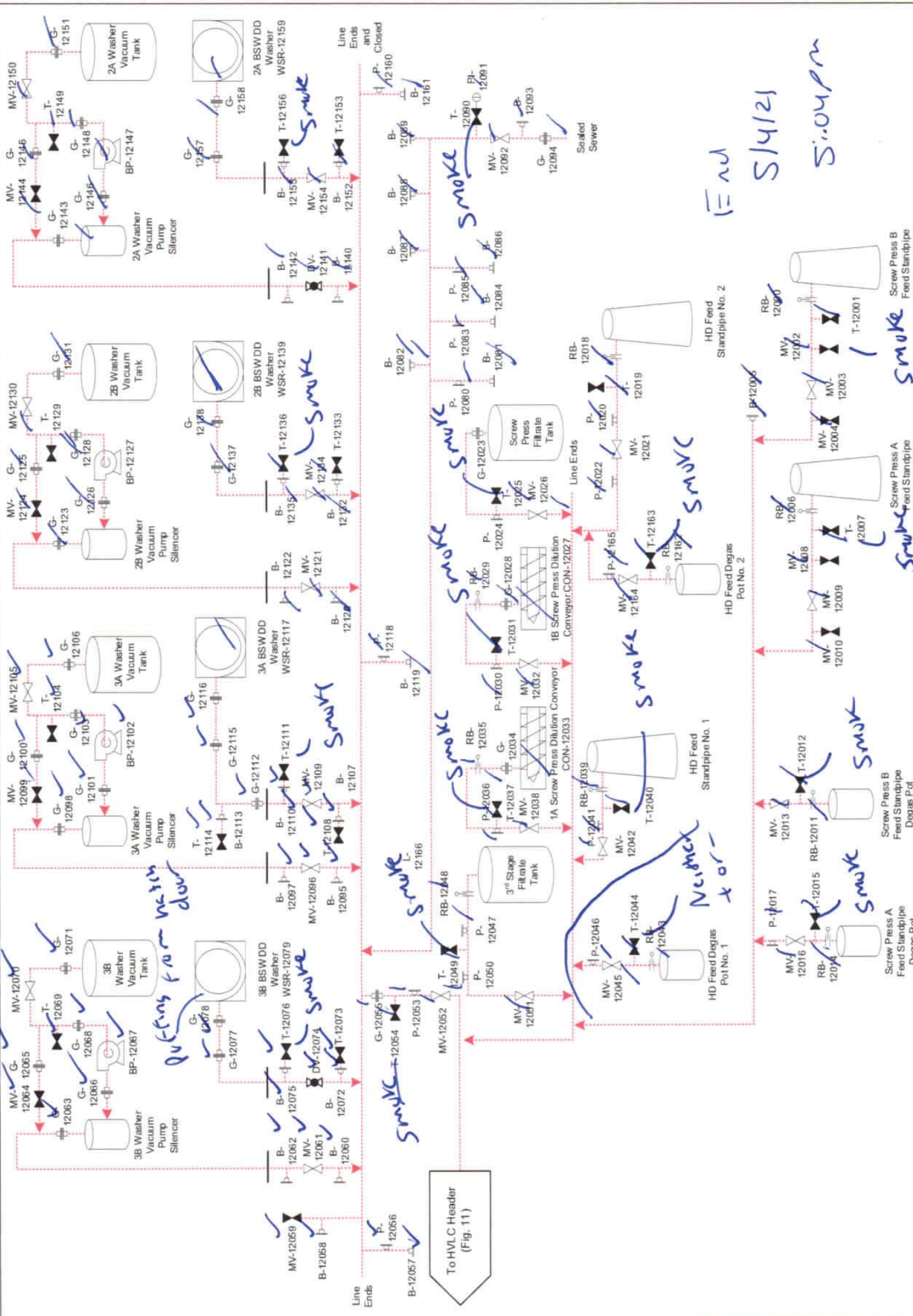
Pulp Mill BSWs

Completed Date/Time: 5/4/21 5:03 PM

Number	Type	Pressure (+/-)	Background	VOC Reading	Is Component Free of Leaks or Defects?	Comments
12081	B	—			yes	
12082	B				Y	
12083	P				Y	
12084	B				Y	
12085	P				Y	
12086	B				Y	
12087	B				Y	
12088	B				Y	
12089	B				Y	
12090	T				Y	
12091	PI				Y	Smok
12092	MV				Y	
12093	B				Y	
12094	G				Y	
12095	B				Y	
12096	MV				Y	
12097	B				Y	
12098	G				Y	
12099	MV				Y	
12100	G				Y	
12101	G				Y	
12102	BP				Y	
12103	G				Y	
12104	T				Y	
12105	MV				Y	
12106	G				Y	
12107	B				Y	
12108	T				Y	
12109	MV				Y	
12110	B				Y	
12111	T				Y	
12112	G				Y	
12113	B				Y	
12114	T				Y	
12115	G				Y	
12116	G				Y	
12117	WSR				Y	
12118	P				Y	
12119	B				Y	
12120	B				Y	
12121	MV				Y	
12122	B				Y	
12123	G				Y	

12124	MV							
12125	G							yes
12126	G							Y
12127	BP							Y
12128	G							Y
12129	T							Y
12130	MV							Y
12131	G							Y
12132	B							Y
12133	T							Y
12134	MV							Y
12135	B							Y
12136	T							Y
12137	G							Y
12138	G							Y
12139	WSR							Y
12140	B							Y
12141	DV							Y
12142	B							Y
12143	G							Y
12144	MV							Y
12145	G							Y
12146	G							Y
12147	BP							Y
12148	G							Y
12149	T							Y
12150	MV							Y
12151	G							Y
12152	B							Y
12153	T							Y
12154	MV							Y
12155	B							Y
12156	T							Y
12157	G							Y
12158	G							Y
12159	WSR							Y
12160	P							Y
12161	B							Y
12162	RB							Y
12163	T							Y
12164	MV							Y
12165	P							Y
12166	L							Y

YAB



Pulp Mill BSWs

Completed Date/Time:

5/4/21 5:03pm

Number	Type	Pressure (+/-)	Background	VOC Reading	Is Component Free of Leaks or Defects?	Comments
12000	RB	-			yes	
12001	T				y	
12002	MV				y	Smoke
12003	MV				y	
12004	MV				y	
12005	B				y	
12006	RB				y	
12007	T				y	Smoke
12008	MV				y	
12009	MV				y	
12010	MV				y	
12011	RB				y	
12012	T				y	Smoke
12013	MV				y	
12014	RB				y	
12015	T				y	Smoke
12016	MV				y	
12017	P				y	
12018	RB				y	
12019	T				y	
12020	P				y	
12021	MV				y	
12022	P				y	
12023	G				y	
12024	P				y	
12025	T				y	Smoke
12026	MV				y	
12027	CON				y	
12028	G				y	
12029	RB				y	
12030	P				y	
12031	T				y	Smoke
12032	MV				y	
12033	CON				y	
12034	G				y	
12035	RB				y	
12036	P				y	
12037	T				y	Smoke
12038	MV				y	

12039	RB					
12040	T					
12041	P					
12042	MV					
12043	RB					
12044	T					
12045	MV					
12046	P					
12047	P					
12048	RB					
12049	T					
12050	P					
12051	MV					
12052	MV					
12053	P					
12054	T					
12055	G					
12056	P					
12057	B					
12058	B					
12059	MV					
12060	B					
12061	MV					
12062	B					
12063	G					
12064	MV					
12065	G					
12066	G					
12067	BP					
12068	G					
12069	T					
12070	MV					
12071	G					
12072	B					
12073	T					
12074	DV					
12075	B					
12076	T					
12077	G					
12078	G					
12079	WSR					
12080	P					

monthly/visual

Smoke

Smoke

Smoke

Puffing

yes

yes

yes

yes

yes

yes

yes

yes

yes

yes

yes

yes

yes

yes

yes

yes

yes

yes

yes

yes

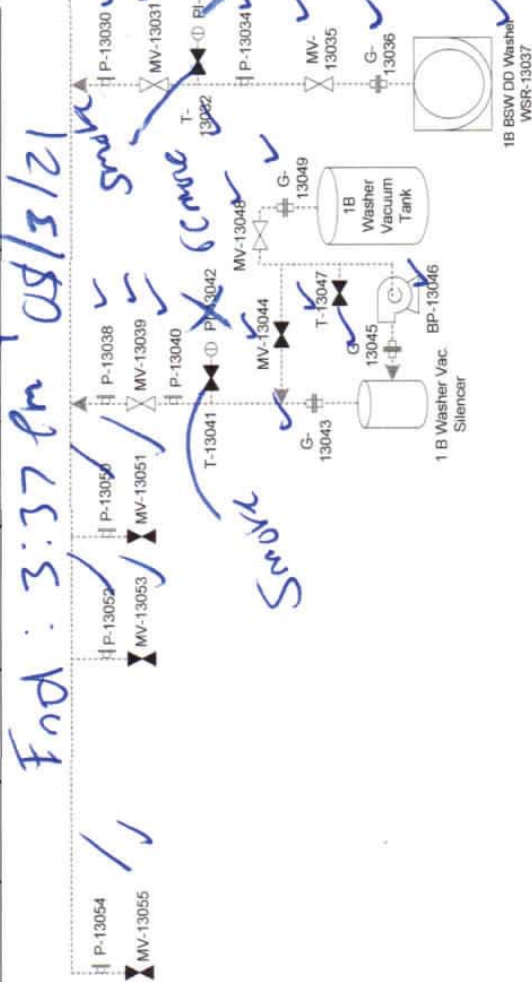
yes

yes

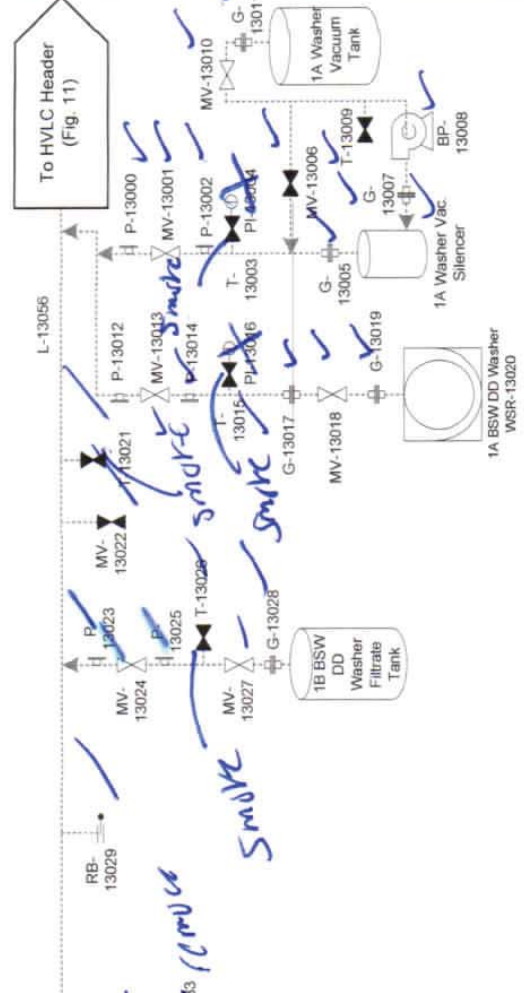
yes

**HVLC System at Pulp Mill (2 of 2)**  
 Completed Date/Time: 5/13/21 3:37 PM

Number	Type	Pressure (+/-)	Background	VOC Reading	Is Component Free of Leaks or Defects?	Comments
13000	P	-			YES	
13001	MV	-			Y	
13002	P	-			Y	
13003	T	-			Y	
13004	PI	-			YES	Smoke Remedy
13005	G	-			Y	
13006	MV	-			Y	
13007	G	-			Y	
13008	BP	-			Y	
13009	T	-			Y	
13010	MV	-			Y	
13011	G	-			Y	
13012	P	-			Y	
13013	MV	-			Y	
13014	P	-			Y	
13015	T	-			Y	
13016	PI	-			Y	Smoke Remedy
13017	G	-			Y	
13018	MV	-			Y	
13019	G	-			Y	
13020	WSR	-			Y	
13021	T	-			Y	
13022	MV	-			Y	
13023	P	-			Y	
13024	MV	-			Y	



13025	P	-			Y	
13026	T	-			Y	Smoke
13027	MV	-			Y	
13028	G	-			Y	
13029	RB	-			Y	
13030	P	-			Y	
13031	MV	-			Y	
13032	T	-			Y	Smoke Remedy
13033	PI	-			Y	
13034	P	-			Y	
13035	MV	-			Y	
13036	G	-			Y	
13037	WSR	-			Y	
13038	P	-			Y	
13039	MV	-			Y	
13040	P	-			Y	
13041	T	-			Y	
13042	PI	-			Y	Smoke Remedy
13043	G	-			Y	
13044	MV	-			Y	
13045	G	-			Y	
13046	BP	-			Y	
13047	T	-			Y	
13048	MV	-			Y	
13049	G	-			Y	
13050	P	-			Y	
13051	MV	-			Y	
13052	P	-			Y	
13053	MV	-			Y	
13054	P	-			Y	
13055	MV	-			Y	
13056	L	-			Y	



- ..... Vent Gases
- Condensates
- Liquor/Stock Lines
- Process Lines
- ◁ To Another Page and Indicated Equipment
- ◁ From Another Page and Indicated Equipment



New Indy Containerboard – Catawba Mill  
 LDAR Inspection and Testing Diagrams  
 HVLC System at Pulp Mill (2 of 2)

Rev. Date  
 March 2021  
 Figure 13

Inspection Date: June 7th, 2021



New Indy Containerboard - Catawba Mill  
5300 Cureton Ferry Rd.  
Catawba, SC 29704

**2021 Monthly LDAR Inspection Summary Report**

**Table 1: Visual Inspection Summary Table**

Equipment Number	Date	Description of Leak or Visual Defect
CTK-1000	6/7/2021	Stripper Feed Tank CTK-1000 is puffing from top of tank.
MV-1008 (Old ID Number)	6/7/2021	Manual Valve (old MV-1008) is located on the foul condensate line at the outlet of No. 1 Pre-Heater). The valve is the bypass valve for the stripped condensate and is dripping from valve stem.
T-3030 (Old ID Number)	6/7/2021	Tap valve (old T-3030) is located on SOG line near Trim Reflux Condenser and above the Stripper Column. The valve is leaking from threaded connection with a VOC reading of 788 ppm.
CV-5026	6/7/2021	Control valve CV-5026 is located on the LVHC line at outlet of Steam Ejector and prior to the mist eliminators. The valve is not collecting gases.
PT-5032	6/7/2021	Pressure transmitter PT-5032 is located on LVHC line between mist eliminator and rupture disc on steam ejector platform. The transmitter is puffing from threaded connection.
WSR-12079	6/7/2021	The 3B BSW DD Washer is puffing around hatch door.
<b>First Attempt to Repair must be completed by:</b>	5 Days from Inspection Date	Not Applicable if no leaks were found.
<b>Repairs must be completed by:</b>	15 Days from Inspection Date	Not Applicable if no leaks were found.

This report provides a summary of leaks and visual defects found during the visual inspection of the closed-vent and condensate-collection systems and complies with the record keeping requirements of 63.454(b)(1-2, 4-5).

The facility must initiate repairs to any defects within five (5) calendar days from this inspection and the defects must be repaired within fifteen (15) calendar days of the inspection. If the leak or defect requires the system to be shutdown in order to make repairs, or more emissions would occur from attempting the repair than delaying the repair, then the repairs may be delayed until the next process unit shutdown. A report must be supplied with the repair date and associated information, or the reason for the delay if the repairs are not completed within the 15-day period. These response requirements are specific to 40 CFR 63, specifically 63.453(k)(6), 63.453(l)(3), and 63.964(b)(1-2). Documentation of all repair attempts made and any leaks/defects requiring a process unit shutdown must be completed according to 63.454(b)(6-11).

I certify that the results of the visual inspection are accurate and complete to the best of my knowledge.

Inspector Name: Josh Howard

Signature: Josh Howard

Daily Calibration Sheet



Name: Josh Howard

Company: Environmental 360, Inc.

Date: 6/7/2021

Time: 3:14 PM

Client Name: New Fryer cctawby  
 Closed-Vent and Condensate-Collection Systems  
 Method 21 Testing

VOC Analyzer Model #: TVA2020 A2S1B1  
 VOC Analyzer Serial #: 202015010799

Zero Gas Concentration: Zero Grade Air	Expiration Date: <u>09/24/24</u>	Lot#: <u>304-40196627-1</u>	Actual Value: <u>&lt;0.1</u>
Span Gas Concentration: 500 PPM Methane	<u>11/20/24</u>	<u>304-401969513-1</u>	<u>503</u>
Span Gas Concentration: <10,000 PPM Methane	<u>11/20/24</u>	<u>304-401969514-1</u>	<u>9989</u>

Cylinder calibration gases must be analyzed and certified by the manufacturer within 2% accuracy.

	Reading	Actual Value	Precision (%)
500 PPM Methane Calibration Precision 1:	<u>505</u>	<u>503</u>	<u>0</u>
500 PPM Methane Calibration Precision 2:	<u>502</u>	<u>503</u>	<u>0</u>
500 PPM Methane Calibration Precision 3:	<u>502</u>	<u>503</u>	<u>0</u>
500 PPM Methane Calibration Precision 1 w/ Tubing:	<u>496</u>	<u>503</u>	<u>1</u>
500 PPM Methane Calibration Precision 2 w/ Tubing:	<u>495</u>	<u>503</u>	<u>2</u>
500 PPM Methane Calibration Precision 3 w/ Tubing:	<u>496</u>	<u>503</u>	<u>1</u>
<10,000 PPM Methane Calibration Precision 1:	<u>9952</u>	<u>9989</u>	<u>0</u>
<10,000 PPM Methane Calibration Precision 2:	<u>9962</u>	<u>9989</u>	<u>0</u>
<10,000 PPM Methane Calibration Precision 3:	<u>9983</u>	<u>9989</u>	<u>0</u>
<10,000 PPM Methane Calibration Precision 1 w/ Tubing:	<u>9975</u>	<u>9989</u>	<u>0</u>
<10,000 PPM Methane Calibration Precision 2 w/ Tubing:	<u>9990</u>	<u>9989</u>	<u>0</u>
<10,000 PPM Methane Calibration Precision 3 w/ Tubing:	<u>9953</u>	<u>9989</u>	<u>0</u>

The Calibration Precision must **not** have variability greater than 10%.

Response Factor: 1 The Response Factor must **not** be greater than 10.

Response Time: 3 sec The Response Time must **not** be greater than 30 seconds. All probes and extensions used during the testing must be attached while measuring the response time.

Response Time with 20 Ft. Extension Tubing: 8 sec  
 Calibration Check: 488 / 503 = 3 %  
 Calibration Check Time: 8:11 PM

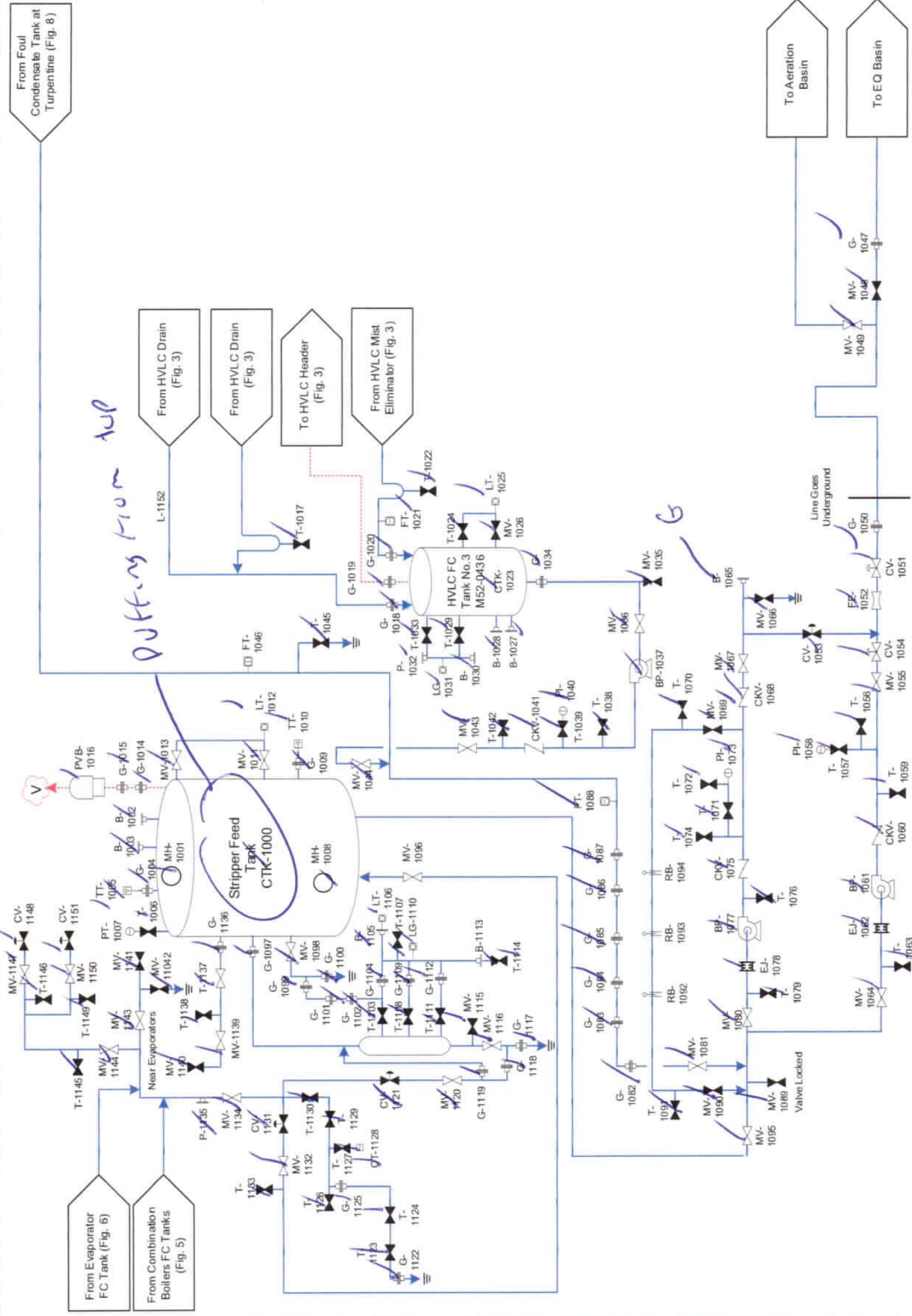
Comments: \_\_\_\_\_

I certify that calibration occurred prior to use and that all regulations and requirements were met.

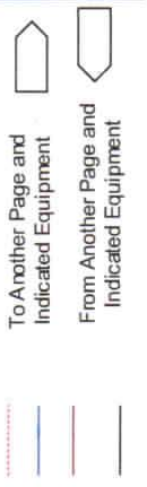
Signed: Josh Howard

From Foul  
Condensate Tank at  
Turpentine (Fig. 8)

*Outflows from top*



- Vent Gases
- Condensates
- Liquor/Stock Lines
- Process Lines
- To Another Page and Indicated Equipment
- From Another Page and Indicated Equipment



**ENVIRONMENTAL360**

New Indy Containerboard – Catawba Mill  
LDAR Inspection and Testing Diagrams  
Stripper System Foul Condensate

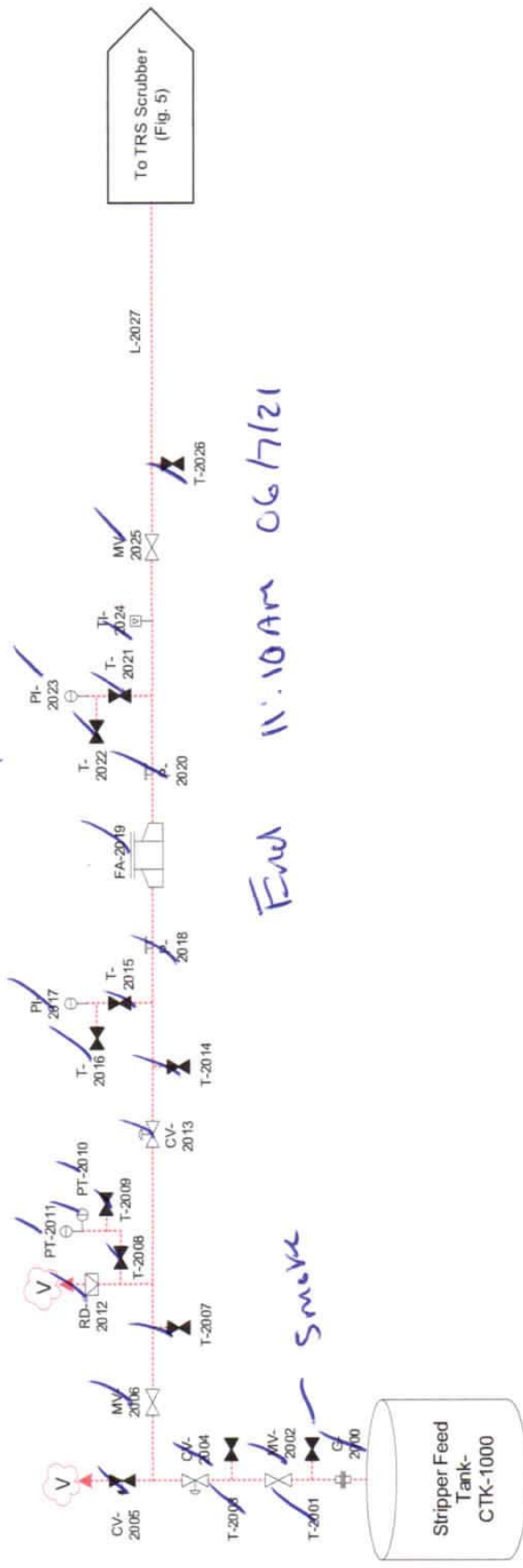
Rev. Date  
May 2021  
Figure 1





Stripper Feed Tank  
Completed Date/Time: 06/07/21 11:10 AM

Number	Type	Pressure (+/-)	Background	VOC Reading	Is Component Free of Leaks or Defects?	Comments
2000	G				YES	
2001	T				Y	
2002	MV				Y	
2003	T				Y	
2004	CV				Y	
2005	CV				Y	
2006	MV				Y	
2007	T				Y	
2008	T				Y	
2009	T				Y	
2010	PT				Y	
2011	PT				Y	
2012	RD				Y	
2013	CV				Y	
2014	T				Y	
2015	T				Y	
2016	T				Y	
2017	PI				Y	
2018	P				Y	
2019	FA				Y	
2020	P				Y	
2022	T				Y	
2023	PI				Y	
2024	TI				Y	
2025	MV				Y	
2026	T				Y	
2027	L				Y	



End 11:10 AM 06/07/21

- Vent Gases
- Condensates
- Liquor/Stock Lines
- Process Lines
- To Another Page and Indicated Equipment
- From Another Page and Indicated Equipment

Stripper Feed Tank  
CTK-1000



New Indy Containerboard – Catawba Mill  
LDAR Inspection and Testing Diagrams  
Stripper Feed Tank

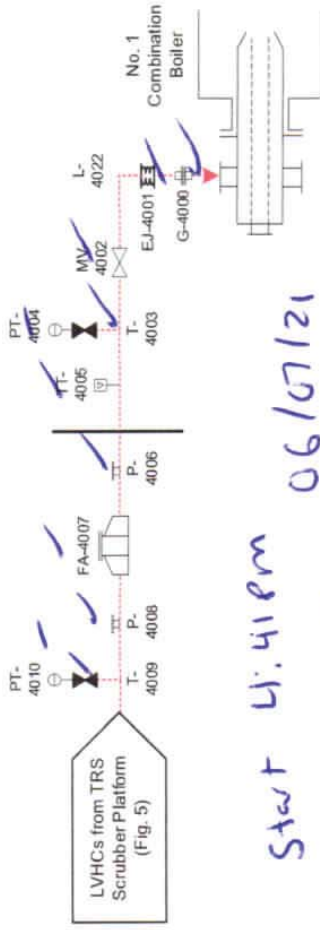
Rev. Date  
May 2021  
Figure 2



Combination Boiler LVHC Incineration

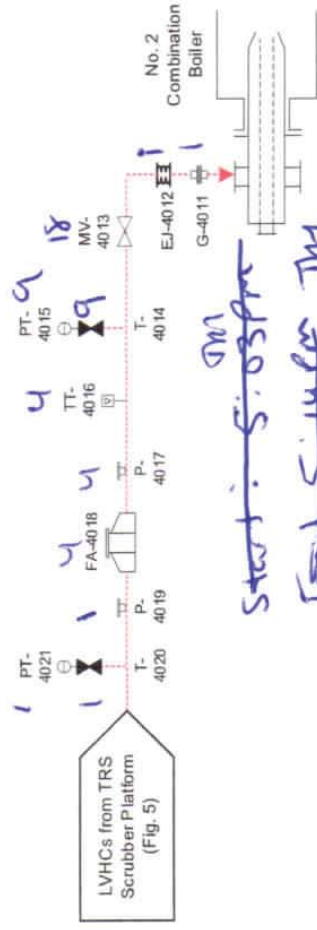
Completed Date/Time: 06/07/21 5:14pm

Number	Type	Pressure (+/-)	Background	VOC Reading	Is Component Free of Leaks or Defects?	Comments
4000	G				Yes	Monthly
4001	EJ				Y	
4002	MV				Y	
4003	T				Y	
4004	PT				Y	
4005	TT				Y	
4006	P				Y	
4007	FA				Y	
4008	P				Y	
4009	T				Y	
4010	PT				Y	
4011	G			1	Y	
4012	EJ			1	Y	
4013	MV			18	Y	
4014	T			9	Y	
4015	PT			9	Y	
4016	TT			5	Y	
4017	P			5	Y	
4018	FA			5	Y	
4019	P			5	Y	
4020	T			1	Y	
4021	PT			1	Y	
4022	L				Y	



Start 4:41pm 06/07/21  
 End 4:50pm  
 Start JKU

BG-1



Start: 5:03pm JM  
 End: 5:44pm JM  
 06/07/21

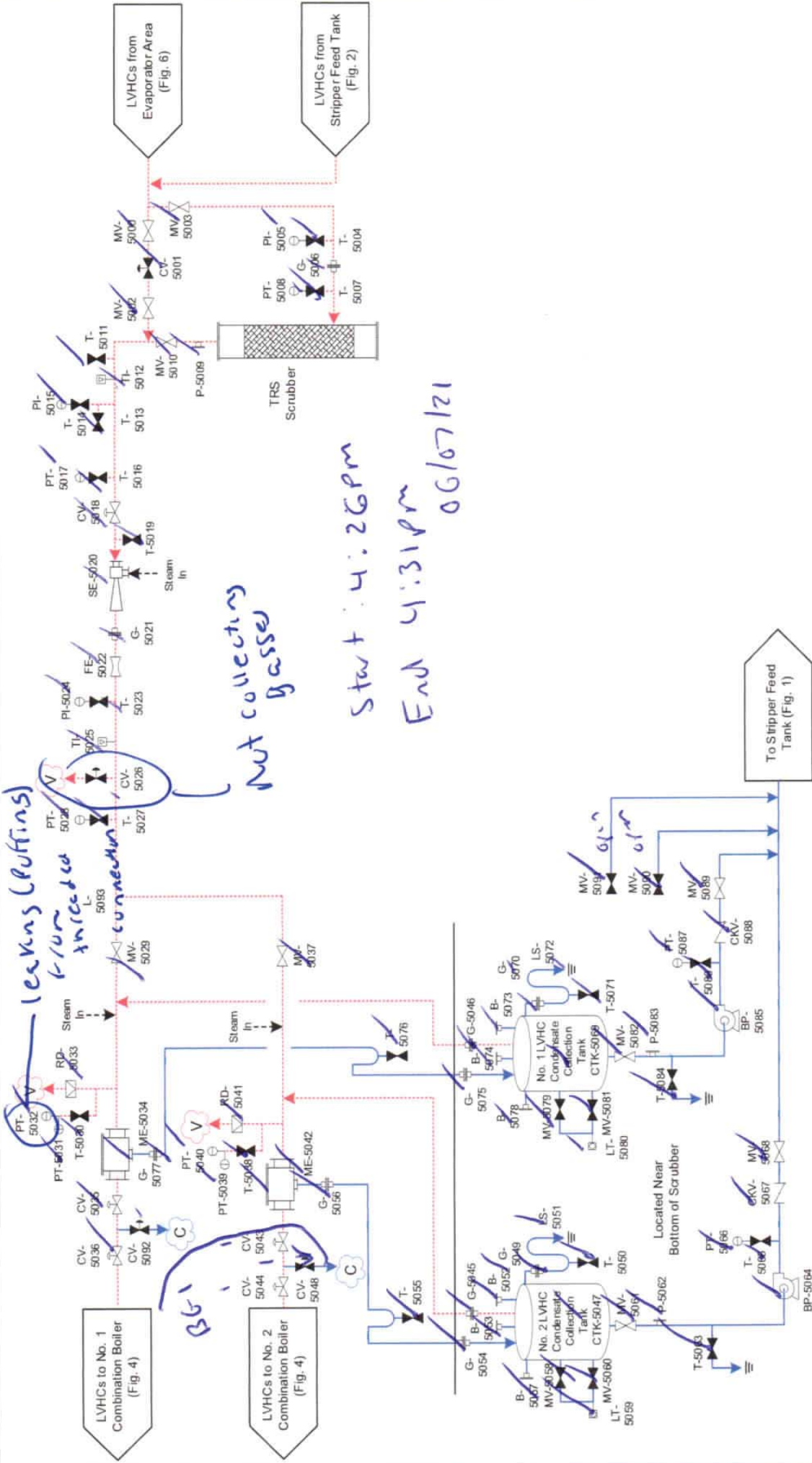
Vent Gases  
 Condensates  
 Liquor/Stock Lines  
 Process Lines

To Another Page and Indicated Equipment  
 From Another Page and Indicated Equipment



New Indy Containerboard - Catawba Mill  
 LDAR Inspection and Testing Diagrams  
 Combination Boiler LVHC Incineration

Rev. Date  
 May 2021  
 Figure 4



Rev. Date  
May 2021

New Indy Containerboard – Catawba Mill  
LDAR Inspection and Testing Diagrams  
TRS Scrubber Platform

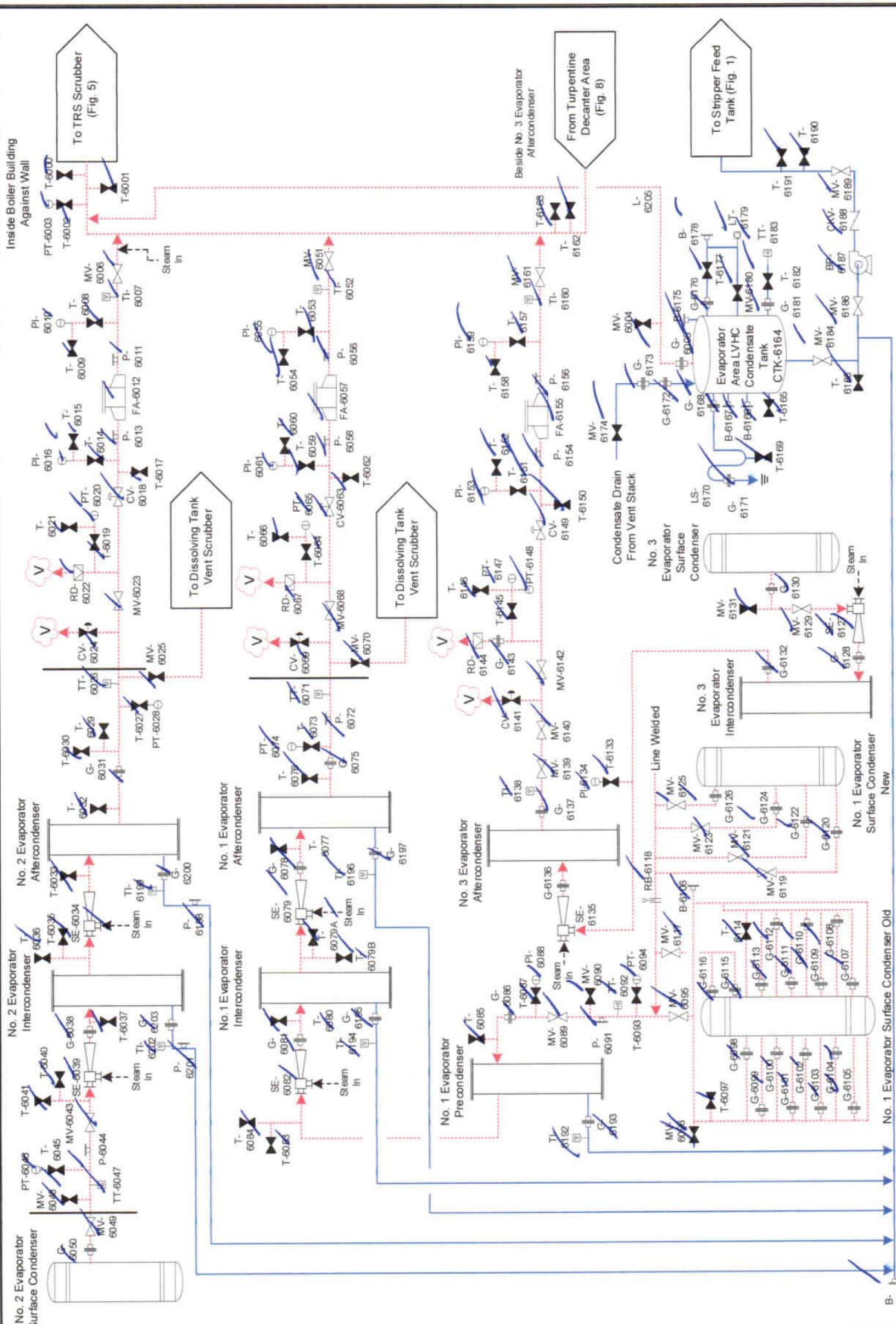


To Another Page and Indicated Equipment

From Another Page and Indicated Equipment

Figure 5





<p>Rev. Date May 2021</p>	<p>New Indy Containerboard – Catawba Mill LDAR Inspection and Testing Diagrams Evaporator System</p>		<p>To Another Page and Indicated Equipment</p> <p>From Another Page and Indicated Equipment</p> <p>Vent Gases</p> <p>Condensates</p> <p>Liquor/Stock Lines</p> <p>Process Lines</p>
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Figure 6



Evaporator System  
Completed Date/Time: 6/7/21

Number	Type	Pressure (+/-)	Background	VOC Reading	Is Component Free of Leaks or Defects?	Comments
6100	G				Y	
6101	G				Y	
6102	G				Y	
6103	G				Y	
6104	G				Y	
6105	G				Y	
6106	B				Y	
6107	G				Y	
6108	G				Y	
6109	G				Y	
6110	G				Y	
6111	G				Y	
6112	G				Y	
6113	G				Y	
6114	T				Y	
6115	G				Y	
6116	G				Y	
6117	MV				Y	
6118	RB				Y	
6119	MV				Y	
6120	G				Y	
6121	MV				Y	
6122	G				Y	
6123	MV				Y	
6124	G				Y	
6125	MV				Y	
6126	G				Y	
6127	SE				Y	
6128	G				Y	
6129	MV				Y	
6130	G				Y	
6131	MV				Y	
6132	G				Y	
6133	T				Y	
6134	PI				Y	
6135	SE				Y	
6136	G				Y	
6137	G				Y	
6138	TI				Y	
6139	MV				Y	
6140	MV				Y	
6141	CV				Y	
6142	MV				Y	
6143	G				Y	
6144	RD				Y	
6145	T				Y	
6146	T				Y	
6147	PT				Y	
6148	PT				Y	
6149	CV				Y	
6150	T				Y	
6151	T				Y	
6152	T				Y	

6153	PI					Y
6154	P					Y
6155	FA					Y
6156	P					Y
6157	T					Y
6158	T					Y
6159	PI					Y
6160	TI					Y
6161	MV					Y
6162	T					Y
6163	T					Y
6164	CTK					Y
6165	T					Y
6166	B					Y
6167	B					Y
6168	G					Y
6169	T					Y
6170	LS					Y
6171	G					Y
6172	G					Y
6173	G					Y
6174	MV					Y
6175	B					Y
6176	G					Y
6177	T					Y
6178	B					Y
6179	LT					Y
6180	MV					Y
6181	G					Y
6182	T					Y
6183	TT					Y
6184	MV					Y
6185	T					Y
6186	MV					Y
6187	BP					Y
6188	CKV					Y
6189	MV					Y
6190	T					Y
6191	T					Y
6192	TI					Y
6193	G					Y
6194	TI					Y
6195	G					Y
6196	TI					Y
6197	G					Y
6198	P					Y
6199	TI					Y
6200	G					Y
6201	P					Y
6202	TI					Y
6203	G					Y
6204	B					Y
6205	L					Y



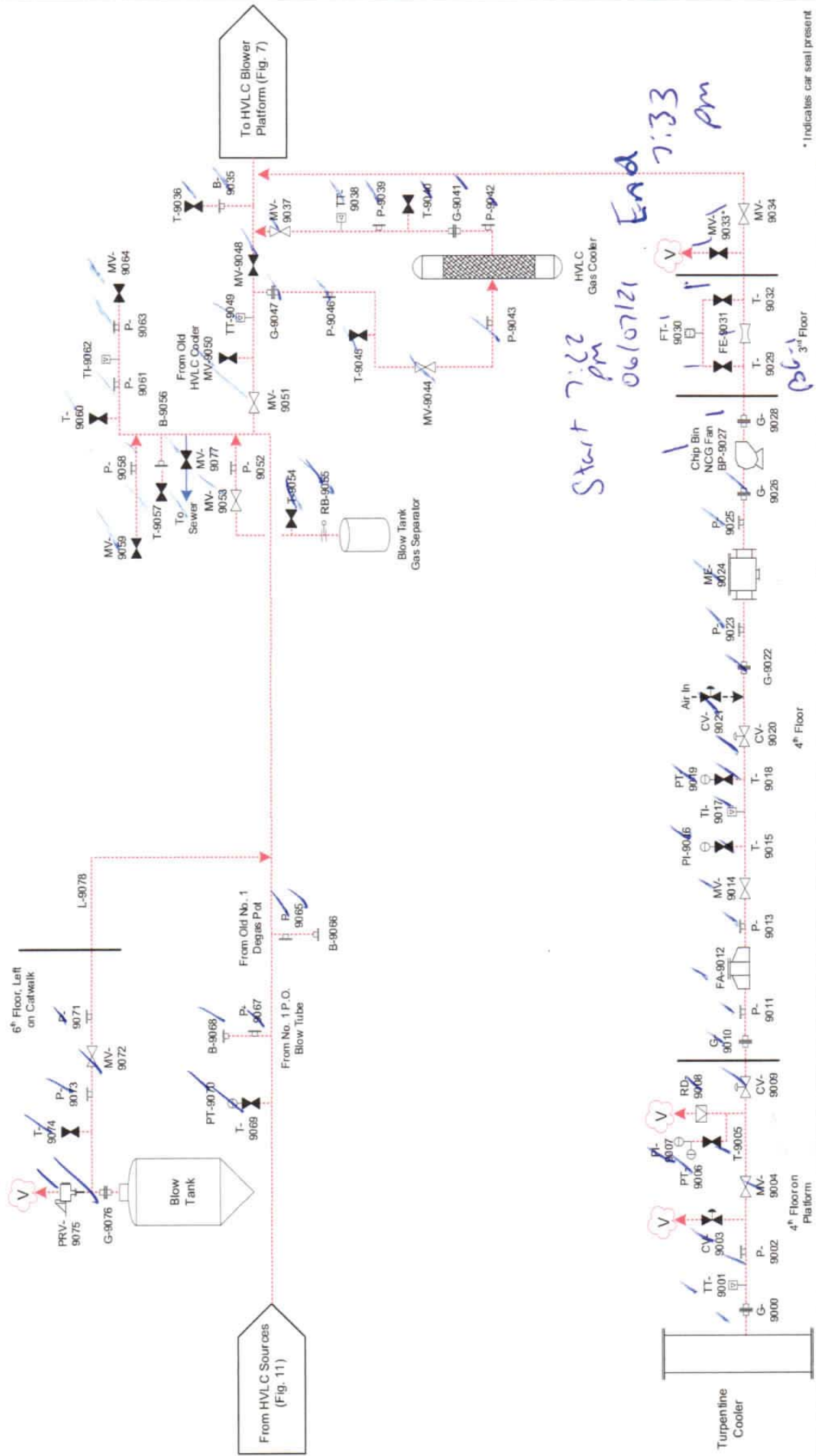


HVLC Blower Platform

Completed Date/Time: 06/17/21

Number	Type	Pressure (+/-)	Background	VOC Reading	Is Component Free of Leaks or Defects?	Comments
7000	B				YES	
7001	T				Y	
7002	T				Y	
7003	PI				Y	
7004	TI				Y	
7005	T				Y	
7006	TT				Y	
7007	CV				Y	
7008	MV				Y	
7009	CV				Y	
7010	T				Y	
7011	G				Y	
7012	P				Y	
7013	ME				Y	
7014	T				Y	
7015	G				Y	
7016	G				Y	
7017	BP				Y	
7018	G				Y	
7019	T				Y	
7020	PI				Y	
7021	TI				Y	
7022	MV				Y	
7023	MV				Y	Car seal present
7024	MV				Y	
7025	G				Y	
7026	BP				Y	
7027	G				Y	
7028	MV				Y	
7029	T				Y	
7030	T				Y	
7031	FT				Y	
7032	FE				Y	
7033	T				Y	
7034	T				Y	
7035	MV				Y	
7036	P				Y	
7037	G				Y	
7038	T				Y	
7039	MV				Y	

7040	G					Y
7041	G					Y
7042	G					Y
7043	G					Y
7044	CTK					Y
7045	G					Y
7046	MV					Y
7047	G					Y
7048	MV					Y
7049	BP					Y
7050	G					Y
7051	T					Y
7052	PI					Y
7053	T					Y
7054	MV					Y
7055	MV					Y
7056	FT					Y
7057	FT					Y
7058	MV					Y
7059	FT					Y
7060	B					Y
7061	T					Y
7062	LS					Y
7063	G					Y
7064	G					Y
7065	T					Y
7066	T					Y
7067	G					Y
7068	G					Y
7069	G					Y
7070	T					Y
7071	FT					Y
7072	G					Y
7073	G					Y
7074	G					Y
7075	G					Y
7076	T					Y
7077	T					Y
7078	LT					Y
7079	MV					Y
7080	T					Y
7081	P					Y
7082	LG					Y
7083	B					Y
7084	T					Y
7085	L					Y



3rd Floor

4th Floor

4th Floor on Platform

6th Floor, Left on Catwalk

From Old HVL Gas Cooler

To Sewer

From Old No. 1 Degas Pot

From No. 1 P.O. Blow Tube

From HVL Sources (Fig. 11)

To HVL Blower Platform (Fig. 7)

Chip Bin NCG Fan BP-9027

FT-1 9030

FE-9031

MV-9033

T-9032

T-9029

T-9028

G-9026

G-9025

P-9025

ME-9024

P-9023

G-9022

CV-9020

CV-9018

PT-9018

TL-9017

PI-9016

T-9015

MV-9014

FA-9012

P-9013

P-9011

G-9010

CV-9009

CV-9008

RD-9008

PT-9007

PT-9006

T-9005

CV-9004

P-9002

TT-9001

G-9000

TH-9062

P-9051

P-9058

MV-9059

T-9057

MV-9053

MV-9077

MV-9050

From Old HVL Gas Cooler

B-9056

TT-9049

MV-9048

MV-9047

G-9047

MV-9037

B-9035

T-9036

TT-9038

P-9039

T-9040

G-9041

P-9042

P-9043

MV-9044

T-9045

P-9046

RB-9055

RB-9054

MV-9051

G-9052

MV-9052

From Old HVL Gas Cooler

B-9056

TT-9049

MV-9048

MV-9047

G-9047

MV-9037

B-9035

T-9036

TT-9038

P-9039

T-9040

G-9041

P-9042

P-9043

MV-9044

T-9045

P-9046

RB-9055

RB-9054

MV-9051

G-9052

MV-9052

From Old HVL Gas Cooler

B-9056

TT-9049

MV-9048

MV-9047

G-9047

MV-9037

B-9035

T-9036

TT-9038

P-9039

T-9040

G-9041

P-9042

P-9043

MV-9044

T-9045

P-9046

RB-9055

RB-9054

MV-9051

G-9052

MV-9052

From Old HVL Gas Cooler

B-9056

TT-9049

MV-9048

MV-9047

G-9047

MV-9037

B-9035

T-9036

TT-9038

P-9039

T-9040

G-9041

P-9042

P-9043

MV-9044

T-9045

P-9046

RB-9055

RB-9054

MV-9051

G-9052

MV-9052

From Old HVL Gas Cooler

B-9056

TT-9049

MV-9048

MV-9047

G-9047

MV-9037

B-9035

T-9036

TT-9038

P-9039

T-9040

G-9041

P-9042

P-9043

MV-9044

T-9045

P-9046

RB-9055

RB-9054

MV-9051

G-9052

MV-9052

From Old HVL Gas Cooler

B-9056

TT-9049

MV-9048

MV-9047

G-9047

MV-9037

B-9035

T-9036

TT-9038

P-9039

T-9040

G-9041

P-9042

P-9043

MV-9044

T-9045

P-9046

RB-9055

RB-9054

MV-9051

G-9052

MV-9052

From Old HVL Gas Cooler

B-9056

TT-9049

MV-9048

MV-9047

G-9047

MV-9037

B-9035

T-9036

TT-9038

P-9039

T-9040

G-9041

P-9042

P-9043

MV-9044

T-9045

P-9046

RB-9055

RB-9054

MV-9051

G-9052

MV-9052

From Old HVL Gas Cooler

B-9056

TT-9049

MV-9048

MV-9047

G-9047

MV-9037

B-9035

T-9036

TT-9038

P-9039

T-9040

G-9041

P-9042

P-9043

MV-9044

T-9045

P-9046

RB-9055

RB-9054

MV-9051

G-9052

MV-9052

From Old HVL Gas Cooler

B-9056

TT-9049

MV-9048

MV-9047

G-9047

MV-9037

B-9035

T-9036

TT-9038

P-9039

T-9040

G-9041

P-9042

P-9043

MV-9044

T-9045

P-9046

RB-9055

RB-9054

MV-9051

G-9052

MV-9052

From Old HVL Gas Cooler

B-9056

TT-9049

MV-9048

MV-9047

G-9047

MV-9037

B-9035

T-9036

TT-9038

P-9039

T-9040

G-9041

P-9042

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T-9045

P-9046

RB-9055

RB-9054

MV-9051

G-9052

MV-9052

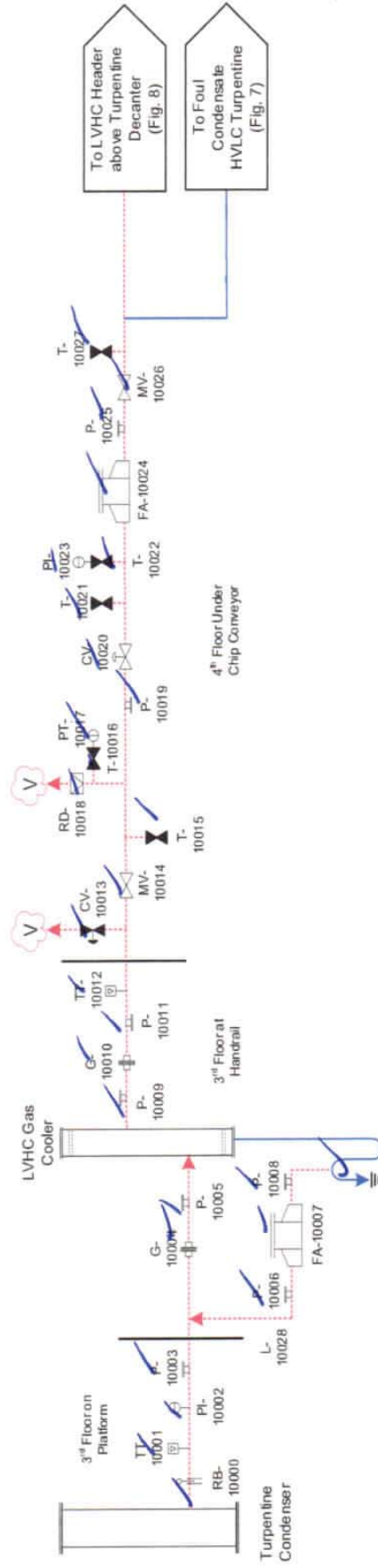


Turpentine Condenser and LVHC Gas Cooler

Completed Date/Time: 06/07/24

Number	Type	Pressure (+/-)	Background	VOC Reading	Is Component Free of Leaks or Defects?	Comments
10013	CV					YES
10014	MV					Y
10015	T					Y
10016	T					Y
10017	PT					Y
10018	RD					Y
10019	P					Y
10020	CV					Y
10021	T					Y
10022	T					Y
10023	PI					Y
10024	FA					Y
10025	P					Y
10026	MV					Y
10027	T					Y
10028	L					Y

Number	Type	Pressure (+/-)	Background	VOC Reading	Is Component Free of Leaks or Defects?	Comments
10000	RB				YES	
10001	TT				Y	
10002	PI				Y	
10003	P				Y	
10004	G				Y	
10005	P				Y	
10006	P				Y	
10007	FA				Y	
10008	P				Y	
10009	P				Y	
10010	G				Y	
10011	P				Y	
10012	TT				Y	



ENVIRONMENTAL 360

To Another Page and Indicated Equipment

From Another Page and Indicated Equipment

Vent Gases

Condensates

Liquor/Stock Lines

Process Lines

New Indy Containerboard – Catawba Mill

LDAR Inspection and Testing Diagrams

Turpentine Condenser and LVHC Gas Cooler

Rev. Date  
May 2021

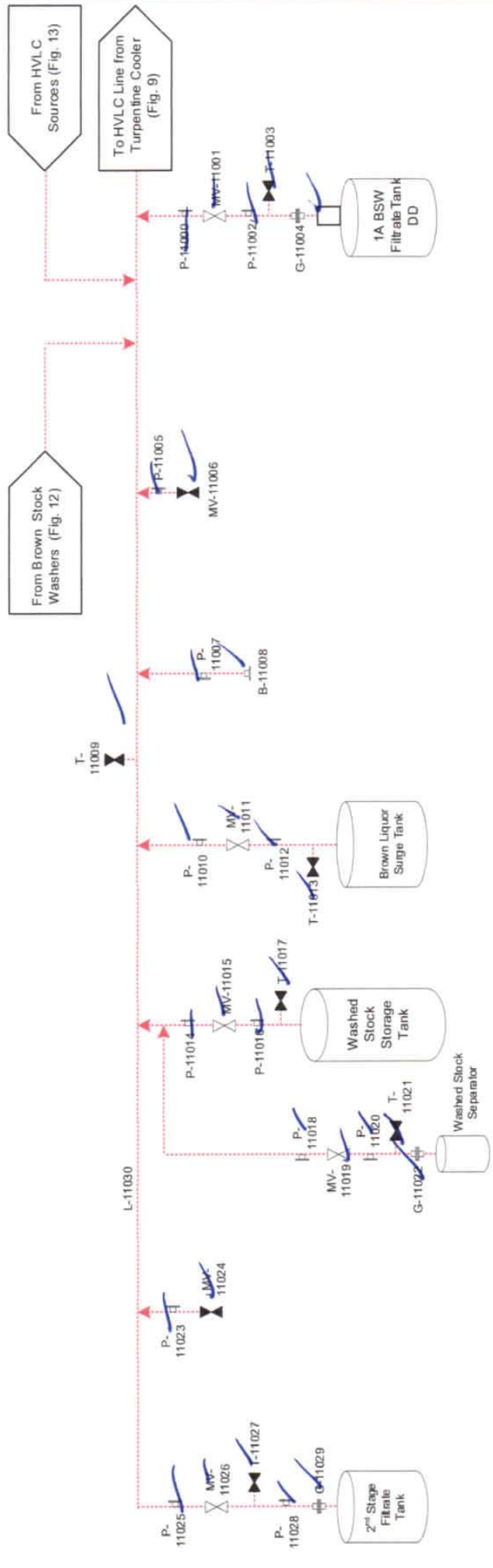
Figure 10

HVLC System at Pulp Mill (1 of 2)

Completed Date/Time: 06/07/21

Number	Type	Pressure (+/-)	Background	VOC Reading	Is Component Free of Leaks or Defects?	Comments
11000	P				Yes	
11001	MV				Y	
11002	P				Y	
11003	T				Y	
11004	G				Y	
11005	P				Y	
11006	MV				Y	
11007	P				Y	
11008	B				Y	
11009	T				Y	
11010	P				Y	
11011	MV				Y	
11012	P				Y	
11013	T				Y	

11014	P				Yes	
11015	MV				Y	
11016	P				Y	
11017	T				Y	
11018	P				Y	
11019	MV				Y	
11020	P				Y	
11021	T				Y	
11022	G				Y	
11023	P				Y	
11024	MV				Y	
11025	P				Y	
11026	MV				Y	
11027	T				Y	
11028	P				Y	
11029	G				Y	
11030	L				Y	



ENVIRONMENTAL 360

Rev. Date  
May 2021

Figure 11

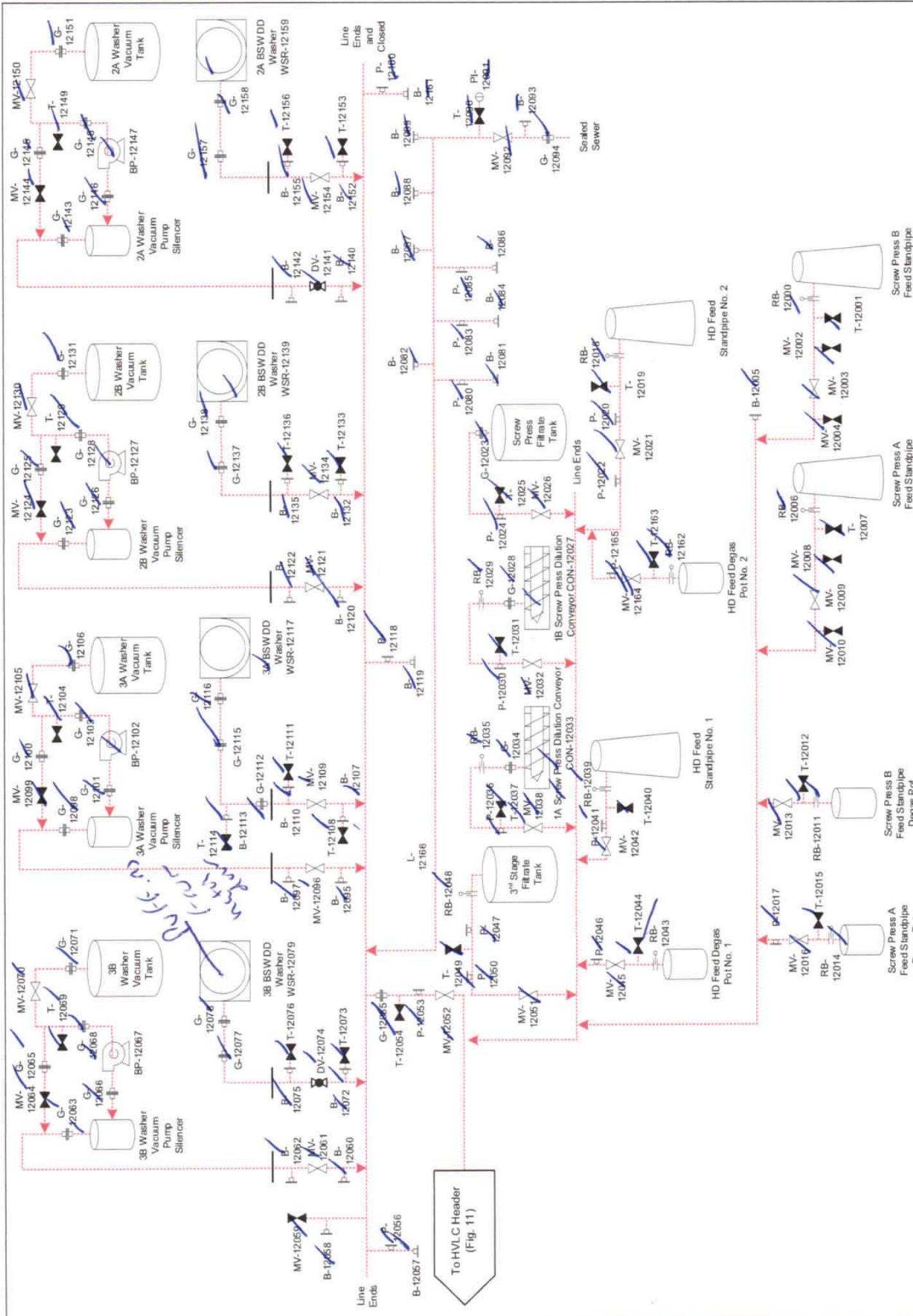
New Indy Containerboard – Catawba Mill

LDAR Inspection and Testing Diagrams

HVLC System at Pulp Mill (1 of 2)

To Another Page and Indicated Equipment

From Another Page and Indicated Equipment



Rev. Date  
May 2021

Figure 12

New Indy Containerboard – Catawba Mill

LDAR Inspection and Testing Diagrams

Pulp Mill BSWS

ENVIRONMENTAL 360

To Another Page and Indicated Equipment

From Another Page and Indicated Equipment

Vent Gases

Bleach Gases

Condensates

Liquor/Stock Lines

Process Lines

Screw Press A Feed Standpipe Degas Pot

Screw Press B Feed Standpipe Degas Pot

Screw Press A Feed Standpipe

Screw Press B Feed Standpipe

Pulp Mill BSW's

Completed Date/Time: 6/7/21

Number	Type	Pressure (+/-)	Background	VOC Reading	Is Component Free of Leaks or Defects?	Comments
12000	RB				Yes	
12001	T				Y	
12002	MV				Y	
12003	MV				Y	
12004	MV				Y	
12005	B				Y	
12006	RB				Y	
12007	T				Y	
12008	MV				Y	
12009	MV				Y	
12010	MV				Y	
12011	RB				Y	
12012	T				Y	
12013	MV				Y	
12014	RB				Y	
12015	T				Y	
12016	MV				Y	
12017	P				Y	
12018	RB				Y	
12019	T				Y	
12020	P				Y	
12021	MV				Y	
12022	P				Y	
12023	G				Y	
12024	P				Y	
12025	T				Y	
12026	MV				Y	
12027	CON				Y	
12028	G				Y	
12029	RB				Y	
12030	P				Y	
12031	T				Y	
12032	MV				Y	
12033	CON				Y	
12034	G				Y	
12035	RB				Y	
12036	P				Y	
12037	T				Y	
12038	MV				Y	
12039	RB				Y	
12040	T				Y	
12041	P				Y	
12042	MV				Y	
12043	RB				Y	
12044	T				Y	
12045	MV				Y	
12046	P				Y	
12047	P				Y	
12048	RB				Y	
12049	T				Y	
12050	P				Y	
12051	MV				Y	
12052	MV				Y	
12053	P				Y	
12054	T				Y	
12055	G				Y	
12056	P				Y	
12057	B				Y	
12058	B				Y	
12059	MV				Y	
12060	B				Y	
12061	MV				Y	
12062	B				Y	
12063	G				Y	
12064	MV				Y	
12065	G				Y	
12066	G				Y	
12067	BP				Y	
12068	G				Y	
12069	T				Y	
12070	MV				Y	
12071	G				Y	
12072	B				Y	
12073	T				Y	
12074	DV				Y	
12075	B				Y	
12076	T				Y	
12077	G				Y	
12078	G				Y	
12079	WSR				Y	
12080	P				Y	

Puffing from both doors



Pulp Mill BSWs

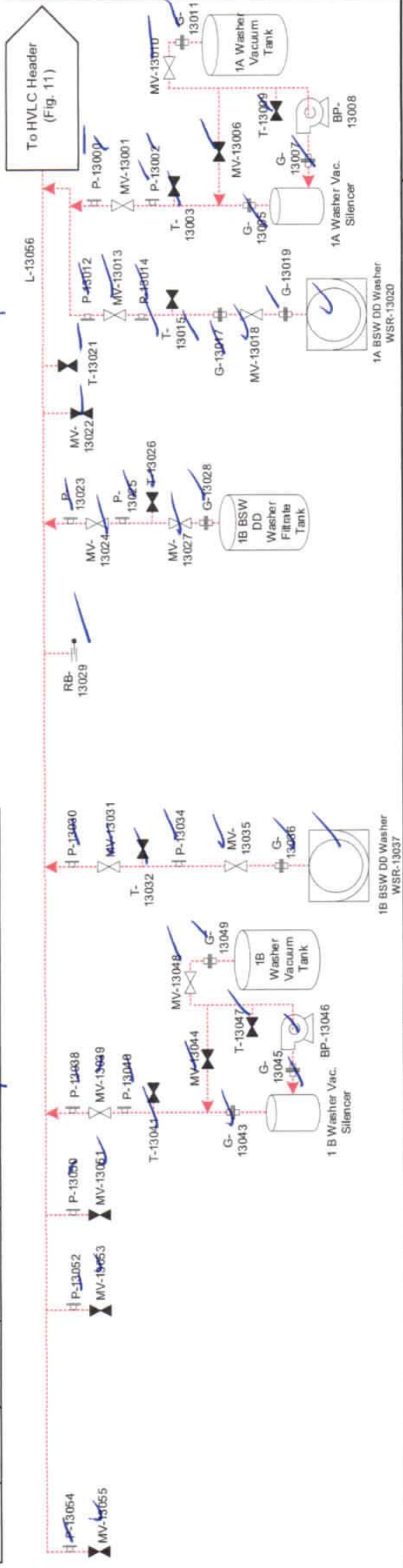
Completed Date/Time: 06/07/21

Number	Type	Pressure (+/-)	Background	VOC Reading	Is Component Free of Leaks or Defects?	Comments
12081	B				Y	
12082	B				Y	
12083	P				Y	
12084	B				Y	
12085	P				Y	
12086	B				Y	
12087	B				Y	
12088	B				Y	
12089	B				Y	
12090	T				Y	
12091	PI				Y	
12092	MV				Y	
12093	B				Y	
12094	G				Y	
12095	B				Y	
12096	MV				Y	
12097	B				Y	
12098	G				Y	
12099	MV				Y	
12100	G				Y	
12101	G				Y	
12102	BP				Y	
12103	G				Y	
12104	T				Y	
12105	MV				Y	
12106	G				Y	
12107	B				Y	
12108	T				Y	
12109	MV				Y	
12110	B				Y	
12111	T				Y	
12112	G				Y	
12113	B				Y	
12114	T				Y	
12115	G				Y	
12116	G				Y	
12117	WSR				Y	
12118	P				Y	
12119	B				Y	
12120	B				Y	
12121	MV				Y	
12122	B				Y	
12123	G				Y	
12124	MV				Y	
12125	G				Y	
12126	G				Y	
12127	BP				Y	
12128	G				Y	
12129	T				Y	
12130	MV				Y	
12131	G				Y	
12132	B				Y	
12133	T				Y	
12134	MV				Y	
12135	B				Y	
12136	T				Y	
12137	G				Y	
12138	G				Y	
12139	WSR				Y	
12140	B				Y	
12141	DV				Y	
12142	B				Y	
12143	G				Y	
12144	MV				Y	
12145	G				Y	
12146	G				Y	
12147	BP				Y	
12148	G				Y	
12149	T				Y	
12150	MV				Y	
12151	G				Y	
12152	B				Y	
12153	T				Y	
12154	MV				Y	
12155	B				Y	
12156	T				Y	
12157	G				Y	
12158	G				Y	
12159	WSR				Y	
12160	P				Y	
12161	B				Y	
12162	RB				Y	
12163	T				Y	
12164	MV				Y	
12165	P				Y	
12166	L				Y	

**HVLC System at Pulp Mill (2 of 2)**  
 Completed Date/Time: 06/07/21

Number	Type	Pressure (+/-)	Background	VOC Reading	Is Component Free of Leaks or Defects?	Comments
13000	P				Yes	
13001	MV				Y	
13002	P				Y	
13003	T				Y	
13005	G				Y	
13006	MV				Y	
13007	G				Y	
13008	BP				Y	
13009	T				Y	
13010	MV				Y	
13011	G				Y	
13012	P				Y	
13013	MV				Y	
13014	P				Y	
13015	T				Y	
13017	G				Y	
13018	MV				Y	
13019	G				Y	
13020	WSR				Y	
13021	T				Y	
13022	MV				Y	
13023	P				Y	
13024	MV				Y	
13025	P				Y	

13026	T					
13027	MV					
13028	G					
13029	RB					
13030	P					
13031	MV					
13032	T					
13034	P					
13035	MV					
13036	G					
13037	WSR					
13038	P					
13039	MV					
13040	P					
13041	T					
13043	G					
13044	MV					
13045	G					
13046	BP					
13047	T					
13048	MV					
13049	G					
13050	P					
13051	MV					
13052	P					
13053	MV					
13054	P					
13055	MV					



ENVIRONMENTAL 360

**New Indy Containerboard – Catawba Mill**

LDAR Inspection and Testing Diagrams

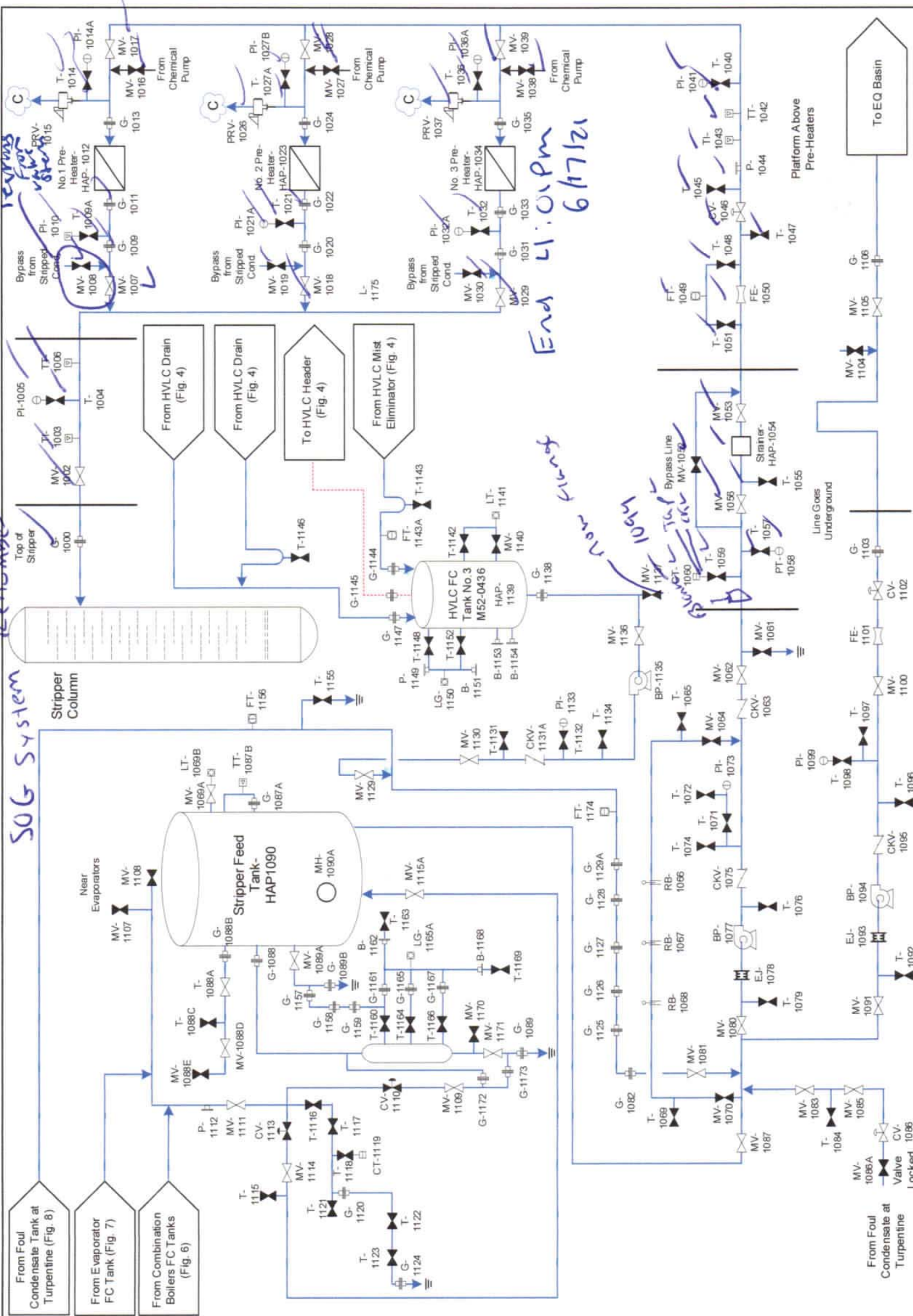
HVLC System at Pulp Mill (2 of 2)

Rev. Date  
May 2021

Figure 13

— Vent Gases  
— Condensates  
— Liquor/Stock Lines  
— Process Lines

  To Another Page and Indicated Equipment  
  From Another Page and Indicated Equipment



*Return*

*End 4:00pm 6/17/20*

*new*

*100%*

*Bypass Line*

*Line Goes Underground*

Rev. Date  
July 2020

New-Indy - Catawba Mill  
LDAR Inspection and Testing Diagrams  
Stripper System Foul Condensate

**ENVIRONMENTAL360**

To Another Page and Indicated Equipment  
From Another Page and Indicated Equipment

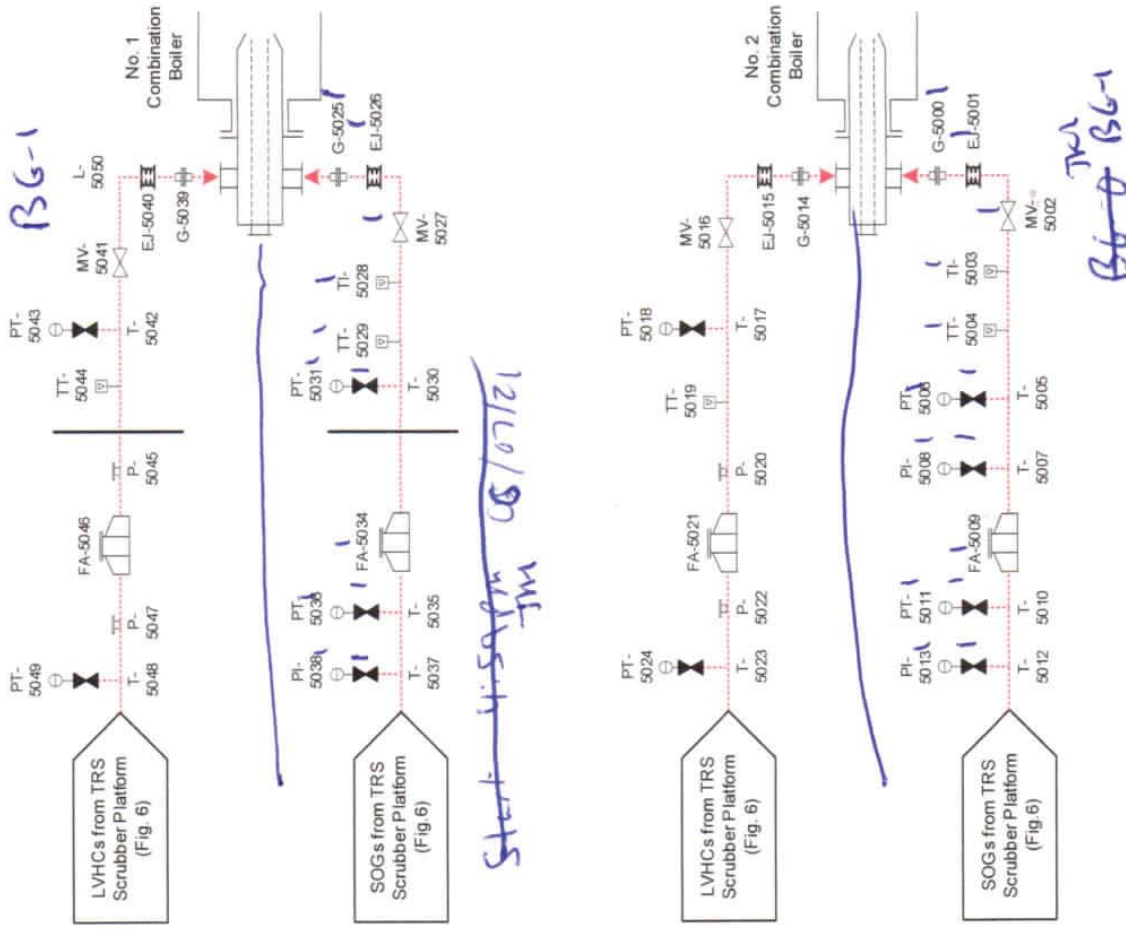
Vent Gases  
Condensates  
Liquor/Stock Lines  
Process Lines

Figure 1



Combination Boiler SOG and LVHC Incineration  
 Completed Date/Time: 06/17/21 5:14 PM

Start 4:35 PM  
 End 5:41 PM



Start 4:55 PM  
 JM  
 06/17/21

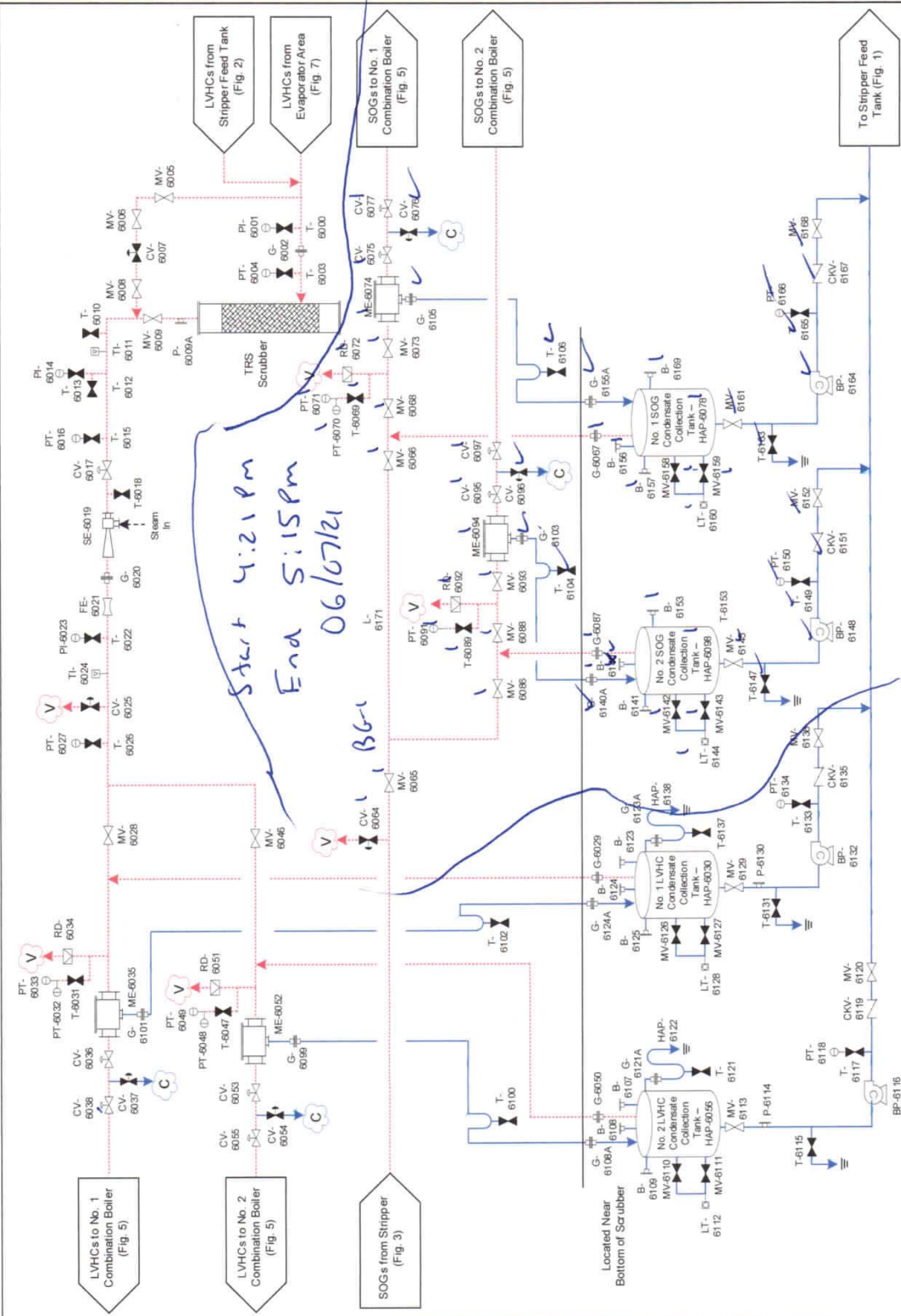
TM  
 BG-1

Number	Type	Equip. Number	Pressure (+/-)	Background	VOC Reading	Is Component Free of Leaks or Defects?	Comments
5000	G						Reviewed
5001	EJ						
5002	MV	37-MV-0283					
5003	TI						
5004	TT						
5005	T						
5006	PT	37-PT-032					
5007	T						
5008	PI						
5009	FA						
5010	T						
5011	PT						
5012	T						
5013	PI						
5014	G						
5015	EJ						
5016	MV	37-MV-0313					
5017	T						
5018	PT	37-PT-385					
5019	TT	37-TT-384					
5020	P						
5021	FA						
5022	P						
5023	T						
5024	PT	37-PT-383					
5025	G						
5026	EJ						
5027	MV						
5028	TI						
5029	TT	26-TT-034					
5030	T						
5031	PT	26-PT-033					
5034	FA						
5035	T						
5036	PT	26-PT-031					
5037	T						
5038	PI						
5039	G						
5040	EJ						
5041	MV	26-MV-0532					
5042	T						
5043	PT	26-PT-377					
5044	TT						
5045	P						
5046	FA						
5047	P						
5048	T						
5049	PT	26-PT-375					
5050	L						



New-Indy - Catawba Mill  
 LDAR Inspection and Testing Diagrams  
 Combination Boiler SOG and LVHC Incineration

Rev. Date  
 July 2020  
 Figure 5



<p>Vent Gases</p> <p>Condensates</p> <p>Liquor/Stock Lines</p> <p>Process Lines</p>	<p>To Another Page and Indicated Equipment</p> <p>From Another Page and Indicated Equipment</p>		<p>New-Indy – Catawba Mill</p>	<p>Rev. Date</p> <p>July 2020</p>
			<p>LDAR Inspection and Testing Diagrams</p>	<p>Figure 6</p>



New-Indy – Catawba Mill

LDAR Inspection and Testing Diagrams

TRS Scrubber Platform

Rev. Date

July 2020

Figure 6

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**APPENDIX B - WESTON SOLUTIONS AIR EMISSIONS ANALYSIS  
REPORT**

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April 16, 2021

Via Electronic Mail (reecemc@dhec.sc.gov)

Myra Reece  
Director of Environmental Affairs  
South Carolina Department of  
Health and Environmental Control  
2600 Bull Street  
Columbia, South Carolina 29201

Re: New-Indy Catawba LLC – Weston Solutions, Inc. Odor Testing Report

Dear Myra:

As we have discussed, New-Indy has been diligently investigating its operations to determine whether the mill could be the source of odor complaints submitted to DHEC, New-Indy and others. In connection with that review, New-Indy has engaged consultants to evaluate New-Indy's processes for potential odor sources. Consistent with our goal of working cooperatively and professionally with DHEC to identify potential sources of these odors, we introduced one of our consultants to DHEC staff last week to facilitate frank discussion regarding the consultant's work and findings. As we noted in our call last Friday, our consultant Weston Solutions, Inc. is an experienced environmental engineering firm that has been performing testing with respect to odor-related issues since the late 1980's. Weston Solutions personnel who conducted the testing and developed the Testing Report have a combined total of 75 years of emission testing experience. Following up on our conversation last Friday, please find enclosed Weston Solutions' Odor Testing Report.

We engaged Weston Solutions to conduct an expedited screening analysis to determine if the mill is generating significant odors. As you will see from the Testing Report, during the periods of March 16 through 18 and 23 through 25, 2021, Weston Solutions observed mill operations, collected samples from a variety of sources in and around the mill and its wastewater treatment operations, and performed testing to determine if the compounds typically associated with the odor described in the complaints (total reduced sulfur, methanol and terpenes) are present at the New-Indy mill in significant concentrations that would cause such intense odors many miles from the mill. Please note that, although New-Indy still is involved with significant construction and ramp-up activities, the consultants' work was conducted while the mill was in operation. As the Testing Report indicates, Weston Solutions did not detect those compounds in any meaningful concentration that would equate to intense odors. To understand the odor complaints better, Weston Solutions personnel also traveled to several off-site locations. As indicated in the Testing Report, Weston Solutions personnel did not detect off-site mill-type odors, but did detect odors from a fire, and sewage-related odors.

While the Weston Solutions report is a helpful and encouraging screening tool, we are continuing to investigate mill operations and off-site sources in an effort to resolve this situation and will provide additional data as it becomes available. For example, using the Weston Test Report as a basis for further analysis, we have engaged TRC to conduct continuous ambient monitoring of compounds typically associated with odor for an extended monitoring period.

— — — — — **NEW-INDY CONTAINERBOARD LLC** — — — — —

3500 PORSCHEWAY, SUITE 150 • ONTARIO, CALIFORNIA 91764 • [WWW.NEWINDYCONTAINERBOARD.COM](http://WWW.NEWINDYCONTAINERBOARD.COM)  
PHONE (909) 296-3400 • FAX  
(909) 941-5351



Myra Reece  
April 16, 2021  
Page 2

Given the public interest in this topic and our interest in working together to resolve this, we would be grateful if you would include Weston's Test Report on DHEC's website with the other reports on this issue. (<https://scdhec.gov/environment/environmental-sites-projects-permits-interest/lancaster-york-counties-odor-investigation>).

Sincerely,

A handwritten signature in black ink, appearing to read "Tony Hobson", written in a cursive style.

Tony Hobson  
Vice President of Manufacturing

Enclosure



**Weston Solutions, Inc.**  
 1625 Pumphrey Avenue  
 Auburn, Alabama 36832-4303  
 334-466-5600 ♦ Fax 334-466-5660  
 www.westonsolutions.com

13 April 2021

Mr. Tony Hobson  
 New-Indy Catawba, LLC  
 5300 Cureton Ferry Road  
 Catawba, South Carolina 29704

Work Order No. 15730.001.006

Re: New-Indy Catawba Mill Odor Testing

Dear Mr. Hobson:

This letter with attachments constitutes our report of odor testing performed at the New-Indy Catawba, South Carolina facility. In an effort to identify potential sources of odor and the constituents, WESTON set up an EPA Method 16 GC to monitor total reduced sulfur (TRS). Data was collected from a single GC with the capability to move to different locations based on wind direction. No significant or sustained ambient TRS was detected at the mill. Wastewater and condensate samples were also collected and analyzed for methanol and terpenes by the Auburn, Alabama laboratory. Mr. Templeton Simpkins, Mr. Chris Hartsky, and Mr. Jack Short of Weston Solutions, Inc. (WESTON®) performed the testing during 16-18 and 23-25 March 2021 for in-house engineering use by New-Indy personnel. The mill was in operation during sampling.

Along with the TRS, methanol, and terpenes testing, New-Indy personnel requested that WESTON travel to several off-site locations in the local area around the mill to determine if there were odors. On Monday, 22 March 2021, WESTON personnel travelled to Rock Hill, South Carolina and stopped at a Marathon gas station at approximately 18:30. An acrid sulfur dioxide (SO<sub>2</sub>) smell was detected that WESTON presumes was from a fire in the area. Haze from the presumed fire was observed by WESTON personnel. Several customers were observed rubbing their eyes and commenting on the smoke-like odor. On Wednesday, 24 March 2021, WESTON personnel travelled to Waxhaw, North Carolina and stopped at 16:35 at the Food Lion parking lot, and no odor was detected. WESTON personnel then drove to Indian Land, South Carolina and arrived at 2024 Drawbridge Drive at 18:30. An odor from a possible sewage leak was detected.

Attachment A to this letter presents the results of the testing in tabular form. Attachments B, C, and D include copies of field, laboratory, and quality control data, respectively.

Total reduced sulfur sampling and analysis were conducted according to EPA Reference Method 16. The methanol and terpenes condensate samples were analyzed by NCASI Method DI/MeOH-94.03 and NIOSH Method 1552, respectively.

We appreciate the opportunity to serve you on this project. If you have any questions or require additional information, please call me at 334-466-5627.

Sincerely,

WESTON SOLUTIONS, INC.

Templeton Simpkins  
 Client Service Manager

jb

Enclosure

Sincerely,

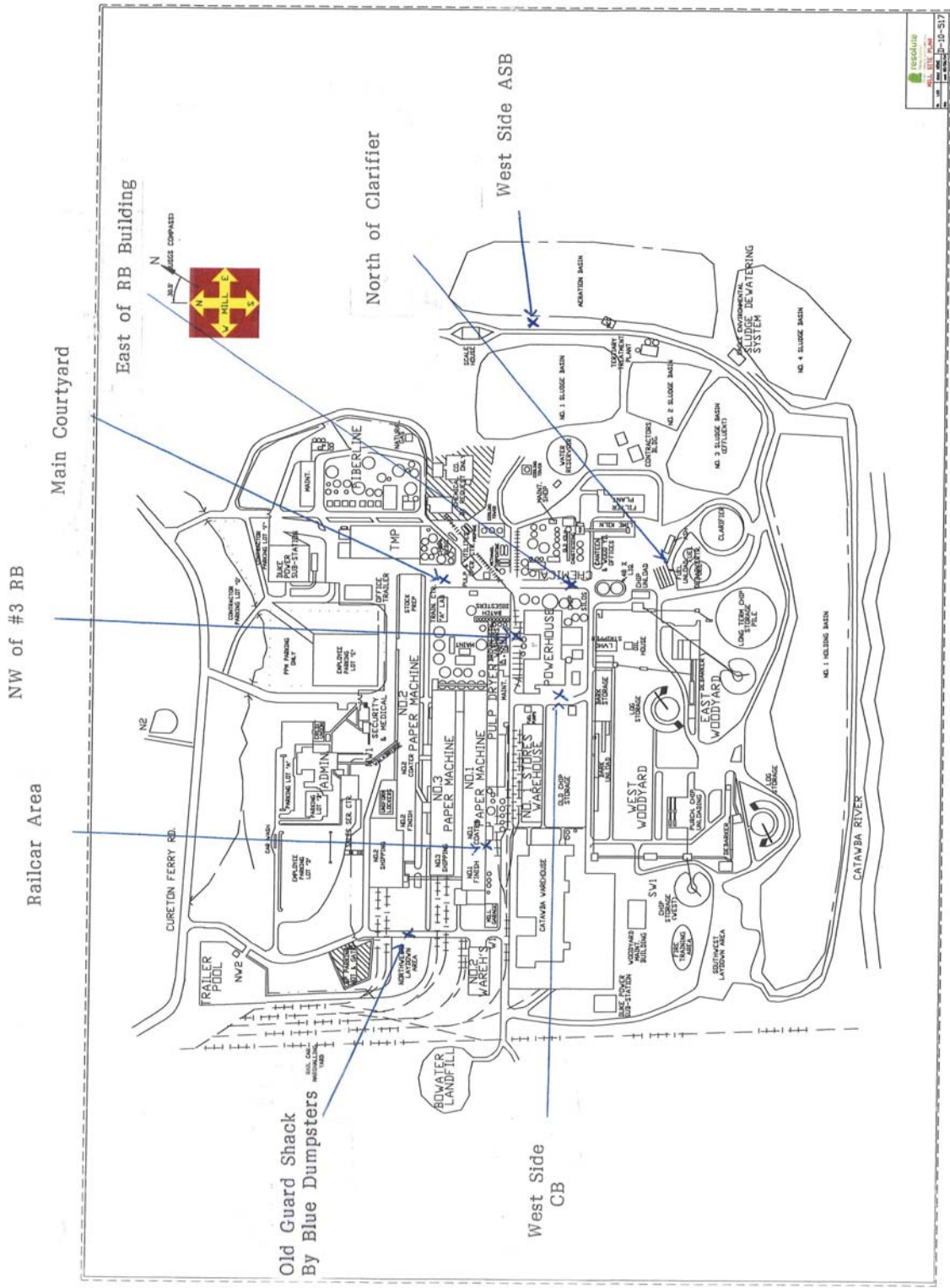
WESTON SOLUTIONS, INC.

Natalie Hammonds  
 Quality Assurance Manager

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## SAMPLING LOCATIONS FOR TRS TESTING



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## WESTON SOLUTIONS, INC. (WESTON®) QUALIFICATIONS

Since the company's inception in 1957, WESTON has provided high quality environmental engineering and consulting services to a variety of commercial, industrial and governmental clients. We have been performing emissions testing for more than 40 years and have developed an extensively experienced team of professionals, dedicated to partnering with our clients to achieve their regulatory compliance and operational goals.

WESTON's Auburn Alabama operations has been performing emission testing in support of odor-related compounds including but not limited to speciated sulfur compounds since the late 80's and was instrumental in development of the gas chromatograph (GC) methods such as EPA Method 16 for total reduced sulfur sampling and analysis. Since that time, WESTON has performed hundreds of test programs where we implemented online and continuous GC measurement and analysis for compliance and industrial engineering applications.

Our emissions testing group has over 60 professionals dedicated principally to conducting emissions testing services. Many of our client service managers, project managers, and project leaders have over 20 to 40 years of stack testing experience.

Over the past 40 years, we have performed emissions testing for a wide variety of commercial, industrial, and governmental clients including:

- Power/Utility
- Pulp & Paper
- Chemical
- Wood Products
- Petrochemical/Refineries
- Cement
- Pharmaceutical
- Steel/Specialty Metals
- Manufacturing
- Air Pollution Control Equipment Vendors

WESTON is certified as an Air Emissions Testing Body (AETB) under ASTM D7036 "Standard Practice for Competence of Air Emission Testing Bodies". We have over 25 employees who are certified as Qualified Individuals (QI) in accordance with ASTM D7036 as required by 40 CFR Part 75. Additionally, we have several employees who have received certification as Qualified Stack Testing Individuals (QSTI) from the Source Evaluation Society (SES). QSTI certification is not required by regulation but is an additional step in the assurance of the quality of our staff.

WESTON is a sustaining member of the National Council for Air and Stream Improvement (NCASI) - independent research institute for the forest products industry.

Emission testing services are conducted using resources in three WESTON offices: Auburn, Alabama; West Chester, Pennsylvania; and Houston, Texas.

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**WESTON SOLUTIONS, INC. (WESTON®)**  
**EMISSION TESTING PRACTICE – AUBURN OPERATIONS**  
**ACCREDITATION STIPULATION**

<b>Laboratory:</b>	Weston Solutions, Inc.
<b>Accreditor(s):</b>	Louisiana Environmental Laboratory Accreditation Program (LELAP) – Laboratory and Emission Testing Practice
<b>Accreditation ID:</b>	LELAP – 03024
<b>Scope:</b>	Total Reduced Sulfur, Methanol, and Terpenes Sampling and Analysis
<b>Effective:</b>	LELAP – 21 December 2001
<b>Expires:</b>	LELAP – 30 June 2021

These results meet all requirements of TNI unless otherwise specified.

The results within this report relate only to the samples listed in the body of this report.

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## Data Qualifiers



The following are general reporting notes that are applicable to all WESTON reports, unless otherwise noted.

- **NL** denotes data that was not from a LELAP accredited method.
- **LNL** denotes lab results that are not from an accredited LELAP laboratory.
- **NN** denotes data that was not from The NELAC Institute (TNI) accredited method.
- **NNL** denotes lab results that are not from an accredited TNI laboratory.
- **ED** denotes data that is not to be used for compliance purposes and may deviate from approved procedures.
- **Q** denotes data whose QA/QC check did not fall within the specified range. This data is still considered valid.
- **A** denotes data that is anomalously high with no explanation for the outlier.
- **BDL** denotes values that were below the limit of detection of the analyzer and 2% of the span gas was used to calculate an emission rate.
- **DF** denotes a dilution factor.
- **NAP** denotes emission testing performed by personnel from a non-TNI accredited laboratory.
- **S** denotes analysis that has been subcontracted.
- All values are reported on a “dry” basis, unless otherwise designated as “actual” or “wet” basis.



**ATTACHMENT A  
SUMMARY OF RESULTS**

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Tables A-1 through A-4 present detailed summaries of the results of the emission testing. Measurement uncertainty is not shown in results but has been taken into consideration during method development. Any differences between the calculated results presented in the appendices and the results reported in the summary tables are due to rounding for presentation.

**TABLE A-1  
SUMMARY OF AMBIENT TRS MONITORING**

<b>Date/Time</b>	<b>Location</b>	<b>TRS (ppm)</b>
3/16/21 & 3/17/21 1815-0805	West Side ASB	0.02
3/17/21 0946-1553	West Side ASB	0.02
3/17/21 & 3/18/21 1645-0759	North Clarifier	0.02
3/18/21 1021-1428	Trailer South of Old Guard Shack by Blue Dumpsters	0.03
3/23/21 & 3/24/21 0906-0810	Multiple Locations: East of RB Building in Ally; West Side CB; NW of No. 3 RB Stack; Rail Car Area	0.07
3/24/21 0931-1014	Rail Car Area	0.10
3/24/21 1017-1029	PM Roof Edge	0.00
3/24/21 1031-1043	PM Roof Vent 2	0.00
3/24/21 1058-1540	Multiple Locations: NW Side of Mill	0.03

Table A-2 presents the results of a TRS purge conducted on various process liquids. The purge analysis was conducted to determine the concentration of TRS in each of the liquid samples.

**TABLE A-2**  
**SUMMARY OF TRS RESULTS**  
**(25 MARCH 2021)**

<b>Source ID</b>	<b>H<sub>2</sub>S (µg/mL)</b>	<b>MeSH (µg/mL)</b>	<b>DMS (µg/mL)</b>	<b>DMDS (µg/mL)</b>	<b>TRS as S (µg/mL)</b>
Stripper Feed	48.8	9.3	11.7	6.1	62.2
Acid Sewer	0.13	<0.07	<0.06	0.20	0.26
Clarifier Overflow	0.25	<0.1	1.2	0.57	1.24
ASB Effluent	0.20	<0.1	<0.08	<0.06	0.18
ASB Influent	0.10	<0.06	0.65	0.23	0.58
Screw Press Filtrate	0.14	<0.05	<0.04	<0.03	0.13
PM3 Whitewater	0.04	<0.05	0.18	<0.03	0.13

Table A-3 presents the results of the methanol analysis conducted on various wastewater samples collected during the test program. The samples were prepared and analyzed in accordance with NCASI Method DI/MeOH-94.03.

**TABLE A-3  
SUMMARY OF METHANOL LABORATORY RESULTS**

Source ID	Concentration (µg/mL)
No. 3 Foul Condensate	7,170
No. 3 Combined Condensate	1,210
No. 2 Foul Condensate	2,320
No. 2 Combined Condensate	188
No. 2 Condenser Condensate	1,590
No. 1 Old Condensate	1,340
No. 1 Foul Condensate	688
No. 1 Combined Condensate	103
No. 1 Auxiliary Condensate	2,510
M52-0453 Combined Condensate	539
M52-0432 HVLC Condensate	160
Stripper Feed Tank	1,860
Acid Sewer	43.8
Clarifier Overflow	185
ASB Effluent	49.4
ASB Influent	117
Screw Press Filtrate	54.1
PM3 Whitewater	14.5

Table A-4 presents the results of the terpenes analysis conducted on various wastewater samples collected during the test program. The samples were prepared and analyzed in accordance with NCASI Method 1552.

**TABLE A-4**  
**SUMMARY OF TERPENES LABORATORY RESULTS**

<b>Source ID</b>	<b>Total Concentration (µg/mL)</b>
No. 3 Foul Condensate	6011
No. 3 Combined Condensate	229
No. 2 Foul Condensate	196
No. 2 Combined Condensate	127
No. 2 Condenser Condensate	516
No. 1 Old Condensate	265
No. 1 Foul Condensate	132
No. 1 Combined Condensate	142
No. 1 Auxiliary Condensate	422
M52-0453 Combined Condensate	166
M52-0432 HVLC Condensate	62.0
Stripper Feed Tank	2,396
Acid Sewer	29.1



**ATTACHMENT B**  
**FIELD DATA**

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## TOTAL REDUCED SULFUR



**16-17 MARCH 2021**

# RUN SUMMARY

Number 1

Client: **New Indy**  
Location: **Catawba, SC**  
Source:

Method **16**  
Calibration **1**

Project Number: **15730.001.006**  
Operator: **T. Simpkins**  
Date: **16 Mar 2021**

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**Start Time 18:15    End Time 08:05**

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**Average Measured TRS Conc.    0.02 ppm**  
**Recovery Missing**



# RUN DATA

Number 1

Client: **New Indy**  
Location: **Catawba, SC**  
Source:

Method **16**  
Calibration **1**

Project Number: **15730.001.006**  
Operator: **T. Simpkins**  
Date: **16 Mar 2021**

Time	H <sub>2</sub> S		MeSH		DMS		DMDS		TRS
	area	ppm	area	ppm	area	ppm	area	ppm	ppm
<b>West Side ASB</b>									
18:15	3	0.04	<2	<0.025	<2	<0.035	2	0.01	0.07
18:18	3	0.05	<2	<0.025	<2	<0.035	<2	<0.009	0.05
18:21	3	0.04	<2	<0.025	<2	<0.035	<2	<0.009	0.04
18:24	3	0.04	<2	<0.025	<2	<0.035	4	0.01	0.07
18:27	3	0.04	<2	<0.025	<2	<0.035	<2	<0.009	0.04
18:30	6	0.06	<2	<0.025	<2	<0.035	<2	<0.009	0.06
18:33	3	0.04	<2	<0.025	<2	<0.035	<2	<0.009	0.04
18:36	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
18:39	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
18:42	2	0.04	<2	<0.025	<2	<0.035	5	0.02	0.07
18:45	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
18:48	<2	<0.035	<2	<0.025	<2	<0.035	2	0.01	0.02
18:51	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
18:54	2	0.04	<2	<0.025	<2	<0.035	<2	<0.009	0.04
18:57	2	0.04	<2	<0.025	<2	<0.035	<2	<0.009	0.04
19:00	4	0.05	<2	<0.025	<2	<0.035	<2	<0.009	0.05
19:03	6	0.06	<2	<0.025	<2	<0.035	<2	<0.009	0.06
19:06	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
19:09	2	0.04	<2	<0.025	<2	<0.035	<2	<0.009	0.04
19:12	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
19:15	3	0.04	<2	<0.025	<2	<0.035	<2	<0.009	0.04
19:18	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
19:21	2	0.04	<2	<0.025	<2	<0.035	<2	<0.009	0.04
19:24	2	0.04	<2	<0.025	<2	<0.035	<2	<0.009	0.04
19:27	4	0.05	<2	<0.025	<2	<0.035	<2	<0.009	0.05
19:30	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
19:33	3	0.04	<2	<0.025	<2	<0.035	<2	<0.009	0.04
19:36	2	0.04	<2	<0.025	<2	<0.035	3	0.01	0.06
19:39	2	0.03	<2	<0.025	<2	<0.035	<2	<0.009	0.03
19:42	4	0.05	<2	<0.025	4	0.05	<2	<0.009	0.10
19:45	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
19:48	2	0.04	<2	<0.025	<2	<0.035	<2	<0.009	0.04
19:51	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
19:54	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
19:57	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
20:00	<2	<0.035	<2	<0.025	<2	<0.035	4	0.01	0.03
20:03	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
20:06	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
20:09	2	0.04	<2	<0.025	<2	<0.035	<2	<0.009	0.04

# RUN DATA

Number 1

Client: **New Indy**  
Location: **Catawba, SC**  
Source:

Method **16**  
Calibration **1**

Project Number: **15730.001.006**  
Operator: **T. Simpkins**  
Date: **16 Mar 2021**

Time	H <sub>2</sub> S		MeSH		DMS		DMDS		TRS ppm
	area	ppm	area	ppm	area	ppm	area	ppm	
20:12	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
20:15	3	0.04	<2	<0.025	<2	<0.035	<2	<0.009	0.04
20:18	2	0.04	<2	<0.025	4	0.05	<2	<0.009	0.09
20:21	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
20:24	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
20:28	<2	<0.035	<2	<0.025	5	0.06	<2	<0.009	0.06
20:31	2	0.04	<2	<0.025	<2	<0.035	<2	<0.009	0.04
20:34	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
20:37	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
20:40	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
20:43	7	0.07	<2	<0.025	<2	<0.035	<2	<0.009	0.07
20:46	3	0.04	<2	<0.025	<2	<0.035	<2	<0.009	0.04
20:49	4	0.05	<2	<0.025	<2	<0.035	<2	<0.009	0.05
20:52	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
20:55	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
20:58	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
21:01	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
21:04	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
21:07	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
21:10	3	0.04	<2	<0.025	<2	<0.035	<2	<0.009	0.04
21:13	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
21:16	2	0.04	<2	<0.025	<2	<0.035	5	0.02	0.07
21:19	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
21:22	<2	<0.035	<2	<0.025	<2	<0.035	3	0.01	0.02
21:25	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
21:28	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
21:31	5	0.06	<2	<0.025	<2	<0.035	<2	<0.009	0.06
21:34	3	0.04	<2	<0.025	<2	<0.035	<2	<0.009	0.04
21:37	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
21:40	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
21:43	<2	<0.035	<2	<0.025	<2	<0.035	2	0.01	0.02
21:46	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
21:49	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
21:52	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
21:55	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
21:58	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
22:01	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
22:04	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
22:07	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
22:10	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-

**RUN DATA**

Number 1

Client: **New Indy**  
Location: **Catawba, SC**  
Source:Method **16**  
Calibration **1**Project Number: **15730.001.006**  
Operator: **T. Simpkins**  
Date: **16 Mar 2021**

Time	H <sub>2</sub> S		MeSH		DMS		DMDS		TRS ppm
	area	ppm	area	ppm	area	ppm	area	ppm	
22:13	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
22:16	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
22:19	2	0.04	<2	<0.025	<2	<0.035	<2	<0.009	0.04
22:22	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
22:25	3	0.05	<2	<0.025	<2	<0.035	7	0.02	0.09
22:28	5	0.06	<2	<0.025	<2	<0.035	<2	<0.009	0.06
22:31	4	0.05	<2	<0.025	<2	<0.035	<2	<0.009	0.05
22:34	2	0.04	<2	<0.025	<2	<0.035	<2	<0.009	0.04
22:37	4	0.05	<2	<0.025	<2	<0.035	<2	<0.009	0.05
22:40	5	0.06	<2	<0.025	<2	<0.035	<2	<0.009	0.06
22:43	3	0.04	<2	<0.025	<2	<0.035	<2	<0.009	0.04
22:46	2	0.04	<2	<0.025	<2	<0.035	<2	<0.009	0.04
22:49	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
22:52	5	0.06	<2	<0.025	<2	<0.035	<2	<0.009	0.06
22:55	6	0.06	<2	<0.025	5	0.06	<2	<0.009	0.12
22:58	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
23:01	<2	<0.035	<2	<0.025	<2	<0.035	3	0.01	0.02
23:04	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
23:07	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
23:10	4	0.05	<2	<0.025	<2	<0.035	<2	<0.009	0.05
23:13	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
23:16	2	0.04	<2	<0.025	<2	<0.035	<2	<0.009	0.04
23:19	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
23:22	4	0.05	<2	<0.025	<2	<0.035	<2	<0.009	0.05
23:25	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
23:28	2	0.04	<2	<0.025	2	0.04	11	0.03	0.13
23:31	7	0.07	<2	<0.025	3	0.05	<2	<0.009	0.12
23:34	2	0.04	2	0.03	<2	<0.035	<2	<0.009	0.06
23:37	4	0.05	<2	<0.025	<2	<0.035	<2	<0.009	0.05
23:40	8	0.07	<2	<0.025	<2	<0.035	<2	<0.009	0.07
23:43	4	0.06	<2	<0.025	<2	<0.035	<2	<0.009	0.06
23:46	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
23:49	9	0.08	<2	<0.025	<2	<0.035	<2	<0.009	0.08
23:52	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
23:55	5	0.06	<2	<0.025	<2	<0.035	<2	<0.009	0.06
23:58	<2	<0.035	<2	<0.025	5	0.06	<2	<0.009	0.06
00:01	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
00:04	3	0.04	<2	<0.025	<2	<0.035	<2	<0.009	0.04
00:07	<2	<0.035	<2	<0.025	6	0.06	2	0.01	0.08
00:10	<2	<0.035	<2	<0.025	3	0.04	<2	<0.009	0.04

# RUN DATA

Number 1

Client: **New Indy**  
Location: **Catawba, SC**  
Source:

Method **16**  
Calibration **1**

Project Number: **15730.001.006**  
Operator: **T. Simpkins**  
Date: **16 Mar 2021**

Time	H <sub>2</sub> S		MeSH		DMS		DMDS		TRS ppm
	area	ppm	area	ppm	area	ppm	area	ppm	
00:13	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
00:16	2	0.04	<2	<0.025	<2	<0.035	<2	<0.009	0.04
00:19	35	0.18	<2	<0.025	<2	<0.035	<2	<0.009	0.18
00:22	8	0.07	<2	<0.025	2	0.04	<2	<0.009	0.11
00:25	3	0.04	<2	<0.025	2	0.04	<2	<0.009	0.08
00:28	<2	<0.035	<2	<0.025	5	0.06	<2	<0.009	0.06
00:31	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
00:34	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
00:37	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
00:40	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
00:43	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
00:46	2	0.04	<2	<0.025	<2	<0.035	<2	<0.009	0.04
00:49	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
00:52	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
00:55	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
00:58	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
01:01	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
01:04	2	0.04	<2	<0.025	<2	<0.035	<2	<0.009	0.04
01:07	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
01:10	<2	<0.035	<2	<0.025	<2	<0.035	3	0.01	0.02
01:13	<2	<0.035	3	0.03	<2	<0.035	<2	<0.009	0.03
01:16	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
01:19	2	0.04	<2	<0.025	<2	<0.035	<2	<0.009	0.04
01:22	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
01:25	2	0.04	<2	<0.025	<2	<0.035	<2	<0.009	0.04
01:28	7	0.07	<2	<0.025	<2	<0.035	<2	<0.009	0.07
01:31	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
01:34	2	0.04	<2	<0.025	4	0.05	<2	<0.009	0.09
01:37	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
01:40	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
01:43	6	0.06	<2	<0.025	<2	<0.035	<2	<0.009	0.06
01:46	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
01:49	2	0.04	<2	<0.025	<2	<0.035	<2	<0.009	0.04
01:52	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
01:55	<2	<0.035	<2	<0.025	<2	<0.035	3	0.01	0.02
01:58	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
02:01	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
02:04	2	0.04	<2	<0.025	<2	<0.035	<2	<0.009	0.04
02:07	4	0.05	<2	<0.025	<2	<0.035	3	0.01	0.08
02:10	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-

# RUN DATA

Number 1

Client: **New Indy**  
Location: **Catawba, SC**  
Source:

Method **16**  
Calibration **1**

Project Number: **15730.001.006**  
Operator: **T. Simpkins**  
Date: **16 Mar 2021**

Time	H <sub>2</sub> S		MeSH		DMS		DMDS		TRS ppm
	area	ppm	area	ppm	area	ppm	area	ppm	
02:13	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
02:16	<2	<0.035	<2	<0.025	<2	<0.035	3	0.01	0.02
02:19	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
02:22	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
02:25	<2	<0.035	<2	<0.025	<2	<0.035	7	0.02	0.04
02:29	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
02:32	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
02:35	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
02:38	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
02:41	<2	<0.035	<2	<0.025	3	0.04	<2	<0.009	0.04
02:44	6	0.07	<2	<0.025	<2	<0.035	<2	<0.009	0.07
02:47	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
02:50	2	0.04	<2	<0.025	<2	<0.035	<2	<0.009	0.04
02:53	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
02:56	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
02:59	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
03:02	2	0.04	<2	<0.025	<2	<0.035	<2	<0.009	0.04
03:05	<2	<0.035	<2	<0.025	<2	<0.035	3	0.01	0.02
03:08	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
03:11	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
03:14	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
03:17	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
03:20	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
03:23	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
03:26	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
03:29	3	0.05	<2	<0.025	<2	<0.035	<2	<0.009	0.05
03:32	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
03:35	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
03:38	<2	<0.035	7	0.05	<2	<0.035	<2	<0.009	0.05
03:41	<2	<0.035	<2	<0.025	<2	<0.035	4	0.01	0.03
03:44	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
03:47	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
03:50	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
03:53	3	0.05	<2	<0.025	<2	<0.035	<2	<0.009	0.05
03:56	<2	<0.035	<2	<0.025	<2	<0.035	2	0.01	0.02
03:59	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
04:02	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
04:05	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
04:08	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
04:11	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-

# RUN DATA

Number 1

Client: **New Indy**  
Location: **Catawba, SC**  
Source:

Method **16**  
Calibration **1**

Project Number: **15730.001.006**  
Operator: **T. Simpkins**  
Date: **16 Mar 2021**

Time	H <sub>2</sub> S		MeSH		DMS		DMDS		TRS ppm
	area	ppm	area	ppm	area	ppm	area	ppm	
04:14	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
04:17	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
04:20	4	0.05	<2	<0.025	<2	<0.035	<2	<0.009	0.05
04:23	3	0.04	<2	<0.025	<2	<0.035	<2	<0.009	0.04
04:26	5	0.06	<2	<0.025	3	0.04	<2	<0.009	0.10
04:29	7	0.07	<2	<0.025	<2	<0.035	<2	<0.009	0.07
04:32	5	0.06	<2	<0.025	<2	<0.035	<2	<0.009	0.06
04:35	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
04:38	3	0.04	<2	<0.025	<2	<0.035	<2	<0.009	0.04
04:41	2	0.04	<2	<0.025	<2	<0.035	2	0.01	0.06
04:44	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
04:47	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
04:50	4	0.05	<2	<0.025	<2	<0.035	<2	<0.009	0.05
04:53	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
04:56	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
04:59	3	0.05	<2	<0.025	<2	<0.035	<2	<0.009	0.05
05:02	<2	<0.035	<2	<0.025	<2	<0.035	2	0.01	0.02
05:05	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
05:08	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
05:11	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
05:14	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
05:17	2	0.04	<2	<0.025	<2	<0.035	<2	<0.009	0.04
05:20	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
05:23	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
05:26	<2	<0.035	<2	<0.025	3	0.04	<2	<0.009	0.04
05:29	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
05:32	<2	<0.035	<2	<0.025	<2	<0.035	3	0.01	0.02
05:35	<2	<0.035	<2	<0.025	<2	<0.035	4	0.01	0.03
05:38	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
05:41	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
05:44	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
05:47	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
05:50	4	0.05	<2	<0.025	<2	<0.035	<2	<0.009	0.05
05:53	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
05:56	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
05:59	<2	<0.035	<2	<0.025	<2	<0.035	3	0.01	0.02
06:02	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
06:05	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
06:08	6	0.06	<2	<0.025	<2	<0.035	<2	<0.009	0.06
06:11	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-

# RUN DATA

Number 1

Client: **New Indy**  
Location: **Catawba, SC**  
Source:

Method **16**  
Calibration **1**

Project Number: **15730.001.006**  
Operator: **T. Simpkins**  
Date: **16 Mar 2021**

Time	H <sub>2</sub> S		MeSH		DMS		DMDS		TRS
	area	ppm	area	ppm	area	ppm	area	ppm	ppm
06:14	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
06:17	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
06:20	<2	<0.035	<2	<0.025	<2	<0.035	3	0.01	0.03
06:23	3	0.04	<2	<0.025	<2	<0.035	<2	<0.009	0.04
06:26	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
06:29	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
06:32	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
06:35	3	0.05	<2	<0.025	<2	<0.035	2	0.01	0.07
06:38	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
06:41	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
06:44	<2	<0.035	<2	<0.025	<2	<0.035	3	0.01	0.03
06:47	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
06:50	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
06:53	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
06:56	2	0.04	<2	<0.025	<2	<0.035	<2	<0.009	0.04
06:59	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
07:02	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
07:05	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
07:08	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
07:11	<2	<0.035	4	0.04	<2	<0.035	<2	<0.009	0.04
07:14	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
07:17	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
07:20	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
07:23	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
07:26	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
07:29	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
07:32	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
07:35	6	0.07	<2	<0.025	<2	<0.035	2	0.01	0.09
07:38	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
07:41	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
07:44	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
07:47	6	0.06	<2	<0.025	<2	<0.035	<2	<0.009	0.06
07:50	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
07:53	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
07:56	<2	<0.035	<2	<0.025	<2	<0.035	2	0.01	0.02
07:59	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
08:02	<2	<0.035	<2	<0.025	<2	<0.035	<2	<0.009	-
<b>Average</b>		<b>&lt;0.035</b>		<b>&lt;0.025</b>		<b>&lt;0.035</b>		<b>&lt;0.009</b>	<b>-</b>

# CALIBRATION DATA

Number 1

Client: **New Indy**  
Location: **Catawba, SC**  
Source:

Project Number: **15730.001.006**  
Operator: **T. Simpkins**  
Date: **15 Mar 2021**

Method 16

		Ambient Temperature: 72°C		Barometric Pressure: 30.20 in. Hg				
Analyte		<b>H<sub>2</sub>S</b>		<b>MeSH</b>		<b>DMS</b>		<b>DMDS</b>
Perm. Device ID		T-53950		33-56671		89-56661		89-56665
Perm. Rate, nL/min		422		455		306		217
Ret. Time, sec		19.0		32.5		70.0		125.0
<b>1 Flow = 49.5 mL/Min</b>		<b>8.53 ppm</b>		<b>9.20 ppm</b>		<b>6.18 ppm</b>		<b>4.39 ppm</b>
<b>Time: 13:19</b>		<b>Peak Areas, mv-sec</b>						
		32537		39496		20950		58413
		32418		39230		21200		58902
		31825		38696		21077		58586
<b>Average Area</b>		<b>32260 /</b>		<b>39141 /</b>		<b>21076 /</b>		<b>58634 /</b>
<b>2 Flow = 108 mL/Min</b>		<b>3.92 ppm</b>		<b>4.22 ppm</b>		<b>2.83 ppm</b>		<b>2.01 ppm</b>
<b>Time: 13:46</b>		<b>Peak Areas, mv-sec</b>						
		8799		12079		5689		18833
		9054		11850		5632		17770
		8930		11712		5606		17267
<b>Average Area</b>		<b>8928 /</b>		<b>11880 /</b>		<b>5642 /</b>		<b>17956 /</b>
<b>3 Flow = 263 mL/Min</b>		<b>1.61 ppm</b>		<b>1.73 ppm</b>		<b>1.16 ppm</b>		<b>0.83 ppm</b>
<b>Time: 13:59</b>		<b>Peak Areas, mv-sec</b>						
		1643		2427		1065		3746
		1726		2386		1071		3552
		1698		2306		1049		3468
<b>Average Area</b>		<b>1689 /</b>		<b>2373 /</b>		<b>1062 /</b>		<b>3589 /</b>



# CALIBRATION SUMMARY

Number 1

Client: **New Indy**  
Location: **Catawba, SC**  
Source:

Project Number: **15730.001.006**  
Operator: **T. Simpkins**  
Date: **15 Mar 2021**

Method **16**

H <sub>2</sub> S	1	2	3		
Time	13:19	13:46	13:59		
Concentration, ppm	8.53	3.92	1.61		
Area, mv-sec	32260	8928	1689		
Calc. Conc., ppm	8.38	4.05	1.58		
% Error	-1.8	3.5	-1.6		
<u>Calibration Curve</u>	<b>Slope</b>	<b>Intercept</b>	<b>Corr. Coeff.</b>	<b>Min. Area</b>	<b>Det. Lim.</b>
	1.7682	2.8763	0.9994	2	0.035

MeSH	1	2	3		
Time	13:19	13:46	13:59		
Concentration, ppm	9.20	4.22	1.73		
Area, mv-sec	39141	11880	2373		
Calc. Conc., ppm	8.98	4.42	1.69		
% Error	-2.4	4.7	-2.1		
<u>Calibration Curve</u>	<b>Slope</b>	<b>Intercept</b>	<b>Corr. Coeff.</b>	<b>Min. Area</b>	<b>Det. Lim.</b>
	1.6811	2.9904	0.9989	2	0.025

DMS	1	2	3		
Time	13:19	13:46	13:59		
Concentration, ppm	6.18	2.83	1.16		
Area, mv-sec	21076	5642	1062		
Calc. Conc., ppm	6.09	2.92	1.15		
% Error	-1.5	2.9	-1.3		
<u>Calibration Curve</u>	<b>Slope</b>	<b>Intercept</b>	<b>Corr. Coeff.</b>	<b>Min. Area</b>	<b>Det. Lim.</b>
	1.7909	2.9192	0.9996	2	0.035

DMDS	1	2	3		
Time	13:19	13:46	13:59		
Concentration, ppm	4.39	2.01	0.83		
Area, mv-sec	58634	17956	3589		
Calc. Conc., ppm	4.28	2.11	0.81		
% Error	-2.5	4.9	-2.2		
<u>Calibration Curve</u>	<b>Slope</b>	<b>Intercept</b>	<b>Corr. Coeff.</b>	<b>Min. Area</b>	<b>Det. Lim.</b>
	1.6755	3.7107	0.9988	2	0.009

# CALIBRATION DATA

Number 2

Client: **New Indy**  
Location: **Catawba, SC**  
Source:

Project Number: **15730.001.006**  
Operator: **T. Simpkins**  
Date: **17 Mar 2021**

Method 16

Ambient Temperature: 72°C

Barometric Pressure: 30.20 in. Hg

Analyte	H <sub>2</sub> S	MeSH	DMS	DMDS
Perm. Device ID	T-53950	33-56671	89-56661	89-56665
Perm. Rate, nL/min	422	455	306	217
Ret. Time, sec	19.0	32.5	70.0	125.0

1 Flow = 43.1 mL/Min      9.80 ppm      10.6 ppm      7.09 ppm      5.04 ppm

Time: 08:28

Peak Areas, mv-sec

32885	40065	21703	62655	
32377	40847	22337	64423	
33445	40700	22722	65189	
<b>Average Area</b>	<b>32902</b> ✓	<b>40537</b> ✓	<b>22254</b> ✓	<b>64089</b> ✓

2 Flow = 91.6 mL/Min      4.61 ppm      4.97 ppm      3.34 ppm      2.37 ppm

Time: 08:45

Peak Areas, mv-sec

10234	12405	6217	19301	
9896	12664	6278	19254	
10029	12369	6218	19511	
<b>Average Area</b>	<b>10053</b> ✓	<b>12479</b> ✓	<b>6238</b> ✓	<b>19355</b> ✓

3 Flow = 215 mL/Min      1.96 ppm      2.12 ppm      1.42 ppm      1.01 ppm

Time: 09:10

Peak Areas, mv-sec

2028	2745	1321	4433	
2061	2708	1308	4367	
2026	2706	1300	4291	
<b>Average Area</b>	<b>2038</b> ✓	<b>2720</b> ✓	<b>1310</b> ✓	<b>4364</b> ✓

# CALIBRATION SUMMARY

Number 2

Client: **New Indy**  
Location: **Catawba, SC**  
Source:

Project Number: **15730.001.006**  
Operator: **T. Simpkins**  
Date: **17 Mar 2021**

Method **16**

H <sub>2</sub> S	1	2	3		
Time	08:28	08:45	09:10		
Concentration, ppm	9.80	4.61	1.96		
Area, mv-sec	32902	10053	2038		
Calc. Conc., ppm	9.56	4.83	1.92		
% Error	-2.4	4.7	-2.1		
<u>Calibration Curve</u>	<b>Slope</b>	<b>Intercept</b>	<b>Corr. Coeff.</b>	<b>Min. Area</b>	<b>Det. Lim.</b>
	1.7338	2.8171	0.9988	2	0.035

MeSH	1	2	3		
Time	08:28	08:45	09:10		
Concentration, ppm	10.6	4.97	2.12		
Area, mv-sec	40537	12479	2720		
Calc. Conc., ppm	10.4	5.15	2.08		
% Error	-1.9	3.6	-1.6		
<u>Calibration Curve</u>	<b>Slope</b>	<b>Intercept</b>	<b>Corr. Coeff.</b>	<b>Min. Area</b>	<b>Det. Lim.</b>
	1.6833	2.8984	0.9993	2	0.029

DMS	1	2	3		
Time	08:28	08:45	09:10		
Concentration, ppm	7.09	3.34	1.42		
Area, mv-sec	22254	6238	1310		
Calc. Conc., ppm	7.01	3.41	1.41		
% Error	-1.1	2.2	-1.0		
<u>Calibration Curve</u>	<b>Slope</b>	<b>Intercept</b>	<b>Corr. Coeff.</b>	<b>Min. Area</b>	<b>Det. Lim.</b>
	1.7640	2.8552	0.9997	2	0.036

DMDS	1	2	3		
Time	08:28	08:45	09:10		
Concentration, ppm	5.04	2.37	1.01		
Area, mv-sec	64089	19355	4364		
Calc. Conc., ppm	4.97	2.43	1.00		
% Error	-1.3	2.5	-1.2		
<u>Calibration Curve</u>	<b>Slope</b>	<b>Intercept</b>	<b>Corr. Coeff.</b>	<b>Min. Area</b>	<b>Det. Lim.</b>
	1.6735	3.6414	0.9996	2	0.010

# ANALYTES AND STANDARDS

Client: **New Indy**  
Location: **Catawba, SC**  
Source:

Project Number: **15730.001.006**  
Operator: **T. Simpkins**  
Date: **15 Mar 2021**

Method **16**

Analyte	H <sub>2</sub> S	MeSH	DMS	DMDS
<b>Molecular Weight</b>	34.08	48.11	62.14	94.20
<b>Retention Time, sec</b>	19.0	32.5	70.0	125.0
<b>Peak Detection Window, sec</b>	3.0	5.0	10.0	10.0
<b>Minimum Peak Area, mv-sec</b>	2	2	2	2
<b>Minimum Peak Height, mv</b>	1	1	1	1
<b>Beginning Peak Width, sec</b>	1.0	1.0	2.0	3.0
<b>Ending Peak Width, sec</b>	2.0	3.0	4.0	5.0
<b>Permeation Device ID</b>	T-53950	33-56671	89-56661	89-56665
<b>Permeation Rate, ng/min</b>	600 ✓	913 ✓	792 ✓	852 ✓
<b>Permeation Rate, nL/min*</b>	422	455	306	217

**Barometric Pressure:** 30.20 in. Hg      **Ambient Temperature:** 72 °F  
No Oxygen Correction

\*Permeation rates are gravimetrically determined by the manufacturer with results by weight in ng/min. Permeation rates by volume, in nL/min, are calculated from the permeation rates by weight as follows:

$$PR_{nl} = PR_{ng} \times (V_{mol} / W_{mol}) \times [(460^\circ + T_a) / T_s] \times (P_s / P_b)$$

Where:

- PR<sub>nl</sub>** = Permeation Rate by volume, nL/min
- PR<sub>ng</sub>** = Permeation Rate by weight, ng/min
- V<sub>mol</sub>** = Molar Volume of any gas @32 °F & 29.92 mm Hg = 22.4 L/mole
- W<sub>mol</sub>** = Molecular Weight of compound
- T<sub>a</sub>** = Ambient Temperature, °F
- T<sub>s</sub>** = Standard Temperature = 492°R (32 °F)
- P<sub>s</sub>** = Standard Pressure = 29.92 in Hg
- P<sub>b</sub>** = Barometric Pressure, in Hg

For example, H<sub>2</sub>S:

$$PR_{nl} = 600 \times (22.4 / 34.08) \times [(460 + 72) / 492] \times (29.92 / 30.20) = 422 \text{ nL/min}$$

To calculate concentrations:

$$C = PR_{nl} / F_d$$

Where:

- C** = Concentration, ppmv
- PR<sub>nl</sub>** = Permeation Rate by volume, nL/min
- F<sub>d</sub>** = Flow rate of diluent, mL/min

**INSTRUMENT INFORMATION**

Client: **New Indy**  
 Location: **Catawba, SC**  
 Source:

Method **16**

Project Number: **15730.001.006**  
 Operator: **T. Simpkins**  
 Date: **15 Mar 2021**

File: C:\Data\TrsData1.trs  
 Program Version: 2.0, built 15 May 2017 File Version: 2.0  
 Computer: DESKTOP-A1IJDGT Trailer: 88

Analog Input Device: Keithley KUSB-3108 GC Channel: 16

Sampling Rate: 0.050 sec. Data Interval: 0.5 sec.

Gas Chromatograph: Shimadzu GC8A Serial No. GC 1  
 Detector Range: 10

Gases			Temperatures, °C	Columns
	Press. psi	Flow mL/min	Column: 100 Detector: 120	Primary: Carbopack Secondary: N/A Sample Loop: 4"
H <sub>2</sub>	30	50		
Air	30	60		
Carrier	50	30		

**Injection Cycle**

Total Length: 180 sec Sampling Time: 170 sec Load/Backflush Time: 80 sec

**Default Integration Parameters**

Signal Threshold 0.67 mv Peak detection window ±10 sec  
 Minimum peak area 2 mv-sec Minimum peak height 1 mv above baseline

**Dynacalibrator**

Chamber Temperature 50.0°C  
 Ambient Temperature 72.0°F  
 Barometric Pressure 30.20 in. Hg



**17-18 MARCH 2021**

# RUN SUMMARY

Number 1

Client: **New Indy**  
Location: **Catawba, SC**  
Source:

Method **16**  
Calibration **1**

Project Number: **15730.001.006**  
Operator: **T. Simpkins**  
Date: **17 Mar 2021**

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**Start Time 09:46    End Time 15:53**

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**Average Measured TRS Conc.    0.02 ppm**  
**Recovery Missing**

# RUN SUMMARY

Number 3

Client: **New Indy**  
Location: **Catawba, SC**  
Source:

Method **16**  
Calibration **1**

Project Number: **15730.001.006**  
Operator: **T. Simpkins**  
Date: **17 Mar 2021**

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**Start Time 16:45    End Time 07:59**

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**Average Measured TRS Conc.    0.02 ppm**  
**Recovery Missing**



# RUN DATA

Number 1

Client: **New Indy**  
Location: **Catawba, SC**  
Source:

Method **16**  
Calibration **1**

Project Number: **15730.001.006**  
Operator: **T. Simpkins**  
Date: **17 Mar 2021**

Time	H <sub>2</sub> S		MeSH		DMS		DMDS		TRS ppm
	area	ppm	area	ppm	area	ppm	area	ppm	
09:46	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
09:46	2	0.03	<2	<0.024	<2	<0.030	<2	<0.008	0.03
09:49	2	0.03	<2	<0.024	<2	<0.030	<2	<0.008	0.03
09:52	4	0.04	<2	<0.024	<2	<0.030	<2	<0.008	0.04
09:55	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
09:58	3	0.04	<2	<0.024	<2	<0.030	<2	<0.008	0.04
10:01	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
10:04	3	0.04	<2	<0.024	<2	<0.030	<2	<0.008	0.04
10:07	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
10:10	2	0.03	<2	<0.024	<2	<0.030	2	0.01	0.05
10:13	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
10:16	2	0.03	<2	<0.024	<2	<0.030	<2	<0.008	0.03
10:19	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
10:22	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
10:25	2	0.03	<2	<0.024	<2	<0.030	<2	<0.008	0.03
10:28	5	0.05	<2	<0.024	<2	<0.030	<2	<0.008	0.05
10:31	2	0.03	<2	<0.024	<2	<0.030	<2	<0.008	0.03
10:34	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
10:37	2	0.03	<2	<0.024	<2	<0.030	<2	<0.008	0.03
10:41	2	0.03	<2	<0.024	<2	<0.030	<2	<0.008	0.03
10:44	2	0.03	<2	<0.024	<2	<0.030	<2	<0.008	0.03
10:47	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
10:50	5	0.05	<2	<0.024	<2	<0.030	<2	<0.008	0.05
10:53	6	0.05	<2	<0.024	<2	<0.030	<2	<0.008	0.05
10:56	3	0.03	<2	<0.024	<2	<0.030	<2	<0.008	0.03
10:59	7	0.06	<2	<0.024	<2	<0.030	<2	<0.008	0.06
11:02	5	0.05	<2	<0.024	<2	<0.030	<2	<0.008	0.05
11:05	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
11:08	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
11:11	2	0.03	<2	<0.024	<2	<0.030	<2	<0.008	0.03
11:14	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
11:17	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
11:20	<2	<0.029	3	0.03	<2	<0.030	<2	<0.008	0.03
11:23	8	0.06	<2	<0.024	2	0.03	6	0.02	0.13
11:26	<2	<0.029	3	0.03	<2	<0.030	3	0.01	0.05
11:29	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
11:32	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
11:35	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
11:38	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
11:41	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-

# RUN DATA

Number 1

Client: **New Indy**  
Location: **Catawba, SC**  
Source:

Method **16**  
Calibration **1**

Project Number: **15730.001.006**  
Operator: **T. Simpkins**  
Date: **17 Mar 2021**

Time	H <sub>2</sub> S		MeSH		DMS		DMDS		TRS ppm
	area	ppm	area	ppm	area	ppm	area	ppm	
11:44	3	0.03	<2	<0.024	<2	<0.030	<2	<0.008	0.03
11:47	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
11:50	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
11:53	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
11:56	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
11:59	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
12:02	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
12:05	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
12:08	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
12:11	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
12:14	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
12:17	3	0.04	<2	<0.024	<2	<0.030	<2	<0.008	0.04
12:20	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
12:23	3	0.04	<2	<0.024	2	0.03	<2	<0.008	0.07
12:26	3	0.04	<2	<0.024	<2	<0.030	<2	<0.008	0.04
12:29	2	0.03	<2	<0.024	<2	<0.030	<2	<0.008	0.03
12:32	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
12:35	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
12:38	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
12:41	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
12:44	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
12:47	7	0.06	<2	<0.024	<2	<0.030	<2	<0.008	0.06
12:50	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
12:53	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
12:56	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
12:59	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
13:02	3	0.04	<2	<0.024	4	0.04	<2	<0.008	0.08
13:05	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
13:08	<2	<0.029	<2	<0.024	<2	<0.030	3	0.01	0.02
13:11	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
13:14	2	0.03	<2	<0.024	<2	<0.030	<2	<0.008	0.03
13:17	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
13:20	3	0.04	<2	<0.024	<2	<0.030	<2	<0.008	0.04
13:23	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
13:26	<2	<0.029	<2	<0.024	<2	<0.030	2	0.01	0.02
13:29	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
13:32	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
13:35	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
13:38	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
13:41	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-

# RUN DATA

Number 1

Client: **New Indy**  
Location: **Catawba, SC**  
Source:

Method **16**  
Calibration **1**

Project Number: **15730.001.006**  
Operator: **T. Simpkins**  
Date: **17 Mar 2021**

Time	H <sub>2</sub> S		MeSH		DMS		DMDS		TRS ppm
	area	ppm	area	ppm	area	ppm	area	ppm	
13:44	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
13:47	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
13:50	7	0.06	<2	<0.024	<2	<0.030	<2	<0.008	0.06
13:53	9	0.07	2	0.03	<2	<0.030	<2	<0.008	0.10
13:56	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
13:59	<2	<0.029	3	0.03	<2	<0.030	3	0.01	0.05
14:02	8	0.07	<2	<0.024	<2	<0.030	<2	<0.008	0.07
14:05	7	0.06	<2	<0.024	2	0.03	<2	<0.008	0.09
14:08	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
14:11	<2	<0.029	<2	<0.024	<2	<0.030	3	0.01	0.02
14:14	4	0.05	<2	<0.024	<2	<0.030	<2	<0.008	0.05
14:17	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
14:20	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
14:23	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
14:26	3	0.04	<2	<0.024	<2	<0.030	<2	<0.008	0.04
14:29	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
14:32	6	0.06	<2	<0.024	<2	<0.030	<2	<0.008	0.06
14:35	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
14:38	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
14:41	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
14:44	3	0.03	<2	<0.024	<2	<0.030	<2	<0.008	0.03
14:47	3	0.04	<2	<0.024	<2	<0.030	3	0.01	0.06
14:50	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
14:53	2	0.03	2	0.03	<2	<0.030	<2	<0.008	0.06
14:56	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
14:59	<2	<0.029	<2	<0.024	<2	<0.030	4	0.01	0.03
15:02	<2	<0.029	<2	<0.024	2	0.03	<2	<0.008	0.03
15:05	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
15:08	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
15:11	3	0.04	<2	<0.024	<2	<0.030	<2	<0.008	0.04
15:14	<2	<0.029	<2	<0.024	3	0.03	<2	<0.008	0.03
15:17	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
15:20	3	0.04	<2	<0.024	<2	<0.030	<2	<0.008	0.04
15:23	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
15:26	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
15:29	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
15:32	<2	<0.029	<2	<0.024	<2	<0.030	3	0.01	0.02
15:35	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
15:38	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
15:41	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-

# RUN DATA

Number 1

Client: **New Indy**  
 Location: **Catawba, SC**  
 Source:

Method **16**  
 Calibration **1**

Project Number: **15730.001.006**  
 Operator: **T. Simpkins**  
 Date: **17 Mar 2021**

Time	H <sub>2</sub> S		MeSH		DMS		DMDS		TRS
	area	ppm	area	ppm	area	ppm	area	ppm	ppm
15:44	3	0.04	<2	<0.024	<2	<0.030	5	0.01	0.06
15:47	3	0.04	<2	<0.024	<2	<0.030	<2	<0.008	0.04
15:50	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
<b>Average</b>		<b>&lt;0.029</b>		<b>&lt;0.024</b>		<b>&lt;0.030</b>		<b>&lt;0.008</b>	<b>-</b>

# RUN DATA

Number 3

Client: **New Indy**  
Location: **Catawba, SC**  
Source:

Method **16**  
Calibration **1**

Project Number: **15730.001.006**

Operator: **T. Simpkins**

Date: **17 Mar 2021**

Time	H <sub>2</sub> S		MeSH		DMS		DMDS		TRS
	area	ppm	area	ppm	area	ppm	area	ppm	ppm
<b>North Clarifier</b>									
16:45	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
16:48	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
16:51	3	0.03	<2	<0.024	<2	<0.030	<2	<0.008	0.03
16:54	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
16:57	3	0.04	<2	<0.024	<2	<0.030	<2	<0.008	0.04
17:00	6	0.05	<2	<0.024	<2	<0.030	<2	<0.008	0.05
17:03	<2	<0.029	<2	<0.024	<2	<0.030	4	0.01	0.03
17:06	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
17:09	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
17:12	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
17:15	<2	<0.029	<2	<0.024	<2	<0.030	2	0.01	0.02
17:18	3	0.04	<2	<0.024	<2	<0.030	3	0.01	0.06
17:21	3	0.04	<2	<0.024	<2	<0.030	<2	<0.008	0.04
17:24	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
17:27	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
17:30	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
17:33	3	0.04	<2	<0.024	<2	<0.030	<2	<0.008	0.04
17:36	<2	<0.029	<2	<0.024	<2	<0.030	5	0.01	0.03
17:39	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
17:42	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
17:45	<2	<0.029	<2	<0.024	<2	<0.030	3	0.01	0.02
17:48	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
17:51	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
17:54	<2	<0.029	<2	<0.024	<2	<0.030	3	0.01	0.02
17:57	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
18:00	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
18:03	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
18:06	2	0.03	<2	<0.024	<2	<0.030	<2	<0.008	0.03
18:09	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
18:12	6	0.06	<2	<0.024	<2	<0.030	<2	<0.008	0.06
18:15	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
18:18	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
18:21	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
18:24	<2	<0.029	<2	<0.024	8	0.06	<2	<0.008	0.06
18:27	6	0.05	<2	<0.024	<2	<0.030	<2	<0.008	0.05
18:30	<2	<0.029	4	0.03	<2	<0.030	<2	<0.008	0.03
18:33	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
18:36	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
18:39	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-

# RUN DATA

Number 3

Client: **New Indy**  
Location: **Catawba, SC**  
Source:

Method **16**  
Calibration **1**

Project Number: **15730.001.006**  
Operator: **T. Simpkins**  
Date: **17 Mar 2021**

Time	H <sub>2</sub> S		MeSH		DMS		DMDS		TRS ppm
	area	ppm	area	ppm	area	ppm	area	ppm	
18:42	<2	<0.029	<2	<0.024	3	0.04	<2	<0.008	0.04
18:45	2	0.03	<2	<0.024	<2	<0.030	<2	<0.008	0.03
18:48	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
18:51	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
18:54	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
18:57	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
19:00	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
19:03	<2	<0.029	3	0.03	<2	<0.030	<2	<0.008	0.03
19:06	3	0.04	<2	<0.024	<2	<0.030	<2	<0.008	0.04
19:09	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
19:12	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
19:15	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
19:18	<2	<0.029	2	0.02	<2	<0.030	5	0.01	0.05
19:21	2	0.03	<2	<0.024	<2	<0.030	2	0.01	0.05
19:24	<2	<0.029	<2	<0.024	<2	<0.030	3	0.01	0.02
19:27	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
19:30	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
19:33	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
19:36	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
19:39	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
19:42	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
19:45	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
19:48	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
19:51	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
19:54	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
19:57	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
20:00	2	0.03	<2	<0.024	<2	<0.030	<2	<0.008	0.03
20:03	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
20:06	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
20:09	5	0.05	<2	<0.024	<2	<0.030	<2	<0.008	0.05
20:12	<2	<0.029	<2	<0.024	3	0.04	<2	<0.008	0.04
20:15	4	0.05	<2	<0.024	<2	<0.030	<2	<0.008	0.05
20:18	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
20:21	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
20:24	8	0.06	<2	<0.024	7	0.06	<2	<0.008	0.12
20:27	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
20:30	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
20:33	3	0.04	<2	<0.024	<2	<0.030	<2	<0.008	0.04
20:36	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
20:39	6	0.05	<2	<0.024	<2	<0.030	<2	<0.008	0.05

# RUN DATA

Number 3

Client: **New Indy**  
Location: **Catawba, SC**  
Source:

Method **16**  
Calibration **1**

Project Number: **15730.001.006**  
Operator: **T. Simpkins**  
Date: **17 Mar 2021**

Time	H <sub>2</sub> S		MeSH		DMS		DMDS		TRS ppm
	area	ppm	area	ppm	area	ppm	area	ppm	
20:42	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
20:45	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
20:48	4	0.04	<2	<0.024	<2	<0.030	<2	<0.008	0.04
20:51	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
20:54	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
20:57	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
21:00	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
21:03	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
21:06	<2	<0.029	<2	<0.024	<2	<0.030	3	0.01	0.02
21:09	<2	<0.029	<2	<0.024	3	0.03	<2	<0.008	0.03
21:12	7	0.06	<2	<0.024	<2	<0.030	<2	<0.008	0.06
21:15	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
21:18	3	0.04	<2	<0.024	<2	<0.030	<2	<0.008	0.04
21:21	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
21:24	<2	<0.029	<2	<0.024	2	0.03	<2	<0.008	0.03
21:27	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
21:30	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
21:33	3	0.04	<2	<0.024	<2	<0.030	<2	<0.008	0.04
21:36	4	0.05	2	0.02	<2	<0.030	<2	<0.008	0.07
21:39	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
21:42	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
21:45	<2	<0.029	<2	<0.024	3	0.03	<2	<0.008	0.03
21:48	<2	<0.029	2	0.02	<2	<0.030	<2	<0.008	0.02
21:51	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
21:54	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
21:57	9	0.07	<2	<0.024	2	0.03	<2	<0.008	0.10
22:00	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
22:04	<2	<0.029	<2	<0.024	3	0.04	<2	<0.008	0.04
22:07	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
22:10	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
22:13	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
22:16	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
22:19	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
22:22	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
22:25	<2	<0.029	<2	<0.024	<2	<0.030	4	0.01	0.02
22:28	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
22:31	<2	<0.029	3	0.03	<2	<0.030	<2	<0.008	0.03
22:34	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
22:37	<2	<0.029	<2	<0.024	10	0.07	<2	<0.008	0.07
22:40	<2	<0.029	<2	<0.024	2	0.03	<2	<0.008	0.03

# RUN DATA

Number 3

Client: **New Indy**  
Location: **Catawba, SC**  
Source:

Method **16**  
Calibration **1**

Project Number: **15730.001.006**  
Operator: **T. Simpkins**  
Date: **17 Mar 2021**

Time	H <sub>2</sub> S		MeSH		DMS		DMDS		TRS
	area	ppm	area	ppm	area	ppm	area	ppm	ppm
22:43	10	0.07	<2	<0.024	<2	<0.030	<2	<0.008	0.07
22:46	<2	<0.029	<2	<0.024	<2	<0.030	5	0.02	0.03
22:49	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
22:52	<2	<0.029	<2	<0.024	<2	<0.030	3	0.01	0.02
22:55	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
22:58	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
23:01	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
23:04	<2	<0.029	<2	<0.024	<2	<0.030	3	0.01	0.02
23:07	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
23:10	<2	<0.029	<2	<0.024	5	0.05	<2	<0.008	0.05
23:13	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
23:16	3	0.04	<2	<0.024	<2	<0.030	<2	<0.008	0.04
23:19	3	0.04	<2	<0.024	<2	<0.030	<2	<0.008	0.04
23:22	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
23:25	2	0.03	<2	<0.024	<2	<0.030	<2	<0.008	0.03
23:28	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
23:31	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
23:34	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
23:37	2	0.03	<2	<0.024	<2	<0.030	<2	<0.008	0.03
23:40	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
23:43	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
23:46	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
23:49	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
23:52	4	0.04	<2	<0.024	<2	<0.030	<2	<0.008	0.04
23:55	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
23:58	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
00:01	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
00:04	3	0.04	<2	<0.024	<2	<0.030	<2	<0.008	0.04
00:07	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
00:10	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
00:13	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
00:16	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
00:19	7	0.06	<2	<0.024	<2	<0.030	<2	<0.008	0.06
00:22	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
00:25	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
00:28	3	0.04	<2	<0.024	<2	<0.030	<2	<0.008	0.04
00:31	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
00:34	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
00:37	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
00:40	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-



# RUN DATA

Number 3

Client: **New Indy**  
Location: **Catawba, SC**  
Source:

Method **16**  
Calibration **1**

Project Number: **15730.001.006**  
Operator: **T. Simpkins**  
Date: **17 Mar 2021**

Time	H <sub>2</sub> S		MeSH		DMS		DMDS		TRS
	area	ppm	area	ppm	area	ppm	area	ppm	ppm
00:43	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
00:46	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
00:49	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
00:52	<2	<0.029	<2	<0.024	<2	<0.030	4	0.01	0.02
00:55	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
00:58	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
01:01	4	0.04	<2	<0.024	<2	<0.030	<2	<0.008	0.04
01:04	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
01:07	3	0.04	<2	<0.024	<2	<0.030	10	0.02	0.08
01:10	3	0.03	<2	<0.024	<2	<0.030	<2	<0.008	0.03
01:13	<2	<0.029	<2	<0.024	<2	<0.030	4	0.01	0.03
01:16	2	0.03	<2	<0.024	<2	<0.030	<2	<0.008	0.03
01:19	2	0.03	<2	<0.024	<2	<0.030	<2	<0.008	0.03
01:22	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
01:25	<2	<0.029	3	0.03	<2	<0.030	<2	<0.008	0.03
01:28	<2	<0.029	<2	<0.024	3	0.04	<2	<0.008	0.04
01:31	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
01:34	3	0.04	<2	<0.024	<2	<0.030	<2	<0.008	0.04
01:37	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
01:40	<2	<0.029	<2	<0.024	<2	<0.030	3	0.01	0.02
01:43	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
01:46	<2	<0.029	<2	<0.024	<2	<0.030	3	0.01	0.02
01:49	<2	<0.029	<2	<0.024	2	0.03	<2	<0.008	0.03
01:52	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
01:55	2	0.03	<2	<0.024	<2	<0.030	<2	<0.008	0.03
01:58	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
02:01	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
02:04	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
02:07	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
02:10	<2	<0.029	<2	<0.024	2	0.03	<2	<0.008	0.03
02:13	3	0.03	<2	<0.024	<2	<0.030	<2	<0.008	0.03
02:16	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
02:19	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
02:22	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
02:25	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
02:28	3	0.04	<2	<0.024	<2	<0.030	<2	<0.008	0.04
02:31	<2	<0.029	<2	<0.024	<2	<0.030	2	0.01	0.02
02:34	<2	<0.029	<2	<0.024	<2	<0.030	2	0.01	0.02
02:37	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
02:40	<2	<0.029	<2	<0.024	<2	<0.030	9	0.02	0.04

# RUN DATA

Number 3

Client: **New Indy**  
Location: **Catawba, SC**  
Source:

Method **16**  
Calibration **1**

Project Number: **15730.001.006**  
Operator: **T. Simpkins**  
Date: **17 Mar 2021**

Time	H <sub>2</sub> S		MeSH		DMS		DMDS		TRS
	area	ppm	area	ppm	area	ppm	area	ppm	ppm
02:43	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
02:46	5	0.05	<2	<0.024	<2	<0.030	<2	<0.008	0.05
02:49	4	0.04	<2	<0.024	<2	<0.030	<2	<0.008	0.04
02:52	2	0.03	<2	<0.024	<2	<0.030	6	0.02	0.06
02:55	3	0.04	<2	<0.024	<2	<0.030	<2	<0.008	0.04
02:58	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
03:01	<2	<0.029	<2	<0.024	4	0.05	<2	<0.008	0.05
03:04	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
03:07	3	0.04	<2	<0.024	<2	<0.030	<2	<0.008	0.04
03:10	<2	<0.029	<2	<0.024	<2	<0.030	2	0.01	0.02
03:13	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
03:16	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
03:19	4	0.04	<2	<0.024	<2	<0.030	<2	<0.008	0.04
03:22	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
03:25	3	0.04	<2	<0.024	<2	<0.030	<2	<0.008	0.04
03:28	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
03:31	3	0.04	<2	<0.024	<2	<0.030	<2	<0.008	0.04
03:34	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
03:37	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
03:40	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
03:43	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
03:46	2	0.03	<2	<0.024	<2	<0.030	<2	<0.008	0.03
03:49	<2	<0.029	<2	<0.024	<2	<0.030	2	0.01	0.02
03:52	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
03:55	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
03:58	2	0.03	<2	<0.024	<2	<0.030	<2	<0.008	0.03
04:01	<2	<0.029	<2	<0.024	2	0.03	<2	<0.008	0.03
04:05	3	0.03	<2	<0.024	<2	<0.030	2	0.01	0.05
04:08	<2	<0.029	<2	<0.024	2	0.03	<2	<0.008	0.03
04:11	2	0.03	<2	<0.024	<2	<0.030	<2	<0.008	0.03
04:14	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
04:17	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
04:20	3	0.04	<2	<0.024	<2	<0.030	<2	<0.008	0.04
04:23	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
04:26	5	0.05	<2	<0.024	<2	<0.030	<2	<0.008	0.05
04:29	5	0.05	<2	<0.024	<2	<0.030	<2	<0.008	0.05
04:32	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
04:35	<2	<0.029	<2	<0.024	<2	<0.030	5	0.01	0.03
04:38	<2	<0.029	<2	<0.024	3	0.04	<2	<0.008	0.04
04:41	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-

# RUN DATA

Number 3

Client: **New Indy**  
Location: **Catawba, SC**  
Source:

Method **16**  
Calibration **1**

Project Number: **15730.001.006**  
Operator: **T. Simpkins**  
Date: **17 Mar 2021**

Time	H <sub>2</sub> S		MeSH		DMS		DMDS		TRS ppm
	area	ppm	area	ppm	area	ppm	area	ppm	
04:44	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
04:47	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
04:50	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
04:53	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
04:56	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
04:59	<2	<0.029	<2	<0.024	<2	<0.030	3	0.01	0.02
05:02	9	0.07	<2	<0.024	<2	<0.030	<2	<0.008	0.07
05:05	2	0.03	<2	<0.024	<2	<0.030	<2	<0.008	0.03
05:08	3	0.04	<2	<0.024	<2	<0.030	<2	<0.008	0.04
05:11	3	0.04	<2	<0.024	<2	<0.030	<2	<0.008	0.04
05:14	2	0.03	<2	<0.024	<2	<0.030	<2	<0.008	0.03
05:17	3	0.04	<2	<0.024	<2	<0.030	<2	<0.008	0.04
05:20	3	0.04	<2	<0.024	<2	<0.030	4	0.01	0.06
05:23	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
05:26	2	0.03	<2	<0.024	<2	<0.030	<2	<0.008	0.03
05:29	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
05:32	3	0.04	5	0.04	2	0.03	<2	<0.008	0.11
05:35	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
05:38	<2	<0.029	2	0.02	<2	<0.030	5	0.01	0.05
05:41	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
05:44	4	0.04	<2	<0.024	<2	<0.030	<2	<0.008	0.04
05:47	2	0.03	<2	<0.024	<2	<0.030	2	0.01	0.05
05:50	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
05:53	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
05:56	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
05:59	2	0.03	<2	<0.024	<2	<0.030	<2	<0.008	0.03
06:02	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
06:05	3	0.04	<2	<0.024	<2	<0.030	<2	<0.008	0.04
06:08	3	0.03	3	0.03	<2	<0.030	<2	<0.008	0.06
06:11	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
06:14	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
06:17	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
06:20	6	0.05	<2	<0.024	<2	<0.030	<2	<0.008	0.05
06:23	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
06:26	2	0.03	<2	<0.024	<2	<0.030	<2	<0.008	0.03
06:29	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-
06:32	<2	<0.029	<2	<0.024	<2	<0.030	3	0.01	0.02
06:35	3	0.04	<2	<0.024	<2	<0.030	<2	<0.008	0.04
06:38	3	0.04	<2	<0.024	<2	<0.030	4	0.01	0.07
06:41	<2	<0.029	<2	<0.024	<2	<0.030	<2	<0.008	-



# CALIBRATION DATA

Number 1

Client: **New Indy**  
Location: **Catawba, SC**  
Source:

Project Number: **15730.001.006**  
Operator: **T. Simpkins**  
Date: **17 Mar 2021**

Method 16

		Ambient Temperature: 72°C		Barometric Pressure: 30.20 in. Hg		
Analyte	H <sub>2</sub> S	MeSH	DMS	DMDS		
Perm. Device ID	T-53950	33-56671	89-56661	89-56665		
Perm. Rate, nL/min	422	455	306	217		
Ret. Time, sec	19.0	32.5	70.0	125.0		
<hr/>						
1	Flow = 51.7 mL/Min	8.17 ppm	8.80 ppm	5.91 ppm	4.20 ppm	
	Time: 08:28	Peak Areas, mv-sec				
		32885	40065	21703	62655	
		32377	40847	22337	64423	
		33445	40700	22722	65189	
	<u>Average Area</u>	<b>32902</b> ✓	<b>40537</b> ✓	<b>22254</b> ✓	<b>64089</b> ✓	
<hr/>						
2	Flow = 110 mL/Min	3.84 ppm	4.14 ppm	2.78 ppm	1.98 ppm	
	Time: 08:45	Peak Areas, mv-sec				
		10234	12405	6217	19301	
		9896	12664	6278	19254	
		10029	12369	6218	19511	
	<u>Average Area</u>	<b>10053</b> ✓	<b>12479</b> ✓	<b>6238</b> ✓	<b>19355</b> ✓	
<hr/>						
3	Flow = 258 mL/Min	1.64 ppm	1.76 ppm	1.18 ppm	0.84 ppm	
	Time: 09:10	Peak Areas, mv-sec				
		2028	2745	1321	4433	
		2061	2708	1308	4367	
		2026	2706	1300	4291	
	<u>Average Area</u>	<b>2038</b> ✓	<b>2720</b> ✓	<b>1310</b> ✓	<b>4364</b> ✓	

# CALIBRATION SUMMARY

Number 1

Client: **New Indy**  
Location: **Catawba, SC**  
Source:

Project Number: **15730.001.006**  
Operator: **T. Simpkins**  
Date: **17 Mar 2021**

Method **16**

H <sub>2</sub> S	1	2	3		
Time	08:28	08:45	09:10		
Concentration, ppm	8.17	3.84	1.64		
Area, mv-sec	32902	10053	2038		
Calc. Conc., ppm	7.97	4.02	1.60		
% Error	-2.4	4.7	-2.1		
<u>Calibration Curve</u>	<b>Slope</b>	<b>Intercept</b>	<b>Corr. Coeff.</b>	<b>Min. Area</b>	<b>Det. Lim.</b>
	1.7333	2.9545	0.9988	2	0.029

MeSH	1	2	3		
Time	08:28	08:45	09:10		
Concentration, ppm	8.80	4.14	1.76		
Area, mv-sec	40537	12479	2720		
Calc. Conc., ppm	8.64	4.29	1.74		
% Error	-1.9	3.6	-1.6		
<u>Calibration Curve</u>	<b>Slope</b>	<b>Intercept</b>	<b>Corr. Coeff.</b>	<b>Min. Area</b>	<b>Det. Lim.</b>
	1.6829	3.0318	0.9993	2	0.024

DMS	1	2	3		
Time	08:28	08:45	09:10		
Concentration, ppm	5.91	2.78	1.18		
Area, mv-sec	22254	6238	1310		
Calc. Conc., ppm	5.85	2.84	1.17		
% Error	-1.1	2.2	-1.0		
<u>Calibration Curve</u>	<b>Slope</b>	<b>Intercept</b>	<b>Corr. Coeff.</b>	<b>Min. Area</b>	<b>Det. Lim.</b>
	1.7636	2.9950	0.9997	2	0.030

DMDS	1	2	3		
Time	08:28	08:45	09:10		
Concentration, ppm	4.20	1.98	0.84		
Area, mv-sec	64089	19355	4364		
Calc. Conc., ppm	4.14	2.03	0.83		
% Error	-1.3	2.5	-1.2		
<u>Calibration Curve</u>	<b>Slope</b>	<b>Intercept</b>	<b>Corr. Coeff.</b>	<b>Min. Area</b>	<b>Det. Lim.</b>
	1.6731	3.7739	0.9996	2	0.008

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# CALIBRATION DATA

Number 2

Client: **New Indy**  
Location: **Catawba, SC**  
Source:

Project Number: **15730.001.006**  
Operator: **T. Simpkins**  
Date: **18 Mar 2021**

Method 16

Analyte	Ambient Temperature: 72°C		Barometric Pressure: 30.20 in. Hg		
	H <sub>2</sub> S	MeSH	DMS	DMDS	
Perm. Device ID	T-53950	33-56671	89-56661	89-56665	
Perm. Rate, nL/min	422	455	306	217	
Ret. Time, sec	19.0	32.5	70.0	125.0	

Flow	H <sub>2</sub> S	MeSH	DMS	DMDS
1 Flow = 55.0 mL/Min	7.68 ppm	8.28 ppm	5.56 ppm	3.95 ppm
Time: 08:30	Peak Areas, mv-sec			
	37217	48066	25482	71756
	38155	47820	25458	71884
	37886	48063	25691	71544
<u>Average Area</u>	<b>37753</b> ✓	<b>47983</b> ✓	<b>25544</b> ✓	<b>71728</b> ✓
2 Flow = 108 mL/Min	3.91 ppm	4.21 ppm	2.83 ppm	2.01 ppm
Time: 08:53	Peak Areas, mv-sec			
	11220	15593	6415	19990
	11626	15400	6404	19931
	11251	15235	6408	19816
<u>Average Area</u>	<b>11366</b> ✓	<b>15409</b> ✓	<b>6409</b> ✓	<b>19912</b> ✓
3 Flow = 234 mL/Min	1.80 ppm	1.95 ppm	1.31 ppm	0.93 ppm
Time: 09:08	Peak Areas, mv-sec			
	2385	3436	1360	4560
	2307	3358	1346	4470
	2361	3302	1307	4384
<u>Average Area</u>	<b>2351</b> ✓	<b>3365</b> ✓	<b>1338</b> ✓	<b>4471</b> ✓

*an*

# CALIBRATION SUMMARY

Number 2

Client: **New Indy**  
Location: **Catawba, SC**  
Source:

Project Number: **15730.001.006**  
Operator: **T. Simpkins**  
Date: **18 Mar 2021**

Method **16**

H <sub>2</sub> S	1	2	3		
Time	08:30	08:53	09:08		
Concentration, ppm	7.68	3.91	1.80		
Area, mv-sec	37753	11366	2351		
Calc. Conc., ppm	7.55	4.04	1.78		
% Error	-1.7	3.3	-1.5		
<u>Calibration Curve</u>	<b>Slope</b>	<b>Intercept</b>	<b>Corr. Coeff.</b>	<b>Min. Area</b>	<b>Det. Lim.</b>
	1.9202	2.8914	0.9993	2	0.045

MeSH	1	2	3		
Time	08:30	08:53	09:08		
Concentration, ppm	8.28	4.21	1.95		
Area, mv-sec	47983	15409	3365		
Calc. Conc., ppm	8.11	4.37	1.91		
% Error	-2.0	3.8	-1.7		
<u>Calibration Curve</u>	<b>Slope</b>	<b>Intercept</b>	<b>Corr. Coeff.</b>	<b>Min. Area</b>	<b>Det. Lim.</b>
	1.8384	3.0096	0.9990	2	0.034

DMS	1	2	3		
Time	08:30	08:53	09:08		
Concentration, ppm	5.56	2.83	1.31		
Area, mv-sec	25544	6409	1338		
Calc. Conc., ppm	5.57	2.82	1.31		
% Error	0.1	-0.3	0.1		
<u>Calibration Curve</u>	<b>Slope</b>	<b>Intercept</b>	<b>Corr. Coeff.</b>	<b>Min. Area</b>	<b>Det. Lim.</b>
	2.0366	2.8888	>0.9999	2	0.054

DMDS	1	2	3		
Time	08:30	08:53	09:08		
Concentration, ppm	3.95	2.01	0.93		
Area, mv-sec	71728	19912	4471		
Calc. Conc., ppm	3.94	2.02	0.93		
% Error	-0.2	0.4	-0.2		
<u>Calibration Curve</u>	<b>Slope</b>	<b>Intercept</b>	<b>Corr. Coeff.</b>	<b>Min. Area</b>	<b>Det. Lim.</b>
	1.9169	3.7145	>0.9999	2	0.017

*MW*



# ANALYTES AND STANDARDS

Client: **New Indy**  
Location: **Catawba, SC**  
Source:

Project Number: **15730.001.006**  
Operator: **T. Simpkins**  
Date: **17 Mar 2021**

Method 16

Analyte	H <sub>2</sub> S	MeSH	DMS	DMDS
Molecular Weight	34.08	48.11	62.14	94.20
Retention Time, sec	19.0	32.5	70.0	125.0
Peak Detection Window, sec	3.0	5.0	10.0	10.0
Minimum Peak Area, mv-sec	2	2	2	2
Minimum Peak Height, mv	1	1	1	1
Beginning Peak Width, sec	1.0	1.0	2.0	3.0
Ending Peak Width, sec	2.0	3.0	4.0	5.0
Permeation Device ID	T-53950	33-56671	89-56661	89-56665
Permeation Rate, ng/min	600	913	792	852
Permeation Rate, nL/min*	422	455	306	217

**Barometric Pressure:** 30.20 in. Hg      **Ambient Temperature:** 72 °F  
No Oxygen Correction

\*Permeation rates are gravimetrically determined by the manufacturer with results by weight in ng/min. Permeation rates by volume, in nL/min, are calculated from the permeation rates by weight as follows:

$$PR_{nl} = PR_{ng} \times (V_{mol} / W_{mol}) \times [(460^\circ + T_a) / T_s] \times (P_s / P_b)$$

Where:

- $PR_{nl}$  = Permeation Rate by volume, nL/min
- $PR_{ng}$  = Permeation Rate by weight, ng/min
- $V_{mol}$  = Molar Volume of any gas @32 °F & 29.92 mm Hg = 22.4 L/mole
- $W_{mol}$  = Molecular Weight of compound
- $T_a$  = Ambient Temperature, °F
- $T_s$  = Standard Temperature = 492°R (32 °F)
- $P_s$  = Standard Pressure = 29.92 in Hg
- $P_b$  = Barometric Pressure, in Hg

For example, H<sub>2</sub>S:

$$PR_{nl} = 600 \times (22.4 / 34.08) \times [(460 + 72) / 492] \times (29.92 / 30.20) = 422 \text{ nL/min}$$

To calculate concentrations:

$$C = PR_{nl} / F_d$$

Where:

- $C$  = Concentration, ppmv
- $PR_{nl}$  = Permeation Rate by volume, nL/min
- $F_d$  = Flow rate of diluent, mL/min

# INSTRUMENT INFORMATION

Client: **New Indy**  
Location: **Catawba, SC**  
Source:

Project Number: **15730.001.006**  
Operator: **T. Simpkins**  
Date: **17 Mar 2021**

Method **16**

File: C:\Data\NIC\Trs Data 17 March 2021 A.trs  
Program Version: 2.0, built 15 May 2017 File Version: 2.0  
Computer: DESKTOP-A1IJDGT Trailer: 88

Analog Input Device: Keithley KUSB-3108 GC Channel: 16

Sampling Rate: 0.050 sec. Data Interval: 0.5 sec.

Gas Chromatograph: Shimadzu GC8A Serial No. GC 1  
Detector Range: 10

Gases			Temperatures, °C	Columns
	Press.	Flow		
	psi	mL/min	Column: 100	Primary: Carbo-pack
H <sub>2</sub>	30	50	Detector: 120	Secondary: N/A
Air	30	60		Sample Loop: 4"
Carrier	50	30		

## Injection Cycle

Total Length: 180 sec Sampling Time: 170 sec Load/Backflush Time: 80 sec

## Default Integration Parameters

Signal Threshold 0.67 mv Peak detection window ±10 sec  
Minimum peak area 2 mv-sec Minimum peak height 1 mv above baseline

## Dynacalibrator

Chamber Temperature 50.0°C  
Ambient Temperature 72.0°F  
Barometric Pressure 30.20 in. Hg



ATTACHMENT B

**18 MARCH 2021**

# RUN SUMMARY

Number 1

Client: **New Indy**  
Location: **Catawba, SC**  
Source:

Method **16**  
Calibration **1**

Project Number: **15730.001.006**  
Operator: **T. Simpkins**  
Date: **18 Mar 2021**

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**Start Time 10:21    End Time 14:28**

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**Average Measured TRS Conc.    0.03 ppm**  
**Recovery Missing**

# RUN DATA

Number 1

Client: **New Indy**  
Location: **Catawba, SC**  
Source:

Method **16**  
Calibration **1**

Project Number: **15730.001.006**  
Operator: **T. Simpkins**  
Date: **18 Mar 2021**

Time	H <sub>2</sub> S		MeSH		DMS		DMDS		TRS ppm	
	area	ppm	area	ppm	area	ppm	area	ppm		
<b>trailer south of old guard shack- by blue dumpsters</b>										
<b>wind from south to north</b>										
10:21	4	0.06	<2	<0.030	<2	<0.049	<2	<0.015	0.06	
10:24	<2	<0.041	<2	<0.030	<2	<0.049	5	0.02	0.05	
10:27	<2	<0.041	<2	<0.030	<2	<0.049	<2	<0.015	-	
10:30	3	0.05	<2	<0.030	<2	<0.049	2	0.02	0.08	
10:33	<2	<0.041	5	0.05	<2	<0.049	<2	<0.015	0.05	
10:36	<2	<0.041	<2	<0.030	<2	<0.049	<2	<0.015	-	
10:39	<2	<0.041	<2	<0.030	<2	<0.049	<2	<0.015	-	
10:42	2	0.04	<2	<0.030	<2	<0.049	<2	<0.015	0.04	
10:45	2	0.04	2	0.03	<2	<0.049	<2	<0.015	0.08	
10:48	<2	<0.041	<2	<0.030	<2	<0.049	4	0.02	0.04	
10:51	5	0.07	<2	<0.030	<2	<0.049	<2	<0.015	0.07	
10:54	<2	<0.041	<2	<0.030	<2	<0.049	2	0.02	0.03	
10:57	<2	<0.041	2	0.03	<2	<0.049	<2	<0.015	0.03	
11:00	12	0.11	<2	<0.030	<2	<0.049	<2	<0.015	0.11	
11:03	<2	<0.041	<2	<0.030	<2	<0.049	<2	<0.015	-	
11:06	<2	<0.041	<2	<0.030	<2	<0.049	<2	<0.015	-	
11:09	<2	<0.041	<2	<0.030	<2	<0.049	<2	<0.015	-	
11:12	<2	<0.041	<2	<0.030	<2	<0.049	<2	<0.015	-	
11:15	4	0.06	<2	<0.030	<2	<0.049	<2	<0.015	0.06	
11:18	2	0.04	<2	<0.030	<2	<0.049	<2	<0.015	0.04	
11:21	<2	<0.041	<2	<0.030	<2	<0.049	<2	<0.015	-	
11:24	<2	<0.041	<2	<0.030	3	0.06	<2	<0.015	0.06	
11:27	2	0.04	5	0.05	<2	<0.049	5	0.02	0.14	
11:30	<2	<0.041	<2	<0.030	<2	<0.049	<2	<0.015	-	
11:33	<2	<0.041	<2	<0.030	<2	<0.049	2	0.02	0.03	
11:36	<2	<0.041	<2	<0.030	<2	<0.049	<2	<0.015	-	
11:39	<2	<0.041	<2	<0.030	3	0.06	<2	<0.015	0.06	
11:42	2	0.04	<2	<0.030	<2	<0.049	<2	<0.015	0.04	
11:45	7	0.08	<2	<0.030	<2	<0.049	<2	<0.015	0.08	
11:48	<2	<0.041	<2	<0.030	<2	<0.049	<2	<0.015	-	
11:51	<2	<0.041	<2	<0.030	<2	<0.049	<2	<0.015	-	
11:54	<2	<0.041	<2	<0.030	<2	<0.049	<2	<0.015	-	
11:57	<2	<0.041	<2	<0.030	<2	<0.049	<2	<0.015	-	
12:00	2	0.04	<2	<0.030	<2	<0.049	<2	<0.015	0.04	
12:03	<2	<0.041	3	0.04	<2	<0.049	2	0.02	0.07	
12:06	<2	<0.041	3	0.04	<2	<0.049	<2	<0.015	0.04	
12:09	3	0.05	<2	<0.030	<2	<0.049	<2	<0.015	0.05	
12:12	<2	<0.041	<2	<0.030	<2	<0.049	<2	<0.015	-	

# RUN DATA

Number 1

Client: **New Indy**  
Location: **Catawba, SC**  
Source:

Method **16**  
Calibration **1**

Project Number: **15730.001.006**  
Operator: **T. Simpkins**  
Date: **18 Mar 2021**

Time	H <sub>2</sub> S		MeSH		DMS		DMDS		TRS ppm
	area	ppm	area	ppm	area	ppm	area	ppm	
12:15	<2	<0.041	<2	<0.030	<2	<0.049	<2	<0.015	-
12:18	<2	<0.041	<2	<0.030	<2	<0.049	<2	<0.015	-
12:21	<2	<0.041	<2	<0.030	<2	<0.049	<2	<0.015	-
12:24	<2	<0.041	<2	<0.030	<2	<0.049	<2	<0.015	-
12:27	<2	<0.041	<2	<0.030	2	0.05	2	0.02	0.08
12:30	<2	<0.041	<2	<0.030	<2	<0.049	<2	<0.015	-
12:33	3	0.05	<2	<0.030	<2	<0.049	<2	<0.015	0.05
12:37	<2	<0.041	<2	<0.030	<2	<0.049	3	0.02	0.04
12:40	<2	<0.041	<2	<0.030	<2	<0.049	<2	<0.015	-
12:43	<2	<0.041	<2	<0.030	<2	<0.049	<2	<0.015	-
12:46	<2	<0.041	<2	<0.030	<2	<0.049	<2	<0.015	-
12:49	<2	<0.041	<2	<0.030	<2	<0.049	<2	<0.015	-
12:52	<2	<0.041	<2	<0.030	5	0.08	<2	<0.015	0.08
12:55	<2	<0.041	<2	<0.030	<2	<0.049	<2	<0.015	-
				<b>moving trailer</b>					
12:58	<2	<0.041	3	0.03	<2	<0.049	<2	<0.015	0.03
13:01	3	0.05	<2	<0.030	<2	<0.049	<2	<0.015	0.05
13:04	<2	<0.041	<2	<0.030	<2	<0.049	<2	<0.015	-
13:07	3	0.05	<2	<0.030	<2	<0.049	<2	<0.015	0.05
13:10	<2	<0.041	<2	<0.030	<2	<0.049	<2	<0.015	-
13:13	<2	<0.041	<2	<0.030	<2	<0.049	<2	<0.015	-
13:16	<2	<0.041	<2	<0.030	<2	<0.049	<2	<0.015	-
13:19	<2	<0.041	<2	<0.030	<2	<0.049	<2	<0.015	-
				<b>lower contractor parking</b>					
13:22	<2	<0.041	<2	<0.030	25	0.17	<2	<0.015	0.17
13:25	<2	<0.041	5	0.05	<2	<0.049	<2	<0.015	0.05
13:28	<2	<0.041	<2	<0.030	<2	<0.049	<2	<0.015	-
				<b>upper contractor parking lot</b>					
13:31	<2	<0.041	<2	<0.030	<2	<0.049	<2	<0.015	-
13:34	<2	<0.041	<2	<0.030	<2	<0.049	<2	<0.015	-
13:37	4	0.06	<2	<0.030	<2	<0.049	<2	<0.015	0.06
13:40	<2	<0.041	4	0.04	<2	<0.049	<2	<0.015	0.04
13:43	<2	<0.041	<2	<0.030	<2	<0.049	<2	<0.015	-
13:46	2	0.04	<2	<0.030	<2	<0.049	<2	<0.015	0.04
13:49	<2	<0.041	<2	<0.030	<2	<0.049	<2	<0.015	-
13:52	<2	<0.041	<2	<0.030	<2	<0.049	<2	<0.015	-
13:55	<2	<0.041	<2	<0.030	<2	<0.049	<2	<0.015	-
13:58	<2	<0.041	<2	<0.030	<2	<0.049	<2	<0.015	-
14:01	3	0.05	<2	<0.030	<2	<0.049	<2	<0.015	0.05
14:04	<2	<0.041	<2	<0.030	<2	<0.049	<2	<0.015	-

# RUN DATA

Number 1

Client: **New Indy**  
Location: **Catawba, SC**  
Source:

Method **16**  
Calibration **1**

Project Number: **15730.001.006**  
Operator: **T. Simpkins**  
Date: **18 Mar 2021**

Time	H <sub>2</sub> S		MeSH		DMS		DMDS		TRS ppm
	area	ppm	area	ppm	area	ppm	area	ppm	
14:07	4	0.06	<2	<0.030	<2	<0.049	<2	<0.015	0.06
14:10	<2	<0.041	4	0.04	<2	<0.049	2	0.02	0.08
14:13	<2	<0.041	2	0.03	<2	<0.049	<2	<0.015	0.03
14:16	<2	<0.041	<2	<0.030	<2	<0.049	<2	<0.015	-
14:19	<2	<0.041	<2	<0.030	<2	<0.049	<2	<0.015	-
14:22	<2	<0.041	<2	<0.030	<2	<0.049	<2	<0.015	-
14:25	<2	<0.041	<2	<0.030	<2	<0.049	<2	<0.015	-
<b>Average</b>		<b>&lt;0.041</b>		<b>&lt;0.030</b>		<b>&lt;0.049</b>		<b>&lt;0.015</b>	-

# CALIBRATION DATA

Number 1

Client: **New Indy**  
Location: **Catawba, SC**  
Source:

Project Number: **15730.001.006**  
Operator: **T. Simpkins**  
Date: **18 Mar 2021**

Method 16

Ambient Temperature: 72°C

Barometric Pressure: 30.20 in. Hg

Analyte	H <sub>2</sub> S	MeSH	DMS	DMDS
Perm. Device ID	T-53950	33-56671	89-56661	89-56665
Perm. Rate, nL/min	422	455	306	217
Ret. Time, sec	19.0	32.5	70.0	125.0

1 Flow = 53.0 mL/Min      7.97 ppm      8.59 ppm      5.77 ppm      4.10 ppm

Time: 08:30

Peak Areas, mv-sec

37217	48066	25482	71756
38155	47820	25458	71884
37886	48063	25691	71544
<b>Average Area</b>	<b>37753</b> ✓	<b>47983</b> ✓	<b>25544</b> ✓
			<b>71728</b> ✓

2 Flow = 106 mL/Min      3.98 ppm      4.29 ppm      2.88 ppm      2.05 ppm

Time: 08:53

Peak Areas, mv-sec

11220	15593	6415	19990
11626	15400	6404	19931
11251	15235	6408	19816
<b>Average Area</b>	<b>11366</b> ✓	<b>15409</b> ✓	<b>6409</b> ✓
			<b>19912</b> ✓

3 Flow = 234 mL/Min      1.80 ppm      1.95 ppm      1.31 ppm      0.93 ppm

Time: 09:08

Peak Areas, mv-sec

2385	3436	1360	4560
2307	3358	1346	4470
2361	3302	1307	4384
<b>Average Area</b>	<b>2351</b> ✓	<b>3365</b> ✓	<b>1338</b> ✓
			<b>4471</b> ✓



# CALIBRATION SUMMARY

Number 1

Client: **New Indy**  
Location: **Catawba, SC**  
Source:

Project Number: **15730.001.006**  
Operator: **T. Simpkins**  
Date: **18 Mar 2021**

Method **16**

H <sub>2</sub> S	1	2	3		
Time	08:30	08:53	09:08		
Concentration, ppm	7.97	3.98	1.80		
Area, mv-sec	37753	11366	2351		
Calc. Conc., ppm	7.83	4.12	1.78		
% Error	-1.8	3.4	-1.6		
<u>Calibration Curve</u>	<b>Slope</b>	<b>Intercept</b>	<b>Corr. Coeff.</b>	<b>Min. Area</b>	<b>Det. Lim.</b>
	1.8723	2.9040	0.9992	2	0.041

MeSH	1	2	3		
Time	08:30	08:53	09:08		
Concentration, ppm	8.59	4.29	1.95		
Area, mv-sec	47983	15409	3365		
Calc. Conc., ppm	8.41	4.46	1.91		
% Error	-2.0	4.0	-1.8		
<u>Calibration Curve</u>	<b>Slope</b>	<b>Intercept</b>	<b>Corr. Coeff.</b>	<b>Min. Area</b>	<b>Det. Lim.</b>
	1.7925	3.0232	0.9990	2	0.030

DMS	1	2	3		
Time	08:30	08:53	09:08		
Concentration, ppm	5.77	2.88	1.31		
Area, mv-sec	25544	6409	1338		
Calc. Conc., ppm	5.77	2.88	1.31		
% Error	0.1	-0.2	0.1		
<u>Calibration Curve</u>	<b>Slope</b>	<b>Intercept</b>	<b>Corr. Coeff.</b>	<b>Min. Area</b>	<b>Det. Lim.</b>
	1.9859	2.8950	>0.9999	2	0.049

DMDS	1	2	3		
Time	08:30	08:53	09:08		
Concentration, ppm	4.10	2.05	0.93		
Area, mv-sec	71728	19912	4471		
Calc. Conc., ppm	4.09	2.06	0.93		
% Error	-0.3	0.5	-0.2		
<u>Calibration Curve</u>	<b>Slope</b>	<b>Intercept</b>	<b>Corr. Coeff.</b>	<b>Min. Area</b>	<b>Det. Lim.</b>
	1.8692	3.7132	>0.9999	2	0.015

*Handwritten mark*

## ANALYTES AND STANDARDS

Client: **New Indy**  
Location: **Catawba, SC**  
Source:

Method 16

Project Number: **15730.001.006**  
Operator: **T. Simpkins**  
Date: **18 Mar 2021**

Analyte	H <sub>2</sub> S	MeSH	DMS	DMDS
Molecular Weight	34.08	48.11	62.14	94.20
Retention Time, sec	19.0	32.5	70.0	125.0
Peak Detection Window, sec	3.0	5.0	10.0	10.0
Minimum Peak Area, mv-sec	2	2	2	2
Minimum Peak Height, mv	1	1	1	1
Beginning Peak Width, sec	1.0	1.0	2.0	3.0
Ending Peak Width, sec	2.0	3.0	4.0	5.0
Permeation Device ID	T-53950	33-56671	89-56661	89-56665
Permeation Rate, ng/min	600 ✓	913 ✓	792 ✓	852 ✓
Permeation Rate, nL/min*	422	455	306	217

**Barometric Pressure:** 30.20 in. Hg      **Ambient Temperature:** 72 °F  
No Oxygen Correction

\*Permeation rates are gravimetrically determined by the manufacturer with results by weight in ng/min. Permeation rates by volume, in nL/min, are calculated from the permeation rates by weight as follows:

$$PR_{nl} = PR_{ng} \times (V_{mol} / W_{mol}) \times [(460^\circ + T_a) / T_s] \times (P_s / P_b)$$

Where:

- $PR_{nl}$  = Permeation Rate by volume, nL/min
- $PR_{ng}$  = Permeation Rate by weight, ng/min
- $V_{mol}$  = Molar Volume of any gas @32 °F & 29.92 mm Hg = 22.4 L/mole
- $W_{mol}$  = Molecular Weight of compound
- $T_a$  = Ambient Temperature, °F
- $T_s$  = Standard Temperature = 492°R (32 °F)
- $P_s$  = Standard Pressure = 29.92 in Hg
- $P_b$  = Barometric Pressure, in Hg

For example, H<sub>2</sub>S:

$$PR_{nl} = 600 \times (22.4 / 34.08) \times [(460 + 72) / 492] \times (29.92 / 30.20) \\ = 422 \text{ nL/min}$$

To calculate concentrations:

$$C = PR_{nl} / F_d$$

Where:

- $C$  = Concentration, ppmv
- $PR_{nl}$  = Permeation Rate by volume, nL/min
- $F_d$  = Flow rate of diluent, mL/min

# INSTRUMENT INFORMATION

Client: **New Indy**  
Location: **Catawba, SC**  
Source:

Project Number: **15730.001.006**  
Operator: **T. Simpkins**  
Date: **18 Mar 2021**

Method **16**

File: C:\Data\NIC\Trs Data 18 March 2021 A.trs  
Program Version: 2.0, built 15 May 2017 File Version: 2.0  
Computer: DESKTOP-A1IJDGT Trailer: 88

Analog Input Device: Keithley KUSB-3108 GC Channel: 16

Sampling Rate: 0.050 sec. Data Interval: 0.5 sec.

Gas Chromatograph: Shimadzu GC8A Serial No. GC 1  
Detector Range: 10

Gases			Temperatures, °C	Columns
	Press. psi	Flow mL/min		
H <sub>2</sub>	30	50	Column: 100	Primary: Carbopack
Air	30	60	Detector: 120	Secondary: N/A
Carrier	50	30		Sample Loop: 4"

## Injection Cycle

Total Length: 180 sec Sampling Time: 170 sec Load/Backflush Time: 80 sec

## Default Integration Parameters

Signal Threshold 0.67 mv Peak detection window ±10 sec  
Minimum peak area 2 mv-sec Minimum peak height 1 mv above baseline

## Dynacalibrator

Chamber Temperature 50.0°C  
Ambient Temperature 72.0°F  
Barometric Pressure 30.20 in. Hg



**23-24 MARCH 2021**

# RUN SUMMARY

Number 1

Client: **New Indy**  
Location: **Catawba, SC**  
Source:

Method **16**  
Calibration **1**

Project Number: **15730.001.006**  
Operator: **T. Simpkins**  
Date: **23 Mar 2021**

---

**Start Time 09:06    End Time 08:10**

---

**Average Measured TRS Conc.    0.07 ppm**  
**Recovery Missing**

# RUN DATA

Number 1

Client: **New Indy**  
Location: **Catawba, SC**  
Source:

Method **16**  
Calibration **1**

Project Number: **15730.001.006**  
Operator: **T. Simpkins**  
Date: **23 Mar 2021**

Time	H <sub>2</sub> S		MeSH		DMS		DMDS		TRS ppm	
	area	ppm	area	ppm	area	ppm	area	ppm		
09:06	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-	
<b>East of RB Building in ally</b>										
09:06	3	0.07	<2	<0.053	<2	<0.053	<2	<0.019	0.07	
09:09	4	0.07	<2	<0.053	<2	<0.053	<2	<0.019	0.07	
09:12	3	0.06	<2	<0.053	<2	<0.053	<2	<0.019	0.06	
09:15	2	0.06	<2	<0.053	<2	<0.053	<2	<0.019	0.06	
09:18	3	0.07	<2	<0.053	<2	<0.053	<2	<0.019	0.07	
09:21	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-	
09:24	3	0.06	<2	<0.053	<2	<0.053	<2	<0.019	0.06	
09:27	2	0.06	<2	<0.053	<2	<0.053	<2	<0.019	0.06	
<b>west of CB's west of cb's</b>										
09:30	3	0.06	<2	<0.053	<2	<0.053	<2	<0.019	0.06	
09:33	3	0.06	<2	<0.053	<2	<0.053	<2	<0.019	0.06	
09:36	3	0.06	<2	<0.053	<2	<0.053	3	0.02	0.10	
09:39	2	0.06	<2	<0.053	<2	<0.053	2	0.02	0.10	
09:42	3	0.06	<2	<0.053	<2	<0.053	2	0.02	0.10	
09:46	3	0.06	<2	<0.053	<2	<0.053	<2	<0.019	0.06	
09:49	<2	<0.053	<2	<0.053	2	0.06	<2	<0.019	0.06	
09:52	2	0.06	<2	<0.053	<2	<0.053	<2	<0.019	0.06	
09:55	2	0.06	<2	<0.053	<2	<0.053	2	0.02	0.10	
09:58	2	0.06	<2	<0.053	<2	<0.053	3	0.02	0.10	
10:01	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-	
10:04	3	0.06	<2	<0.053	<2	<0.053	<2	<0.019	0.06	
10:07	6	0.09	<2	<0.053	<2	<0.053	<2	<0.019	0.09	
<b>sdtv bag sample taken from 950-1000</b>										
10:10	<2	<0.053	3	0.07	<2	<0.053	6	0.03	0.14	
10:13	<2	<0.053	6	0.10	<2	<0.053	9	0.04	0.18	
10:16	<2	<0.053	4	0.07	<2	<0.053	7	0.04	0.14	
<b>west side cb's- o citrate</b>										
10:19	2	0.06	<2	<0.053	<2	<0.053	<2	<0.019	0.06	
10:22	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-	
10:25	2	0.05	<2	<0.053	<2	<0.053	3	0.02	0.10	
10:28	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-	
10:31	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-	
10:34	7	0.10	<2	<0.053	<2	<0.053	<2	<0.019	0.10	
10:37	2	0.05	<2	<0.053	<2	<0.053	3	0.02	0.10	
10:40	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-	
10:43	5	0.09	<2	<0.053	<2	<0.053	<2	<0.019	0.09	
10:46	13	0.14	<2	<0.053	<2	<0.053	<2	<0.019	0.14	

# RUN DATA

Number 1

Client: **New Indy**  
Location: **Catawba, SC**  
Source:

Method **16**  
Calibration **1**

Project Number: **15730.001.006**  
Operator: **T. Simpkins**  
Date: **23 Mar 2021**

Time	H <sub>2</sub> S		MeSH		DMS		DMDS		TRS ppm
	area	ppm	area	ppm	area	ppm	area	ppm	
10:49	<2	<0.053	<2	<0.053	<2	<0.053	4	0.03	0.05
10:52	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
10:55	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
10:58	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
11:01	2	0.05	<2	<0.053	25	0.18	<2	<0.019	0.24
11:04	2	0.05	<2	<0.053	<2	<0.053	<2	<0.019	0.05
11:07	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
11:10	<2	<0.053	<2	<0.053	2	0.06	<2	<0.019	0.06
11:13	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
11:16	<2	<0.053	2	0.05	<2	<0.053	<2	<0.019	0.05
11:19	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
11:22	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
11:25	<2	<0.053	<2	<0.053	<2	<0.053	2	0.02	0.04
11:28	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
11:31	<2	<0.053	<2	<0.053	3	0.06	<2	<0.019	0.06
11:34	<2	<0.053	2	0.05	<2	<0.053	<2	<0.019	0.05
11:37	2	0.06	<2	<0.053	<2	<0.053	3	0.02	0.10
11:40	<2	<0.053	<2	<0.053	<2	<0.053	4	0.03	0.05
11:43	3	0.06	<2	<0.053	<2	<0.053	<2	<0.019	0.06
11:46	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
11:49	6	0.10	<2	<0.053	<2	<0.053	<2	<0.019	0.10
11:52	<2	<0.053	<2	<0.053	<2	<0.053	2	0.02	0.04
11:55	<2	<0.053	<2	<0.053	<2	<0.053	4	0.03	0.05
11:58	6	0.09	<2	<0.053	<2	<0.053	<2	<0.019	0.09
12:01	6	0.09	<2	<0.053	<2	<0.053	<2	<0.019	0.09
12:04	<2	<0.053	<2	<0.053	<2	<0.053	4	0.03	0.06
12:07	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
12:10	<2	<0.053	5	0.08	<2	<0.053	<2	<0.019	0.08
12:13	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
12:16	5	0.09	<2	<0.053	<2	<0.053	<2	<0.019	0.09
12:19	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
12:22	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
12:25	<2	<0.053	<2	<0.053	3	0.07	<2	<0.019	0.07
12:28	4	0.08	<2	<0.053	<2	<0.053	<2	<0.019	0.08
12:31	2	0.06	<2	<0.053	<2	<0.053	<2	<0.019	0.06
12:34	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
12:37	2	0.06	<2	<0.053	<2	<0.053	<2	<0.019	0.06
12:40	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
12:43	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
12:46	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-

# RUN DATA

Number 1

Client: **New Indy**  
Location: **Catawba, SC**  
Source:

Method **16**  
Calibration **1**

Project Number: **15730.001.006**  
Operator: **T. Simpkins**  
Date: **23 Mar 2021**

Time	H <sub>2</sub> S		MeSH		DMS		DMDS		TRS ppm	
	area	ppm	area	ppm	area	ppm	area	ppm		
12:49	<2	<0.053	<2	<0.053	<2	<0.053	3	0.02	0.05	
<b>1254 wind still blowing west</b>										
12:52	3	0.07	<2	<0.053	<2	<0.053	<2	<0.019	0.07	
12:55	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-	
12:58	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-	
13:01	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-	
13:04	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-	
13:07	<2	<0.053	<2	<0.053	<2	<0.053	3	0.02	0.05	
13:10	6	0.09	<2	<0.053	<2	<0.053	<2	<0.019	0.09	
13:13	2	0.06	<2	<0.053	<2	<0.053	<2	<0.019	0.06	
<b>moving trailer</b>										
13:16	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-	
13:19	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-	
13:22	8	0.11	<2	<0.053	<2	<0.053	<2	<0.019	0.11	
13:25	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-	
13:28	49	0.27	246	0.62	49	0.25	4	0.03	1.20	
13:31	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-	
13:34	2	0.06	<2	<0.053	<2	<0.053	<2	<0.019	0.06	
13:37	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-	
13:40	<2	<0.053	<2	<0.053	<2	<0.053	3	0.02	0.05	
13:43	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-	
<b>NW of No. 3 RB Stack across street</b>										
13:46	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-	
<b>wind blowing toward NW</b>										
13:49	3	0.07	<2	<0.053	<2	<0.053	2	0.02	0.11	
13:52	14	0.14	96	0.39	23	0.18	6	0.03	0.77	
13:55	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-	
13:58	4	0.08	<2	<0.053	<2	<0.053	<2	<0.019	0.08	
14:01	78	0.34	180	0.53	32	0.21	<2	<0.019	1.07	
14:04	<2	<0.053	3	0.07	<2	<0.053	<2	<0.019	0.07	
14:07	5	0.08	<2	<0.053	3	0.06	<2	<0.019	0.14	
14:10	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-	
14:13	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-	
14:16	62	0.30	6	0.09	6	0.09	<2	<0.019	0.48	
14:19	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-	
14:22	3	0.07	<2	<0.053	<2	<0.053	<2	<0.019	0.07	
14:25	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-	
14:28	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-	
14:31	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-	
14:34	3	0.06	<2	<0.053	<2	<0.053	<2	<0.019	0.06	



# RUN DATA

Number 1

Client: **New Indy**  
Location: **Catawba, SC**  
Source:

Method **16**  
Calibration **1**

Project Number: **15730.001.006**  
Operator: **T. Simpkins**  
Date: **23 Mar 2021**

Time	H <sub>2</sub> S		MeSH		DMS		DMDS		TRS ppm
	area	ppm	area	ppm	area	ppm	area	ppm	
14:37	844	1.13	235	0.61	52	0.26	<2	<0.019	2.00
14:40	<2	<0.053	223	0.59	51	0.26	5	0.03	0.91
14:43	<2	<0.053	407	0.81	118	0.39	6	0.03	1.26
14:46	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
14:49	107	0.40	69	0.33	4	0.08	<2	<0.019	0.80
14:52	3	0.07	<2	<0.053	<2	<0.053	<2	<0.019	0.07
14:55	3	0.06	<2	<0.053	<2	<0.053	<2	<0.019	0.06
14:58	394	0.77	419	0.82	76	0.32	6	0.03	1.97
15:01	<2	<0.053	8	0.11	3	0.07	2	0.02	0.21
15:04	6	0.10	2	0.06	4	0.07	<2	<0.019	0.23
15:07	166	0.50	56	0.29	5	0.08	<2	<0.019	0.87
15:10	22	0.18	8	0.11	4	0.08	<2	<0.019	0.36
15:13	5	0.08	<2	<0.053	<2	<0.053	<2	<0.019	0.08
15:16	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
15:19	4	0.07	<2	<0.053	<2	<0.053	<2	<0.019	0.07
15:22	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
15:25	<2	<0.053	<2	<0.053	<2	<0.053	4	0.02	0.05
15:28	121	0.42	83	0.36	6	0.09	<2	<0.019	0.87
15:31	<2	<0.053	2	0.05	<2	<0.053	<2	<0.019	0.05
15:34	<2	<0.053	3	0.06	4	0.07	<2	<0.019	0.14
15:37	15	0.15	4	0.08	2	0.06	<2	<0.019	0.28
15:40	3	0.07	<2	<0.053	<2	<0.053	5	0.03	0.13
15:43	<2	<0.053	<2	<0.053	2	0.06	<2	<0.019	0.06
15:47	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
15:50	<2	<0.053	2	0.06	<2	<0.053	<2	<0.019	0.06
15:53	2	0.06	<2	<0.053	<2	<0.053	<2	<0.019	0.06
15:56	<2	<0.053	2	0.05	<2	<0.053	<2	<0.019	0.05
15:59	4	0.07	<2	<0.053	<2	<0.053	<2	<0.019	0.07
16:02	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
16:05	2	0.05	<2	<0.053	<2	<0.053	<2	<0.019	0.05
16:08	<2	<0.053	4	0.08	<2	<0.053	<2	<0.019	0.08
16:11	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
16:14	278	0.64	162	0.50	32	0.20	<2	<0.019	1.35
16:17	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
16:20	3	0.07	<2	<0.053	<2	<0.053	<2	<0.019	0.07
16:23	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
<b>rail car area</b>									
<b>Wind Direction NW</b>									
16:26	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
16:29	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-

# RUN DATA

Number 1

Client: **New Indy**  
Location: **Catawba, SC**  
Source:

Method **16**  
Calibration **1**

Project Number: **15730.001.006**  
Operator: **T. Simpkins**  
Date: **23 Mar 2021**

Time	H <sub>2</sub> S		MeSH		DMS		DMDS		TRS ppm
	area	ppm	area	ppm	area	ppm	area	ppm	
16:32	4	0.07	<2	<0.053	<2	<0.053	<2	<0.019	0.07
16:35	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
16:38	<2	<0.053	<2	<0.053	5	0.08	<2	<0.019	0.08
16:41	3	0.07	<2	<0.053	<2	<0.053	<2	<0.019	0.07
16:44	3	0.06	<2	<0.053	<2	<0.053	<2	<0.019	0.06
16:47	3	0.06	<2	<0.053	<2	<0.053	4	0.03	0.11
16:50	3	0.06	<2	<0.053	<2	<0.053	3	0.02	0.11
16:53	<2	<0.053	<2	<0.053	<2	<0.053	3	0.02	0.04
16:56	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
16:59	<2	<0.053	3	0.07	<2	<0.053	<2	<0.019	0.07
17:02	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
17:05	7	0.10	<2	<0.053	<2	<0.053	<2	<0.019	0.10
17:08	3	0.07	<2	<0.053	<2	<0.053	<2	<0.019	0.07
17:11	4	0.07	<2	<0.053	<2	<0.053	<2	<0.019	0.07
17:14	7	0.10	<2	<0.053	<2	<0.053	<2	<0.019	0.10
17:17	2	0.06	<2	<0.053	<2	<0.053	<2	<0.019	0.06
17:20	3	0.06	<2	<0.053	<2	<0.053	<2	<0.019	0.06
17:23	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
17:26	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
17:29	<2	<0.053	<2	<0.053	36	0.22	<2	<0.019	0.22
17:32	3	0.06	<2	<0.053	<2	<0.053	5	0.03	0.12
17:35	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
17:38	3	0.07	<2	<0.053	<2	<0.053	<2	<0.019	0.07
17:41	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
17:44	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
17:47	<2	<0.053	<2	<0.053	12	0.13	<2	<0.019	0.13
17:50	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
17:53	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
17:56	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
17:59	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
18:02	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
18:05	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
18:08	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
18:11	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
18:14	3	0.07	<2	<0.053	<2	<0.053	<2	<0.019	0.07
18:17	<2	<0.053	<2	<0.053	3	0.07	<2	<0.019	0.07
18:20	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
18:23	2	0.05	<2	<0.053	<2	<0.053	3	0.02	0.10
18:26	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
18:29	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-

# RUN DATA

Number 1

Client: **New Indy**  
Location: **Catawba, SC**  
Source:

Method **16**  
Calibration **1**

Project Number: **15730.001.006**  
Operator: **T. Simpkins**  
Date: **23 Mar 2021**

Time	H <sub>2</sub> S		MeSH		DMS		DMDS		TRS ppm
	area	ppm	area	ppm	area	ppm	area	ppm	
18:32	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
18:35	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
18:38	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
18:41	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
18:44	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
18:47	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
18:50	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
18:53	<2	<0.053	4	0.07	<2	<0.053	<2	<0.019	0.07
18:56	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
18:59	<2	<0.053	<2	<0.053	<2	<0.053	5	0.03	0.06
19:02	<2	<0.053	<2	<0.053	<2	<0.053	3	0.02	0.05
19:05	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
19:08	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
19:11	3	0.07	5	0.08	<2	<0.053	3	0.02	0.19
19:14	3	0.06	<2	<0.053	<2	<0.053	<2	<0.019	0.06
19:17	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
19:20	<2	<0.053	<2	<0.053	3	0.06	4	0.03	0.12
19:23	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
19:26	<2	<0.053	<2	<0.053	<2	<0.053	4	0.03	0.05
19:29	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
19:32	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
19:35	<2	<0.053	<2	<0.053	4	0.07	<2	<0.019	0.07
19:38	<2	<0.053	9	0.11	<2	<0.053	<2	<0.019	0.11
19:41	5	0.08	<2	<0.053	<2	<0.053	<2	<0.019	0.08
19:44	5	0.08	<2	<0.053	<2	<0.053	<2	<0.019	0.08
19:47	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
19:50	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
19:53	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
19:56	5	0.08	<2	<0.053	<2	<0.053	<2	<0.019	0.08
19:59	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
20:02	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
20:05	4	0.07	<2	<0.053	<2	<0.053	5	0.03	0.13
20:08	3	0.07	<2	<0.053	<2	<0.053	3	0.02	0.11
20:11	2	0.06	<2	<0.053	<2	<0.053	<2	<0.019	0.06
20:14	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
20:17	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
20:20	<2	<0.053	<2	<0.053	4	0.07	<2	<0.019	0.07
20:23	3	0.06	<2	<0.053	<2	<0.053	<2	<0.019	0.06
20:26	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
20:29	4	0.07	<2	<0.053	<2	<0.053	<2	<0.019	0.07

# RUN DATA

Number 1

Client: **New Indy**  
Location: **Catawba, SC**  
Source:

Method **16**  
Calibration **1**

Project Number: **15730.001.006**  
Operator: **T. Simpkins**  
Date: **23 Mar 2021**

Time	H <sub>2</sub> S		MeSH		DMS		DMDS		TRS ppm
	area	ppm	area	ppm	area	ppm	area	ppm	
20:32	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
20:35	5	0.08	<2	<0.053	<2	<0.053	<2	<0.019	0.08
20:38	<2	<0.053	<2	<0.053	<2	<0.053	2	0.02	0.04
20:41	4	0.08	<2	<0.053	<2	<0.053	<2	<0.019	0.08
20:44	<2	<0.053	<2	<0.053	<2	<0.053	2	0.02	0.04
20:47	<2	<0.053	2	0.05	<2	<0.053	<2	<0.019	0.05
20:50	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
20:53	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
20:56	2	0.06	<2	<0.053	<2	<0.053	3	0.02	0.10
20:59	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
21:02	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
21:05	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
21:08	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
21:11	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
21:14	4	0.08	<2	<0.053	<2	<0.053	<2	<0.019	0.08
21:17	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
21:20	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
21:23	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
21:26	2	0.06	<2	<0.053	<2	<0.053	8	0.04	0.13
21:29	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
21:32	2	0.06	<2	<0.053	<2	<0.053	<2	<0.019	0.06
21:35	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
21:38	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
21:41	<2	<0.053	<2	<0.053	<2	<0.053	4	0.03	0.05
21:44	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
21:48	<2	<0.053	<2	<0.053	<2	<0.053	2	0.02	0.04
21:51	3	0.06	<2	<0.053	4	0.07	<2	<0.019	0.13
21:54	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
21:57	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
22:00	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
22:03	<2	<0.053	<2	<0.053	5	0.08	<2	<0.019	0.08
22:06	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
22:09	2	0.06	<2	<0.053	2	0.06	<2	<0.019	0.12
22:12	2	0.06	<2	<0.053	<2	<0.053	<2	<0.019	0.06
22:15	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
22:18	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
22:21	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
22:24	2	0.06	<2	<0.053	<2	<0.053	<2	<0.019	0.06
22:27	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
22:30	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-

# RUN DATA

Number 1

Client: **New Indy**  
Location: **Catawba, SC**  
Source:

Method **16**  
Calibration **1**

Project Number: **15730.001.006**  
Operator: **T. Simpkins**  
Date: **23 Mar 2021**

Time	H <sub>2</sub> S		MeSH		DMS		DMDS		TRS ppm
	area	ppm	area	ppm	area	ppm	area	ppm	
22:33	4	0.08	<2	<0.053	<2	<0.053	<2	<0.019	0.08
22:36	<2	<0.053	3	0.06	<2	<0.053	<2	<0.019	0.06
22:39	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
22:42	3	0.07	<2	<0.053	<2	<0.053	<2	<0.019	0.07
22:45	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
22:48	4	0.07	5	0.09	<2	<0.053	<2	<0.019	0.16
22:51	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
22:54	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
22:57	<2	<0.053	<2	<0.053	<2	<0.053	3	0.02	0.04
23:00	<2	<0.053	4	0.08	<2	<0.053	<2	<0.019	0.08
23:03	4	0.07	<2	<0.053	<2	<0.053	<2	<0.019	0.07
23:06	3	0.06	<2	<0.053	<2	<0.053	<2	<0.019	0.06
23:09	2	0.05	<2	<0.053	<2	<0.053	<2	<0.019	0.05
23:12	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
23:15	2	0.06	<2	<0.053	<2	<0.053	<2	<0.019	0.06
23:18	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
23:21	2	0.06	<2	<0.053	<2	<0.053	<2	<0.019	0.06
23:24	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
23:27	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
23:30	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
23:33	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
23:36	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
23:39	3	0.07	<2	<0.053	<2	<0.053	<2	<0.019	0.07
23:42	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
23:45	3	0.06	<2	<0.053	<2	<0.053	<2	<0.019	0.06
23:48	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
23:51	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
23:54	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
23:57	<2	<0.053	2	0.06	<2	<0.053	<2	<0.019	0.06
00:00	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
00:03	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
00:06	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
00:09	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
00:12	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
00:15	2	0.05	<2	<0.053	<2	<0.053	<2	<0.019	0.05
00:18	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
00:21	2	0.05	<2	<0.053	<2	<0.053	<2	<0.019	0.05
00:24	3	0.06	<2	<0.053	<2	<0.053	<2	<0.019	0.06
00:27	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
00:30	5	0.08	<2	<0.053	<2	<0.053	<2	<0.019	0.08

# RUN DATA

Number 1

Client: **New Indy**  
Location: **Catawba, SC**  
Source:

Method **16**  
Calibration **1**

Project Number: **15730.001.006**  
Operator: **T. Simpkins**  
Date: **23 Mar 2021**

Time	H <sub>2</sub> S		MeSH		DMS		DMDS		TRS ppm
	area	ppm	area	ppm	area	ppm	area	ppm	
00:33	<2	<0.053	<2	<0.053	<2	<0.053	3	0.02	0.05
00:36	4	0.08	<2	<0.053	<2	<0.053	<2	<0.019	0.08
00:39	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
00:42	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
00:45	4	0.07	<2	<0.053	<2	<0.053	<2	<0.019	0.07
00:48	<2	<0.053	4	0.08	<2	<0.053	<2	<0.019	0.08
00:51	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
00:54	2	0.06	<2	<0.053	<2	<0.053	<2	<0.019	0.06
00:57	3	0.06	<2	<0.053	<2	<0.053	<2	<0.019	0.06
01:00	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
01:03	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
01:06	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
01:09	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
01:12	<2	<0.053	4	0.07	<2	<0.053	<2	<0.019	0.07
01:15	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
01:18	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
01:21	<2	<0.053	<2	<0.053	<2	<0.053	4	0.03	0.05
01:24	2	0.06	<2	<0.053	4	0.08	<2	<0.019	0.13
01:27	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
01:30	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
01:33	<2	<0.053	<2	<0.053	<2	<0.053	5	0.03	0.06
01:36	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
01:39	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
01:42	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
01:45	2	0.05	<2	<0.053	<2	<0.053	<2	<0.019	0.05
01:48	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
01:51	2	0.06	<2	<0.053	<2	<0.053	<2	<0.019	0.06
01:54	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
01:57	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
02:00	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
02:03	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
02:06	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
02:09	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
02:12	3	0.07	<2	<0.053	<2	<0.053	<2	<0.019	0.07
02:15	8	0.10	<2	<0.053	<2	<0.053	<2	<0.019	0.10
02:18	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
02:21	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
02:24	<2	<0.053	<2	<0.053	<2	<0.053	2	0.02	0.04
02:27	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
02:30	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-

# RUN DATA

Number 1

Client: **New Indy**  
Location: **Catawba, SC**  
Source:

Method **16**  
Calibration **1**

Project Number: **15730.001.006**  
Operator: **T. Simpkins**  
Date: **23 Mar 2021**

Time	H <sub>2</sub> S		MeSH		DMS		DMDS		TRS ppm
	area	ppm	area	ppm	area	ppm	area	ppm	
02:33	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
02:36	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
02:39	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
02:42	4	0.08	<2	<0.053	<2	<0.053	<2	<0.019	0.08
02:45	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
02:48	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
02:51	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
02:54	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
02:57	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
03:00	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
03:03	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
03:06	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
03:09	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
03:12	3	0.07	<2	<0.053	<2	<0.053	2	0.02	0.11
03:15	11	0.12	<2	<0.053	<2	<0.053	<2	<0.019	0.12
03:18	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
03:21	2	0.06	<2	<0.053	<2	<0.053	<2	<0.019	0.06
03:24	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
03:27	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
03:30	6	0.10	<2	<0.053	<2	<0.053	<2	<0.019	0.10
03:33	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
03:36	2	0.06	<2	<0.053	<2	<0.053	<2	<0.019	0.06
03:39	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
03:42	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
03:45	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
03:49	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
03:52	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
03:55	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
03:58	<2	<0.053	2	0.05	<2	<0.053	3	0.02	0.10
04:01	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
04:04	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
04:07	4	0.07	<2	<0.053	<2	<0.053	<2	<0.019	0.07
04:10	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
04:13	3	0.06	<2	<0.053	<2	<0.053	<2	<0.019	0.06
04:16	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
04:19	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
04:22	<2	<0.053	<2	<0.053	3	0.06	<2	<0.019	0.06
04:25	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
04:28	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
04:31	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-

# RUN DATA

Number 1

Client: **New Indy**  
Location: **Catawba, SC**  
Source:

Method **16**  
Calibration **1**

Project Number: **15730.001.006**  
Operator: **T. Simpkins**  
Date: **23 Mar 2021**

Time	H <sub>2</sub> S		MeSH		DMS		DMDS		TRS ppm
	area	ppm	area	ppm	area	ppm	area	ppm	
04:34	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
04:37	<2	<0.053	3	0.07	<2	<0.053	<2	<0.019	0.07
04:40	4	0.08	<2	<0.053	<2	<0.053	3	0.02	0.12
04:43	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
04:46	2	0.05	<2	<0.053	<2	<0.053	<2	<0.019	0.05
04:49	2	0.05	<2	<0.053	<2	<0.053	<2	<0.019	0.05
04:52	<2	<0.053	<2	<0.053	<2	<0.053	3	0.02	0.04
04:55	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
04:58	7	0.10	<2	<0.053	<2	<0.053	<2	<0.019	0.10
05:01	4	0.07	<2	<0.053	<2	<0.053	<2	<0.019	0.07
05:04	2	0.05	<2	<0.053	<2	<0.053	<2	<0.019	0.05
05:07	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
05:10	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
05:13	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
05:16	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
05:19	3	0.07	<2	<0.053	<2	<0.053	<2	<0.019	0.07
05:22	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
05:25	3	0.07	<2	<0.053	<2	<0.053	<2	<0.019	0.07
05:28	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
05:31	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
05:34	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
05:37	5	0.08	<2	<0.053	<2	<0.053	<2	<0.019	0.08
05:40	7	0.10	<2	<0.053	<2	<0.053	<2	<0.019	0.10
05:43	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
05:46	<2	<0.053	<2	<0.053	<2	<0.053	6	0.03	0.06
05:49	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
05:52	2	0.06	<2	<0.053	<2	<0.053	<2	<0.019	0.06
05:55	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
05:58	<2	<0.053	<2	<0.053	<2	<0.053	5	0.03	0.06
06:01	2	0.06	<2	<0.053	<2	<0.053	<2	<0.019	0.06
06:04	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
06:07	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
06:10	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
06:13	3	0.06	<2	<0.053	<2	<0.053	<2	<0.019	0.06
06:16	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
06:19	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
06:22	2	0.06	<2	<0.053	<2	<0.053	<2	<0.019	0.06
06:25	<2	<0.053	<2	<0.053	22	0.17	<2	<0.019	0.17
06:28	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-
06:31	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-



# RUN DATA

Number 1

Client: **New Indy**  
Location: **Catawba, SC**  
Source:

Method **16**  
Calibration **1**

Project Number: **15730.001.006**  
Operator: **T. Simpkins**  
Date: **23 Mar 2021**

Time	H <sub>2</sub> S		MeSH		DMS		DMDS		TRS ppm	
	area	ppm	area	ppm	area	ppm	area	ppm		
06:34	2	0.06	<2	<0.053	<2	<0.053	<2	<0.019	0.06	
06:37	2	0.06	<2	<0.053	<2	<0.053	2	0.02	0.10	
06:40	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-	
06:43	3	0.07	<2	<0.053	4	0.07	<2	<0.019	0.14	
06:46	<2	<0.053	<2	<0.053	<2	<0.053	4	0.03	0.05	
06:49	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-	
06:52	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-	
06:55	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-	
06:58	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-	
07:01	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-	
07:04	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-	
07:07	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-	
07:10	4	0.07	<2	<0.053	<2	<0.053	<2	<0.019	0.07	
07:13	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-	
07:16	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-	
07:19	4	0.07	<2	<0.053	<2	<0.053	<2	<0.019	0.07	
07:22	<2	<0.053	<2	<0.053	34	0.21	<2	<0.019	0.21	
07:25	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-	
07:28	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-	
07:31	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-	
07:34	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-	
07:37	3	0.07	<2	<0.053	<2	<0.053	<2	<0.019	0.07	
07:40	6	0.09	<2	<0.053	<2	<0.053	<2	<0.019	0.09	
07:43	<2	<0.053	<2	<0.053	<2	<0.053	2	0.02	0.04	
07:46	3	0.07	<2	<0.053	<2	<0.053	<2	<0.019	0.07	
07:49	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-	
07:52	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-	
			<b>wind blowing SW</b>							
07:55	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-	
07:58	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-	
08:01	<2	<0.053	<2	<0.053	2	0.06	<2	<0.019	0.06	
08:04	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-	
08:07	<2	<0.053	<2	<0.053	<2	<0.053	<2	<0.019	-	
<b>Average</b>		<b>&lt;0.053</b>		<b>&lt;0.053</b>		<b>&lt;0.053</b>		<b>&lt;0.019</b>	<b>-</b>	

# CALIBRATION DATA

Number 1

Client: **New Indy**  
Location: **Catawba, SC**  
Source:

Project Number: **15730.001.006**  
Operator: **T. Simpkins**  
Date: **22 Mar 2021**

Method 16

**Ambient Temperature: 72°C**

**Barometric Pressure: 30.12 in. Hg**

Analyte	H <sub>2</sub> S	MeSH	DMS	DMDS
Perm. Device ID	T-53950	33-56671	89-56661	89-56665
Perm. Rate, nL/min	423	456	307	218
Ret. Time, sec	19.0	32.5	70.0	125.0

**1 Flow = 55.0 mL/Min      7.70 ppm      8.30 ppm      5.57 ppm      3.96 ppm**

**Time: 07:30**

**Peak Areas, mv-sec**

36921	39362	26024	72542
36710	38779	26172	73474
36242	38902	26190	73390
<b>Average Area</b>	<b>36624 ✓</b>	<b>39014 ✓</b>	<b>26129 ✓</b>

**2 Flow = 104 mL/Min      4.06 ppm      4.37 ppm      2.94 ppm      2.09 ppm**

**Time: 08:01**

**Peak Areas, mv-sec**

11400	11116	6663	22616
11123	11403	6907	21518
11213	11305	6812	21056
<b>Average Area</b>	<b>11245 ✓</b>	<b>11275 ✓</b>	<b>6794 ✓</b>

**3 Flow = 291 mL/Min      1.46 ppm      1.57 ppm      1.05 ppm      0.75 ppm**

**Time: 08:12**

**Peak Areas, mv-sec**

1408	1530	914	2577
1343	1487	875	2882
1360	1474	866	2897
<b>Average Area</b>	<b>1370 ✓</b>	<b>1497 ✓</b>	<b>885 ✓</b>

# CALIBRATION SUMMARY

Number 1

Client: **New Indy**  
Location: **Catawba, SC**  
Source:

Project Number: **15730.001.006**  
Operator: **T. Simpkins**  
Date: **22 Mar 2021**

Method 16

H <sub>2</sub> S	1	2	3		
Time	07:30	08:01	08:12		
Concentration, ppm	7.70	4.06	1.46		
Area, mv-sec	36624	11245	1370		
Calc. Conc., ppm	7.57	4.17	1.44		
% Error	-1.7	2.8	-1.0		
<u>Calibration Curve</u>	<b>Slope</b>	<b>Intercept</b>	<b>Corr. Coeff.</b>	<b>Min. Area</b>	<b>Det. Lim.</b>
	1.9802	2.8229	0.9996	2	0.053

MeSH	1	2	3		
Time	07:30	08:01	08:12		
Concentration, ppm	8.30	4.37	1.57		
Area, mv-sec	39014	11275	1497		
Calc. Conc., ppm	8.28	4.39	1.57		
% Error	-0.2	0.4	-0.2		
<u>Calibration Curve</u>	<b>Slope</b>	<b>Intercept</b>	<b>Corr. Coeff.</b>	<b>Min. Area</b>	<b>Det. Lim.</b>
	1.9584	2.7936	>0.9999	2	0.053

DMS	1	2	3		
Time	07:30	08:01	08:12		
Concentration, ppm	5.57	2.94	1.05		
Area, mv-sec	26129	6794	885		
Calc. Conc., ppm	5.62	2.89	1.06		
% Error	0.9	-1.5	0.6		
<u>Calibration Curve</u>	<b>Slope</b>	<b>Intercept</b>	<b>Corr. Coeff.</b>	<b>Min. Area</b>	<b>Det. Lim.</b>
	2.0280	2.8960	0.9999	2	0.053

DMDS	1	2	3		
Time	07:30	08:01	08:12		
Concentration, ppm	3.96	2.09	0.75		
Area, mv-sec	73135	21730	2785		
Calc. Conc., ppm	3.92	2.12	0.74		
% Error	-0.9	1.4	-0.5		
<u>Calibration Curve</u>	<b>Slope</b>	<b>Intercept</b>	<b>Corr. Coeff.</b>	<b>Min. Area</b>	<b>Det. Lim.</b>
	1.9658	3.6972	0.9999	2	0.019

*AW*

# ANALYTES AND STANDARDS

Client: **New Indy**  
Location: **Catawba, SC**  
Source:

Method **16**

Project Number: **15730.001.006**  
Operator: **T. Simpkins**  
Date: **22 Mar 2021**

Analyte	H <sub>2</sub> S	MeSH	DMS	DMDS
<b>Molecular Weight</b>	34.08	48.11	62.14	94.20
<b>Retention Time, sec</b>	19.0	32.5	70.0	125.0
<b>Peak Detection Window, sec</b>	3.0	5.0	10.0	10.0
<b>Minimum Peak Area, mv-sec</b>	2	2	2	2
<b>Minimum Peak Height, mv</b>	1	1	1	1
<b>Beginning Peak Width, sec</b>	1.0	1.0	2.0	3.0
<b>Ending Peak Width, sec</b>	2.0	3.0	4.0	5.0
<b>Permeation Device ID</b>	T-53950	33-56671	89-56661	89-56665
<b>Permeation Rate, ng/min</b>	600 ✓	913 ✓	792 ✓	852 ✓
<b>Permeation Rate, nL/min*</b>	423	456	307	218

**Barometric Pressure:** 30.12 in. Hg     **Ambient Temperature:** 72 °F  
No Oxygen Correction

\*Permeation rates are gravimetrically determined by the manufacturer with results by weight in ng/min. Permeation rates by volume, in nL/min, are calculated from the permeation rates by weight as follows:

$$PR_{nl} = PR_{ng} \times (V_{mol} / W_{mol}) \times [(460^\circ + T_a) / T_s] \times (P_s / P_b)$$

Where:

- PR<sub>nl</sub>** = Permeation Rate by volume, nL/min
- PR<sub>ng</sub>** = Permeation Rate by weight, ng/min
- V<sub>mol</sub>** = Molar Volume of any gas @32 °F & 29.92 mm Hg = 22.4 L/mole
- W<sub>mol</sub>** = Molecular Weight of compound
- T<sub>a</sub>** = Ambient Temperature, °F
- T<sub>s</sub>** = Standard Temperature = 492°R (32 °F)
- P<sub>s</sub>** = Standard Pressure = 29.92 in Hg
- P<sub>b</sub>** = Barometric Pressure, in Hg

For example, H<sub>2</sub>S:

$$PR_{nl} = 600 \times (22.4 / 34.08) \times [(460 + 72) / 492] \times (29.92 / 30.12) = 423 \text{ nL/min}$$

To calculate concentrations:

$$C = PR_{nl} / F_d$$

Where:

- C** = Concentration, ppmv
- PR<sub>nl</sub>** = Permeation Rate by volume, nL/min
- F<sub>d</sub>** = Flow rate of diluent, mL/min

# INSTRUMENT INFORMATION

Client: **New Indy**  
Location: **Catawba, SC**  
Source:

Method **16**

Project Number: **15730.001.006**  
Operator: **T. Simpkins**  
Date: **22 Mar 2021**

File: C:\Data\NIC\Trs Data 23 March 2021.trs  
Program Version: 2.0, built 15 May 2017 File Version: 2.0  
Computer: DESKTOP-A1IJDGT Trailer: 88

Analog Input Device: Keithley KUSB-3108 GC Channel: 16

Sampling Rate: 0.050 sec. Data Interval: 0.5 sec.

Gas Chromatograph: Shimadzu GC8A Serial No. GC 1  
Detector Range: 10

Gases			Temperatures, °C	Columns
	Press. psi	Flow mL/min	Column: 100 Detector: 120	Primary: Carbopack Secondary: N/A Sample Loop: 4"
H <sub>2</sub>	30	50		
Air	30	60		
Carrier	50	30		

## Injection Cycle

Total Length: 180 sec Sampling Time: 170 sec Load/Backflush Time: 80 sec

## Default Integration Parameters

Signal Threshold 0.67 mv Peak detection window ±10 sec  
Minimum peak area 2 mv-sec Minimum peak height 1 mv above baseline

## Dynacalibrator

Chamber Temperature 50.0°C  
Ambient Temperature 72.0°F  
Barometric Pressure 30.12 in. Hg



ATTACHMENT B

**24 MARCH 2021**

# RUN SUMMARY

Number 1

Client: **New Indy**  
Location: **Catawba, SC**  
Source:

Method **16**  
Calibration **1**

Project Number: **15730.001.006**  
Operator: **T. Simpkins**  
Date: **24 Mar 2021**

---

**Start Time 09:31    End Time 10:14**

---

**Average Measured TRS Conc.    0.10 ppm**  
**Recovery Missing**

# RUN SUMMARY

Number 2

Client: **New Indy**  
Location: **Catawba, SC**  
Source:

Method **16**  
Calibration **1**

Project Number: **15730.001.006**  
Operator: **T. Simpkins**  
Date: **24 Mar 2021**

---

**Start Time 10:17    End Time 10:29**

---

**Average Measured TRS Conc.    0.00 ppm**  
**Recovery Missing**



# RUN SUMMARY

Number 3

Client: **New Indy**  
Location: **Catawba, SC**  
Source:

Method **16**  
Calibration **1**

Project Number: **15730.001.006**  
Operator: **T. Simpkins**  
Date: **24 Mar 2021**

---

**Start Time 10:31    End Time 10:43**

---

**Average Measured TRS Conc.    0.00 ppm**  
**Recovery Missing**

# RUN SUMMARY

Number 4

Client: **New Indy**  
Location: **Catawba, SC**  
Source:

Method **16**  
Calibration **1**

Project Number: **15730.001.006**  
Operator: **T. Simpkins**  
Date: **24 Mar 2021**

---

**Start Time** 10:58    **End Time** 15:40

---

**Average Measured TRS Conc.**    0.03 ppm  
**Recovery Missing**

# RUN DATA

Number 1

Client: **New Indy**  
Location: **Catawba, SC**  
Source:

Method **16**  
Calibration **1**

Project Number: **15730.001.006**  
Operator: **T. Simpkins**  
Date: **24 Mar 2021**

Time	H <sub>2</sub> S		MeSH		DMS		DMDS		TRS
	area	ppm	area	ppm	area	ppm	area	ppm	ppm
09:31	<2	<0.044	579	0.81	<2	<0.052	8	0.04	0.88
09:34	<2	<0.044	67	0.25	<2	<0.052	3	0.02	0.29
09:37	<2	<0.044	<2	<0.038	<2	<0.052	<2	<0.017	-
09:40	<2	<0.044	<2	<0.038	<2	<0.052	<2	<0.017	-
09:43	<2	<0.044	<2	<0.038	<2	<0.052	<2	<0.017	-
09:46	<2	<0.044	<2	<0.038	<2	<0.052	<2	<0.017	-
09:49	<2	<0.044	<2	<0.038	<2	<0.052	2	0.02	0.04
09:52	<2	<0.044	<2	<0.038	<2	<0.052	<2	<0.017	-
09:55	<2	<0.044	<2	<0.038	<2	<0.052	<2	<0.017	-
09:58	<2	<0.044	<2	<0.038	<2	<0.052	6	0.03	0.06
10:01	<2	<0.044	<2	<0.038	<2	<0.052	5	0.03	0.06
10:05	<2	<0.044	<2	<0.038	<2	<0.052	<2	<0.017	-
10:08	3	0.05	<2	<0.038	2	0.06	<2	<0.017	0.11
10:11	<2	<0.044	<2	<0.038	<2	<0.052	<2	<0.017	-
<b>Average</b>		<b>&lt;0.044</b>		<b>0.08</b>		<b>&lt;0.052</b>		<b>&lt;0.017</b>	<b>0.10</b>

# RUN DATA

Number 2

Client: **New Indy**  
Location: **Catawba, SC**  
Source:

Method **16**  
Calibration **1**

Project Number: **15730.001.006**  
Operator: **T. Simpkins**  
Date: **24 Mar 2021**

Time	H <sub>2</sub> S		MeSH		DMS		DMDS		TRS
	area	ppm	area	ppm	area	ppm	area	ppm	
<b>PM Roof Vent - Edge 935-940</b>									
10:17	<2	<0.044	<2	<0.038	<2	<0.052	<2	<0.017	-
10:20	<2	<0.044	<2	<0.038	<2	<0.052	<2	<0.017	-
10:23	<2	<0.044	<2	<0.038	<2	<0.052	<2	<0.017	-
10:26	<2	<0.044	<2	<0.038	<2	<0.052	<2	<0.017	-
<b>Average</b>		<b>&lt;0.044</b>		<b>&lt;0.038</b>		<b>&lt;0.052</b>		<b>&lt;0.017</b>	<b>-</b>

# RUN DATA

Number 3

Client: **New Indy**  
 Location: **Catawba, SC**  
 Source:

Method **16**  
 Calibration **1**

Project Number: **15730.001.006**  
 Operator: **T. Simpkins**  
 Date: **24 Mar 2021**

Time	H <sub>2</sub> S		MeSH		DMS		DMDS		TRS ppm
	area	ppm	area	ppm	area	ppm	area	ppm	
<b>PM Roof Vent 2- 955-1000</b>									
10:31	<2	<0.044	<2	<0.038	<2	<0.052	<2	<0.017	-
10:34	<2	<0.044	<2	<0.038	<2	<0.052	<2	<0.017	-
10:37	<2	<0.044	<2	<0.038	<2	<0.052	<2	<0.017	-
10:40	<2	<0.044	<2	<0.038	<2	<0.052	<2	<0.017	-
<b>Average</b>		<b>&lt;0.044</b>		<b>&lt;0.038</b>		<b>&lt;0.052</b>		<b>&lt;0.017</b>	<b>-</b>

# RUN DATA

Number 4

Client: **New Indy**  
Location: **Catawba, SC**  
Source:

Method **16**  
Calibration **1**

Project Number: **15730.001.006**  
Operator: **T. Simpkins**  
Date: **24 Mar 2021**

Time	H <sub>2</sub> S		MeSH		DMS		DMDS		TRS ppm	
	area	ppm	area	ppm	area	ppm	area	ppm		
<b>Moving trailer to NW side of mill</b>										
10:58	<2	<0.044	<2	<0.038	<2	<0.052	<2	<0.017	-	
<b>sdtv bag 2- 1045-1050</b>										
11:01	<2	<0.044	<2	<0.038	<2	<0.052	<2	<0.017	-	
11:04	<2	<0.044	<2	<0.038	<2	<0.052	<2	<0.017	-	
<b>sdtv bag done</b>										
11:07	<2	<0.044	<2	<0.038	<2	<0.052	<2	<0.017	-	
11:10	<2	<0.044	<2	<0.038	<2	<0.052	<2	<0.017	-	
11:13	<2	<0.044	<2	<0.038	<2	<0.052	<2	<0.017	-	
11:16	<2	<0.044	<2	<0.038	<2	<0.052	<2	<0.017	-	
<b>NW side of ill near old guard shack stack plumes going straight up right now</b>										
11:19	<2	<0.044	<2	<0.038	<2	<0.052	<2	<0.017	-	
11:22	<2	<0.044	3	0.05	<2	<0.052	<2	<0.017	0.05	
11:25	<2	<0.044	<2	<0.038	<2	<0.052	<2	<0.017	-	
11:28	<2	<0.044	<2	<0.038	<2	<0.052	<2	<0.017	-	
11:31	2	0.05	<2	<0.038	<2	<0.052	<2	<0.017	0.05	
11:34	<2	<0.044	<2	<0.038	<2	<0.052	<2	<0.017	-	
11:37	<2	<0.044	<2	<0.038	<2	<0.052	<2	<0.017	-	
11:40	<2	<0.044	<2	<0.038	<2	<0.052	<2	<0.017	-	
11:43	<2	<0.044	<2	<0.038	<2	<0.052	<2	<0.017	-	
11:46	<2	<0.044	<2	<0.038	<2	<0.052	<2	<0.017	-	
11:49	<2	<0.044	9	0.09	<2	<0.052	2	0.02	0.12	
11:52	<2	<0.044	<2	<0.038	<2	<0.052	<2	<0.017	-	
11:55	<2	<0.044	<2	<0.038	<2	<0.052	<2	<0.017	-	
11:58	<2	<0.044	<2	<0.038	<2	<0.052	<2	<0.017	-	
12:01	<2	<0.044	<2	<0.038	<2	<0.052	3	0.02	0.04	
12:04	<2	<0.044	<2	<0.038	<2	<0.052	<2	<0.017	-	
12:07	<2	<0.044	<2	<0.038	<2	<0.052	<2	<0.017	-	
12:10	<2	<0.044	<2	<0.038	<2	<0.052	<2	<0.017	-	
12:13	<2	<0.044	<2	<0.038	<2	<0.052	<2	<0.017	-	
12:16	3	0.06	<2	<0.038	<2	<0.052	<2	<0.017	0.06	
12:19	<2	<0.044	<2	<0.038	<2	<0.052	2	0.02	0.04	
12:22	2	0.05	<2	<0.038	<2	<0.052	<2	<0.017	0.05	
12:25	<2	<0.044	<2	<0.038	8	0.10	<2	<0.017	0.10	
12:28	3	0.06	<2	<0.038	6	0.09	<2	<0.017	0.15	
12:31	2	0.05	<2	<0.038	<2	<0.052	<2	<0.017	0.05	
12:34	<2	<0.044	<2	<0.038	<2	<0.052	2	0.02	0.04	
12:37	<2	<0.044	<2	<0.038	<2	<0.052	<2	<0.017	-	
12:40	<2	<0.044	<2	<0.038	<2	<0.052	<2	<0.017	-	

# RUN DATA

Number 4

Client: **New Indy**  
Location: **Catawba, SC**  
Source:

Method **16**  
Calibration **1**

Project Number: **15730.001.006**  
Operator: **T. Simpkins**  
Date: **24 Mar 2021**

Time	H <sub>2</sub> S		MeSH		DMS		DMDS		TRS ppm
	area	ppm	area	ppm	area	ppm	area	ppm	
12:43	<2	<0.044	<2	<0.038	<2	<0.052	<2	<0.017	-
12:46	<2	<0.044	<2	<0.038	<2	<0.052	<2	<0.017	-
12:49	<2	<0.044	<2	<0.038	<2	<0.052	<2	<0.017	-
<b>in main courtyard of mill next to Wood tent</b>									
<b>NE</b>									
<b>wins going toward</b>									
12:52	<2	<0.044	<2	<0.038	<2	<0.052	<2	<0.017	-
12:55	4	0.06	<2	<0.038	<2	<0.052	3	0.02	0.10
12:58	<2	<0.044	<2	<0.038	<2	<0.052	<2	<0.017	-
13:01	2	0.05	<2	<0.038	<2	<0.052	<2	<0.017	0.05
13:04	<2	<0.044	<2	<0.038	2	0.05	<2	<0.017	0.05
13:07	<2	<0.044	<2	<0.038	5	0.08	<2	<0.017	0.08
13:10	<2	<0.044	<2	<0.038	<2	<0.052	<2	<0.017	-
13:13	4	0.06	<2	<0.038	<2	<0.052	7	0.03	0.12
13:16	<2	<0.044	<2	<0.038	<2	<0.052	<2	<0.017	-
13:19	3	0.05	<2	<0.038	<2	<0.052	<2	<0.017	0.05
13:22	<2	<0.044	<2	<0.038	<2	<0.052	<2	<0.017	-
13:25	<2	<0.044	<2	<0.038	<2	<0.052	<2	<0.017	-
13:28	2	0.05	<2	<0.038	<2	<0.052	<2	<0.017	0.05
13:31	5	0.07	<2	<0.038	27	0.19	<2	<0.017	0.26
13:34	<2	<0.044	<2	<0.038	<2	<0.052	<2	<0.017	-
13:37	<2	<0.044	<2	<0.038	<2	<0.052	4	0.02	0.05
13:40	<2	<0.044	<2	<0.038	<2	<0.052	<2	<0.017	-
13:43	4	0.06	<2	<0.038	<2	<0.052	<2	<0.017	0.06
13:46	7	0.09	<2	<0.038	25	0.19	4	0.02	0.32
13:49	<2	<0.044	<2	<0.038	3	0.06	<2	<0.017	0.06
13:52	<2	<0.044	<2	<0.038	<2	<0.052	<2	<0.017	-
13:55	<2	<0.044	<2	<0.038	<2	<0.052	<2	<0.017	-
13:58	<2	<0.044	<2	<0.038	<2	<0.052	3	0.02	0.04
14:01	2	0.05	<2	<0.038	<2	<0.052	<2	<0.017	0.05
14:04	<2	<0.044	<2	<0.038	<2	<0.052	<2	<0.017	-
14:07	13	0.12	<2	<0.038	<2	<0.052	<2	<0.017	0.12
14:10	<2	<0.044	<2	<0.038	<2	<0.052	<2	<0.017	-
14:13	5	0.07	<2	<0.038	<2	<0.052	<2	<0.017	0.07
14:16	8	0.09	<2	<0.038	<2	<0.052	<2	<0.017	0.09
14:19	<2	<0.044	<2	<0.038	<2	<0.052	<2	<0.017	-
14:22	3	0.05	<2	<0.038	<2	<0.052	<2	<0.017	0.05
14:25	<2	<0.044	<2	<0.038	<2	<0.052	<2	<0.017	-
14:28	<2	<0.044	<2	<0.038	<2	<0.052	<2	<0.017	-
14:31	<2	<0.044	<2	<0.038	<2	<0.052	<2	<0.017	-

# RUN DATA

Number 4

Client: **New Indy**  
Location: **Catawba, SC**  
Source:

Method **16**  
Calibration **1**

Project Number: **15730.001.006**  
Operator: **T. Simpkins**  
Date: **24 Mar 2021**

Time	H <sub>2</sub> S		MeSH		DMS		DMDS		TRS ppm
	area	ppm	area	ppm	area	ppm	area	ppm	
14:34	<2	<0.044	<2	<0.038	<2	<0.052	<2	<0.017	-
14:37	<2	<0.044	<2	<0.038	<2	<0.052	<2	<0.017	-
14:40	<2	<0.044	<2	<0.038	<2	<0.052	<2	<0.017	-
14:43	3	0.05	<2	<0.038	<2	<0.052	<2	<0.017	0.05
14:46	2	0.04	<2	<0.038	<2	<0.052	2	0.02	0.08
14:49	<2	<0.044	<2	<0.038	<2	<0.052	<2	<0.017	-
14:52	<2	<0.044	<2	<0.038	<2	<0.052	4	0.02	0.05
14:55	<2	<0.044	<2	<0.038	<2	<0.052	2	0.02	0.04
14:58	<2	<0.044	<2	<0.038	<2	<0.052	<2	<0.017	-
15:01	3	0.05	<2	<0.038	<2	<0.052	2	0.02	0.09
15:04	<2	<0.044	<2	<0.038	<2	<0.052	<2	<0.017	-
15:07	<2	<0.044	<2	<0.038	<2	<0.052	<2	<0.017	-
15:10	4	0.06	<2	<0.038	<2	<0.052	<2	<0.017	0.06
<b>wind blowing toward NE</b>									
15:13	4	0.06	<2	<0.038	<2	<0.052	<2	<0.017	0.06
15:16	<2	<0.044	<2	<0.038	<2	<0.052	3	0.02	0.05
15:19	<2	<0.044	<2	<0.038	30	0.20	<2	<0.017	0.20
15:22	<2	<0.044	<2	<0.038	<2	<0.052	<2	<0.017	-
15:25	<2	<0.044	<2	<0.038	<2	<0.052	<2	<0.017	-
15:28	<2	<0.044	<2	<0.038	<2	<0.052	<2	<0.017	-
15:31	<2	<0.044	<2	<0.038	<2	<0.052	4	0.02	0.05
15:34	<2	<0.044	<2	<0.038	<2	<0.052	<2	<0.017	-
15:37	<2	<0.044	<2	<0.038	<2	<0.052	<2	<0.017	-
<b>Average</b>		<b>&lt;0.044</b>		<b>&lt;0.038</b>		<b>&lt;0.052</b>		<b>&lt;0.017</b>	<b>-</b>



# CALIBRATION DATA

Number 1

Client: **New Indy**  
Location: **Catawba, SC**  
Source:

Project Number: **15730.001.006**  
Operator: **T. Simpkins**  
Date: **24 Mar 2021**

Method 16

Ambient Temperature: 72°C

Barometric Pressure: 30.12 in. Hg

Analyte	H <sub>2</sub> S	MeSH	DMS	DMDS
Perm. Device ID	T-53950	33-56671	89-56661	89-56665
Perm. Rate, nL/min	423	456	307	218
Ret. Time, sec	19.0	32.5	70.0	125.0

1 Flow = 55.0 mL/Min      7.70 ppm      8.30 ppm      5.57 ppm      3.96 ppm

Time: 08:25

Peak Areas, mv-sec

36213	43418	23287	63725	
36413	42776	23331	64081	
36421	43380	23930	65240	
<b>Average Area</b>	<b>36349</b> ✓	<b>43191</b> ✓	<b>23516</b> ✓	<b>64349</b> ✓

2 Flow = 120 mL/Min      3.53 ppm      3.80 ppm      2.55 ppm      1.81 ppm

Time: 08:40

Peak Areas, mv-sec

8717	10940	4796	15534	
9003	11114	4780	14544	
8846	10903	4727	14462	
<b>Average Area</b>	<b>8855</b> ✓	<b>10986</b> ✓	<b>4768</b> ✓	<b>14847</b> ✓

3 Flow = 331 mL/Min      1.28 ppm      1.38 ppm      0.93 ppm      0.66 ppm

Time: 08:53

Peak Areas, mv-sec

1189	1564	654	2164	
1219	1539	643	2101	
1185	1516	632	2063	
<b>Average Area</b>	<b>1198</b> ✓	<b>1540</b> ✓	<b>643</b> ✓	<b>2109</b> ✓

*AN*

# CALIBRATION SUMMARY

Number 1

Client: **New Indy**  
Location: **Catawba, SC**  
Source:

Project Number: **15730.001.006**  
Operator: **T. Simpkins**  
Date: **24 Mar 2021**

Method **16**

H <sub>2</sub> S	1	2	3		
Time	08:25	08:40	08:53		
Concentration, ppm	7.70	3.53	1.28		
Area, mv-sec	36349	8855	1198		
Calc. Conc., ppm	7.59	3.62	1.27		
% Error	-1.4	2.5	-1.1		
<u>Calibration Curve</u>	<b>Slope</b>	<b>Intercept</b>	<b>Corr. Coeff.</b>	<b>Min. Area</b>	<b>Det. Lim.</b>
	1.9048	2.8836	0.9997	2	0.044

MeSH	1	2	3		
Time	08:25	08:40	08:53		
Concentration, ppm	8.30	3.80	1.38		
Area, mv-sec	43191	10986	1540		
Calc. Conc., ppm	8.16	3.91	1.36		
% Error	-1.6	2.9	-1.2		
<u>Calibration Curve</u>	<b>Slope</b>	<b>Intercept</b>	<b>Corr. Coeff.</b>	<b>Min. Area</b>	<b>Det. Lim.</b>
	1.8614	2.9379	0.9996	2	0.038

DMS	1	2	3		
Time	08:25	08:40	08:53		
Concentration, ppm	5.57	2.55	0.93		
Area, mv-sec	23516	4768	643		
Calc. Conc., ppm	5.61	2.53	0.93		
% Error	0.6	-1.0	0.5		
<u>Calibration Curve</u>	<b>Slope</b>	<b>Intercept</b>	<b>Corr. Coeff.</b>	<b>Min. Area</b>	<b>Det. Lim.</b>
	2.0039	2.8712	>0.9999	2	0.052

DMDS	1	2	3		
Time	08:25	08:40	08:53		
Concentration, ppm	3.96	1.81	0.66		
Area, mv-sec	64349	14847	2109		
Calc. Conc., ppm	3.94	1.83	0.66		
% Error	-0.4	0.7	-0.3		
<u>Calibration Curve</u>	<b>Slope</b>	<b>Intercept</b>	<b>Corr. Coeff.</b>	<b>Min. Area</b>	<b>Det. Lim.</b>
	1.9051	3.6735	>0.9999	2	0.017

AW

## ANALYTES AND STANDARDS

Client: **New Indy**  
Location: **Catawba, SC**  
Source:

Project Number: **15730.001.006**  
Operator: **T. Simpkins**  
Date: **24 Mar 2021**

Method **16**

Analyte	H <sub>2</sub> S	MeSH	DMS	DMDS
<b>Molecular Weight</b>	34.08	48.11	62.14	94.20
<b>Retention Time, sec</b>	19.0	32.5	70.0	125.0
<b>Peak Detection Window, sec</b>	3.0	5.0	10.0	10.0
<b>Minimum Peak Area, mv-sec</b>	2	2	2	2
<b>Minimum Peak Height, mv</b>	1	1	1	1
<b>Beginning Peak Width, sec</b>	1.0	1.0	2.0	3.0
<b>Ending Peak Width, sec</b>	2.0	3.0	4.0	5.0
<b>Permeation Device ID</b>	T-53950	33-56671	89-56661	89-56665
<b>Permeation Rate, ng/min</b>	600 ✓	913	792 ✓	852 ✓
<b>Permeation Rate, nL/min*</b>	423	456	307	218

**Barometric Pressure:** 30.12 in. Hg      **Ambient Temperature:** 72 °F  
No Oxygen Correction

\*Permeation rates are gravimetrically determined by the manufacturer with results by weight in ng/min. Permeation rates by volume, in nL/min, are calculated from the permeation rates by weight as follows:

$$PR_{nl} = PR_{ng} \times (V_{mol} / W_{mol}) \times [(460^\circ + T_a) / T_s] \times (P_s / P_b)$$

Where:

**PR<sub>nl</sub>** = Permeation Rate by volume, nL/min

**PR<sub>ng</sub>** = Permeation Rate by weight, ng/min

**V<sub>mol</sub>** = Molar Volume of any gas @32 °F & 29.92 mm Hg = 22.4 L/mole

**W<sub>mol</sub>** = Molecular Weight of compound

**T<sub>a</sub>** = Ambient Temperature, °F

**T<sub>s</sub>** = Standard Temperature = 492°R (32 °F)

**P<sub>s</sub>** = Standard Pressure = 29.92 in Hg

**P<sub>b</sub>** = Barometric Pressure, in Hg

For example, H<sub>2</sub>S:

$$PR_{nl} = 600 \times (22.4 / 34.08) \times [(460 + 72) / 492] \times (29.92 / 30.12) \\ = 423 \text{ nL/min}$$

To calculate concentrations:

$$C = PR_{nl} / F_d$$

Where:

**C** = Concentration, ppmv

**PR<sub>nl</sub>** = Permeation Rate by volume, nL/min

**F<sub>d</sub>** = Flow rate of diluent, mL/min

# INSTRUMENT INFORMATION

Client: **New Indy**  
Location: **Catawba, SC**  
Source:

Method **16**

Project Number: **15730.001.006**  
Operator: **T. Simpkins**  
Date: **24 Mar 2021**

File: D:\NIC\Trs Data 24 March 2021 B.trs  
Program Version: 2.0, built 15 May 2017 File Version: 2.0  
Computer: DESKTOP-A1IJDGT Trailer: 88

Analog Input Device: Keithley KUSB-3108 GC Channel: 16

Sampling Rate: 0.050 sec. Data Interval: 0.5 sec.

Gas Chromatograph: Shimadzu GC8A Serial No. GC 1  
Detector Range: 10

Gases			Temperatures, °C	Columns
	Press. psi	Flow mL/min		
H <sub>2</sub>	30	50	Column: 100	Primary: Carbopack
Air	30	60	Detector: 120	Secondary: N/A
Carrier	50	30		Sample Loop: 4"

## Injection Cycle

Total Length: 180 sec Sampling Time: 170 sec Load/Backflush Time: 80 sec

## Default Integration Parameters

Signal Threshold 0.67 mv Peak detection window ±10 sec  
Minimum peak area 2 mv-sec Minimum peak height 1 mv above baseline

## Dynacalibrator

Chamber Temperature 50.0°C  
Ambient Temperature 72.0°F  
Barometric Pressure 30.12 in. Hg



**25 MARCH 2021**

New Indy Catawba Sample Analysis  
Work Order No. 15730.001.006  
Analyzed 25 March 2021

Sample	H <sub>2</sub> S µg / mL	MeSH µg / mL	DMS µg / mL	DMDS µg / mL	TRS as S µg / mL
Stripper Feed, AX3930	48.8 ✓	9.3 ✓	11.7 ✓	6.1 ✓	62.2 ✓
Acid Sewer, AX3931	0.13 ✓	<0.07 ✓	<0.06 ✓	0.20 ✓	0.26 ✓
Clarifier Overflow, AX3932	0.25 ✓	<0.1 ✓	1.2 ✓	0.57 ✓	1.24 ✓
ASB Effluent, AX3933	0.20 ✓	<0.1 ✓	<0.08 ✓	<0.06 ✓	0.18 ✓
ASB Influent, AX3934	0.10 ✓	<0.06 ✓	0.65 ✓	0.23 ✓	0.58 ✓
Screw Press Filtrate, AX3935	0.14 ✓	<0.05 ✓	<0.04 ✓	<0.03 ✓	0.13 ✓
PM 3 Whitewater, AX3936	0.04 ✓	<0.05 ✓	0.18 ✓	<0.03 ✓	0.13 ✓

✓ JBT

New Indy Catawba Sample Analysis  
Work Order No. 15730.001.006  
Analyzed 25 March 2021

Sample	Stripper Feed, AX3930				
Aliquot, mL	2.5				
Purge					
Nitrogen Flow Rate, mL/min	948				
Purge Time, min	10.00				
Gas Volume in Bag, L	9.480				
Analysis	H <sub>2</sub> S	MeSH	DMS	DMDS	TRS as S
Conc. in Bag, ppm	9.08	1.23	1.19	0.41	12.32
Mass in Bag, µg	122 ✓	23.3 ✓	29.2 ✓	15.2 ✓	155 ✓
Conc. in Sample, µg/mL	48.8 ✓	9.3 ✓	11.7 ✓	6.1 ✓	62.2 ✓

✓  
P

✓ JWB

New Indy Catawba Sample Analysis  
 Work Order No. 15730.001.006  
 Analyzed 25 March 2021

Sample	Acid Sewer, AX3931				
Aliquot, mL	15.0				
Purge					
Nitrogen Flow Rate, mL/min	945				
Purge Time, min	2.00				
Gas Volume in Bag, L	1.890				
Analysis	H <sub>2</sub> S	MeSH	DMS	DMDS	TRS as S
Conc. in Bag, ppm	0.73	<0.25	<0.16	0.40	1.53
Mass in Bag, µg	2.0 ✓	<0.95 ✓	<0.79 ✓	3.0 ✓	3.8 ✓
Conc. in Sample, µg/mL	0.13 ✓	<0.07 ✓	<0.06 ✓	0.20 ✓	0.26 ✓

*✓✓✓*



New Indy Catawba Sample Analysis  
 Work Order No. 15730.001.006  
 Analyzed 25 March 2021

Sample	Clarifier Overflow, AX3932				
Aliquot, mL	10.0				
Purge					
Nitrogen Flow Rate, mL/min	987				
Purge Time, min	2.00				
Gas Volume in Bag, L	1.974				
Analysis	H <sub>2</sub> S	MeSH	DMS	DMDS	TRS as S
Conc. in Bag, ppm	0.91	<0.25	2.33	0.74	4.72
Mass in Bag, µg	2.55	<1.0	11.9	5.72	12.4
Conc. in Sample, µg/mL	0.25	<0.1	1.2	0.57	1.24

*✓ JLB*

New Indy Catawba Sample Analysis  
Work Order No. 15730.001.006  
Analyzed 25 March 2021

Sample	ASB Effluent, AX3933				
Aliquot, mL	10.0				
Purge					
Nitrogen Flow Rate, mL/min	962				
Purge Time, min	2.00				
Gas Volume in Bag, L	1.924				
Analysis	H <sub>2</sub> S	MeSH	DMS	DMDS	TRS as S
Conc. in Bag, ppm	0.72	<0.25	<0.16	<0.07	0.72
Mass in Bag, µg	2.0	<1.0	<0.8	<0.53	1.8
Conc. in Sample, µg/mL	0.20	<0.1	<0.08	<0.06	0.18

*✓*

New Indy Catawba Sample Analysis  
 Work Order No. 15730.001.006  
 Analyzed 25 March 2021

Sample	ASB Influent, AX3934				
Aliquot, mL	20.0				
Purge					
Nitrogen Flow Rate, mL/min	1033				
Purge Time, min	2.00				
Gas Volume in Bag, L	2.066				
Analysis	H <sub>2</sub> S	MeSH	DMS	DMDS	TRS as S
Conc. in Bag, ppm	0.66	<0.25	2.43	0.58	4.25
Mass in Bag, µg	1.9 ✓	<1.04 ✓	13.0 ✓	4.7 ✓	11.7 ✓
Conc. in Sample, µg/mL	0.10 ✓	<0.06 ✓	0.65 ✓	0.23 ✓	0.58 ✓

✓ with

New Indy Catawba Sample Analysis  
Work Order No. 15730.001.006  
Analyzed 25 March 2021

		Screw Press Filtrate, AX3935				
Sample						
Aliquot, mL					20.0	
Purge						
Nitrogen Flow Rate, mL/min					985	
Purge Time, min					2.00	
Gas Volume in Bag, L					1.970	
Analysis	H <sub>2</sub> S	MeSH	DMS	DMDS	TRS as S	
Conc. in Bag, ppm	0.99	<0.25	<0.16	<0.07	0.99	
Mass in Bag, µg	2.8	<1.0	<0.82	<0.55	2.6	
Conc. in Sample, µg/mL	0.14	<0.05	<0.04	<0.03	0.13	

✓ JMB

New Indy Catawba Sample Analysis  
Work Order No. 15730.001.006  
Analyzed 25 March 2021

Sample	PM 3 Whitewater, AX3936				
Aliquot, mL	20.0				
Purge					
Nitrogen Flow Rate, mL/min	998				
Purge Time, min	2.00				
Gas Volume in Bag, L	1.996				
Analysis	H <sub>2</sub> S	MeSH	DMS	DMDS	TRS as S
Conc. in Bag, ppm	0.27	<0.25	0.71	<0.07	0.98
Mass in Bag, µg	0.76	<1.0	3.7	<0.55	2.6
Conc. in Sample, µg/mL	0.04	<0.05	0.18	<0.03	0.13

*VJD*

# RUN DATA

Number 1

15730.001.006  
New-Indy Catawba  
Odor Testing

Client: **New Indy**  
Location: **Catawba, SC**  
Source:

Method **16**  
Calibration **1**

Project Number:  
Operator: **J. Short**  
Date: **25 Mar 2021**

Time	H <sub>2</sub> S		MeSH		DMS		DMDS		TRS ppm
	area	ppm	area	ppm	area	ppm	area	ppm	
<b>PM3 Whitewater AX3936</b>									
10:49	4	0.23	<2	<0.25	35	0.68	<2	<0.070	0.91
10:52	4	0.23	<2	<0.25	41	0.73	<2	<0.070	0.96
10:55	8	0.34	<2	<0.25	40	0.72	<2	<0.070	1.06
<b>Average</b>		<b>0.27</b>		<b>&lt;0.25</b>		<b>0.71</b>		<b>&lt;0.070</b>	<b>0.98</b>

# RUN DATA

Number 2

15730.001.006  
New-Indy Catawba  
Odor Testing

Client: **New Indy**  
Location: **Catawba, SC**  
Source:

Method **16**  
Calibration **1**

Project Number:  
Operator: **J. Short**  
Date: **25 Mar 2021**

Time	H <sub>2</sub> S		MeSH		DMS		DMDS		TRS ppm
	area	ppm	area	ppm	area	ppm	area	ppm	
<b>Screw Press Filtrate AX3935</b>									
11:29	67	0.97	<2	<0.25	<2	<0.16	<2	<0.070	0.97
11:32	78	1.04	<2	<0.25	<2	<0.16	<2	<0.070	1.04
11:35	69	0.98	<2	<0.25	<2	<0.16	<2	<0.070	0.98
<b>Average</b>		<b>0.99</b>		<b>&lt;0.25</b>		<b>&lt;0.16</b>		<b>&lt;0.070</b>	<b>0.99</b>

# RUN DATA

Number 3

15730.001.006  
New-Indy Catawba  
Odor Testing

Client: **New Indy**  
Location: **Catawba, SC**  
Source:

Method **16**  
Calibration **1**

Project Number:  
Operator: **J. Short**  
Date: **25 Mar 2021**

Time	H <sub>2</sub> S		MeSH		DMS		DMDS		TRS ppm
	area	ppm	area	ppm	area	ppm	area	ppm	
<b>ASB Influent AX3934</b>									
11:45	30	0.65	<2	<0.25	415	2.36	137	0.60	4.22
11:48	30	0.65	<2	<0.25	446	2.45	103	0.52	4.14
11:51	32	0.67	<2	<0.25	453	2.47	148	0.62	4.39
<b>Average</b>		<b>0.66</b>		<b>&lt;0.25</b>		<b>2.43</b>		<b>0.58</b>	<b>4.25</b>



# RUN DATA

Number 6

Client: **New Indy**  
 Location: **Catawba, SC**  
 Source:

Method **16**  
 Calibration **1**

Project Number:  
 Operator: **J. Short**  
 Date: **25 Mar 2021**

Time	H <sub>2</sub> S		MeSH		DMS		DMDS		TRS ppm
	area	ppm	area	ppm	area	ppm	area	ppm	
<b>ASB Effluent AX3933</b>									
12:54	35	0.70	<2	<0.25	<2	<0.16	<2	<0.070	0.70
12:57	39	0.74	<2	<0.25	<2	<0.16	<2	<0.070	0.74
13:00	37	0.72	<2	<0.25	<2	<0.16	<2	<0.070	0.72
<b>Average</b>		<b>0.72</b>		<b>&lt;0.25</b>		<b>&lt;0.16</b>		<b>&lt;0.070</b>	<b>0.72</b>

# RUN DATA

Number 7

15730.001.006  
New-Indy Catawba  
Odor Testing

Client: **New Indy**  
Location: **Catawba, SC**  
Source:

Method **16**  
Calibration **1**

Project Number:  
Operator: **J. Short**  
Date: **25 Mar 2021**

Time	H <sub>2</sub> S		MeSH		DMS		DMDS		TRS ppm
	area	ppm	area	ppm	area	ppm	area	ppm	
<b>Clarifier overflow AX3932</b>									
13:03	53	0.86	<2	<0.25	395	2.30	207	0.74	4.65
13:06	65	0.95	<2	<0.25	398	2.32	212	0.75	4.76
13:09	59	0.91	<2	<0.25	415	2.36	200	0.73	4.73
<b>Average</b>		<b>0.91</b>		<b>&lt;0.25</b>		<b>2.33</b>		<b>0.74</b>	<b>4.71</b>

# RUN DATA

Number 8

15730.001.006  
New-Indy Catawba  
Odor Testing

Client: **New Indy**  
Location: **Catawba, SC**  
Source:

Method **16**  
Calibration **1**

Project Number:  
Operator: **J. Short**  
Date: **25 Mar 2021**

Time	H <sub>2</sub> S		MeSH		DMS		DMDS		TRS ppm
	area	ppm	area	ppm	area	ppm	area	ppm	
<b>Acid Sewer AX3931</b>									
13:25	39	0.74	<2	<0.25	<2	<0.16	62	0.40	1.54
13:28	37	0.72	<2	<0.25	<2	<0.16	53	0.37	1.46
13:31	37	0.72	<2	<0.25	<2	<0.16	72	0.43	1.58
<b>Average</b>		<b>0.73</b>		<b>&lt;0.25</b>		<b>&lt;0.16</b>		<b>0.40</b>	<b>1.53</b>

# RUN DATA

Number 9

15730.001.006  
New-Indy Catawba  
Odor Testing

Client: **New Indy**  
Location: **Catawba, SC**  
Source:

Method 16  
Calibration 1

Project Number:  
Operator: **J. Short**  
Date: **25 Mar 2021**

Time	H <sub>2</sub> S		MeSH		DMS		DMDS		TRS ppm
	area	ppm	area	ppm	area	ppm	area	ppm	
<b>Stripper Feed AX3930</b>									
14:10	6015	8.99	50	1.16	115	1.24	63	0.40	12.2
14:13	5820	8.85	58	1.24	91	1.10	64	0.41	12.0
14:16	6579	9.40	63	1.30	113	1.23	68	0.42	12.8
<b>Average</b>		<b>9.08</b>		<b>1.23</b>		<b>1.19</b>		<b>0.41</b>	<b>12.3</b>

# CALIBRATION DATA

Number 1

15730.001.005  
New-Indy Catawba  
Odor Testing

Client: **New Indy**  
Location: **Catawba, SC**  
Source:

Method 16

Project Number:  
Operator: **J. Short**  
Date: **25 Mar 2021**

Ambient Temperature: 72°C

Barometric Pressure: 30.04 in. Hg

Analyte	H <sub>2</sub> S	MeSH	DMS	DMDS
Perm. Device ID	T-53935	33-56672	89-56663	89-53970
Perm. Rate, nL/min	425	439	271	200
Ret. Time, sec	17.0	28.0	60.0	101.5

1 Flow = 30.8 mL/Min      13.8 ppm      14.3 ppm      8.81 ppm      6.49 ppm

Time: 08:51

Peak Areas, mv-sec

13428	8757	5211	13721
14531	9664	5583	14836
14535	9586	5637	15008
<b>Average Area</b>	<b>14165</b>	<b>5477</b>	<b>14522</b>

2 Flow = 62.9 mL/Min      6.76 ppm      6.98 ppm      4.31 ppm      3.18 ppm

Time: 09:06

Peak Areas, mv-sec

3408	2165	1413	3808
3446	2160	1465	3622
3435	2121	1322	3658
<b>Average Area</b>	<b>3430</b>	<b>1400</b>	<b>3696</b>

3 Flow = 118 mL/Min      3.62 ppm      3.74 ppm      2.31 ppm      1.70 ppm

Time: 09:22

Peak Areas, mv-sec

967	560	395	1069
938	573	378	1018
950	576	395	1055
<b>Average Area</b>	<b>951</b>	<b>389</b>	<b>1047</b>

# CALIBRATION SUMMARY

Number 1

15730.001.006  
New-Indy Catawba  
Odor Testing

Client: **New Indy**  
Location: **Catawba, SC**  
Source:

Project Number:  
Operator: **J. Short**  
Date: **25 Mar 2021**

Method **16**

<b>H<sub>2</sub>S</b>	<b>1</b>	<b>2</b>	<b>3</b>		
<b>Time</b>	08:51	09:06	09:22		
<b>Concentration, ppm</b>	13.8	6.76	3.62		
<b>Area, mv-sec</b>	14165	3430	951		
<b>Calc. Conc., ppm</b>	13.8	6.81	3.60		
<b>% Error</b>	-0.3	0.7	-0.4		
<b>Calibration Curve</b>	<b>Slope</b>	<b>Intercept</b>	<b>Corr. Coeff.</b>	<b>Min. Area</b>	<b>Det. Lim.</b>
	2.0162	1.8561	>0.9999	2	0.17

<b>MeSH</b>	<b>1</b>	<b>2</b>	<b>3</b>		
<b>Time</b>	08:51	09:06	09:22		
<b>Concentration, ppm</b>	14.3	6.98	3.74		
<b>Area, mv-sec</b>	9336	2149	570		
<b>Calc. Conc., ppm</b>	14.2	7.03	3.72		
<b>% Error</b>	-0.3	0.7	-0.4		
<b>Calibration Curve</b>	<b>Slope</b>	<b>Intercept</b>	<b>Corr. Coeff.</b>	<b>Min. Area</b>	<b>Det. Lim.</b>
	2.0875	1.5641	>0.9999	2	0.25

<b>DMS</b>	<b>1</b>	<b>2</b>	<b>3</b>		
<b>Time</b>	08:51	09:06	09:22		
<b>Concentration, ppm</b>	8.81	4.31	2.31		
<b>Area, mv-sec</b>	5477	1400	389		
<b>Calc. Conc., ppm</b>	8.74	4.38	2.29		
<b>% Error</b>	-0.7	1.6	-0.8		
<b>Calibration Curve</b>	<b>Slope</b>	<b>Intercept</b>	<b>Corr. Coeff.</b>	<b>Min. Area</b>	<b>Det. Lim.</b>
	1.9730	1.8806	0.9998	2	0.16

<b>DMDS</b>	<b>1</b>	<b>2</b>	<b>3</b>		
<b>Time</b>	08:51	09:06	09:22		
<b>Concentration, ppm</b>	6.49	3.18	1.70		
<b>Area, mv-sec</b>	14522	3696	1047		
<b>Calc. Conc., ppm</b>	6.46	3.22	1.69		
<b>% Error</b>	-0.5	1.2	-0.6		
<b>Calibration Curve</b>	<b>Slope</b>	<b>Intercept</b>	<b>Corr. Coeff.</b>	<b>Min. Area</b>	<b>Det. Lim.</b>
	1.9629	2.5716	0.9999	2	0.070

# ANALYTES AND STANDARDS

15730.001.006  
New-Indy Catawba  
Odor Testing

Client: **New Indy**  
Location: **Catawba, SC**  
Source:

Method 16

Project Number:  
Operator: **J. Short**  
Date: **25 Mar 2021**

Analyte	H <sub>2</sub> S	MeSH	DMS	DMDS
Molecular Weight	34.08	48.11	62.14	94.20
Retention Time, sec	17.0	28.0	60.0	101.5
Peak Detection Window, sec	5.0	5.0	10.0	10.0
Minimum Peak Area, mv-sec	2	2	2	2
Minimum Peak Height, mv	1	1	1	1
Beginning Peak Width, sec	1.0	1.0	2.0	3.0
Ending Peak Width, sec	2.0	3.0	4.0	5.0
Permeation Device ID	T-53935	33-56672	89-56663	89-53970
Permeation Rate, ng/min	600 ✓	876	699 ✓	781 ✓
Permeation Rate, nL/min*	425	439	271	200

**Barometric Pressure:** 30.04 in. Hg      **Ambient Temperature:** 72 °F  
No Oxygen Correction

\*Permeation rates are gravimetrically determined by the manufacturer with results by weight in ng/min. Permeation rates by volume, in nL/min, are calculated from the permeation rates by weight as follows:

$$PR_{nl} = PR_{ng} \times (V_{mol} / W_{mol}) \times [(460^\circ + T_a) / T_s] \times (P_s / P_b)$$

Where:

- PR<sub>nl</sub>** = Permeation Rate by volume, nL/min
- PR<sub>ng</sub>** = Permeation Rate by weight, ng/min
- V<sub>mol</sub>** = Molar Volume of any gas @32 °F & 29.92 in. Hg = 22.4 L/mole
- W<sub>mol</sub>** = Molecular Weight of compound
- T<sub>a</sub>** = Ambient Temperature, °F
- T<sub>s</sub>** = Standard Temperature = 492°R (32 °F)
- P<sub>s</sub>** = Standard Pressure = 29.92 in. Hg
- P<sub>b</sub>** = Barometric Pressure, in. Hg

For example, H<sub>2</sub>S:

$$PR_{nl} = 600 \times (22.4 / 34.08) \times [(460 + 72) / 492] \times (29.92 / 30.04) = 425 \text{ nL/min}$$

To calculate concentrations:

$$C = PR_{nl} / F_d$$

Where:

- C** = Concentration, ppmv
- PR<sub>nl</sub>** = Permeation Rate by volume, nL/min
- F<sub>d</sub>** = Flow rate of diluent, mL/min

# INSTRUMENT INFORMATION

15730.001.006  
New-Indy Catawba  
Odor Testing

Client: **New Indy**  
Location: **Catawba, SC**  
Source:

Project Number:  
Operator: **J. Short**  
Date: **25 Mar 2021**

Method **16**

File: J:\Misc\NewIndy\03-25-21.trs  
Program Version: 2.0, built 28 Oct 2020 File Version: 2.0  
Computer: JWS-PROGRAMMING Trailer: 221

Analog Input Device: MCC USB-1608G GC Channel: 16

Sampling Rate: 0.050 sec. Data Interval: 0.5 sec.

Gas Chromatograph: Shimadzu GC-8A Serial No. C10493414707  
Detector Range: 10

Gases			Temperatures, °C	Columns
	Press.	Flow		
	psi	mL/min		
H <sub>2</sub>	30	50	Column: 100	Primary: 6'
Air	30	60	Detector: 120	Secondary: none
Carrier	50	30		Sample Loop: 6"

## Injection Cycle

Total Length: 180 sec Sampling Time: 160 sec Load/Backflush Time: 70 sec

## Default Integration Parameters

Signal Threshold 0.67 mv Peak Detection Window ±10 sec  
Minimum Peak Area 2 mv-sec Minimum Peak Height 1 mv above baseline

## Dynacalibrator

Chamber Temperature -1.0°C  
Ambient Temperature 72.0°F  
Barometric Pressure 30.04 in. Hg





## ATTACHMENT C LABORATORY DATA

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## METHANOL

# Inter-Office Memorandum



15730.001.006  
New-Indy Catwaba  
Odor Testing

1625 Pumphrey Avenue, Auburn, AL 36832  
334.466.5600

TO: Temp Simpkins, Project Manager  
FROM: Staci Hickman, Laboratory Manager  
PROJECT: New Indy Catwaba  
W.O. NO: 15730.001.006  
SUBJECT: Methanol Analysis Results

cc: File

Date: 23 March 2021

JOB NO.: 2021-091

ACTION: Analysis of samples received on 20 March 2021

NELAC Accreditation ID: 03024

## NARRATIVE:

This letter with analytical results constitutes our report for the analysis of the condensate samples collected by New Indy personnel and submitted to the laboratory on 20 March 2021 for methanol analysis. The samples arrived in accordance with the Chain-of-Custody. The samples were prepared and analyzed on 22 March 2021 according to NCASI Method DI/MeOH-94.03.

Enclosed is a copy of the Chain-of-Custody record, acknowledging receipt of these samples. Please note that any unused portion of the samples will be discarded 90 days after the date of receipt.

The results of this report relate only to the samples listed in the body of this report.

This report shall not be reproduced by any organization outside of Weston Solutions, Inc. in part or in full, without the written approval from Weston Solutions, Inc.

These results meet all requirements of TNI, unless otherwise specified.

## QUALITY ASSURANCE AND QUALITY CONTROL:

Quality control procedures conformed to the requirements of the referenced method and our quality assurance program.

All quality control results associated with this sample set were within acceptable limits and/or do not adversely affect the reported results. The quality control analysis results as well as the acceptance criteria are shown in the Quality Control section.

We appreciate the opportunity to work with you in performing this analysis. If we can be of any other assistance, please contact me at (334) 466-5683.

Attachments



Analytical Laboratory  
 1625 Pumphrey Ave. Auburn AL 36832  
 334-466-5600

Client : New Indy Catwaba  
 Proposal # : 15730.001.006  
 WESTON Lab Job # : 2021-091  
 Dates Received : 20-Mar-21

Instrument ID: GC/FID-Lil Red  
 Analyst: SH  
 Date(s) Prepped: 3/22/2021  
 Date (s) Analyzed: 3/22/2021

Limit of Quantification for Methanol (µg/mL): 1.15

Source ID	Date Collected	Lab ID	Sample Methanol Concentration (µg/mL)
#3 Foul Condensate	3/17/2021	AX 3919	7170
#3 Combined Condensate	3/17/2021	AX 3920	1210
#2 Foul Condensate	3/17/2021	AX 3921	2320
#2 Combined Condensate	3/17/2021	AX 3922	188
#2 Condenser Condensate	3/17/2021	AX 3923	1590
#1 Old Condensate	3/17/2021	AX 3924	1340
#1 Foul Condensate	3/17/2021	AX 3925	688
#1 Combined Condensate	3/17/2021	AX 3926	103
#1 Auxillary Condensate	3/17/2021	AX 3927	2510
M52-0453 Combined Condensate	3/17/2021	AX 3928	539
M52-0432 HVLC Condensate	3/17/2021	AX 3929	160
Stripper Feed Tank	3/17/2021	AX 3930	1860
Acid Sewer	3/17/2021	AX 3931	43.8
Clarifying Overflow	3/17/2021	AX 3932	185
ASB Effluent	3/18/2021	AX 3933	49.4
ASB Influent	3/18/2021	AX 3934	117
Screw Press Filtrate	3/18/2021	AX 3935	54.1
PM3 Whitewater	3/18/2021	AX 3936	14.5

Some samples were diluted 1:5 to reduce potential interferences.

*Staci Hickman*

Staci Hickman, Laboratory Manager  
 Printed: 3/23/2021



Analytical Laboratory  
1625 Pumphrey Ave. Auburn AL 36832  
334-466-5600

Client: New Indy Catwaba WESTON Lab Job # 2021-091 WESTON W.O. # 15730.001.006

**Table 1.1**

**Calibration Curve Verification Standards**

Analysis Date	Laboratory ID	Methanol		
		Actual Value (µg/mL)	Calculated Value (µg/mL)	Difference (%)
3/22/2021	9339-42-07	46.1	46.1	0.1%
3/22/2021	9339-42-05	576	578	0.4%
3/22/2021	LCS 5459400	2008	2008	0.0%
3/22/2021	9339-42-05	576	559	2.9%
3/22/2021	9339-42-05	576	547	5.0%
3/22/2021	9339-42-03	2303	2418	5.0%

**Table 1.2**

**Replicate Analysis**

Analysis Date	Laboratory ID	Methanol		
		Original Value (µg/mL)	Replicate Value (µg/mL)	Difference (%)
3/22/2021	AX 3919	7165	7598	2.9%
3/22/2021	AX 3929	160	160	0.0%

**Table 1.3**

**Duplicate Analysis**

Analysis Date	Laboratory ID	Methanol		
		Original Value (µg/mL)	Duplicate Value (µg/mL)	Difference (%)
3/22/2021	AX 3920	1207	1217	0.4%
3/22/2021	AX 3930	1859	1847	0.3%

**Table 1.4**

**Spike Analysis**

Analysis Date	Laboratory ID	Methanol				Recovery (%)
		Original Value (µg/mL)	Spiked Value (µg/mL)	Recovered Amount (µg/mL)	Spiked Amount (µg/mL)	
3/22/2021	AX 3920	1207	2728	1521	1582	96%
3/22/2021	AX 3930	372	2825	2453	2373	103%

- Note- For QC purposes the actual analytical result rather than the LOQ was used when the analytical result was less than the LOQ.
- Consequently, certain differences in actual and calculated values may be skewed.

**Calculations:**

- Standard % Difference =  $(\frac{|(\text{Actual Value} - \text{Calculated Value})|}{(\text{Actual Amount})}) * 100$ .
- Replicate/Duplicate % Difference =  $(\frac{|(\text{Average Value} - \text{Original Value})|}{(\text{Average Value})}) * 100$ .
- Spike % Recovery =  $(\frac{\text{Recovered Amount}}{(\text{Spiked Amount})}) * 100$

**Acceptance Criteria:**

- The CCV Acceptance Criterion is ± 10 % for Methanol.
- The Replicate and Duplicate Percent Difference Acceptance Criterion is ± 10 percent.
- The LCS Acceptance Criterion is ± 15 percent for methanol.
- The Spike Recovery Acceptance Criterion is 100 percent ± 30 percent.

**Lot #s:**

Spike Lot # Neat - 145647  
Internal Lot # 9339-39-00

*Staci Hickman*

Staci Hickman, Laboratory Manager  
Printed: 3/23/2021





## TERPENES

## Inter-Office Memorandum



1625 Pumphrey Avenue, Auburn, AL 36832

334.466.5600

TO: Temp Simpkins, Project Manager  
FROM: Staci Hickman, Laboratory Manager  
PROJECT: New Indy Catwaba  
W.O. NO: 15370.001.006  
SUBJECT: Terpene Analysis Results  
ACTION: Analysis of samples received on 20 March 2021

Date: 12 April 2021

JOB NO.: 2021-094

### NARRATIVE:

This memo with analytical results constitutes our report for the condensate samples submitted to the laboratory for terpene analysis. The samples arrived in accordance with the Chain-of-Custody. The samples were prepared on 22 March 2021 and analyzed on 23 March through 24 March 2021 per NIOSH Method 1552. Each sample was analyzed for  $\alpha$ -pinene,  $\beta$ -pinene and total terpenoids. The unidentified terpenoid amount was determined using the response factor for  $\alpha$ -pinene to quantify individual terpenoid peaks and adding the combined concentrations to determine total unidentified terpenoid concentration.

Enclosed is a copy of the Chain-of-Custody record, acknowledging receipt of the samples. Please note that any unused portion of the sample will be discarded 90 days after the date of receipt.

These results of this report relate only to the samples listed in the body of this report.

This report shall not be reproduced by any organization outside of Weston Solutions, Inc. in part or in full, without the written approval from Weston Solutions, Inc.

This analysis is outside the scope of our TNI accreditation.

### QUALITY ASSURANCE AND QUALITY CONTROL:

Quality control procedures conformed to the requirements of NIOSH 1552 modified for condensate terpenes and our quality assurance program. All samples were analyzed in replicate. The replicates had differences of 3.5% or less for  $\alpha$  and  $\beta$ -pinene, and 4.9% or less for the unidentified terpenoids.

All quality control results associated with this sample set were within acceptable limits and/or do not adversely affect the reported results. The quality control analysis results as well as the acceptance criteria are shown in the following tables of the Quality Control Report.

We appreciate the opportunity to work with you in performing these analyses. If we can be of any other assistance, please contact me at (334) 466-5683.

Sincerely,

WESTON SOLUTIONS:

Staci Hickman  
Laboratory Manager



Client : New Indy Catwaba  
WESTON W.O. # : 15370.001.006  
Lab Job #: 2021-094  
Date Received : 3/20/2021  
Date Prepared : 3/22/2021  
Instrument ID: GC/FID-Green Machine  
Analyst: SH  
Date(s) Analyzed: 3/23/2021-3/24/2021  
Limit of Quantification for a-pinene(µg/mL): 0.69 µg/mL  
Limit of Quantification for β-pinene(µg/mL) 0.69 µg/mL

Source ID	Date Collected	Sample Volume (mL)	Dilution	Sample ID	Analyzed a-Pinene (µg/mL)	Analyzed β-Pinene (µg/mL)	Total Terpenoids (µg/mL)	Analyzed Other Terpenoids (µg/mL)
#3 Foul Condensate	3/17/2021	43	1	AX 3937	3430	1308	6011	1274
#3 Combined Condensate	3/17/2021	43	1	AX 3938	25.8	11.2	229	192
#2 Foul Condensate	3/17/2021	43	1	AX 3939	1.57	0.88	196	194
#2 Combined Condensate	3/17/2021	43	1	AX 3940	<0.69	<0.69	127	127
#2 Condenser Condensate	3/17/2021	43	1	AX 3941	205	79.4	516	232
#1 Old Condensate	3/17/2021	43	1	AX 3942	76.2	35.4	265	154
#1 Foul Condensate	3/17/2021	43	1	AX 3943	2.67	1.25	132	128
#1 Combined Condensate	3/17/2021	43	1	AX 3944	<0.69	<0.69	142	142
#1 Auxillary Condensate	3/17/2021	43	1	AX 3945	113	53.8	422	255
M52-0453 Combined Condensate	3/17/2021	43	1	AX 3946	4.85	2.40	166	159
M52-0432 HVLC Condensate	3/17/2021	43	1	AX 3947	1.79	1.11	62.0	59.1
Stripper Feed Tank	3/17/2021	43	1	AX 3948	1309	512	2396	575
Acid Sewer	3/17/2021	43	1	AX 3949	2.85	1.28	29.1	25.0

*Staci Hickman*  
Staci Hickman, Laboratory Manager

Client: New Indy Catwaba

Weston Job #: 2021-094

Weston WO#: 15370.001.006

**Table 1.1**  
**Continuing Calibration Curve Verification Standards**

Analysis Date	Laboratory ID	α-Pinene			β-Pinene		
		Actual Value (µg/mL)	Calculated Value (µg/mL)	Difference (%)	Actual Value (µg/mL)	Calculated Value (µg/mL)	Difference (%)
3/23/2021	9339-48-06	2.74	2.75	0.4%	2.76	2.77	0.4%
3/23/2021	9339-48-03	686	633	7.7%	689	634	8.0%
3/23/2021	LCS 9339-47-00	945	970	2.7%	923	914	1.0%
3/24/2021	9339-48-05	34.3	30.2	12%	34.5	30.7	11%
3/24/2021	9339-48-04	68.6	62.8	8.5%	68.9	63.1	8.4%
3/24/2021	9339-48-01	3428	3649	6.5%	3446	3702	7.4%
3/24/2021	9339-48-03	686	639	6.9%	689	641	6.9%

**Table 1.2**  
**Duplicate Analysis**

Analysis Date	Laboratory ID	α-Pinene			β-Pinene		
		Original Value (µg/mL)	Duplicate Value (µg/mL)	Difference (%)	Original Value (µg/mL)	Duplicate Value (µg/mL)	Difference (%)
3/23/2021	AX 3938	25.8	26.2	0.8%	11.2	11.5	1.1%
3/24/2021	AX 3948	1309	1341	1.2%	512	524	1.1%

**Table 1.3**  
**Spike Analysis**

Analysis Date	Laboratory ID	α-Pinene					β-Pinene				
		Original Value (µg/mL)	Spiked Value (µg/mL)	Recovered Amount (µg/mL)	Spiked Amount (µg/mL)	Recovery (%)	Original Value (µg/mL)	Spiked Value (µg/mL)	Recovered Amount (µg/mL)	Spiked Amount (µg/mL)	Recovery (%)
3/23/2021	AX 3938	25.8	94.7	68.9	68.6	100%	11.2	83.6	72.3	68.9	105%
3/24/2021	AX 3948	1341	1400	58.8	68.6	86%	512	589	76.3	68.9	111%

- Note the actual analytical result rather than the LOQ was used when the analytical result was less than the LOQ.
- Consequently, certain differences in actual and calculated values may be skewed.

**Calculations:**

- Standard % Difference =  $\left( \frac{|(\text{Actual Value} - \text{Calculated Value})|}{(\text{Actual Amount})} \right) * 100$ .
- Duplicate % Difference =  $\left( \frac{|(\text{Original Value} + \text{Duplicate Value}) - 2 * \text{Original Value}|}{(\text{Average Value})} \right) * 100$ .
- Spike % Recovery =  $\left( \frac{\text{Recovered Amount}}{(\text{Spiked Amount})} \right) * 100$ .

**Acceptance Criteria:**

- The CCV Acceptance Criterion is ± 15 percent.
- The LCS Acceptance Criterion is ± 15 percent.
- The Duplicate Percent Difference Acceptance Criterion is ± 10 percent.
- The Spike Recovery Acceptance Criterion is 100 percent ± 30 percent.

*Staci Hickman*

Staci Hickman, Laboratory Manager



Lab Tracking Number

### Chain-of-Custody Record/Lab Work Request

Page      of     

Client	New Ind. Catwaba, SC		
Work Order Number	15730.001.006	45730001-04 (SN)	Phone Number 334-728-0127
Contact Person	Templeton Simpkins	Turn Around Time	

Lab ID	Field Sample ID	Sample Collection Date	Analyses Requested/Other Info				Sample Check-off
			Terpenes Analysis	NIOSH 1552			
Ax 3937	NI-#3FoulCondensate	3/17/2021	X				
3938	NI-#3CombinedCondensate	3/17/2021	X				
3939	NI-#2FoulCondensate	3/17/2021	X				
3940	NI-#2CombinedCondensate	3/17/2021	X				
3941	NI-#2CondenserCondensate	3/17/2021	X				
3942	NI-#1OldCondensate	3/17/2021	X				
3943	NI-#1FoulCondensate	3/17/2021	X				
3944	NI-#1CombinedCondensate	3/17/2021	X				
3945	NI-#1AuxillaryCondensate	3/17/2021	X				
3946	NI-M52-0453CombinedCondensate	3/17/2021	X				
3947	NI-M52-0432HVLCCCondensate	3/17/2021	X				
3948	NI-StripperFeedTank	3/17/2021	X				
3949	NI-AcidSewer	3/17/2021	X				
	NI-ClarifyingOverflow	3/17/2021					
	NI-ASBEffluent	3/18/2021					
	NI-ASBInfluent	3/18/2021					
	NI-ScrewPressFiltrate	3/18/2021					
	NI-PM3Whitewater	3/18/2021					

Notes: NI-ASBEffluent 3/18/2021

LAB JOB NO: 2021-094  
SAMPLE TEMP: 5.4°C

Relinquished By	Received By	Date	Time	Lab Use Only	
<i>[Signature]</i>	Stacy Hickman	3/20/21	14:00	Shipper	Air Bill #
				Opened By	Date/Time
				Temp °C	Condition
				Custody Seals: Yes No None N/A	

Laboratory Comments:



## ATTACHMENT D QUALITY CONTROL DATA

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## AUDIT CYLINDER CERTIFICATE

# CERTIFICATE OF ANALYSIS

## Grade of Product: EPA Protocol

Part Number:	E02AI99E15A00U0	Reference Number:	122-401930615-1
Cylinder Number:	CC507346	Cylinder Volume:	146.2 CF
Laboratory:	124 - Durham (SAP) - NC	Cylinder Pressure:	2015 PSIG
PGVP Number:	B22020	Valve Outlet:	330
Gas Code:	H2S,O2,BALN	Certification Date:	Oct 21, 2020

**Expiration Date: Oct 21, 2023**

Certification performed in accordance with "EPA Traceability Protocol for Assay and Certification of Gaseous Calibration Standards (May 2012)" document EPA 600/R-12/531, using the assay procedures listed. Analytical Methodology does not require correction for analytical interference. This cylinder has a total analytical uncertainty as stated below with a confidence level of 95%. There are no significant impurities which affect the use of this calibration mixture. All concentrations are on a mole/mole basis unless otherwise noted.

Do Not Use This Cylinder below 100 psig, i.e. 0.7 megapascals.

ANALYTICAL RESULTS					
Component	Requested Concentration	Actual Concentration	Protocol Method	Total Relative Uncertainty	Assay Dates
HYDROGEN SULFIDE	7.000 PPM	7.427 PPM	G1	+/- 0.9% NIST Traceable	10/14/2020, 10/21/2020
AIR	Balance				

CALIBRATION STANDARDS					
Type	Lot ID	Cylinder No	Concentration	Uncertainty	Expiration Date
GMIS	122401645168101	CC163645	10.10 PPM HYDROGEN SULFIDE/NITROGEN	+/- 0.80	Jan 23, 2023
RGM	12332	CC183693	10.07 PPM HYDROGEN SULFIDE/NITROGEN	+/- 0.8%	Dec 18, 2017

The SRM, PRM or RGM noted above is only in reference to the GMIS used in the assay and not part of the analysis.

ANALYTICAL EQUIPMENT		
Instrument/Make/Model	Analytical Principle	Last Multipoint Calibration
Applied Analytics OMA-406 AA210266	Ultraviolet	Oct 16, 2020

Triad Data Available Upon Request



\_\_\_\_\_  
Signature on file  
Approved for Release

# RUN DATA

Number 2

Client: **New Indy**  
Location: **Catawba, SC**  
Source:

Method **16**  
Calibration **1**

Project Number: **15730.001.006**  
Operator: **T. Simpkins**  
Date: **17 Mar 2021**

Time	H <sub>2</sub> S		MeSH		DMS		DMDS		TRS
	area	ppm	area	ppm	area	ppm	area	ppm	ppm
16:32	32304	7.89	<2	<0.024	<2	<0.030	<2	<0.008	7.89
16:33	33396	8.04	<2	<0.024	<2	<0.030	<2	<0.008	8.04
<b>Average</b>		<b>7.96</b>		<b>&lt;0.024</b>		<b>&lt;0.030</b>		<b>&lt;0.008</b>	<b>7.96</b>

# RUN DATA

# RUN DATA

Number 1

Client: **New Indy**  
Location: **Catawba, SC**  
Source:

Method **16**  
Calibration **1**

Project Number: **15730.001.006**  
Operator: **T. Simpkins**  
Date: **18 Mar 2021**

Time	H <sub>2</sub> S		MeSH		DMS		DMDS		TRS
	area	ppm	area	ppm	area	ppm	area	ppm	ppm
09:36	36240	7.66	<2	<0.030	<2	<0.049	<2	<0.015	7.66
09:39	36179	7.65	<2	<0.030	<2	<0.049	<2	<0.015	7.65
<b>Average</b>		<b>7.65</b>		<b>&lt;0.030</b>		<b>&lt;0.049</b>		<b>&lt;0.015</b>	<b>7.65</b>



# RUN DATA

Number 1

Client: **New Indy**  
Location: **Catawba, SC**  
Source:

Method **16**  
Calibration **1**

Project Number: **15730.001.006**  
Operator: **T. Simpkins**  
Date: **23 Mar 2021**

Time	H <sub>2</sub> S		MeSH		DMS		DMDS		TRS
	area	ppm	area	ppm	area	ppm	area	ppm	ppm
08:42	36227	7.53	<2	<0.053	<2	<0.053	<2	<0.019	7.53
08:45	36413	7.55	<2	<0.053	<2	<0.053	<2	<0.019	7.55
<b>Average</b>		<b>7.54</b>		<b>&lt;0.053</b>		<b>&lt;0.053</b>		<b>&lt;0.019</b>	<b>7.54</b>

# RUN DATA

Number 0

Client: **New Indy**  
Location: **Catawba, SC**  
Source:

Method **16**  
Calibration **1**

Project Number: **15730.001.006**  
Operator: **T. Simpkins**  
Date: **24 Mar 2021**

Time	H <sub>2</sub> S		MeSH		DMS		DMDS		TRS ppm
	area	ppm	area	ppm	area	ppm	area	ppm	
09:13	33726	7.30	<2	<0.038	<2	<0.052	<2	<0.017	7.30
09:16	33952	7.32	<2	<0.038	<2	<0.052	<2	<0.017	7.32
09:19	34010	7.33	<2	<0.038	<2	<0.052	<2	<0.017	7.33
09:22	33998	7.33	<2	<0.038	<2	<0.052	<2	<0.017	7.33
<b>Average</b>		<b>7.32</b>		<b>&lt;0.038</b>		<b>&lt;0.052</b>		<b>&lt;0.017</b>	<b>7.32</b>



## PROJECT TEAM QUALIFICATIONS

## Weston Solutions, Inc. Integrated Air Services Employee Qualifications

Name	Title/Position	Education/Training	QSTI	Years of Experience	
				Total	Emission Testing
Bryant, Ashley	Report Coordinator	BS - English Ed. - Jacksonville State University (2011) MA - English - Jacksonville State University (2012)	QSTI 1	8	8
Hammonds, Natalie	Quality Manager	BS - Environmental Science Auburn University (1998)	QSTI 1	23	18
Hartsky, Chris	Emission Testing Specialist	BA - Environmental Studies Washington College (2016)		10	5
Short, Jack	CEMS Operator	BS - Biology - Auburn University (1973) MS - Botany - Auburn University (1978) BS - Zoology Auburn University (1997)	QSTI 1, 2 & 3	32	32
Simpkins, Templeton	Project Manager		QSTI 1 & 3	20	20

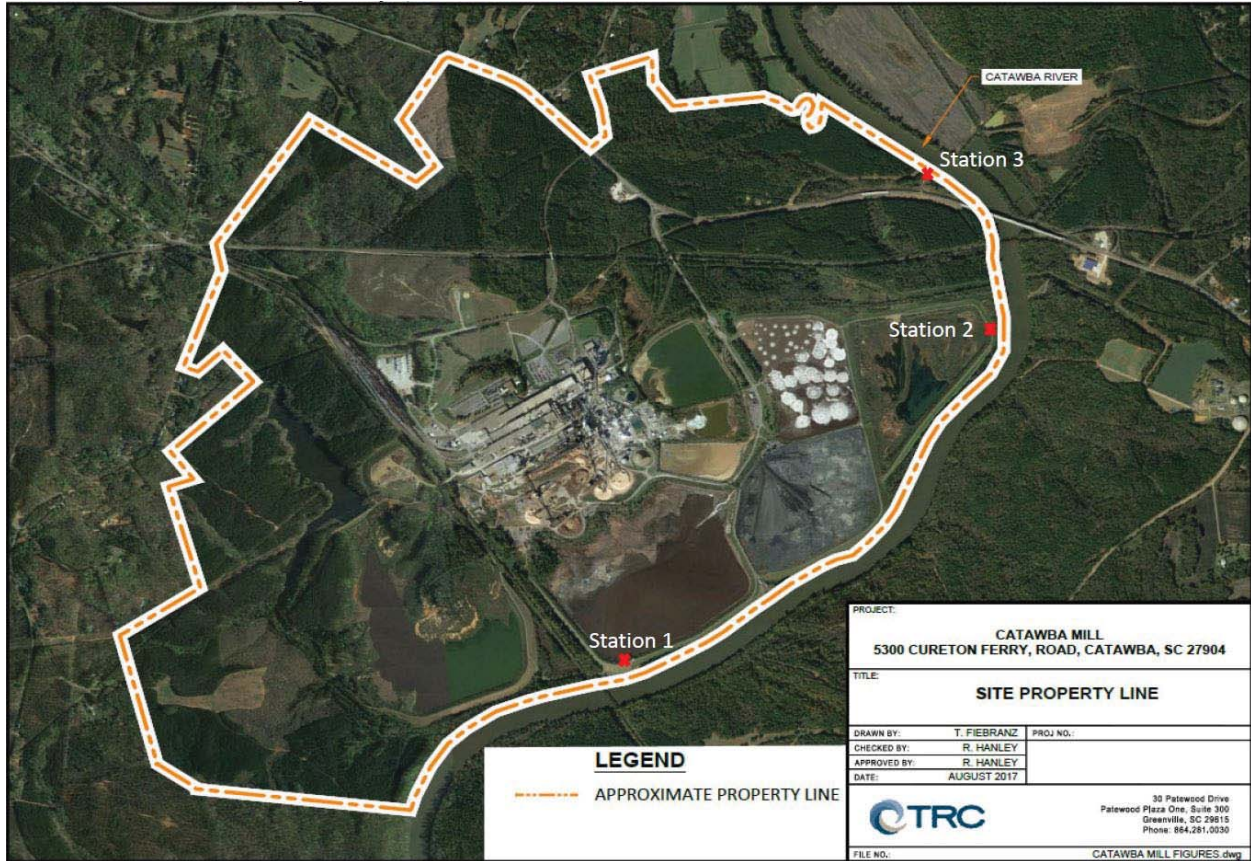
**END  
OF  
DOCUMENT**

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## APPENDIX C - ONSITE AMBIENT MONITOR LOCATIONS MAP

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# Ambient Monitoring Stations: Current "Fence Line" Locations



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## APPENDIX D - ONSITE AMBIENT MONITOR DATA

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## Ambient H2S Monitoring Data

## Initial Onsite Locations

Date	Avg ppb	Avg ppb	Avg ppb	Avg mph	Avg Degrees
	Station 1 Ballfield	Station 2 On ASB	Station 3 Hwy 5	Wind Speed	Wind Direction
4/11/2021	0.32	12.39		5.8	246
4/12/2021	0.31	144.94		4.0	251
4/13/2021	5.11	156.51		2.2	179
4/14/2021	34.19	173.81		3.7	212
4/15/2021	0.34	27.72		4.1	271
4/16/2021	0.21	95.11		2.6	228
4/17/2021	4.37	125.68		2.4	179
4/18/2021	4.02	102.93		2.3	187
4/19/2021	17.33	184.62		3.1	198
4/20/2021	33.27	104.17		4.2	183
4/21/2021	0.15	54.07		5.7	240
4/22/2021	0.05	103.79		3.4	240
4/23/2021	3.92	108.33		2.4	184
4/24/2021	67.82	331.94		3.5	182
4/25/2021	0.21	60.84		3.6	220
4/26/2021	2.81	221.37		2.2	194
4/27/2021	0.19	183.69		3.6	221
4/28/2021	0.10	35.27		3.6	212
4/29/2021	0.25	26.29	22.50	5.6	216
4/30/2021	0.15	11.45	1.23	5.2	270
5/1/2021	1.86	107.38	2.05	2.6	196
5/2/2021	0.29	96.91	26.33	3.5	220
5/3/2021	0.24	45.56	34.45	5.0	201
5/4/2021	0.94	28.56	16.30	4.0	219
5/5/2021	0.64	11.59	7.09	5.5	243
5/6/2021	1.43	27.76	0.90	2.6	210
5/7/2021	1.21	26.13	0.91	4.4	265
5/8/2021	0.24	77.80	17.44	4.0	250
5/9/2021	3.34	78.47	16.56	4.1	194
5/10/2021	0.35	23.26	28.98	4.0	232
5/11/2021	0.42	40.98	1.05	2.9	108
5/12/2021	0.19	66.02	0.90	3.1	138
5/13/2021	0.14	45.97	0.59	2.8	165
5/14/2021	1.37	25.91	0.61	2.0	174
5/15/2021	1.45	56.35	2.03	1.9	181
5/16/2021	13.63	58.78	19.16	2.6	235
5/17/2021	0.98	60.80	0.86	1.9	154
5/18/2021	3.87	27.48	0.65	1.9	151
5/19/2021	1.26	18.11	0.58	2.8	168
5/20/2021	3.63	39.48	0.62	2.7	170
5/21/2021	0.84	19.84	0.59	2.8	155
5/22/2021	2.97	45.42	2.33	1.6	208
5/23/2021	0.53	91.53	2.98	2.4	201
5/24/2021	1.74	83.63	2.32	2.0	186

## Ambient H2S Monitoring

## Current Fence Line Data

Date	Station 1			Station 2			Station 3		
	H2S Avg ppb	Wind Speed mph	Wind Direction degrees (from)	H2S Avg ppb	Wind Speed mph	Wind Direction degrees (from)	H2S Avg ppb	Wind Speed mph	Wind Direction degrees (from)
05 / 26 / 2021				44.10			1.31		
05 / 27 / 2021	18.09	24.9	227	18.40			11.30		
05 / 28 / 2021	53.54	7.5	223	7.48			7.00		
05 / 29 / 2021	20.94	8.4	223	8.15			19.22		
05 / 30 / 2021	235.80	12.8	90	1.29			0.20		
05 / 31 / 2021	176.90	5.4	144	0.20			0.48		
06 / 01 / 2021	53.09	2.5	156	1.20			1.23		
06 / 02 / 2021	67.27	2.2	174	6.51			6.88		
06 / 03 / 2021	90.40	2.4	148	0.24			0.63		
06 / 04 / 2021	184.20	4.2	169	0.31	1.0	198	2.15	0.4	191
06 / 05 / 2021	171.70	3.1	210	3.96	1.1		2.44	0.4	202
06 / 06 / 2021	7.46	3.0	163	0.90	0.6	165	3.10	0.5	170
06 / 07 / 2021	1.20	3.4	179	0.62	1.0	179	2.06	0.8	173
06 / 08 / 2021	0.91	2.3	187	2.11	0.6	164	11.26	0.2	159
06 / 09 / 2021	1.53	4.0	190	1.36	1.4	198	9.80	0.8	195
06 / 10 / 2021	35.31	4.6	201	5.93	2.2	212	16.17	0.4	191
06 / 11 / 2021	40.82	4.5	200	9.37	1.9	204	24.56	0.9	189
06 / 12 / 2021	89.90	4.5	210	10.82	2.3	199	20.21	1.0	205
06 / 13 / 2021	186.80	4.0	159	10.43	0.9	181	7.21	0.4	199
06 / 14 / 2021	300.70	5.7	85	0.27	0.7	144	8.04	0.7	149

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**APPENDIX E - ENVIRONMENTAL BUSINESS SOLUTIONS  
WASTEWATER TREATMENT SYSTEM REPORTS**

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# New Indy - Catawba Wastewater Service Report

Tuesday, May 11, 2021

## Today's Visit

Tuesday, May 11, 2021

## Previous Visit

	Inlet	ASB Mid	ASB Effluent	Holding Pond Effluent
pH	9.51	8.11	7.66	8.01
Temp. (°C)	44.0	33.1	31.3	26.0
Dissolved Oxygen (mg/L)		0.64	0.59	0.27
ORP	-169.40	-23.60	-164.50	-241.80
Ammonia (as N, mg/L)	3.05	0.38	0.09	2.60
Soluble o-PO4 (as P, mg/L)	0.58	0.12	0.20	0.62
Sulfide (µg/L)				
DOUR (mg/L/hr)	6.9	10.5	4.7	3.3
FED DOUR (mg/L/hr)	630	118	83	48
TSS (mg/L)				
VSS (mg/L)				
%VSS				
ICOD (mg/L)	1468			806
sCOD (mg/L)	873	539	510	646
<b>Bacteria Abundance (0 - 3)</b>				
Flagellates		2.0	2.0	
Free Swimming Ciliates		0	13	
Stalked Ciliates		0	4	
Rotifers		0	0	
Total Indicators Observed		0	17	
Maturity Index		#DIV/0!	1.2	

	Inlet	ASB Mid	ASB Effluent	Holding Pond Effluent
pH				
Temp. (°C)				
Dissolved Oxygen (mg/L)				
ORP				
Ammonia (as N, mg/L)				
Soluble o-PO4 (as P, mg/L)				
Sulfide (µg/L)				
DOUR (mg/L/hr)				
FED DOUR (mg/L/hr)				
TSS (mg/L)				
VSS (mg/L)				
%VSS				
sCOD (mg/L)				
ICOD (mg/L)				
<b>Bacteria Abundance (0 - 3)</b>				
Flagellates				
Free Swimming Ciliates				
Stalked Ciliates				
Rotifers				
Total Indicators Observed				
Maturity Index				

**Summary:**

- The soluble COD data showed a 42% reduction from the ASB Inlet to the ASB Effluent. This reduction in soluble COD is indicative of a reduction in BOD across the ASB. The DOUR of 6.9 mg/L/hr indicates an active biomass at the ASB midpoint, and the reduction in DOUR from the midpoint to the ASB Effluent to the Holding Pond Effluent is another indicator of BOD reduction across the system. A "Fed" DOUR was run at the ASB Midpoint, where the sample was artificially spiked with additional BOD (ASB Inflow was added), and the increase in DOUR indicates the biomass will increase its metabolic rate when presented with additional "food" at this point in the system.
- The micro exam showed a moderate to high abundance of dispersed bacteria in the ASB Midpoint and ASB Effluent samples, as well as a moderate abundance of pin floc in both samples. No higher life forms (protozoa/metazoa) were observed at the ASB Midpoint, but the ASB Effluent showed several flagellates and a few free swimming ciliates. Ciliates are generally considered indicators of aerobic, non-toxic conditions in ASB treatment systems. A low to moderate abundance of fiber was observed at the ASB midpoint sample, and a moderate abundance of grit and debris were observed in both samples.
- The excess paper stock in the front end of the system is an indication of previous primary clarification malfunction, and is what we call "phantom" BOD in the ASB at this time. Phantom BOD is insoluble organic material in a treatment system that slowly breaks down into soluble BOD over time. It's called "phantom" BOD because it will not show up on the influent BOD data (fiber takes longer than 5 days to degrade), but will make a BOD contribution to the treatment system over time as the fiber is broken down.
- While dissolved oxygen residuals weren't completely bottomed out at the ASB Midpoint and ASB Effluent, we generally consider D.O. concentrations under 1 mg/L in ASBs to be oxygen deficient. Getting the out of commission aerators back online in the front end of the system will increase the BOD removal capacity of the ASB, and promote more aerobic conditions.
- The TSS of 630 mg/L at the ASB Inflow is elevated, indicating poor primary clarification efficiency and elevated solids loading into the ASB at this time.
- Ammonia and ortho-phosphate concentrations were over 0.1 mg/L at the ASB midpoint, which indicates adequate nitrogen and phosphorus availability for the biomass. Bacteria require macronutrients (N & P) at a ratio of 100:2.5:0.5 (BOD:N:P) for optimal BOD removal. Target residuals are 0.1-0.3 mg/L for both N & P in an ASB. The increase in ammonia from the ASB Effluent to the Holding Pond Effluent is due to benthic feedback, where settled sludge breaks down and releases ammonia and phosphate into the water.
- pH values were within the target range of 6.5 - 8.5 across the system.

If you have any questions about the report please let me know.

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## New Indy - Catawba Wastewater Service Report

Tuesday, May 25, 2021

### Today's Visit Tuesday, May 25, 2021

	Inlet	ASB Mid	ASB Effluent	Holding Pond Effluent
pH	10.19	7.05	7.28	7.79
Temp. (°C)	44.6	32.2	29.1	26.8
Dissolved Oxygen (mg/L)		0.21	0.42	0.46
ORP	-131.30	-29.10	-46.50	-124.50
Ammonia (as N, mg/L)	3.02	0.03	0.03	3.14
Soluble o-PO4 (as P, mg/L)	0.38	0.08	0.07	0.45
Sulfide (µg/L)				
DOUR (mg/L/h)		4.3	2.6	2.9
FED DOUR (mg/L/hr)		12.2		
TSS (mg/L)	793	271	134	45
VSS (mg/L)	720	204	115	35
%VSS	91%	75%	85%	77%
ICOD (mg/L)	130.3	407	231	323
sCOD (mg/L)	0.35	0.14	0.13	1.94
Sulfide (mg/L)				
<b>Bacteria Abundance (0 - 3)</b>		2.5	2.0	
Flagellates		3	3	
Free Swimming Ciliates		0	2	
Stalked Ciliates		2	0	
Rotifers		0	0	
Total Indicators Observed		5	5	
Maturity Index		1.8	1.4	

### Previous Visit Tuesday, May 11, 2021

	Inlet	ASB Mid	ASB Effluent	Holding Pond Effluent
pH	9.51	8.11	7.66	8.01
Temp. (°C)	44.0	33.1	31.3	26.0
Dissolved Oxygen (mg/L)		0.64	0.59	0.27
ORP	-169.40	-23.60	-164.50	-241.80
Ammonia (as N, mg/L)	3.05	0.38	0.09	2.80
Soluble o-PO4 (as P, mg/L)	0.58	0.12	0.20	0.62
Sulfide (µg/L)				
DOUR (mg/L/h)		6.9	4.7	3.3
FED DOUR (mg/L/hr)		10.5		
TSS (mg/L)	630	118	83	48
VSS (mg/L)				
%VSS				
ICOD (mg/L)	1468			806
sCOD (mg/L)	873	539	510	646
Sulfide (mg/L)				
<b>Bacteria Abundance (0 - 3)</b>		2.0	2.0	
Flagellates		0	13	
Free Swimming Ciliates		0	4	
Stalked Ciliates		0	0	
Rotifers		0	0	
Total Indicators Observed		0	17	
Maturity Index		#DIV/0!	1.2	

#### Summary:

- Sulfide concentrations were measured in the ASB and Holding Pond today. Concentrations were low in the influent and ASB samples, but increased to 1.94 mg/L in the Holding Pond Effluent sample. This increase can be attributed to sulfate reducing bacteria in the Holding Pond converting sulfate to hydrogen sulfide. Sulfate reducing bacteria will metabolize BOD and produce sulfides when oxygen or nitrate are not available.
- The soluble COD data indicated elevated organic loading into the ASB today. The significant 82% drop in soluble COD is indicative of a reduction in BOD across the ASB. The increase in oxygen uptake in the Spiked DOOR (added 30 mL of influent to the sample) at the ASB Midpoint indicates the biomass is uninhibited and will increase its metabolic rate when presented with additional BOD.
- The TSS in the influent continues to be elevated, indicating poor primary clarification efficiency and high solids loading into the ASB.
- The micro exam showed higher life forms (protozoa) in both the ASB midpoint and ASB Effluent. Two stalked ciliates were observed at the ASB Midpoint and ASB Effluent. Two free swimming ciliates were observed at the ASB Outfall as well. The ASB midpoint sample showed a high abundance of grit and debris, as well as pin floc and a few small compact pieces of floc. There was no floc larger than pin floc observed at the ASB Outfall, and the abundance of grit/debris decreased in this sample. Dispersed bacteria abundance was high in the midpoint (2.5 out of 3), and moderate to high in the ASB Effluent (2 out of 3).
- While dissolved oxygen concentrations were low at the ASB Midpoint, ASB Effluent, and Holding Pond (less than 0.5 mg/L), the Oxidation Reduction Potential (ORP) of these samples were increased from the previous visit, indicating more aerobic conditions than previously observed. We commonly utilize ORP to determine how anaerobic/aerobic an environment is where D.O. concentrations are low, as a lower value is a more "electron rich", reduced environment and indicates anaerobic conditions. For example, a sample with a D.O. of 0.2 mg/L and an ORP of -50 mV is significantly more aerobic than a sample with a D.O. of 0.2 mg/L and an ORP of -350 mV.
- Ammonia and ortho-phosphate concentrations were below the target range of 0.1 mg/L in the ASB today. While oxygen deficiency is the most important limiting growth pressure at this time, we should also be addressing nutrient deficiency at this time. Adding additional bioavailable nitrogen and phosphorus (ammonium and phosphate) to the ASB will improve the rate of BOD conversion and make the biomass more resilient to loading swings.

Please let me know if you have any questions or additional input at this time.

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## New Indy - Catawba Wastewater Service Report

Wednesday, June 9, 2021

### Today's Visit Wednesday, June 9, 2021

	EQ	Clarifier Out	ASB Mid	ASB Effluent	Holding Pond Effluent
pH	8.59	9.24	8.87	8.17	8.07
Temp. (°C)	47.6	47.5	33.6	33.6	29.5
Dissolved Oxygen (mg/L)	-238.90	-189.80	0.90	0.13	0.30
ORP	3.02	0.18	-6.40	-173.90	-207.30
Ammonia (as N, mg/L)	0.50	0.50	0.04	0.08	2.20
Soluble o-Po4 (as P, mg/L)	0.50	0.50	0.13	0.15	0.34
DOUR (mg/L/m)			3.5	4.7	1.3
FED DOUR (mg/L/m)			9.9		
TSS (mg/L)	1860	84	187	103	36
VSS (mg/L)	1380	72	133	88	32
%VSS	74%	86%	71%	85%	89%
ICOD (mg/L)			3.65	3.76	3.42
sCOD (mg/L)	1168	1059	0.11	0.1	2.5
Sulfide (mg/L)	0.14	0.3	0.11	0.1	0.1
<b>Bacteria Abundance (0 - 3)</b>			2.5	2.0	
Flagellates			10	6	
Free Swimming Ciliates			2	1	
Stalked Ciliates			0	3	
Rotifers			0	0	
Total Indicators Observed			14	10	
Maturity Index			1.4	1.7	

### Previous Visit Tuesday, May 25, 2021

	EQ	Clarifier Out	ASB Mid	ASB Effluent	Holding Pond Effluent
pH	7.75	10.19	7.85	7.38	7.09
Temp. (°C)		44.6	32.2	29.1	26.8
Dissolved Oxygen (mg/L)		-131.30	0.21	0.42	0.46
ORP		3.02	-29.10	-46.50	-124.50
Ammonia (as N, mg/L)		0.38	0.03	0.03	3.14
Soluble o-Po4 (as P, mg/L)		0.38	0.08	0.07	0.45
DOUR (mg/L/m)			4.3	2.6	2.9
FED DOUR (mg/L/m)			12.2		
TSS (mg/L)		703	271	134	45
VSS (mg/L)		720	204	115	35
%VSS		91%	75%	85%	77%
ICOD (mg/L)		1303	407	231	323
sCOD (mg/L)		0.35	0.14	0.13	1.94
Sulfide (mg/L)					
<b>Bacteria Abundance (0 - 3)</b>			2.5	2.0	
Flagellates			3	3	
Free Swimming Ciliates			0	2	
Stalked Ciliates			2	0	
Rotifers			5	5	
Total Indicators Observed			18	14	
Maturity Index			1.8	1.4	

#### Summary:

The sulfide concentration at #1 Holding Pond was 2.5 mg/L today. Concentrations continue to be low in the influent and ASB samples, indicating H2S formation is occurring primarily in the Holding Pond.

The micro exam showed stalked ciliates and free swimming ciliates at the ASB Mid, and ASB Out sample points. Stalked ciliates are generally considered indicators of good biomass health, as they are sensitive microorganisms that don't survive in toxic or anaerobic conditions. There was abundant grit and debris observed in the ASB Mid sample, with the abundance decreasing in the ASB Out. This corresponds with the lower percent VSS observed in the ASB Mid sample, as there is a higher fraction of inorganic gridd debris in this part of the ASB.

Samples of the clarifier overflow and EQ basin effluent were sampled today. The EQ effluent TSS is elevated and is contributing to high solids loading into the ASB. The clarifier overflow TSS was low, and would normally indicate good primary clarification if the EQ solids weren't mixed in.

There was a 64% reduction in soluble COD from the clarifier overflow to the ASB Midpoint, and the drop is primarily due to soluble BOD treatment. The DOUR and sCOD data indicates the majority of BOD is treated by the ASB Mid sample. The holding pond DOUR is within a range that suggests low soluble BOD in the effluent.

The D.O. and ORP at the ASB Midpoint sample indicate more aerobic conditions than the previous service visits. Mark and I performed a D.O. and ORP profile of the ASB today, and several measurements showed D.O. concentrations above 1 mg/L, with a few being over 2 mg/L in the ASB, mostly in deeper areas closer to aerators.

Ammonia concentrations were under the recommended ASB range of 0.1 - 0.3 mg/L. Adequate concentrations of bioavailable nitrogen and phosphorus (ammonium and ortho-phosphate) will speed up the rate of BOD conversion in the ASB and make the biomass more resilient to loading swings.

On the next report I will create a compiled data tab so we can keep track of trended data.

Please let me know if you have any questions or additional input at this time.

Tripp McElwee  
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